

Storno

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MAINTENANCE
MANUAL

STORNOPHONE 700
MAINTENANCE MANUAL
VOLUME II

Volume II

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STORNOPHONE 700
 MAINTENANCE MANUAL
 VOLUME II
 Section 1

TITLE	Description	Code
AA701	Description	60.182-E1
	Schematic	D401.216/3
	Part List	X401.318/2
AA702	Description	60.183-E1
	Schematic	D401.713
	Part List	X401.938
AA702a	Schematic	D402.206
	Part List	X401.939
AA705	See MC704	
AA706	See MT704	
AA707	See MT704	
BF713	Schematic	D401.990
BF762	Schematic	D401.989
BP711	Description	60.186-E1
	Schematic	D401.383
	Part List	X401.381
BP712	Schematic	D402.024
	Part List	X402.270
BP731	Description	60.187-E1
	Schematic	D401.419
	Part List	X401.536
BP761	Description	60.188-E1
	Schematic	D401.325
	Part List	X401.316
BP762	Schematic	D402.010
	Part List	X402.268

MICROPHONE AMPLIFIER AA701

Technical Specifications

Supply Voltage

9 V and 12 V

Output Impedance600 Ω Bandwidth

300 Hz to 3000 Hz

Nominal Output Level

-17 dBm

Maximum Output Level

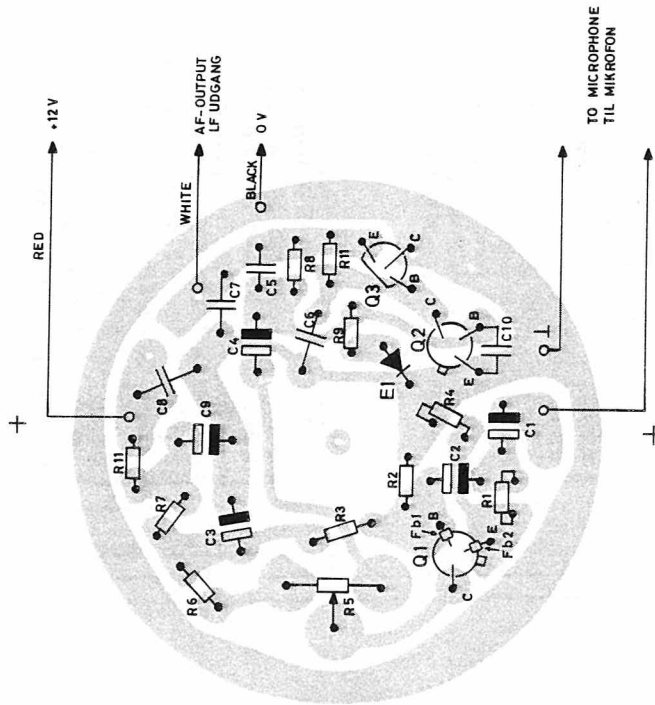
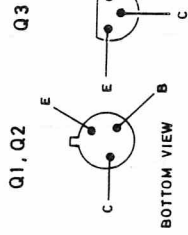
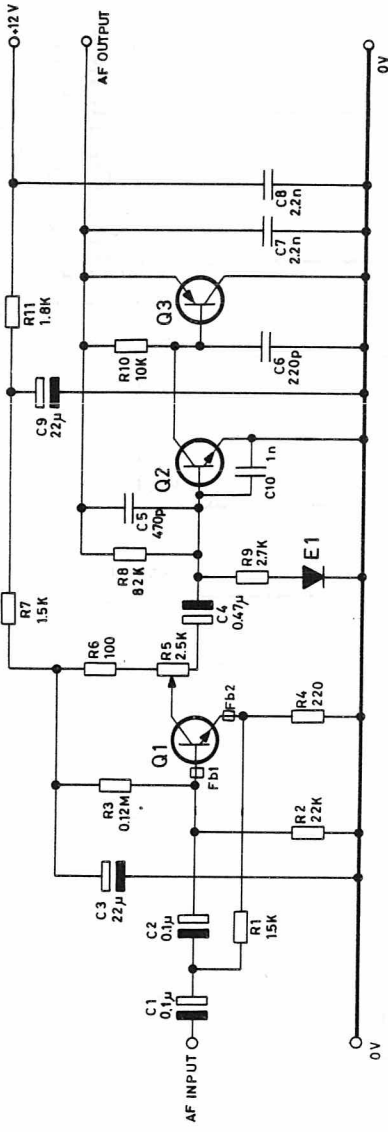
+3 dBm

Distortion at -17 dBm $\leq 3\%$ Gain (at 1000 Hz)

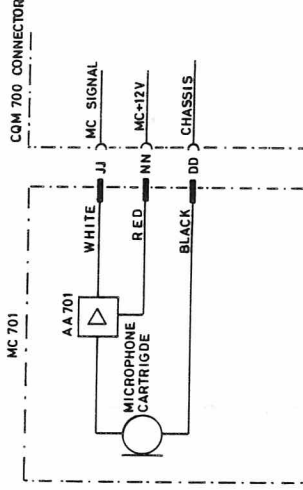
Maximum: 50 dB/- 3 dB

Minimum: 20 dB/+3 dB

Temperature Range-25^o to +60^oCCurrent Drain ≤ 12 mA



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE.



AF AMPLIFIER
LF FORSTÆRKER
AA701

D 401.216/3

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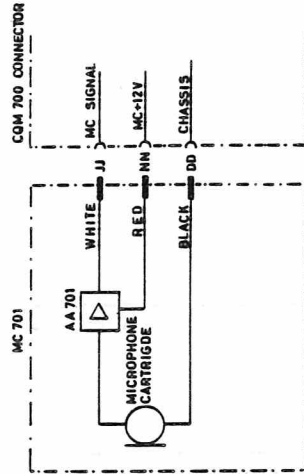
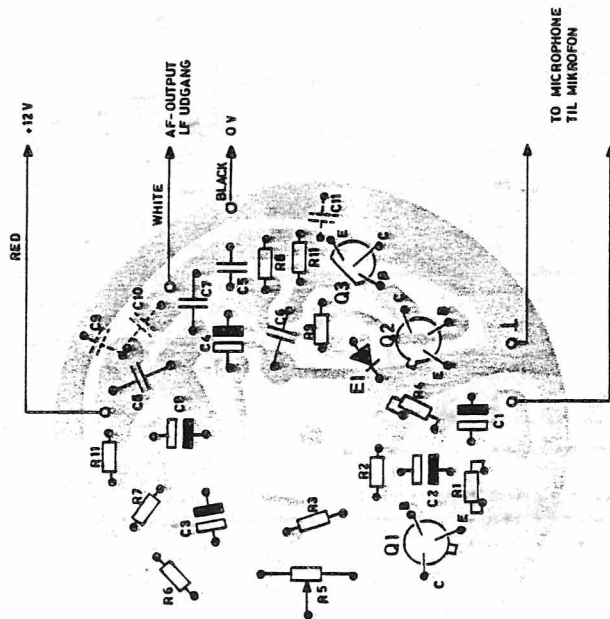
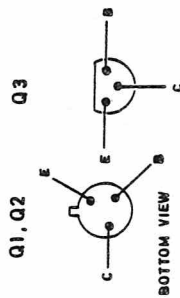
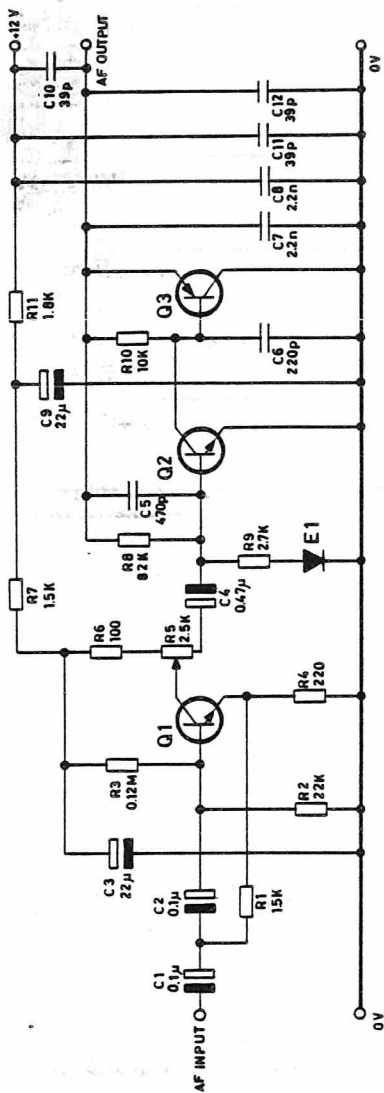
TYPE	NO.	CODE	DATA
AA701		10.2488	Microphone Amplifier
	C1	73.5130	0.1 μ F -20 +60% tantal
	C2	73.5130	0.1 μ F -20 +60% tantal
	C3	73.5127	22 μ F 20% tantal
	C4	73.5134	0.47 μ F -20 +60% tantal
	C5	76.5106	470 pF 5% polystyr TB
	C6	76.5104	220 pF 5% polystyr TB
	C7	76.5059	2.2 nF 10% polyest. FL
	C8	76.5059	2.2 nF 10% polyest. FL
	C9	73.5127	22 μ F 20% tantal
	C10	74.5155	1 nF -20 +80% ceram PL
	R1	80.5251	1.5 K Ω 5% carbon film
	R2	80.5265	22 K Ω 5% carbon film
	R3	80.5274	0.12 M Ω 5% carbon film
	R4	89.5241	220 Ω 5% carbon film
	R5	86.5067	2.5 K Ω 20% potentiometer
	R6	80.5237	100 Ω 5% carbon film
	R7	80.5251	1.5 K Ω 5% carbon film
	R8	80.5272	82 K Ω 5% carbon film
	R9	80.5254	2.7 K Ω carbon film
	R10	80.5261	10 K Ω 5% carbon film
	R11	80.5252	1.8 K Ω carbon film
	E1	99.5028	1N914 Diode
	Q1	99.5121	BC107 Transistor
	Q2	99.5121	BC107 Transistor
	Q3	99.5144-02	BC214 L Transistor
	Fb1	65.5102	Ferrit bead
	Fb2	65.5102	Ferrit bead

TYPE NO. CODE DATA

MICROPHONE AMPLIFIER
MIKROFONFORSTÆRKER

AA701

X401.318/3



**AF AMPLIFIER
LF FORSTÆRKER**

AA701

D 401.216/2

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE.

Storno

TYPE	NO.	CODE	DATA
AA701		10. 2488	Microphone Amplifier
	C1	73. 5130	0. 1 μ F -20 +60% tantal
	C2	73. 5130	0. 1 μ F -20 +60% tantal
	C3	73. 5127	22 μ F 20% tantal
	C4	73. 5134	0. 47 μ F -20 +60% tantal
	C5	76. 5106	470 pF 5% polystyr TB
	C6	76. 5104	220 pF 5% polystyr TB
	C7	76. 5059	2. 2 nF 10% polyest. FL
	C8	76. 5059	2. 2 nF 10% polyest. FL
	C9	73. 5127	22 μ F 20% tantal
	C10	74. 5187	39 pF 10% ceram PL
	C11	74. 5187	39 pF 10% ceram PL
	C12	74. 5187	39 pF 10% ceram PL
	R1	80. 5251	1. 5 K Ω 5% carbon film
	R2	80. 5265	22 K Ω 5% carbon film
	R3	80. 5274	0. 12 M Ω 5% carbon film
	R4	89. 5241	220 Ω 5% carbon film
	R5	86. 5067	2. 5 K Ω 20% potentiometer
	R6	80. 5237	100 Ω 5% carbon film
	R7	80. 5251	1. 5 K Ω 5% carbon film
	R8	80. 5272	82 K Ω 5% carbon film
	R9	80. 5254	2. 7 K Ω carbon film
	R10	80. 5261	10 K Ω 5% carbon film
	E1	99. 5028	1 N914 Diode
	Q1	99. 5121	BC107 Transistor
	Q2	99. 5121	BC107 Transistor
	Q3	99. 5043	NS6063 Transistor

20 V
20 V
16 V
20 V
25 V
25 V
50 V
50 V
16 V
25 V
25 V
25 V
1/8W
1/8W
1/8W
1/8W
0. 1W
1/8W
1/8W
1/8W
1/8W

Storno

TYPE	NO.	CODE	DATA

MICROPHONE AMPLIFIER
MIKROFONFORSTÆRKER

AA701

X401.318/2

MICROPHONE AMPLIFIER AA702

Technical Specifications

Supply Voltage

9 V

Input Impedance600 Ω Output Impedance560 Ω Bandwidth

300 Hz to 3000 Hz

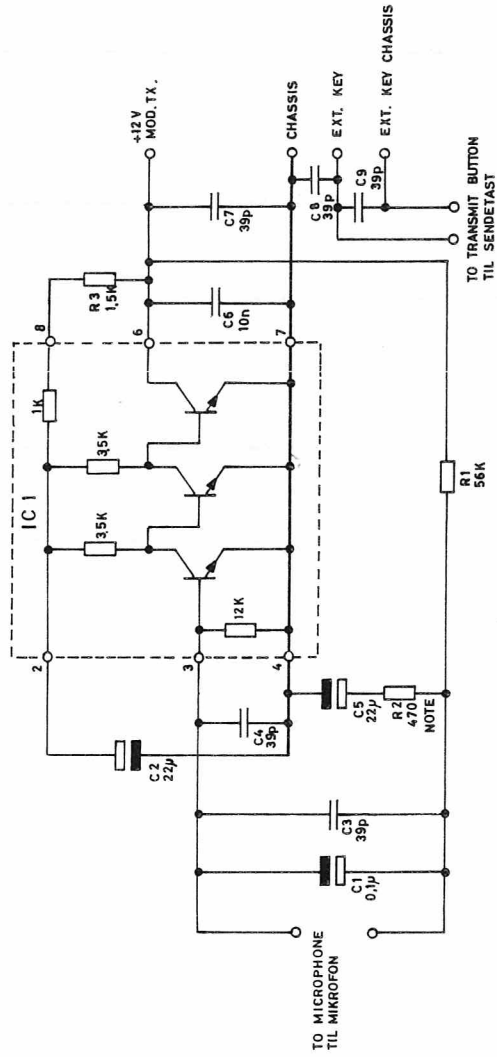
Nominal Output Level

-17 dBm

Maximum Output Level

+ 3dBm

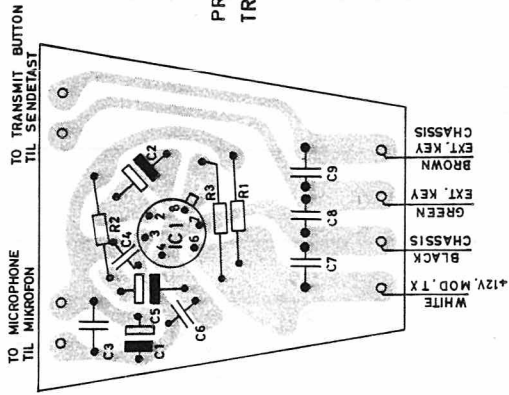
Distortion (-17 dBm to +3 dBm) $\leq 3\%$ GainMaximum: 44 dB \pm 4 dBMinimum: 26 dB \pm 4 dBTemperature Range-25^o to +60^oCCurrent Drain10 mA \pm 2 mA



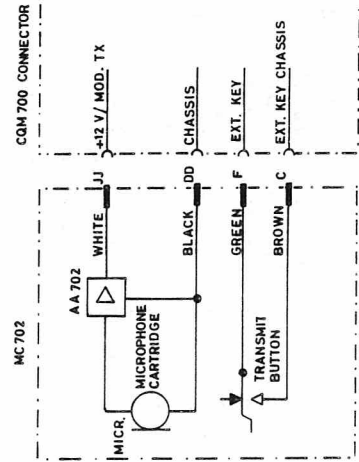
TOP VIEW
SET FRA TOPPEN

NOTE: HIGHER OR LOWER AMPLIFICATION
CAN BE ADJUSTED BY MEANS OF R2

C3, C4, C7, C8 AND C9 ON SOLDERING SIDE



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE.
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN



AF AMPLIFIER
LF FORSTÆRKER
AA702

D401.713

Storno

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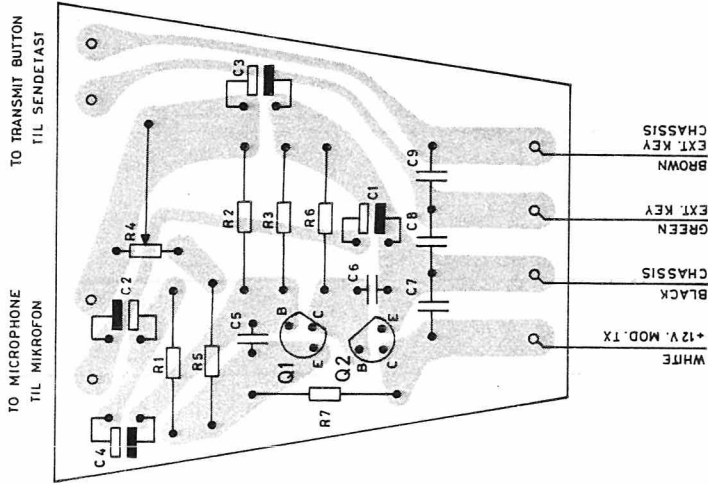
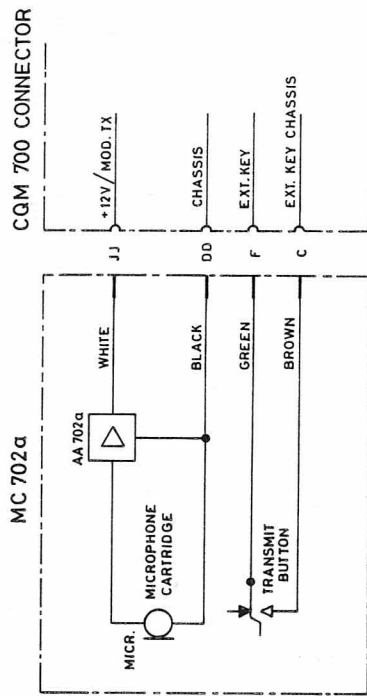
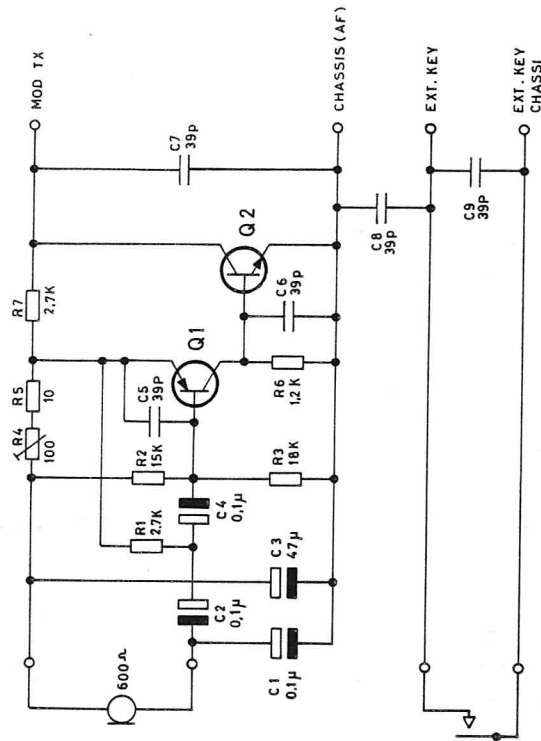
TYPE	NO.	CODE	DATA
AA 702		10. 2548	Microphone Preamplifier
	C1	73. 5089	0. 1 μ F
	C2	73. 5127	22 μ F
	C3	74. 5187	39pF
	C4	74. 5187	39pF
	C5	73. 5127	22 μ F
	C6	76. 5070	10nF
	C7	74. 5187	39pF
	C8	74. 5187	39pF
	C9	74. 5187	39pF
	R1	80. 5270	56k Ω
	R2	80. 5245	470 Ω
	R3	80. 5251	1. 5k Ω
	IC1	14. 5001	Integrated AF Amplifier 65dB
			35V 16V 25V 25V 16V 50V 25V 25V 25V 25V 1/8W 1/8W 1/8W 40mW

TYPE	NO.	CODE	DATA

MICROPHONE PREAMPLIFIER
 MIKROFONFORSTÆRKER

AA702

X401. 938



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE.
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN.

MICROPHONE PREAMPLIFIER
MIKROFONFORSTÆRKER

AA702a

D 402.206

Storno

TYPE	NO.	CODE	DATA	
MC702	01	96.0094-01	Fist Microphone	
		96.5069	Microphone cartridge	
		10.2548-01	AA702a Microphone Preamplifier	
		47.5040	Switch	
	AA702a	C1 C2 C3 C4 C5 C6 C7 C8 C9	10.2548-01	Microphone Preamplifier
			73.5089	0.1μF 20% tantal 35V
			73.5089	0.1μF 20% tantal 35V
			73.5124	47μF 20% tantal 6.3V
			73.5089	0.1μF 20% tantal 30V
74.5137			39pF 10% ceram PL 25V	
74.5137			39pF 10% ceram PL 25V	
74.5137			39pF 10% ceram PL 25V	
74.5137			39pF 10% ceram PL 25V	
R1 R2 R3 R4 R5 R6 R7	80.5254	2.7KΩ 5% carbon film 1/8W		
	80.5262	15KΩ 5% " 1/8W		
	80.5264	18KΩ 5% " 1/8W		
	86.5051	10Ω 20% potentiometer 1/10W		
	80.5225	10Ω 5% carbon film 1/8W		
	80.5254	2.7KΩ 5% " 1/8W		
	80.5254	2.7KΩ 5% " 1/8W		
Q1 Q2	99.5144	BC214L Transistor		
	99.5117	2N2924 Transistor		

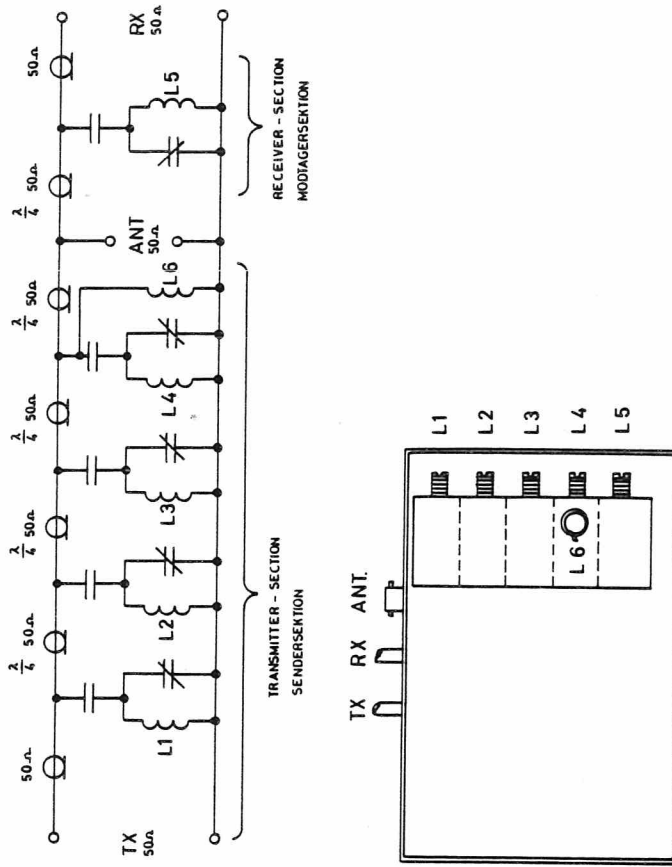
Storno

TYPE	NO.	CODE	DATA

**FIST MICROPHONE
HÅNDMIKROFON**

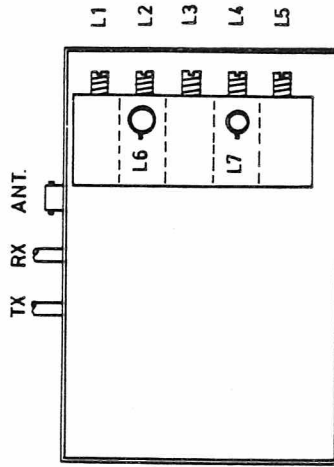
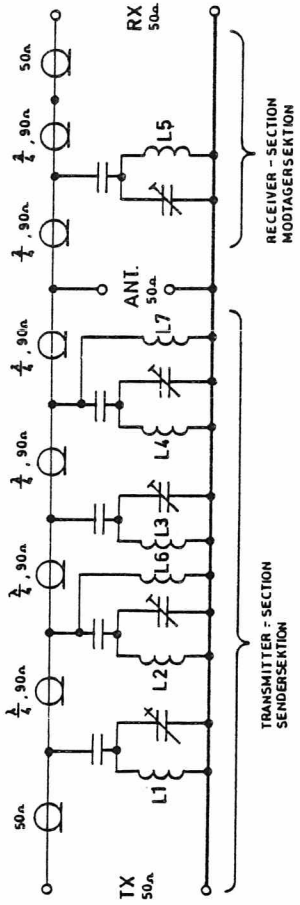
MC702

X401.939



ANTENNA BRANCHING FILTER BF713

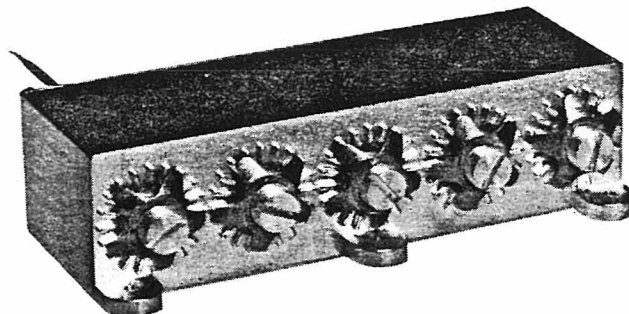
D401990



ANTENNA BRANCHING FILTER BF762

D401.989

BAND-PASS FILTER BP711



Description

Band-pass filter BP711 is a highly selective, 5-element helix filter for the frequency band of 146 - 174 MHz.

BP711 is the preselector in CQM710, where the entire front-end selectivity is derived from this circuit.

The filter is built in a silver-plated metal box where each coil is placed in a separate compartment. Coupling between coils is accomplished through openings in the partitions between enclosures.

The input and output are inductively coupled to the first and last stages, respectively.

The coils are tuned by silver-plated slugs.

Technical Specifications

Frequency Range

146 - 174 MHz

Input Impedance

Nominal 50 Ω

Output Impedance

Nominal 50 Ω

Bandwidth

3 dB bandwidth: 3 MHz

40 dB bandwidth: 8 MHz

Insertion Loss

3.5 dB

Maximum Allowable Deviation from Centre Frequency

(between -30 and $+75^{\circ}\text{C}$): ± 0.4 MHz

Temperature Range

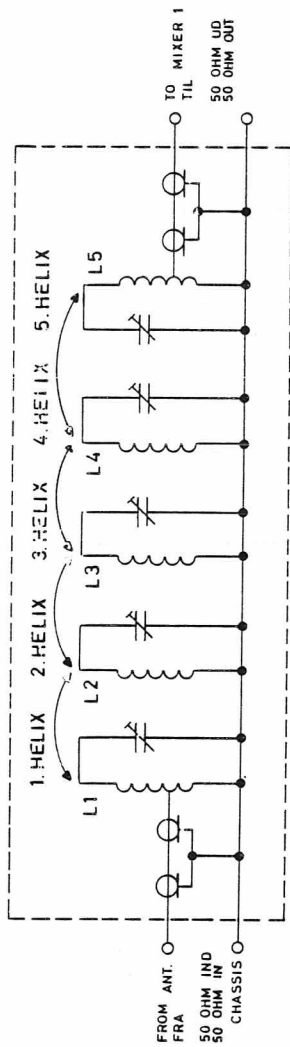
Operating range: -25° to $+70^{\circ}\text{C}$

Functioning range: -30° to $+75^{\circ}\text{C}$

Dimensions in mm:

$h = 24$, $l = 91$, $b = 30$ (without tuning slugs)

$b = 43.5$ (max. with tuning slugs)



BAND PASS FILTER
BÅNDPASFILTER

BP711

D401.383

Storno

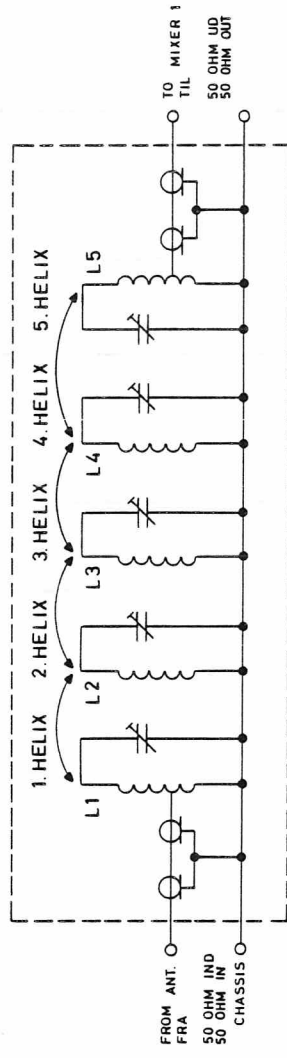
TYPE	NO.	CODE	DATA
BP711		10.2554	Band Pass Filter
	L1	62.0819	RF coil
	L2	62.0819	RF coil
	L3	62.0819	RF coil
	L4	62.0819	RF coil
	L5	62.0819	RF coil

Storno

TYPE	NO.	CODE	DATA

BAND PASS FILTER
 BÅNDPASFILTER
 BP711

X401.381



BAND PASS FILTER BP712

D402.024

Storno

TYPE	Nº	CODE	DATA
BP712		10. 3114-00	Band Pass Filter
	L1	62. 0819	RF coil 146-174 MHz
	L2	62. 0819	RF coil 146-174 MHz
	L3	62. 0819	RF coil 146-174 MHz
	L4	62. 0819	RF coil 146-174 MHz
	L5	62. 0819	RF coil 146-174 MHz

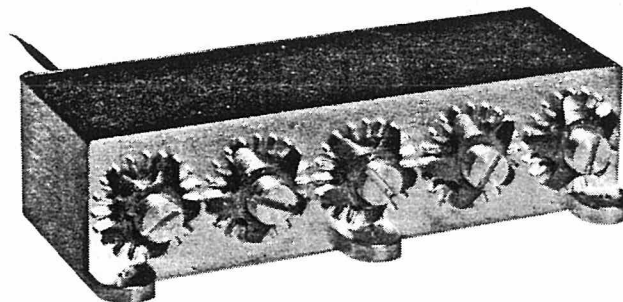
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TYPE	Nº	CODE	DATA
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BAND PASS FILTER BP712

X402.270

BAND-PASS FILTER BP731



Description

Band-pass filter BP731 is a highly selective, 5-element helix filter for the frequency band of 68 - 88 MHz.

BP731 is the preselector in CQM730, where the entire front-end selectivity is derived from this circuit.

The filter is built in a silver-plated metal box where each coil is placed in a separate compartment. Coupling between coils is accomplished through openings in the partitions between enclosures.

The input and output are inductively coupled to the first and last stages, respectively.

The coils are tuned by silver-plated slugs.

Technical Specifications

Frequency Range

68 - 88 MHz

Input Impedance

Nominal 50 Ω

Output Impedance

Nominal 50 Ω

Bandwidth

3 dB bandwidth: 2.5 MHz

40 dB bandwidth: 6.5 MHz

Insertion Loss

3.5 dB

Maximum Allowable Deviation from Centre Frequency

(between -30° and $+75^{\circ}$ C) \pm 0.2 MHz

Temperature Range

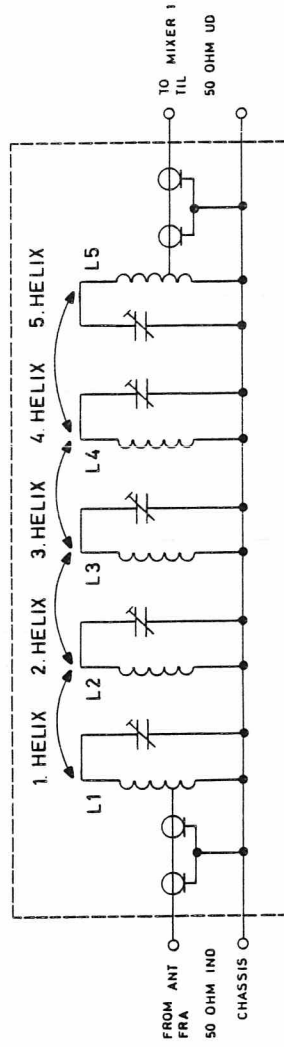
Operating range -25° to $+70^{\circ}$ C

Functioning range -30° to $+75^{\circ}$ C

Dimensions in mm :

$h = 24$, $l = 91$, $b = 30$ (without tuning slugs)

$b = 43.5$ (max. with tuning slugs)



BAND PASS FILTER
BÅNDPASSFILTER

BP731

D401.419

Storno

TYPE	NO.	CODE	DATA
BP731	L1 L2 L3 L4 L5	10.2630-00 62.0833 62.0834 62.0834 62.0834 62.0835	BAND PASS FILTER RF - coil RF - coil RF - coil RF - coil RF - coil

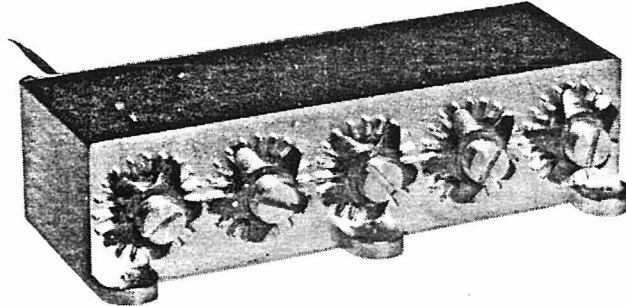
Storno

TYPE	NO.	CODE	DATA
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BAND PASS FILTER BP731
BÅNDPASFILTER

X401.536

BAND-PASS FILTER BP761



Description

Band-pass filter BP761 is a highly selective, 5-element helix filter for the frequency band of 420 - 470 MHz.

BP761 is the preselector in CQM760, where the entire front-end selectivity is derived from this circuit.

The filter is built in a silver-plated metal box where each coil is placed in a separate compartment. Coupling between coils is accomplished through openings in the partitions between enclosures.

The input and output are inductively coupled to the first and last stages, respectively.

The coils are tuned by silver-plated slugs.

Technical Specifications

Frequency Range

420 - 470 MHz

Input Impedance

Nominal 50 Ω

Output Impedance

Nominal 50 Ω

Bandwidth

3 dB bandwidth: 4 MHz

40 dB bandwidth: 12 MHz

Insertion Loss

3.5 dB

Maximum Allowable Deviation from Centre Frequency

(between -30° and $+75^{\circ}$ C): ± 0.6 MHz

Temperature Range

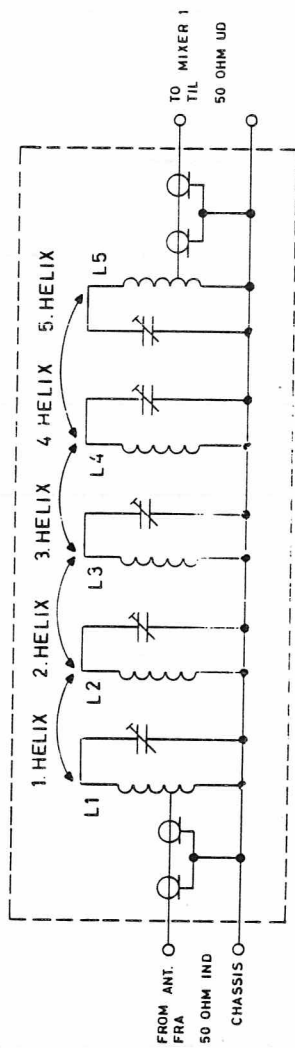
Operating range: -25° to $+70^{\circ}$ C

Functioning range: -30° to $+80^{\circ}$ C

Dimensions in mm

$h = 24$, $l = 91$, $b = 30$ (without tuning slugs)

$b = 43.5$ (max. with tuning slugs)



HELIX FILTER BP761

BAND PASS FILTER BP761

D401.325

Storno

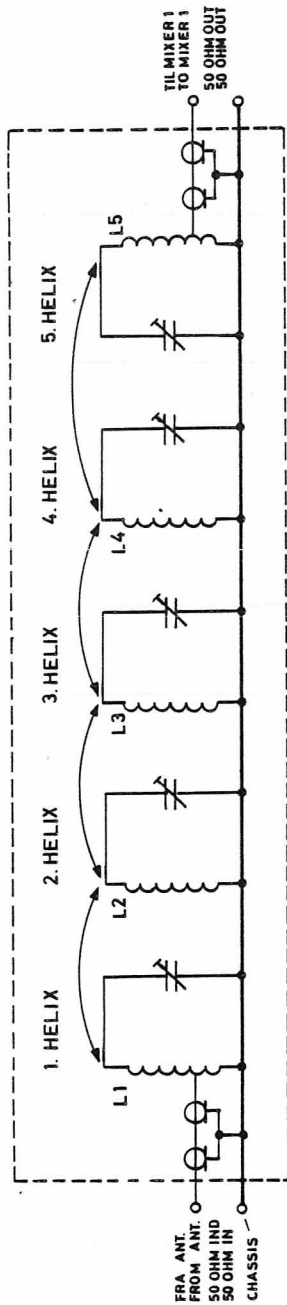
TYPE	NO.	CODE	DATA
BP761		10.2426	Helical Band Pass Filter
	L1	62.0793	Coil
	L2	62.0793	Coil
	L3	62.0793	Coil
	L4	62.0793	Coil
	L5	62.0793	Coil

Storno

TYPE	NO.	CODE	DATA
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BAND PASS FILTER BP761

X401.316



Storno

TYPE	Nº	CODE	DATA
BP762		10.3115-00	Band Pass Filter
	L1	62.0793	Coil
	L2	62.0793	Coil
	L3	62.0793	Coil
	L4	62.0793	Coil
	L5	62.0793	Coil

Storno

TYPE	Nº	CODE	DATA
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BAND PASS FILTER BP762

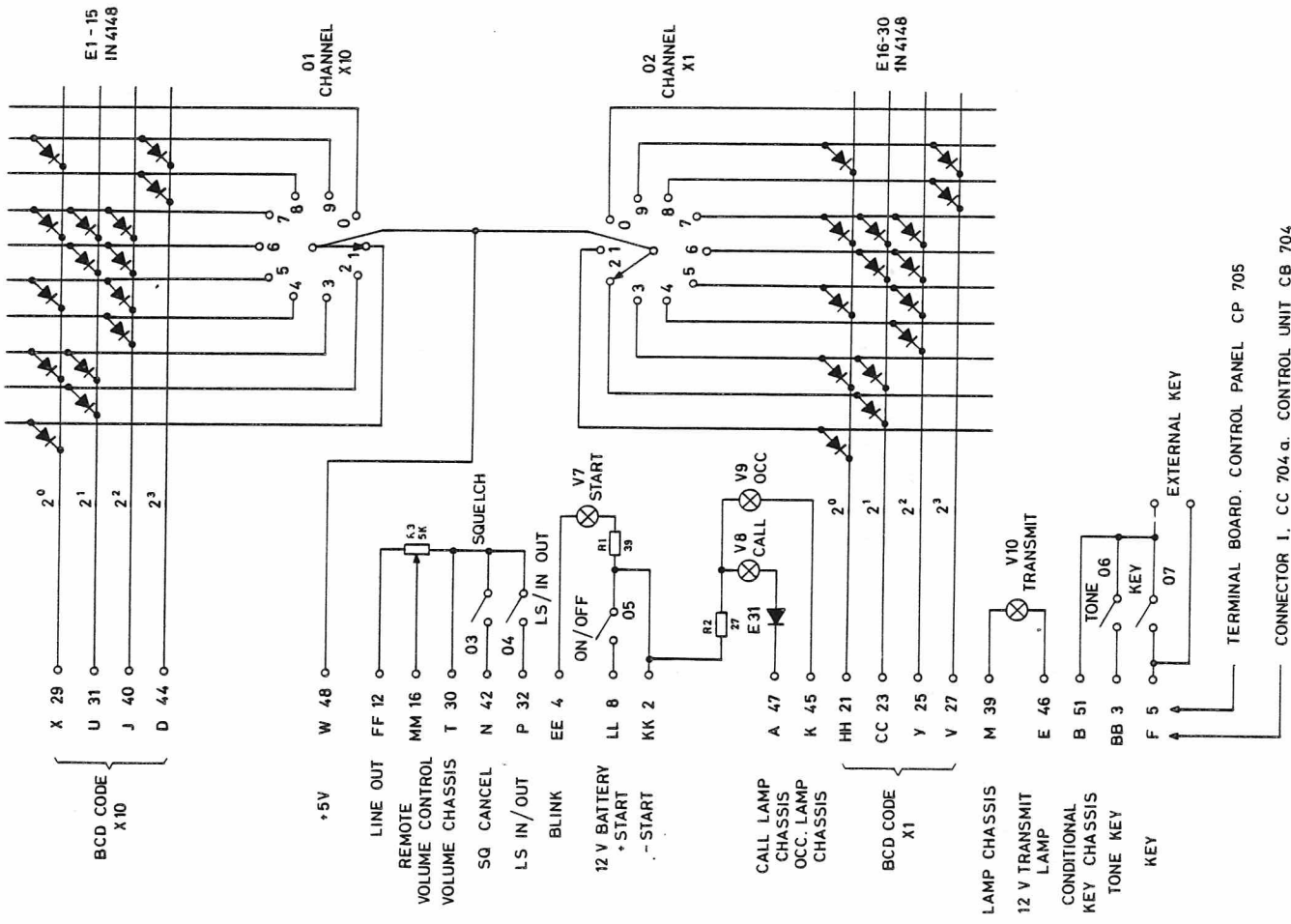
X.402.268

STORNOPHONE 700
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 VOLUME II
 Section 2

TITLE		Code
CB704, CP705	Schematic	D402. 570
	Part List	X402. 560
CB705	Schematic	D402. 386
	Part List	X402. 542
	Component Lay-out	D402. 589
CB706	Schematic	D402. 614
	Part List	X402. 628
	Component Lay-out	D402. 609/2
CB2706	Schematic A+B	D402. 028/2
	Part List A	X402. 029
	Part List B	X402. 036
	Schematic C	D402. 033/2
	Part List C	X402. 036
	Component Lay-out	D402. 167
CC704a	Wiring	D402. 031/2
	Modifying Extension Cable	
CF701 & CF702	CC704	D402. 344/2
	Description 1 - 14	60. 178-E2
CF701	Schematic A3	D401. 296/2
	Component Lay-out	D401. 515
	Part List 1 - 3	X401. 322/2
CF702	Schematic A3	D401. 840
	Component Lay-out	D401. 975
	Part List 1 - 3	X401. 868
CF703, CF704	Description	60. 348-E1
	Schematic A3	D402. 240/3
	Component Lay-ouy	D402. 354
	Part List 1 - 3	X402. 429/2

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CF705	Description	60.345-E2
	Schematic A3	D402.387/2
	Component Lay-out	D402.546
	Part List 1 - 3	X402.554
CL701	Schematic	D402.385
	Part List	X402.464
	Component Lay-out	D402.512
CL702	Schematic	D402.384
	Part List	X402.465
	Component Lay-out	D402.509



CONTROL PANEL CP 705
CONTROL UNIT CB 704

D.402.570

TERMINAL BOARD, CONTROL PANEL CP 705
CONNECTOR I, CC 704 a, CONTROL UNIT CB 704

Storno

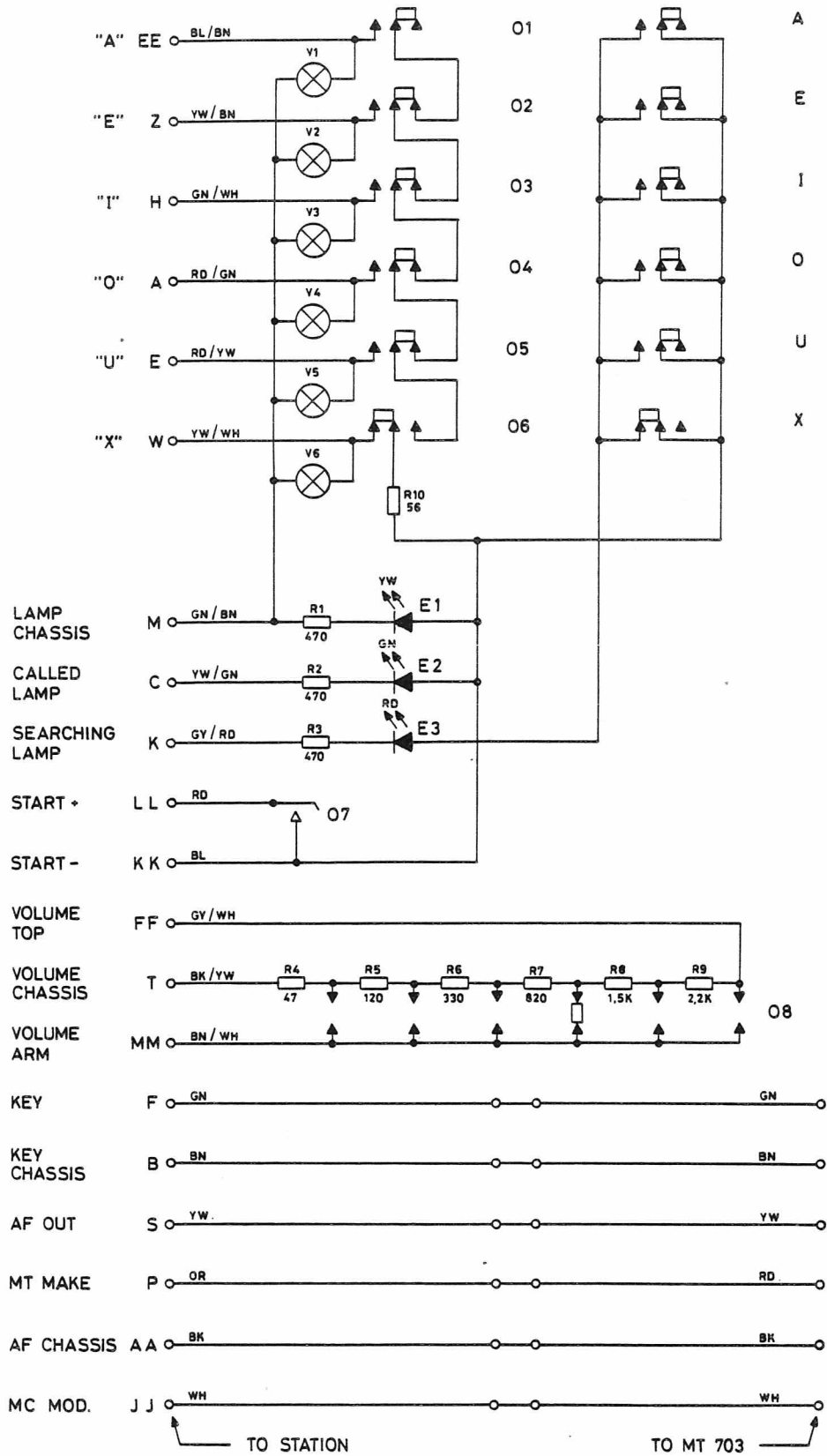
TYPE	Nº	CODE	DATA
CB704	R1	10.2445	Control Unit
	R2	80.5432	39 ohm 5% carbon film 1/4W
	R3	80.5430	27 ohm 5% carbon film 1/4W
	E1-	86.5069	5K ohm 20% potentiometer. log 0.8W
	E30	99.5237	IN 4148 Diode
	V7	92.5098	Lamp 12V/60mA
	V8	92.5098	Lamp 12V/60mA
	V9	92.5098	Lamp 12V/60mA
	V10	92.5098	Lamp 12V/60mA
	01	47.5074	Channel Selector x 10
	02	47.5074	Channel Selector x 1
	03	49.0214	Puch button. Squelch
	04	49.0207	Push button, LS in/out
	05	49.0211	Push button. On/Off
	06	49.0220	Push button. Tone Key
	07	49.0219	Push button. Key

Storno

TYPE	Nº	CODE	DATA
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CONTROL UNIT CB704

X 402.560

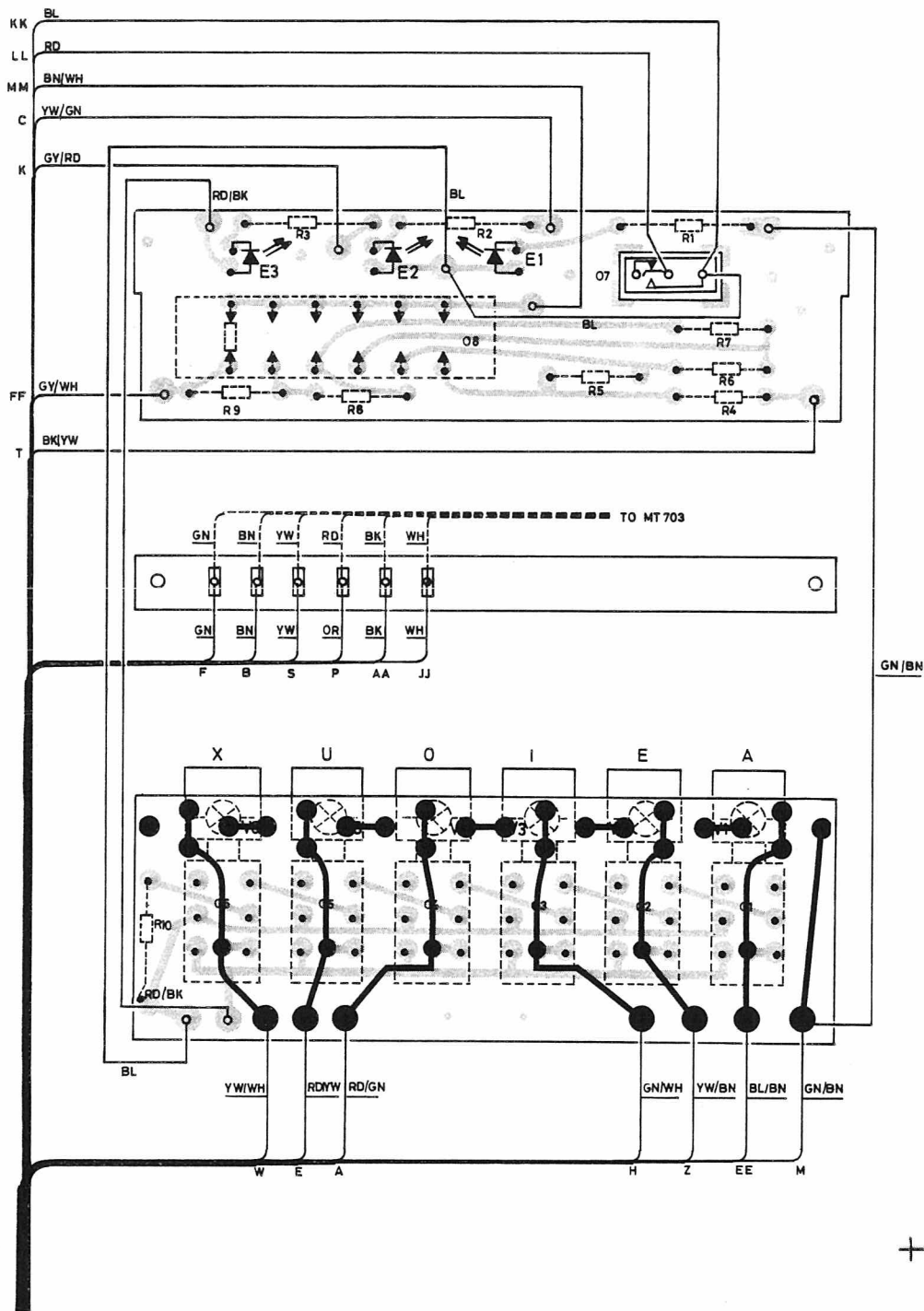


TYPE	Nº	CODE	DATA
		10. 3427	Control Unit CB705
R1		80. 5445	470 Ω 5% carbon film 1/4 W
R2		80. 5445	470 Ω 5% " " 1/4 W
R3		80. 5445	470 Ω 5% " " 1/4 W
R4		80. 5233	47 Ω 5% " " 1/8 W
R5		80. 5238	120 Ω 5% " " 1/8 W
R6		80. 5243	330 Ω 5% " " 1/8 W
R7		80. 5248	820 Ω 5% " " 1/8 W
R8		80. 5251	1.5 kΩ 5% " " 1/8 W
R9		80. 5253	2.2 kΩ 5% " " 1/8 W
R10		80. 5434	56 Ω 5% " " 1/4 W
E1		99. 5325	Yellow LED
E2		99. 5304	Green LED
E3		99. 5303	Red LED
V1		92. 5098	Lamp 12 V 60 mA
V2		92. 5098	Lamp 12 V 60 mA
V3		92. 5098	Lamp 12 V 60 mA
V4		92. 5098	Lamp 12 V 60 mA
V5		92. 5098	Lamp 12 V 60 mA
V6		92. 5098	Lamp 12 V 60 mA
O1		49. 0252	"A" Push button
O2		49. 0253	"O" Push button
O3		49. 0254	"E" Push button
O4		49. 0255	"U" Push button
O5		49. 0256	"I" Push button
O6		49. 0257	"X" Push button
O7		47. 5084	ON/OFF switch
O8		47. 0622	Volume switch

CONTROL UNIT CB705

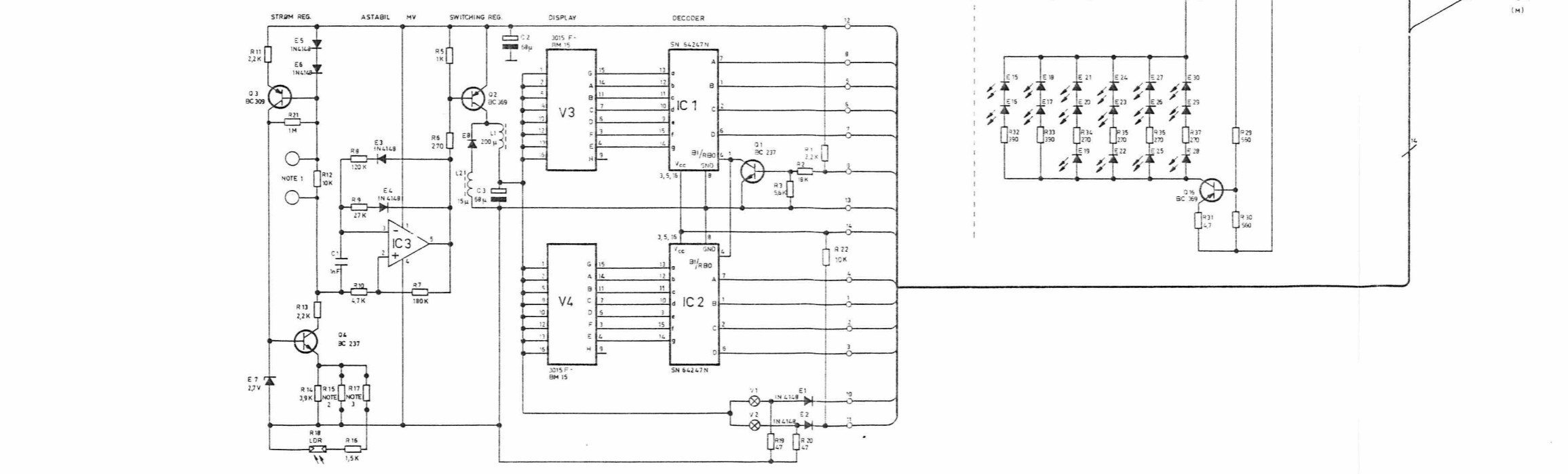
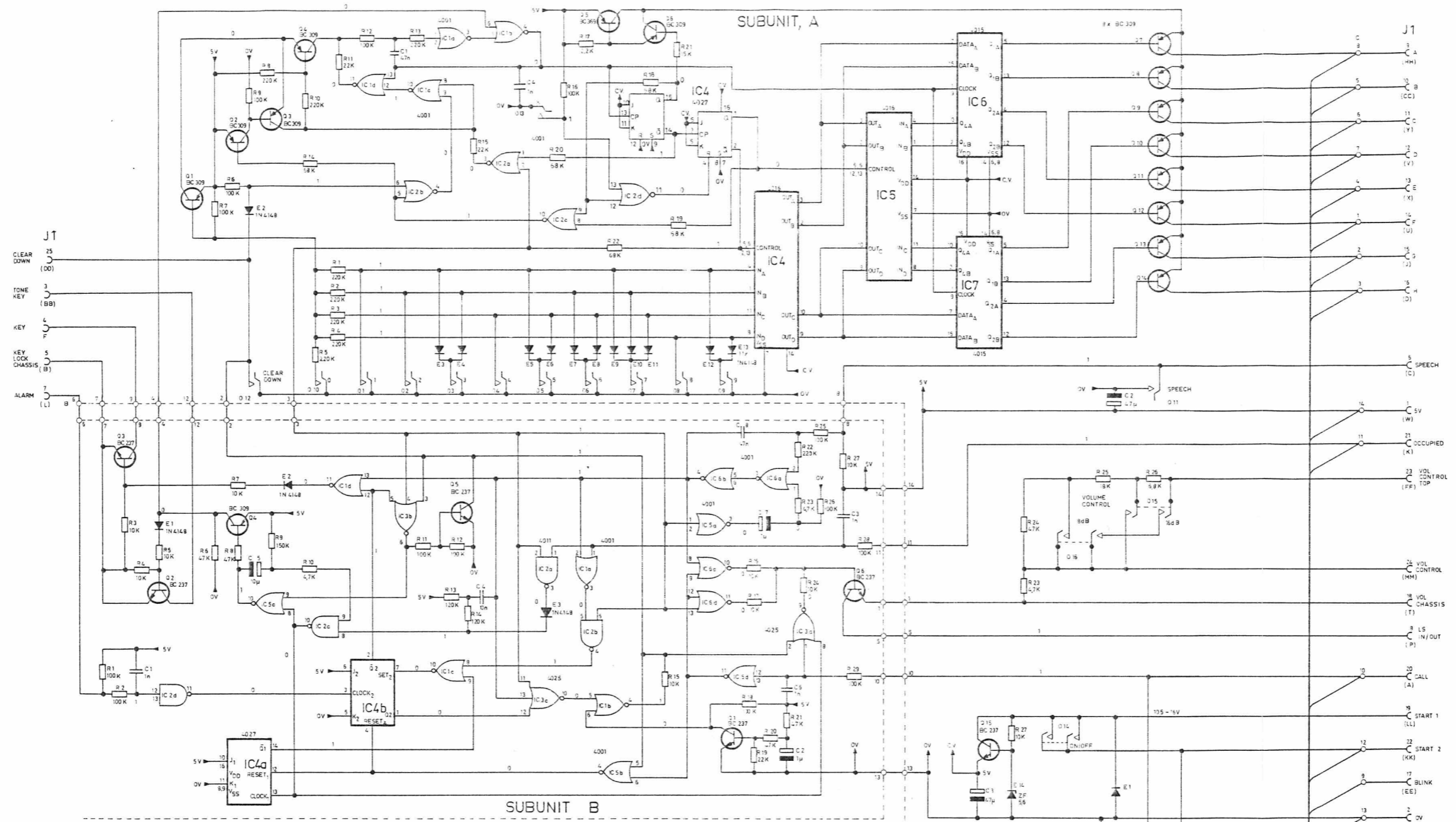
X402. 542

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TO CONNECTOR
IN CQM 713 P3.

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TYPE	NO	CODE	DATA
		10. 3626-00	CB 706 Automatic Control Unit
		15. 0349-00	Subassembly A
		15. 0359-00	Subassembly B
		15. 0360-00	Subassembly C
			<u>Subassembly A</u>
C1	76. 5072	47nF	10% polyester FL
C2	73. 5124	47uF	20% tantal
C3	73. 5124	47uF	20% tantal
C4	74. 5155	1nF	-20/+80% ceram PL
R1	80. 5077	220Kohm	5% carbon film
R2	80. 5077	220Kohm	5% "
R3	80. 5077	220Kohm	5% "
R4	80. 5077	220Kohm	5% "
R5	80. 5077	220Kohm	5% "
R6	80. 5073	100Kohm	5% "
R7	80. 5073	100Kohm	5% "
R8	80. 5077	220Kohm	5% "
R9	80. 5073	100Kohm	5% "
R10	80. 5077	220Kohm	5% "
R11	80. 5065	22Kohm	5% "
R12	80. 5073	100Kohm	5% "
R13	80. 5077	220Kohm	5% "
R14	80. 5071	68Kohm	5% "
R15	80. 5065	22Kohm	5% "
R16	80. 5073	100Kohm	5% "
R17	80. 5053	2. 2Kohm	5% "
R18	80. 5071	68Kohm	5% "
R19	80. 5071	68Kohm	5% "
R20	80. 5071	68Kohm	5% "
R21	80. 5063	15Kohm	5% "
R22	80. 5071	68Kohm	5% "
R23	80. 5057	4. 7Kohm	5% "
R24	80. 5069	47Kohm	5% "
R25	80. 5064	18Kohm	5% "
R26	80. 5059	6. 8Kohm	5% "
R27	80. 5061	10Kohm	5% "
R28			
R29	80. 5246	560ohm	5% "
R30	80. 5046	560ohm	5% "
R31	80. 5221	4. 7ohm	5% "
R32	80. 5244	390ohm	5% "

TYPE	NO	CODE	DATA
	R33	80. 5244	390ohm 5% carbon film
	R34	80. 5242	270ohm 5% "
	R35	80. 5242	270ohm 5% "
	R36	80. 5242	270ohm 5% "
	R37	80. 5242	270ohm 5% "
	E1	99. 5020	IN4004 Diode
	E2	99. 5237	IN4148 Diode
	E3	99. 5237	IN4148 Diode
	E4	99. 5237	IN4148 Diode
	E5	99. 5237	IN4148 Diode
	E6	99. 5237	IN4148 Diode
	E7	99. 5237	IN4148 Diode
	E8	99. 5237	IN4148 Diode
	E9	99. 5237	IN4148 Diode
	E10	99. 5237	IN4148 Diode
	E11	99. 5237	IN4148 Diode
	E12	99. 5237	IN4148 Diode
	E13	99. 5237	IN4148 Diode
	E14	99. 5237	IN4148 Diode
	E15-	99. 5114	5. 6V Zenerdiode
	E30	99. 5338	2. 4V Light Emitting Diode(LED) Green 20mA
	Q1	99. 5115	BC179 (BC309) Transistor
	Q2	99. 5115	BC179 (BC309) "
	Q3	99. 5115	BC179 (BC309) "
	Q4	99. 5115	BC179 (BC309) "
	Q5	99. 5337	BC369 "
	Q6	99. 5115	BC179 (BC309) "
	Q7	99. 5115	BC179 (BC309) "
	Q8	99. 5115	BC179 (BC309) "
	Q9	99. 5115	BC179 (BC309) "
	Q10	99. 5115	BC179 (BC309) "
	Q11	99. 5115	BC179 (BC309) "
	Q12	99. 5115	BC179 (BC309) "
	Q13	99. 5115	BC179 (BC309) "
	Q14	99. 5115	BC179 (BC309) "
	Q15	99. 5121	BC179 (BC309) "
	Q16	99. 5337	BC107 (BC237) "
			BC369 "
	IC1	14. 5074-01	4001B Quad 2 input NAND
	IC2	14. 5074-01	4001B Quad 2 input NAND

AUTOMATIC CONTROL UNIT CB706

X402. 628

TYPE	NO	CODE	DATA
IC3	14. 5094-01	4027B	Dual J-K master-slave FF
IC4	14. 5092	4016B	Quad bilateral switch
IC5	14. 5092	4016B	Quad bilateral switch
IC6	14. 5091	1415B	Dual 4-stage Static shift regist.
IC7	14. 5091	4015B	Dual 4-stage Static shift regist.
O1	47. 5088		Switch, type M-NO
O2	47. 5088	"	"
O3	47. 5088	"	"
O4	47. 5088	"	"
O5	47. 5088	"	"
O6	47. 5088	"	"
O7	47. 5088	"	"
O8	47. 5088	"	"
O9	47. 5088	"	"
O10	47. 5088	"	"
O11	47. 5088	"	"
O12	47. 5088	"	"
O13	47. 5088	"	"
O14	47. 5095		Switch, type A-OO
O15	47. 5095	"	"
O16	47. 5095	"	"
C1	76. 5069		Subassembly B
C2	73. 5114	1nF	10% polyester FL
C3	76. 5069	1uF	20% tantal
C4	76. 5070	1nF	10% polyester FL
C5	73. 5109	10nF	10% polyester FL
C6	76. 5069	10uF	20% tantal
C7	73. 5114	1uF	10% polyester FL
C8	76. 5072	47nF	10% polyester FL
R1	80. 5073	100Kohm	5% carbon film
R2	80. 5073	100Kohm	5% "
R3	80. 5061	10Kohm	5% "
R4	80. 5061	10Kohm	5% "
R5	80. 5061	10Kohm	5% "
R6	80. 5069	47Kohm	5% "
R7	80. 5061	10Kohm	5% "
R8	80. 5069	47Kohm	5% "
R9	80. 5075	150Kohm	5% "
R10	80. 5057	4. 7Kohm	5% "
R11	80. 5073	100Kohm	5% "
R12	80. 5073	100Kohm	5% "

TYPE	NO	CODE	DATA
R13	80. 5074	120Kohm	5% carbon film
R14	80. 5074	120Kohm	5% "
R15	80. 5061	10Kohm	5% "
R16	80. 5061	10Kohm	5% "
R17	80. 5061	10Kohm	5% "
R18	80. 5073	100Kohm	5% "
R19	80. 5065	22Kohm	5% "
R20	80. 5069	47Kohm	5% "
R21	80. 5069	47Kohm	5% "
R22	80. 5077	22Kohm	5% "
R23	80. 5057	4. 7Kohm	5% "
R24	80. 5061	10Kohm	5% "
R25	80. 5073	100Kohm	5% "
R26	80. 5073	100Kohm	5% "
R27	80. 5061	10Kohm	5% "
R28	80. 5073	100Kohm	5% "
R29	80. 5073	100Kohm	5% "
E1	99. 5237	IN4148	Diode
E2	99. 5237	IN4148	Diode
E3	99. 5237	IN4148	Diode
Q1	99. 5121	BC107	Transistor
Q2	99. 5121	BC107	Transistor
Q3	99. 5121	BC107	Transistor
Q4	99. 5115	BC179	Transistor
Q5	99. 5121	BC107	Transistor
Q6	99. 5121	BC107	Transistor
C1	765069	Subassembly C	
C2	73. 5106	1nF	10% polyester. FL
C3	73. 5106	68uF	20% tantal.
R1	80. 5053	2. 2Kohm	5% carbon film
R2	80. 5064	18Kohm	5% "
R3	80. 5058	5. 6Kohm	5% "
R4		Not used	
R5	80. 5049	1Kohm	5% "
R6	80. 5242	270 ohm	5% "
R7	80. 5076	180Kohm	5% "
R8	80. 5074	120Kohm	5% "

AUTOMATIC CONTROL UNIT CB706

X402. 628

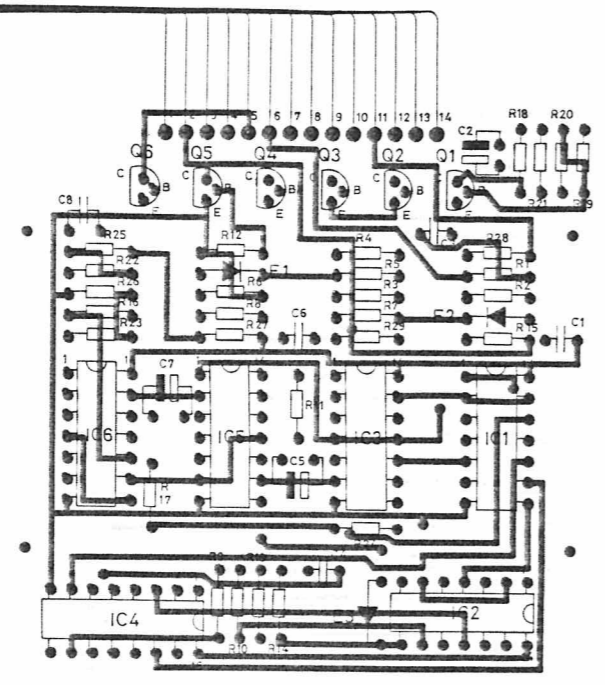
TYPE	Nº	CODE	DATA
R9	80.5066		27Kohm
R10	80.5057		5% carbon film
R11	80.5053		4.7Kohm
R12	80.5061		5%
R13	80.5053		2.2Kohm
R14	80.5056		5%
R15	80.50xx		10Kohm
R16	80.5051		5%
R17	80.50xx		2.2Kohm
R18	80.5081		5%
R19	80.5233		3.9Kohm
R20	80.5233		ADJ
R21	80.5085		5%
R22	80.5261		1.5Kohm
L1	61.5024		ADJ
L2	63.5007		1.5Kohm
E1	99.5237		Light Dependent Resistor (LDR)
E2	99.5237		5% carbon film
E3	99.5237		47ohm
E4	99.5237		5%
E5	99.5237		1Mohm
E6	99.5237		10%
E7	99.5227		10Kohm
E8	99.5296		5%
Q1	99.5121		180uH
Q2	99.5337		Choke
Q3	99.5115		15uH
Q4	99.5121		Choke
IC1	14.5095		IN4148 Diode
IC2	14.5095		IN4148 Diode
IC3	14.5017		IN4148 Diode
V1	92.5119		IN4148 Diode
V2	92.5119		2.7V Zenerdiode
V3	92.5118		BY201/2 Diode
V4	92.5118		BC107 Transistor
			BC369 Transistor
			BC179 Transistor
			BC107 Transistor
			SN64247 BCD 7-segment Decoder/driver
			SN64247 BCD 7-segment Decoder/driver
			TAA765A Operational amplifier.
			Lamp 6-7V
			Lamp 6-7V
			Display
			Display
			500mA

TYPE	Nº	CODE	DATA

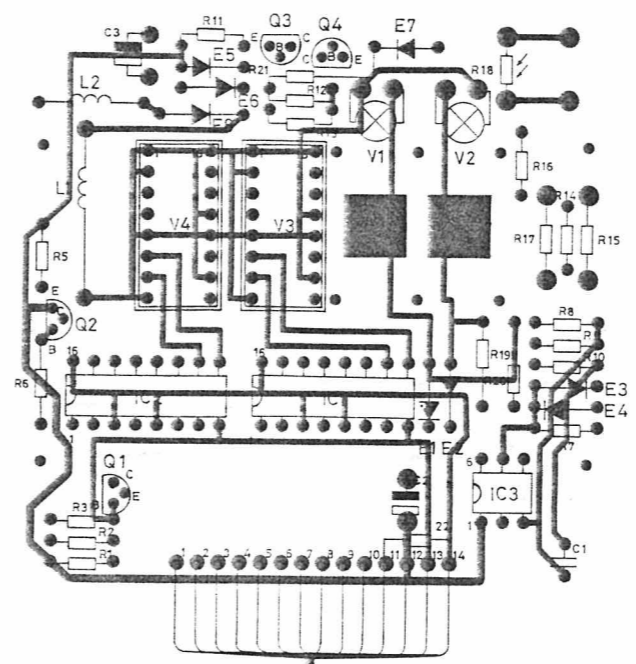
AUTOMATIC CONTROL UNIT CB706

X402.628

B

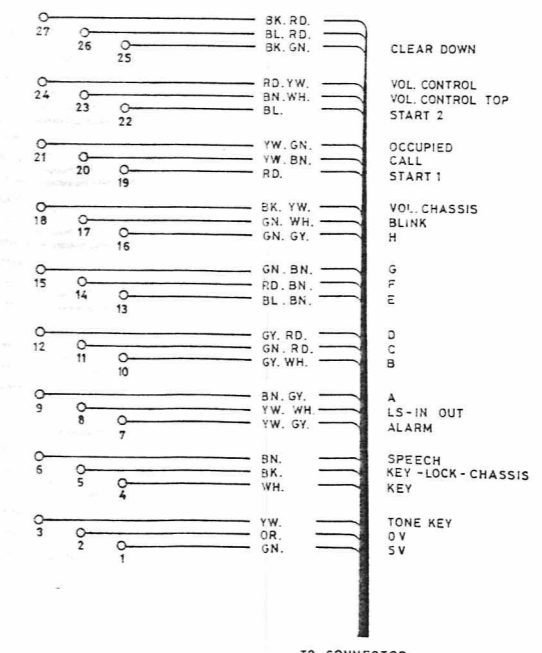
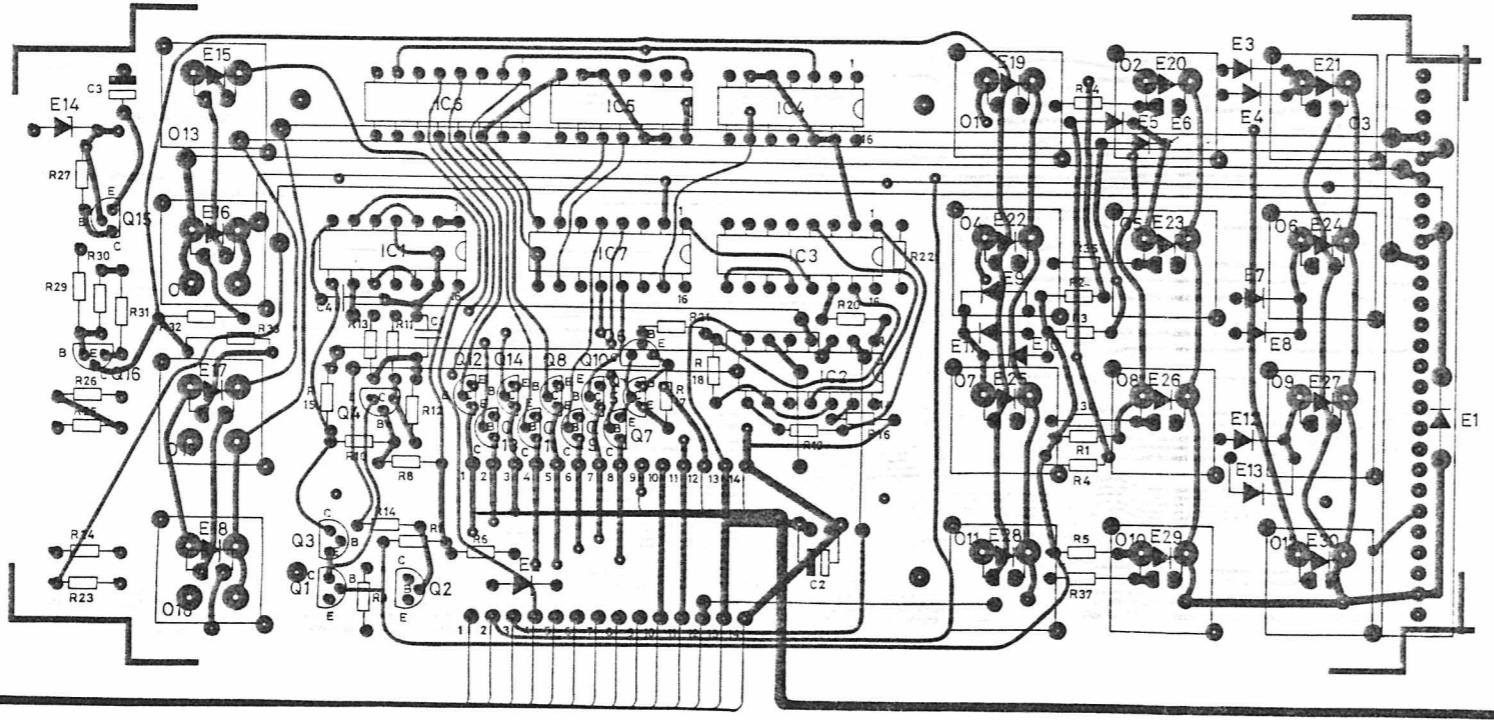


C



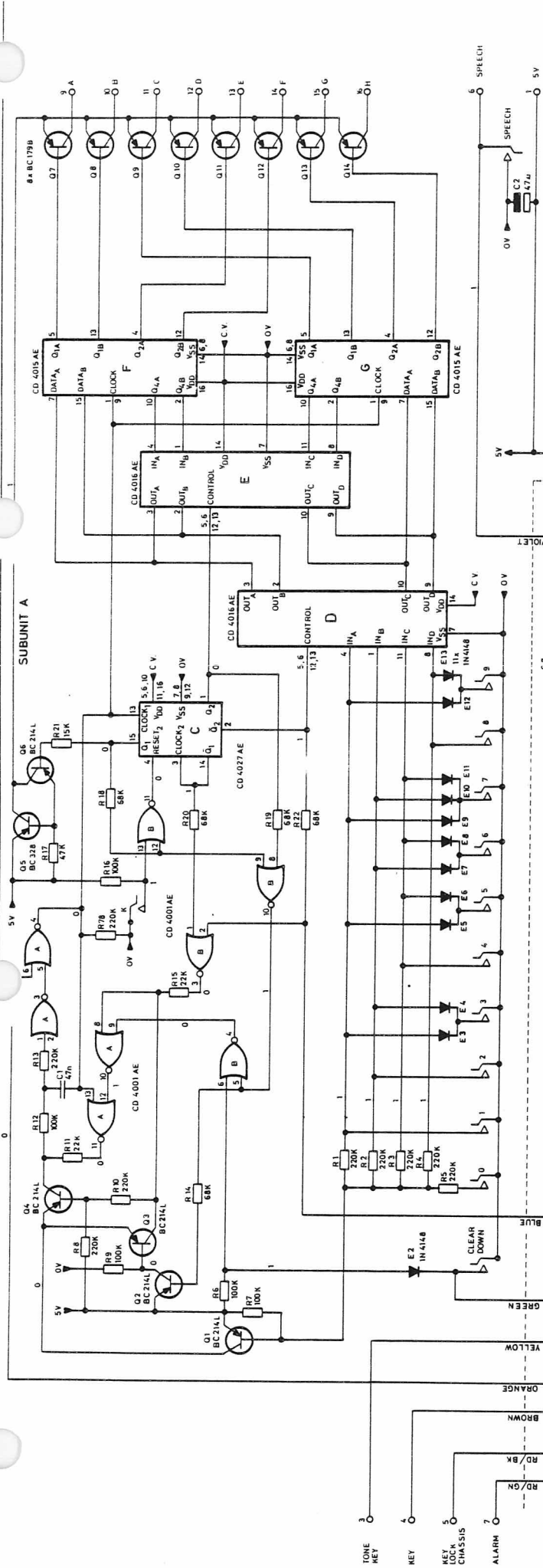
PRINTED CIRCUITS VIEWED FROM COMPONENT SIDE

A

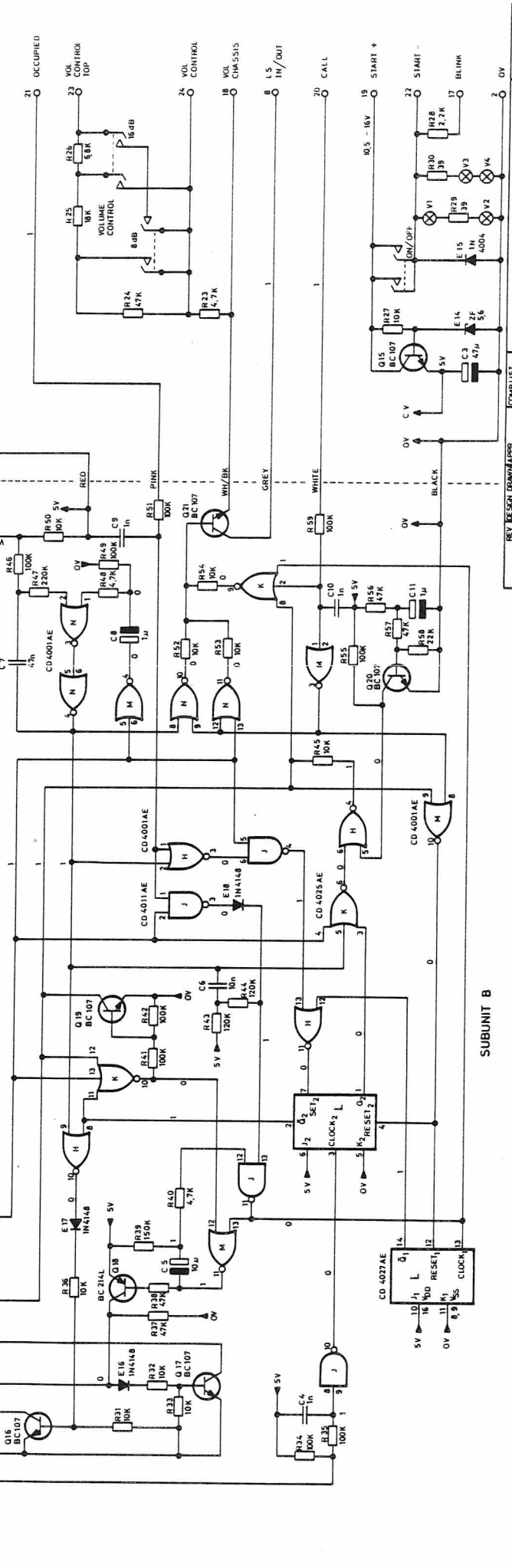


TO CONNECTOR

SUBUNIT A



SUBUNIT B



REV DESGN DRAWN APPR
 24 0 30 450 L1/1950
 27 10 25 400

COMPLETE
 54402 039
 54402 036

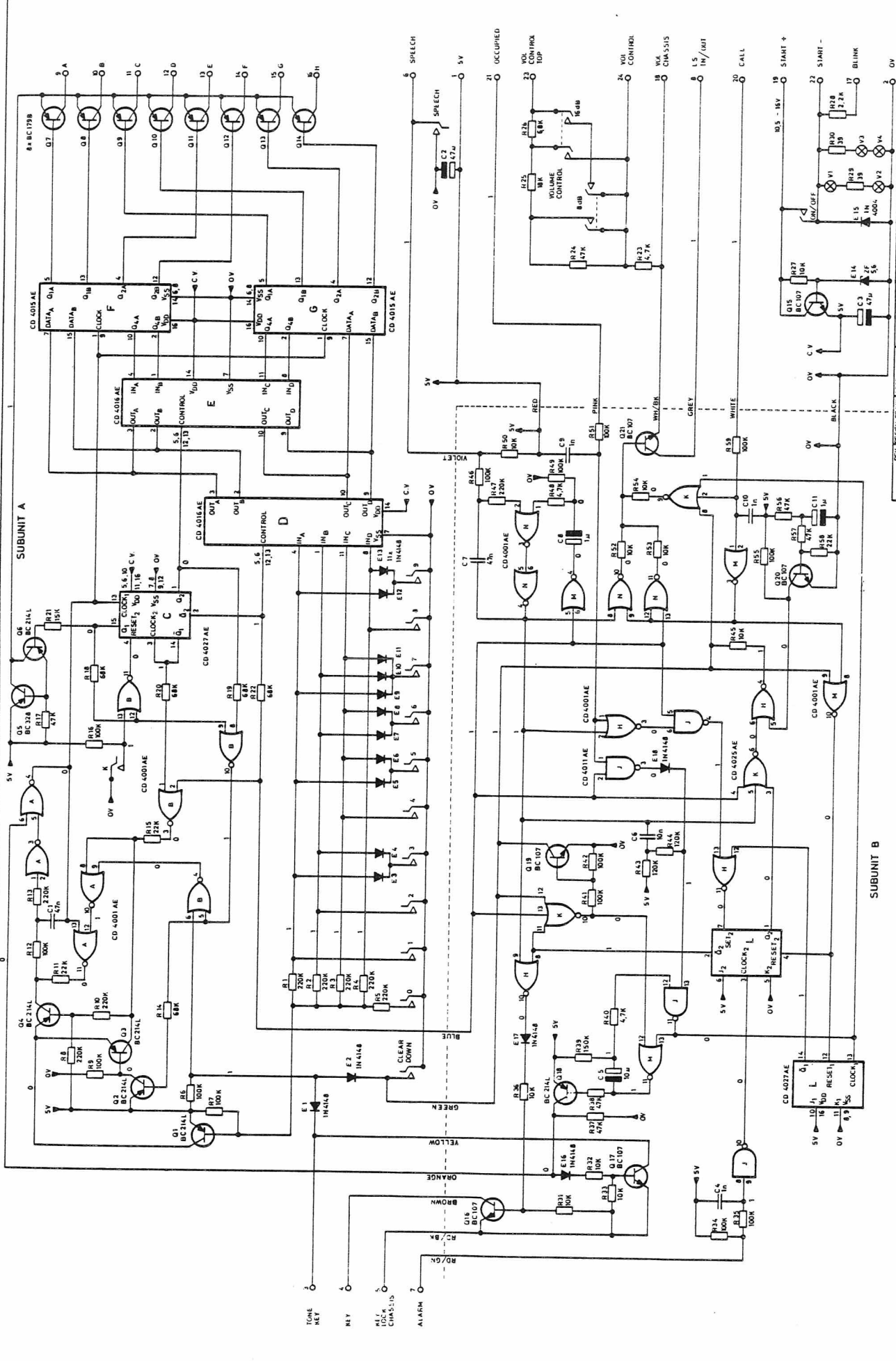
DATE
 21 11 74
 42 BRW/NO

CONTROL BOX FOR 700 AUTOMATIC
 CB 2706

D402 02/8/72



STERNO
 RADIO COMMUNICATION SYSTEMS



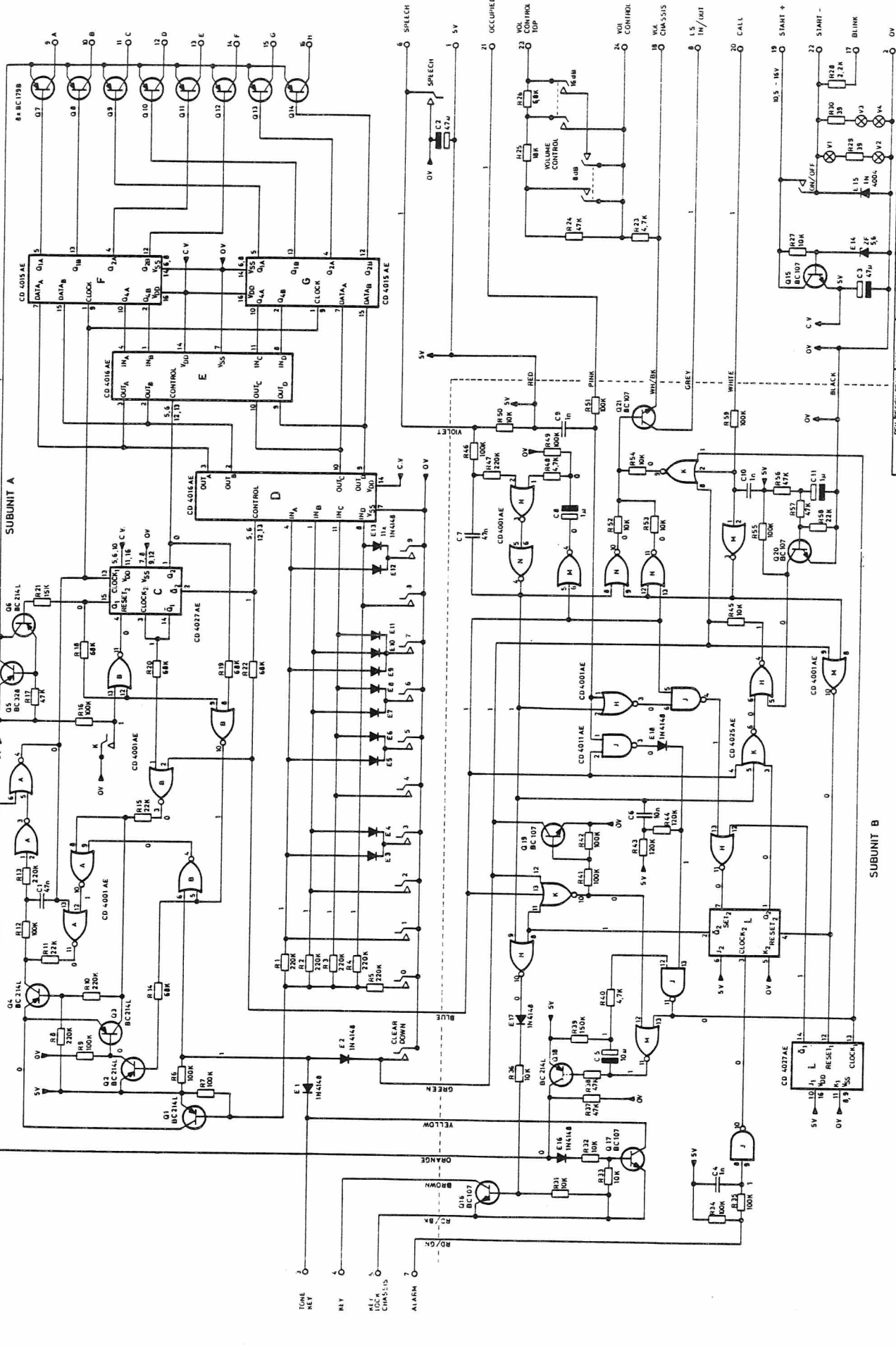
SUBUNIT A

SUBUNIT B

REV. 10/78
 L11/11/80
 COMPLIST
 51402 029
 51402 036

CONTROL BOX FOR 700 AUTOMATIC
 CB 2706

DATE 21.11.78
 DRAWING NO. A28RWG10
 D 402 028



TYPE	NO.	CODE	DATA
		15. 0232-00	Subunit A. Part of CB2706
	C1	76. 5072-00	47 nF 10% Polyester FL 50 W
	C2	73. 5124-00	47 μF 20% Tantalum 6, 3 V
	C3	73. 5124-00	47 μF 20% Tantalum 6, 3 V
	R1	80. 5277-00	220 KΩ 5% Carbon film 1/8 W
	R2	80. 5277-00	220 KΩ 5% Carbon film 1/8 W
	R3	80. 5277-00	220 KΩ 5% Carbon film 1/8 W
	R4	80. 5277-00	220 KΩ 5% Carbon film 1/8 W
	R5	80. 5277-00	220 KΩ 5% Carbon film 1/8 W
	R6	80. 5273-00	100 KΩ 5% Carbon film 1/8 W
	R7	80. 5273-00	100 KΩ 5% Carbon film 1/8 W
	R8	80. 5277-00	220 KΩ 5% Carbon film 1/8 W
	R9	80. 5273-00	100 KΩ 5% Carbon film 1/8 W
	R10	80. 5277-00	220 KΩ 5% Carbon film 1/8 W
	R11	80. 5265-00	22 KΩ 5% Carbon film 1/8 W
	R12	80. 5273-00	100 KΩ 5% Carbon film 1/8 W
	R13	80. 5277-00	220 KΩ 5% Carbon film 1/8 W
	R14	80. 5271-00	68 KΩ 5% Carbon film 1/8 W
	R15	80. 5265-00	22 KΩ 5% Carbon film 1/8 W
	R16	80. 5273-00	100 KΩ 5% Carbon film 1/8 W
	R17	80. 5269-00	47 KΩ 5% Carbon film 1/8 W
	R18	80. 5271-00	68 KΩ 5% Carbon film 1/8 W
	R19	80. 5271-00	68 KΩ 5% Carbon film 1/8 W
	R20	80. 5271-00	68 KΩ 5% Carbon film 1/8 W
	R21	80. 5263-00	15 KΩ 5% Carbon film 1/8 W
	R22	80. 5271-00	68 KΩ 5% Carbon film 1/8 W
	R23	80. 5257-00	4, 7 KΩ 5% Carbon film 1/8 W
	R24	80. 5269-00	47 KΩ 5% Carbon film 1/8 W
	R25	80. 5264-00	18 KΩ 5% Carbon film 1/8 W
	R26	80. 5259-00	6, 8 KΩ 5% Carbon film 1/8 W
	R27	80. 5261-00	10 KΩ 5% Carbon film 1/8 W
	R28	80. 5253-00	2, 2 KΩ 5% Carbon film 1/8 W
	R29	80. 5232-00	39 Ω 5% Carbon film 1/8 W
	R30	80. 5232-00	39 Ω 5% Carbon film 1/8 W
	E1	99. 5237-00	IN4148 Diode
	E2	99. 5237-00	IN4148 Diode
	E3	99. 5237-00	IN4148 Diode
	E4	99. 5237-00	IN4148 Diode
	E5	99. 5237-00	IN4148 Diode
	E6	99. 5237-00	IN4148 Diode
	E7	99. 5237-00	IN4148 Diode
	E8	99. 5237-00	IN4148 Diode
	E9	99. 5237-00	IN4148 Diode
	E10	99. 5237-00	IN4148 Diode
	E11	99. 5237-00	IN4148 Diode

TYPE	NO.	CODE	DATA
	E12	99. 5237-00	IN4148 Diode
	E13	99. 5237-00	IN4148 Diode
	E14	99. 5114-00	5, 6 V 5% Zener diode 0, 25 W
	E15	99. 5020-00	IN4004 Diode
	IC A	14. 5074-00	CD4001 AE Quad 2-input NOR
	IC B	14. 5074-00	CD4001 AE Quad 2-input NOR
	IC C	14. 5094-00	CD4027 AE Dual J-K Master-slave F-F
	IC D	14. 5092-00	CD4016 AE Quad Bilateral switch
	IC E	14. 5092-00	CD4016 AE Quad Bilateral switch
	IC F	14. 5091-00	CD4015 AE Dual 4-stage static shift reg.
	IC G	14. 5091-00	CD4015 AE Dual 4-stage static shift reg.
	Q1	99. 5144-00	BC214L Transistor PNP
	Q2	99. 5144-00	BC214L Transistor PNP
	Q3	99. 5144-00	BC214L Transistor PNP
	Q4	99. 5144-00	BC214L Transistor PNP
	Q5	99. 5305-00	BC328 Transistor PNP
	Q6	99. 5344-00	BC214L Transistor PNP
	Q7	99. 5115-01	BC179 B Transistor PNP
	Q8	99. 5115-01	BC179 B Transistor PNP
	Q9	99. 5115-01	BC179 B Transistor PNP
	Q10	99. 5115-01	BC179 B Transistor PNP
	Q11	99. 5115-01	BC179 B Transistor PNP
	Q12	99. 5115-01	BC179 B Transistor PNP
	Q13	99. 5115-01	BC179 B Transistor PNP
	Q14	99. 5115-01	BC179 B Transistor PNP
	Q15	99. 5121-00	BC109 Transistor NPN
	O 1	47. 5064-00	Push button 1
	O 2	47. 5064-00	Push button 1
	O 3	47. 5064-00	Push button 1
	O 4	47. 5064-00	Push button 1
	O 5	47. 5064-00	Push button 1
	O 6	47. 5064-00	Push button 1
	O 7	47. 5064-00	Push button 1
	O 8	47. 5064-00	Push button 1
	O 9	47. 5064-00	Push button 1
	O 10	47. 5064-00	Push button 1
	O 11	47. 5064-00	Push button 1
	O 12	47. 5064-00	Push button 1
	O 13	47. 5064-00	Push button 1

**CONTROL UNIT CB2706
Subunit A**

X402. 029

Storno

TYPE	NO.	CODE	DATA
	O 14	47.5065-00	Push button 1-1
	O 15	47.5065-00	Push button 1-1
	O 16	47.5065-00	Push button 1-1
	V 1	92.5101-00	Indicator lamp
	V 2	92.5101-00	Indicator lamp
	V 3	92.5101-00	Indicator lamp
	V 4	92.5101-00	Indicator lamp

Storno

TYPE	NO.	CODE	DATA
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CONTROL UNIT CB2706
Subunit A

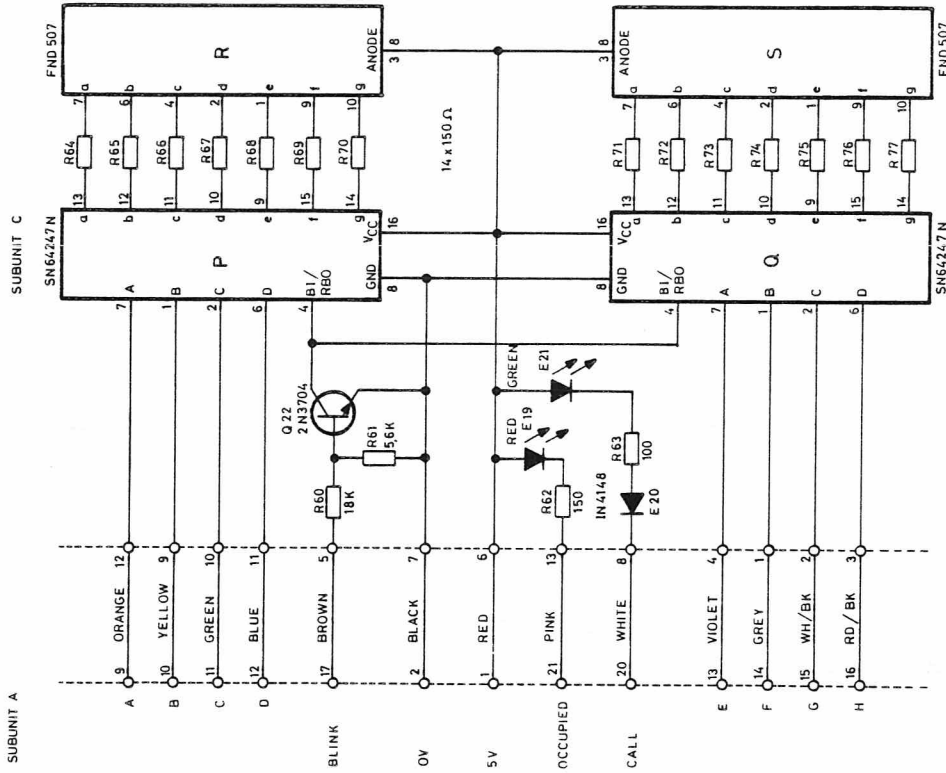
X402.029

TYPE	NO.	CODE	DATA
		15. 0233-00	Subunit B. Part of CB2706
C4		76. 5069-00	1 nF 10% Polyester FL
C5		73. 5109-00	10 μF 20% Tantalum
C6		76. 5070-00	10 nF 10% Polyester FL
C7		76. 5072-00	47 nF 10% Polyester FL
C8		73. 5114-00	1 μF 20% Tantalum
C9		76. 5069-00	1 nF 10% Polyester FL
C10		76. 5069-00	1 nF 10% Polyester FL
C11		73. 5114-00	1 μF 20% Tantalum
R31		80. 5261-00	10 KΩ 5% Carbon film
R32		80. 5261-00	10 KΩ 5% Carbon film
R33		80. 5261-00	10 KΩ 5% Carbon film
R34		80. 5273-00	100 KΩ 5% Carbon film
R35		80. 5273-00	100 KΩ 5% Carbon film
R36		80. 5261-00	10 KΩ 5% Carbon film
R37		80. 5269-00	47 KΩ 5% Carbon film
R38		80. 5269-00	47 KΩ 5% Carbon film
R39		80. 5275-00	150 KΩ 5% Carbon film
R40		80. 5257-00	4.7 KΩ 5% Carbon film
R41		80. 5273-00	100 KΩ 5% Carbon film
R42		80. 5273-00	100 KΩ 5% Carbon film
R43		80. 5274-00	120 KΩ 5% Carbon film
R44		80. 5274-00	120 KΩ 5% Carbon film
R45		80. 5261-00	10 KΩ 5% Carbon film
R46		80. 5273-00	100 KΩ 5% Carbon film
R47		80. 5277-00	220 KΩ 5% Carbon film
R48		80. 5257-00	4.7 KΩ 5% Carbon film
R49		80. 5273-00	100 KΩ 5% Carbon film
R50		80. 5261-00	10 KΩ 5% Carbon film
R51		80. 5273-00	100 KΩ 5% Carbon film
R52		80. 5261-00	10 KΩ 5% Carbon film
R53		80. 5261-00	10 KΩ 5% Carbon film
R54		80. 5261-00	10 KΩ 5% Carbon film
R55		80. 5273-00	100 KΩ 5% Carbon film
R56		80. 5269-00	47 KΩ 5% Carbon film
R57		80. 5269-00	47 KΩ 5% Carbon film
R58		80. 5265-00	22 KΩ 5% Carbon film
R59		80. 5273-00	100 KΩ 5% Carbon film
E16		99. 5237-00	Diode
E17		99. 5237-00	Diode
E18		99. 5237-00	Diode
IC H		CD 4001 AE	Quad 2-input NOR
IC J		CD 4011 AE	Quad 2-input NAND

TYPE	NO.	CODE	DATA
	IC K	14. 5093-00	CD 4025 AE Triple 3-input NOR-Gates
	IC L	14. 5094-00	CD 4027 AE Dual J-K Master-slave F-F
	IC M	14. 5074-00	CD 4001 AE Quad 2-input NOR
	IC N	14. 5074-00	CD 4001 AE Quad 2-input NOR
	Q16	99. 5121-00	BC 107 Transistor NPN
	Q17	99. 5121-00	BC 107 Transistor NPN
	Q18	99. 5144-00	BC 214 L Transistor PNP
	Q19	99. 5121-00	BC 107 Transistor NPN
	Q20	99. 5121-00	BC 107 Transistor NPN
	Q21	99. 5121-00	BC 107 Transistor NPN

CONTROL UNIT CB2706
Subunit B

X402. 036



CONTROL UNIT CB2706
Subunit C

D402.0331/2

Storno

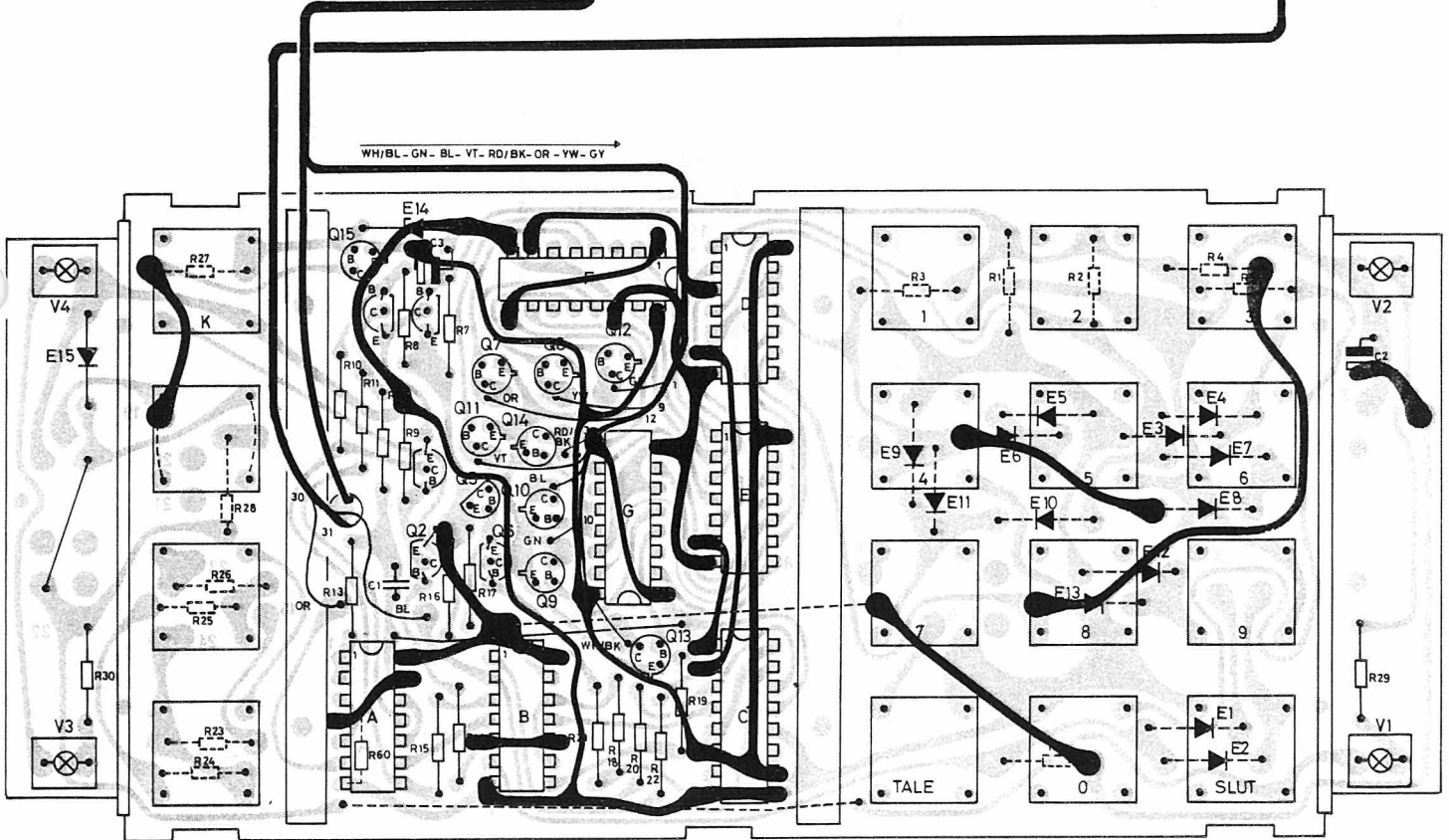
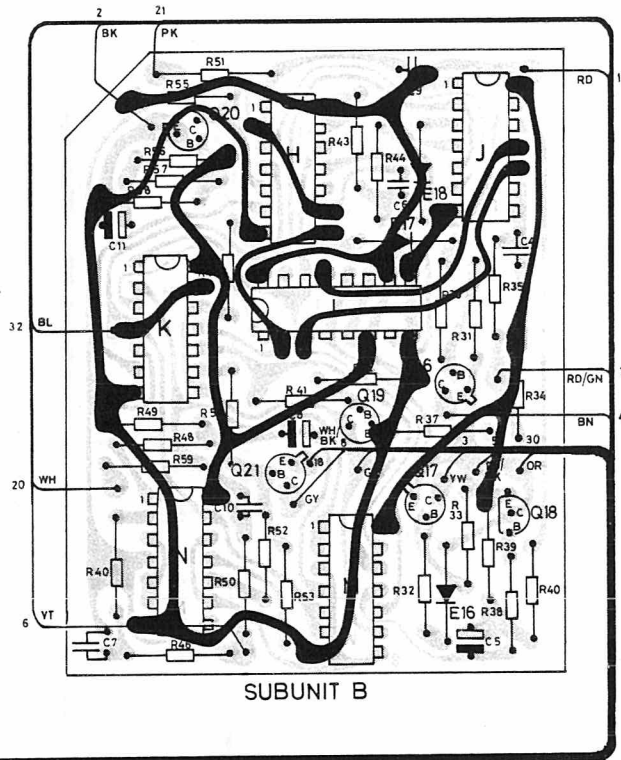
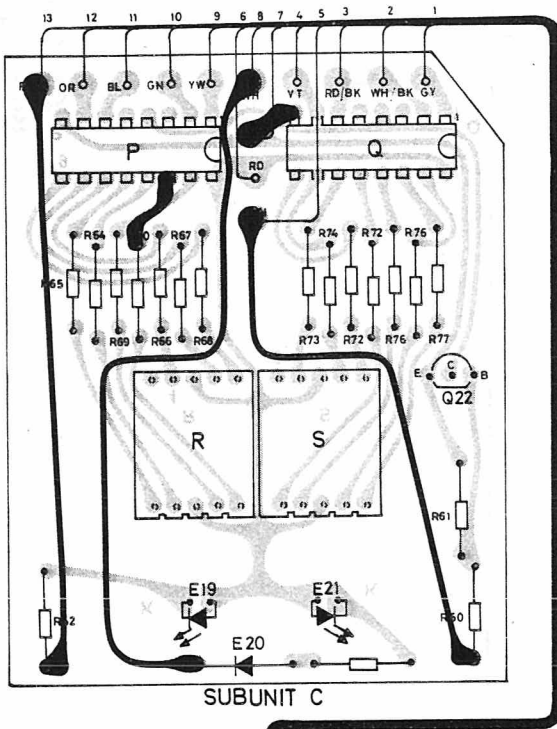
TYPE	NO.	CODE	DATA
		15. 0234-00	Subunit C. Part of CB2706
R60		80. 5264-00	18 KΩ Carbon film 1/8 W
R61		80. 5258-00	Carbon film 1/8 W
R62		80. 5239-00	5, 6 KΩ Carbon film 1/8 W
R63		80. 5237-00	100 Ω Carbon film 1/8 W
R64		80. 5239-00	150 Ω Carbon film 1/8 W
R65		80. 5239-00	150 Ω Carbon film 1/8 W
R66		80. 5239-00	150 Ω Carbon film 1/8 W
R67		80. 5239-00	150 Ω Carbon film 1/8 W
R68		80. 5239-00	150 Ω Carbon film 1/8 W
R69		80. 5239-00	150 Ω Carbon film 1/8 W
R70		80. 5239-00	150 Ω Carbon film 1/8 W
R71		80. 5239-00	150 Ω Carbon film 1/8 W
R72		80. 5239-00	150 Ω Carbon film 1/8 W
R73		80. 5239-00	150 Ω Carbon film 1/8 W
R74		80. 5239-00	150 Ω Carbon film 1/8 W
R75		80. 5239-00	150 Ω Carbon film 1/8 W
R76		80. 5239-00	150 Ω Carbon film 1/8 W
R77		80. 5239-00	150 Ω Carbon film 1/8 W
E19		99. 5303-00	LED 1, 9 V 10mA red
E20		99. 5237-00	1N4148 Diode
E21		99. 5304-00	LED 1, 9 V 10mA green
Q22		99. 5181-00	2N3704 Transistor NPN
IC P		14. 5095-00	SN64 247 N BCD - Seven segment Decoder/Driver
IC Q		14. 5095-00	SN64 247 N BCD - Seven segment Decoder/Driver
IC R		14. 5096-00	FND507 Seven segment Display
IC S		14. 5096-00	FND507 Seven segment Display

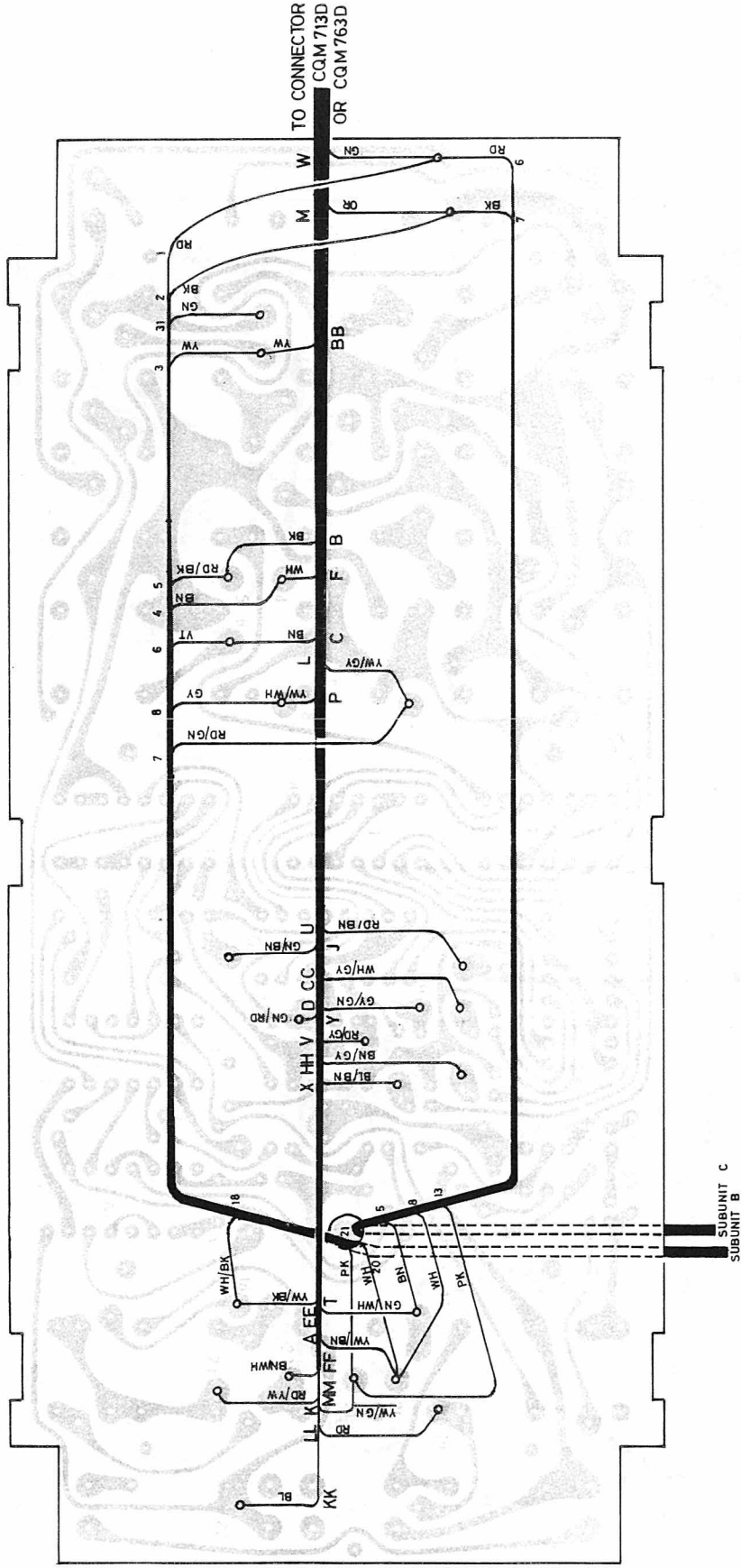
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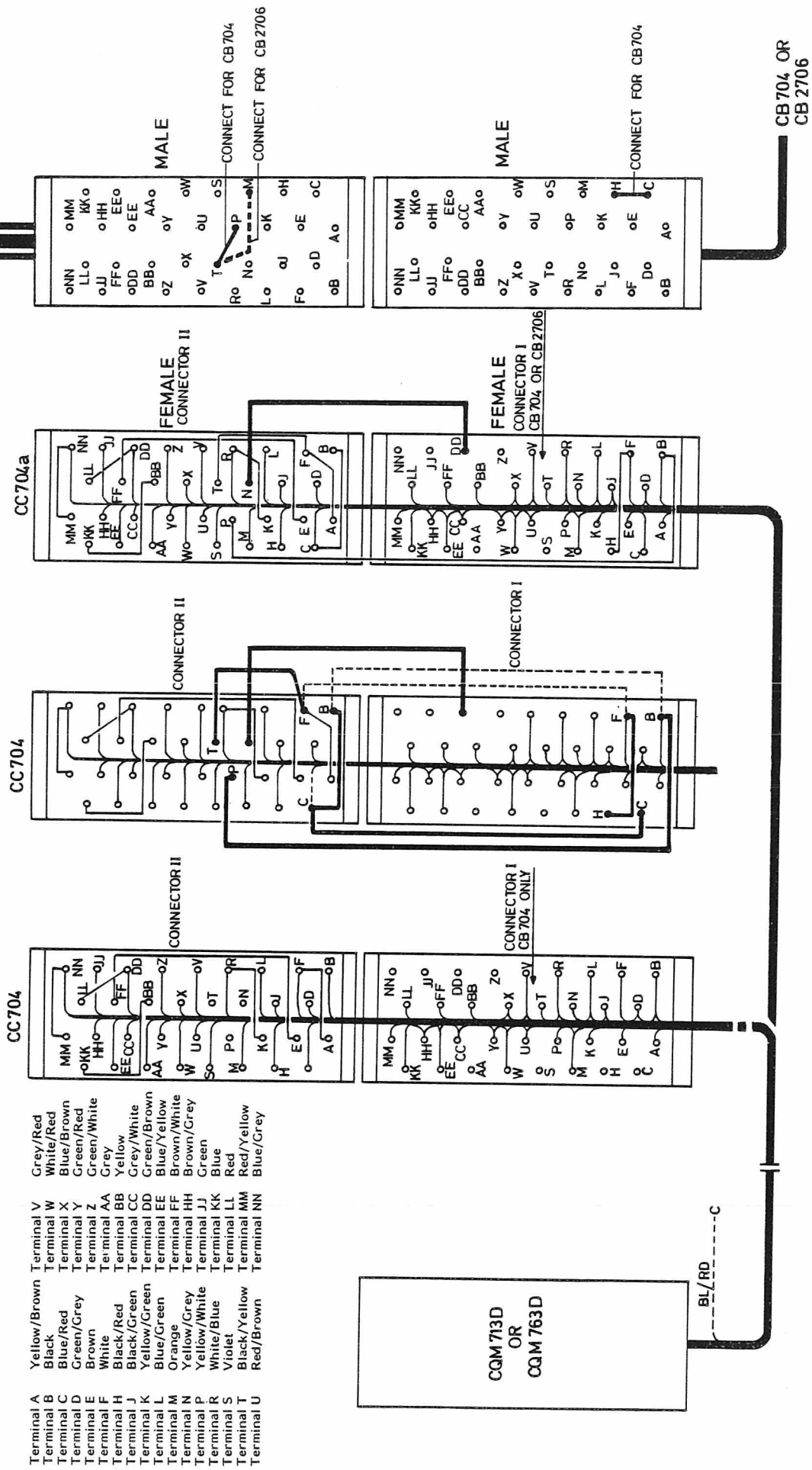
CONTROL UNIT CB2706
Subunit C

X402. 034





CONTROL UNIT CB2706
Wiring



MODIFYING EXTENSION CABLE CC704 TO CC704a

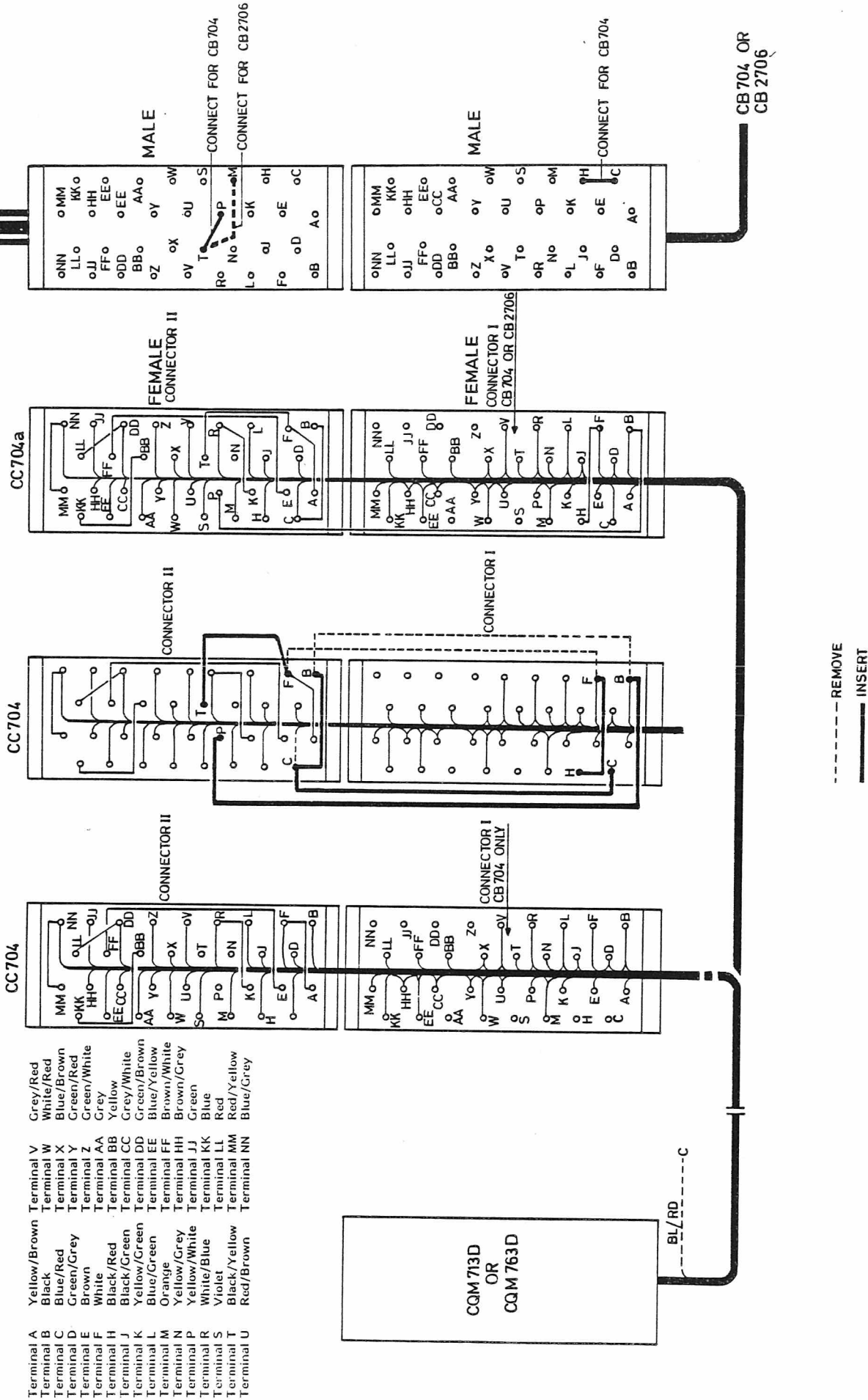
TYPE	NO	CODE	DATA
	R124	80.5230	27 Ω
	R125	80.5237	100 Ω
	R126	80.5213	1 Ω
	R127	80.5252	1.8 KΩ
	L1	61.1132	Squelch coil 75 mH
	L2	61.1131	IA coil 455 kHz
	E1	99.5237	1 N 4148 Diode
	E2	99.5237	1 N 4148 "
	E3	99.5042	Zenerdiode 9.1 V 5%
	E4	99.5209	Stabilizerdiode 1.5 V
	E5	99.5237	1 N 4148 Diode
	E6	99.5237	1 N 4148 "
	E7	99.5237	1 N 4148 "
	E8	99.5237	1 N 4148 "
	E9	99.5020	1 N 4004 "
	E10	99.5237	1 N 4148 "
	E11	99.5209	Stabilizerdiode 1.5 V
	E12	99.5237	1 N 4148 Diode
	E13 E14	99.5237	1 N 4148 "
	E15	99.5224	Zenerdiode 4.7 V 5%
	E16	99.5237	1 N 4148 Diode
	E17	99.5224	Zenerdiode 4.7 V 5%
	E18	99.5209	1.5 V Stab. diode
	Q1	99.5144	Transistor
	Q2	99.5143	"
	Q3	99.5143	"
	Q4	99.5143	"
	Q5	99.5143	"
	Q6	99.5201	"
	Q7	99.5115	"
	Q8	99.5115	"
	Q9	99.5143	"
	Q20	99.5246	"
	Q21	99.5144	"
	Q22	99.5143	"
	Q23	99.5143	"
	Q24	99.5246	"
	Q25	99.5144	"
	Q26	99.5143	"
	Q27	99.5143	"
	Q28	99.5143	"
	Q29	99.5115	"
	Q30	99.5326	"
	Q31	99.5326	"
	Q32	99.5143	"
	T1	61.1130	IA transformer

CF704

TYPE	NO	CODE	DATA
	T2	61.1130	IA transformer
	IC1	14.5105	MC1458 Dual OP-amp.
	IC2	14.5105	MC1458 Dual OP-amp.
	IC3	14.5010	IF Amplifier/Discr. ULN 2111 N
	IC4	14.5104	Audio Power Amplifier TBA 810 AS
	ReA	58.5084	Relay 330 Ω 12 V

COMMON FUNCTIONS CF703, CF704

X402.429/2



MODIFYING EXTENSION CABLE CC704 TO CC704a

TYPE	Nº	CODE	DATA
CF703 CF704	C1	10.3364-00	Common Functions
	C2	10.3499	Common Functions
	C3	76.5070	10 nF 10% 50 V
	C4	73.5127	22 µF 20% 16 V
	C5	73.5126	4.7 µF 20% 35 V
	C6	76.5072	47 nF 10% 50 V
	C7	76.5060	3.3 nF 10% 50 V
	C8	76.5063	220 pF 5% 160 V
	C9	76.5070	10 nF 10% 50 V
	C10	73.5114	1 µF 10% 50 V
	C11	73.5127	22 µF 20% 35 V
	C12	73.5102	2.2 µF 20% 16 V
	C13	76.5071	22 nF 10% 35 V
	C14	73.5114	1 µF 20% 50 V
	C15	76.5072	47 nF 10% 35 V
	C16	76.5061	47 nF 10% 50 V
	C17	74.5155	4.7 nF 10% 50 V
	C18	73.5102	2.2 µF 20% 63 V
	C19	76.5070	10 nF 10% 35 V
	C20	76.5070	10 nF 10% 50 V
	C21	76.5060	3.3 nF 10% 50 V
	C22	76.5060	3.3 nF 10% 50 V
	C23	76.5072	47 nF 10% 50 V
	C24	73.5126	22 µF 20% 50 V
	C25	73.5127	22 µF 20% 16 V
	C26	73.5125	0.47 µF 20% 35 V
	C27	73.5125	0.47 µF 20% 35 V
	C28	74.5161	470 pF -20 + 80% ceram 63 V
	C31	73.5071	100 µF -10 + 50% elko 40 V
	C32	76.5072	47 nF 10% polyester FL 50 V
	C33	74.5187	39 pF 10% ceram PL 25 V
	C34	73.5114	1 µF 20% tantal 35 V
	C35	73.5011	10 µF -10 + 100% elko 16 V
	C36	73.5114	1 µF 20% tantal 35 V
	C37	74.5187	39 pF 10% ceram PL 25 V
	C38	73.5114	1 µF 20% tantal 35 V
	C39	73.5011	10 µF -10 + 50% elko 16 V
	C40	73.5114	1 µF 20% tantal 35 V
	C41	76.5071	22 nF 10% polyester FL 50 V
	C42	73.5114	1 µF 20% tantal 35 V
	C43	76.5071	22 nF 10% polyester FL 50 V
	C44	73.5115	1 µF 20% tantal 35 V
	C45	76.5067	1 nF 5% polystyr TB 160 V
	C46	73.5114	1 µF 20% tantal 35 V
	C47	74.5341	68 pF ceram PL 63 V
C48	76.5067	1 nF 5% polystyr TB 160 V	

TYPE	Nº	CODE	DATA
	C49	73.5114	1 µF 20% tantal
	C50	74.5341	68 pF ceram 35 V
	C51	76.5067	1 nF 5% polystyr TB 160 V
	C52	73.5114	1 µF 20% tantal 35 V
	C53	76.5072	47 nF 10% polyester FL 50 V
	C54	76.5069	1 nF 10% " 50 V
	C55	73.5106	68 µF 20% tantal 16 V
	C56	73.5127	22 µF 20% " 16 V
	C57	73.5151	100 µF -10 + 50% elko 16 V
	C58	76.5071	22 nF 10% polyester FL 50 V
	C59	76.5059	2.2 nF 10% " 50 V
	C60	73.5127	22 µF 20% tantal 16 V
	C61	73.5138	470 µF -10 + 100% elko 25 V
	C62	76.5072	47 nF 10% polyester FL 50 V
	C63	76.5072	47 nF 10% " 50 V
	C64	73.5137	470 µF -10 + 50% elko 16 V
	C65	76.5072	47 nF 10% polyester FL 50 V
	R1	80.5257	4.7 KΩ 5% carbon film 1/8 W
	R2	80.5246	560 Ω 5% " 1/8 W
	R3	80.5254	2.7 KΩ 5% " 1/8 W
	R4	80.5233	47 Ω 5% " 1/8 W
	R6	80.5283	680 KΩ 5% carbon film 1/8 W
	R7	80.5284	820 KΩ 5% trim. carbon 0.1 W
	R8	80.5280	390 KΩ 5% carbon film 1/8 W
	R9	80.5248	820 Ω 5% " 1/8 W
	R10	80.5248	820 Ω 5% " 1/8 W
	R11	80.5266	27 KΩ 5% " 1/8 W
	R12	80.5267	33 KΩ 5% " 1/8 W
	R13	80.5273	100 KΩ 5% " 1/8 W
	R14	80.5278	39 KΩ 5% " 1/8 W
	R15	80.5270	56 KΩ 5% " 1/8 W
	R16	80.5270	56 KΩ 5% " 1/8 W
	R17	80.5273	100 KΩ 5% " 1/8 W
	R18	86.5050	5 KΩ 20% trim carbon 1/8 W
	R19	86.5043	2.2 KΩ 20% " 0.1 W
	R20	80.5250	1.2 KΩ 5% carbon film 1/8 W
	R21	80.5277	220 KΩ 5% " 1/8 W
	R22	80.5278	270 KΩ 5% " 1/8 W
	R23	80.5242	270 Ω 5% " 1/8 W
	R24	80.5242	270 Ω 5% " 1/8 W

COMMON FUNCTIONS CF703, CF704

X402.429

TYPE	NO	CODE	DATA
CF703		10. 3364-00	Common Functions
	R25	80. 5268	39 KΩ 5% 1/8 W
CF704	R26	80. 5263	15 KΩ 5% 1/8 W
	R27	80. 5267	33 KΩ 5% 1/8 W
	R28	80. 5266	27 KΩ 5% 1/8 W
	R29	80. 5262	12 KΩ 5% 1/8 W
	R30	80. 5264	18 KΩ 5% 1/8 W
	R31	80. 5269	47 KΩ 5% 1/8 W
	R32	80. 5258	5.6 KΩ 5% 1/8 W
	R33	80. 5261	10 KΩ 5% 1/8 W
	R34	80. 5264	18 KΩ 5% 1/8 W
	R35	80. 5249	1 KΩ 5% 1/8 W
	R36	80. 5275	150 KΩ 5% 1/8 W
	R37	80. 5264	18 KΩ 5% 1/8 W
	R38	80. 5257	4.7 KΩ 5% 1/8 W
	R39	80. 5244	390 Ω 5% 1/8 W
	R40	80. 5269	47 KΩ 5% 1/8 W
	R41	80. 5265	22 KΩ 5% 1/8 W
	R42	80. 5264	18 KΩ 5% 1/8 W
	R43	80. 5243	330 Ω 5% 1/8 W
	R44	80. 5261	10 KΩ 5% 1/8 W
	R45	80. 5278	270 KΩ 5% 1/8 W
R46	86. 5044	25 KΩ 5% 1/8 W	
R47	80. 5263	15 KΩ 5% 1/8 W	
R48	89. 5010	15 KΩ 20% 0.1 W	
R49	80. 5266	27 KΩ 5% 1/8 W	
R50	80. 5238	120 Ω 5% 1/8 W	
R51	80. 5245	470 Ω 5% 1/8 W	
R52	80. 5248	820 Ω 5% 1/8 W	
R53	80. 5256	3.9 KΩ 5% 1/8 W	
R54	80. 5269	47 KΩ 5% 1/8 W	
R55	80. 5280	390 KΩ 5% 1/8 W	
R56	80. 5261	10 KΩ 5% 1/8 W	
R57	80. 5262	12 KΩ 5% 1/8 W	
R58	80. 5266	27 KΩ 5% 1/8 W	
R59	80. 5266	27 KΩ 5% 1/8 W	
R60	80. 5265	22 KΩ 5% 1/8 W	
R61	80. 5238	120 Ω 5% 1/8 W	
R62	80. 5252	1.8 KΩ 5% 1/8 W	
R63	80. 5243	330 Ω 5% 1/8 W	
R64	80. 5258	5.6 KΩ 5% 1/8 W	
R65	80. 5265	22 KΩ 5% 1/8 W	
R66	80. 5263	15 KΩ 5% 1/8 W	
R67	80. 5240	180 Ω 5% 1/8 W	
R81	80. 5229	22 Ω 5% 1/8 W	
R82	80. 5254	2.7 KΩ 5% 1/8 W	
R83	80. 5249	1 KΩ 5% 1/8 W	

TYPE	NO	CODE	DATA
CF703		10. 3364-00	Common Functions
	R84	80. 5257	4.7 KΩ 5% 1/8 W
CF704	R85	80. 5265	22 KΩ 5% 1/8 W
	R86	80. 5264	18 KΩ 5% 1/8 W
	R87	80. 5262	12 KΩ 5% 1/8 W
	R88	80. 5272	82 KΩ 5% 1/8 W
	R89	80. 5254	2.7 KΩ 5% 1/8 W
	R90	80. 5258	5.6 KΩ 5% 1/8 W
	R91	86. 5039	10 KΩ 20% trim carbon 1/8 W
	R92	80. 5258	5.6 KΩ 5% 1/8 W
	R93	80. 5258	5.6 KΩ 5% 1/8 W
	R94	80. 5274	120 KΩ 5% 1/8 W
	R95	80. 5272	82 KΩ 5% 1/8 W
	R96	80. 5254	2.7 KΩ 5% 1/8 W
	R97	80. 5258	5.6 KΩ 5% 1/8 W
	R98	86. 5039	10 KΩ 20% trim carbon 1/8 W
	R99	80. 5268	39 KΩ 5% 1/8 W
	R100	80. 5266	27 KΩ 5% 1/8 W
	R101	80. 5261	10 KΩ 5% 1/8 W
	R102	80. 5256	3.9 KΩ 5% 1/8 W
	R103	80. 5260	8.2 KΩ 5% 1/8 W
	R104	80. 5254	2.7 KΩ 5% 1/8 W
R105	80. 5246	560 Ω 5% 1/8 W	
R106	80. 5255	3.3 KΩ 5% 1/8 W	
R107	80. 5249	1 KΩ 5% 1/8 W	
R108	80. 5259	6.8 KΩ 5% 1/8 W	
R109	80. 5253	2.2 KΩ 5% 1/8 W	
R110	80. 5258	5.6 KΩ 5% 1/8 W	
R111	80. 5257	4.7 KΩ 5% 1/8 W	
R112	80. 5249	1 KΩ 5% 1/8 W	
R113	80. 5218	2.7 Ω 5% 1/8 W	
R114	80. 5258	5.6 KΩ 5% 1/8 W	
R115	80. 5254	2.7 KΩ 5% 1/8 W	
R116	80. 5230	27 Ω 5% 1/8 W	
R117	80. 5217	2.2 Ω 5% 1/8 W	
R118	80. 5217	2.2 Ω 5% 1/8 W	
R119	80. 5261	10 KΩ 5% 1/8 W	
R120	80. 5256	3.9 KΩ 5% 1/8 W	
R121	80. 5265	22 KΩ 5% 1/8 W	
R122	80. 5264	18 KΩ 5% 1/8 W	
R123	80. 5273	100 KΩ 5% 1/8 W	

COMMON FUNCTIONS CF703, CF704

X402. 429

TYPE	Nº	CODE	DATA
	R124	80. 5230	1/8 W
	R125	80. 5237	1/8 W
	R126	80. 5213	1/8 W
	R127	80. 5252	1/8 W
	L1	61. 1132	Squelch coil 75 mH
	L2	61. 1131	IA coil 455 kHz
	E1	99. 5237	1 N 4148 Diode
	E2	99. 5237	1 N 4148 "
	E3	99. 5042	Zenerdiode 9.1 V 5%
	E4	99. 5209	Stabilizerdiode 1.5 V
	E5	99. 5237	1 N 4148 Diode
	E6	99. 5237	1 N 4148 "
	E7	99. 5237	1 N 4148 "
	E8	99. 5237	1 N 4148 "
	E9	99. 5020	1 N 4004 "
	E10	99. 5237	1 N 4148 "
	E11	99. 5209	Stabilizerdiode 1.5 V
	E12	99. 5237	1 N 4148 Diode
	E13	99. 5237	1 N 4148 "
	E15	99. 5224	Zenerdiode 4.7 V 5%
	E16	99. 5237	1 N 4148 Diode
	E17	99. 5224	Zenerdiode 4.7 V 5%
	E18	99. 5209	1.5 V Stab. diode
	Q1	99. 5144	Transistor
	Q2	99. 5143	BC 214 L
	Q3	99. 5143	BC 238 (BC 108)
	Q4	99. 5143	BC 238 (BC 108)
	Q5	99. 5143	BC 238 (BC 108)
	Q6	99. 5201	BC 238 (BC 108)
	Q7	99. 5115	BC 239 (BC 109)
	Q8	99. 5115	BC 309 (BC 179)
	Q9	99. 5143	BC 309 (BC 179)
	Q20	99. 5246	BC 238 (BC 108)
	Q21	99. 5144	TIP 31
	Q22	99. 5143	BC 214 L
	Q23	99. 5143	BC 238 (BC 108)
	Q24	99. 5143	BC 238 (BC 108)
	Q25	99. 5246	TIP 31
	Q26	99. 5143	BC 214 L
	Q27	99. 5143	BC 238 (BC 108)
	Q28	99. 5143	BC 238 (BC 108)
	Q29	99. 5115	BC 238 (BC 108)
	Q30	99. 5326	BC 308 (BC 178)
	Q31	99. 5326	BF 198
	Q32	99. 5143	BF 198
	T1	61. 1130	IA transformer 455 kHz

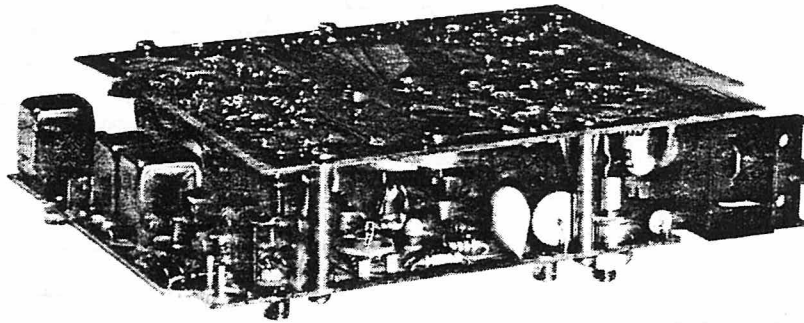
CF704

TYPE	Nº	CODE	DATA
	T2	61. 1130	IA transformer 455 kHz
	IC1	14. 5105	MC1458 Dual OP-amp.
	IC2	14. 5105	MC1458 Dual OP-amp.
	IC3	14. 5010	IF Amplifier/Discr. ULN 2111 N
	IC4	14. 5104	Audio Power Amplifier TBA 810 AS
	ReA	58. 5084	Relay 330 Ω 12 V

COMMON FUNCTIONS CF703, CF704

X402. 429

COMMON FUNCTIONS UNIT CF701



Description

The CF701 module contains all the circuitry for the CQM700 series radiotelephones that is not dependent upon frequency or channel separation. The unit includes the following functions:

- a 455 kHz intermediate frequency amplifier and discriminator
- a de-emphasis network and an audio frequency preamplifier, including an electronic squelching switch
- a squelch circuit
- two 9 V voltage regulators and keying circuitry
- an audio output amplifier
- a modulation amplifier
- a keying circuit for the power amplifier stage

CF701 is constructed on two printed circuit boards mounted in a sandwich assembly. The two p-c boards are held in place with spacers, a small sewn cable taking care of internal connections. The conductive sides of the printed wiring boards face outwards, with the board containing the IF, the AF preamp, the squelch and the voltage regulators fastened to the chassis. External connections to the CF unit are all solder connections with the exception of the battery connection, which is through a plug.

Operating Principle

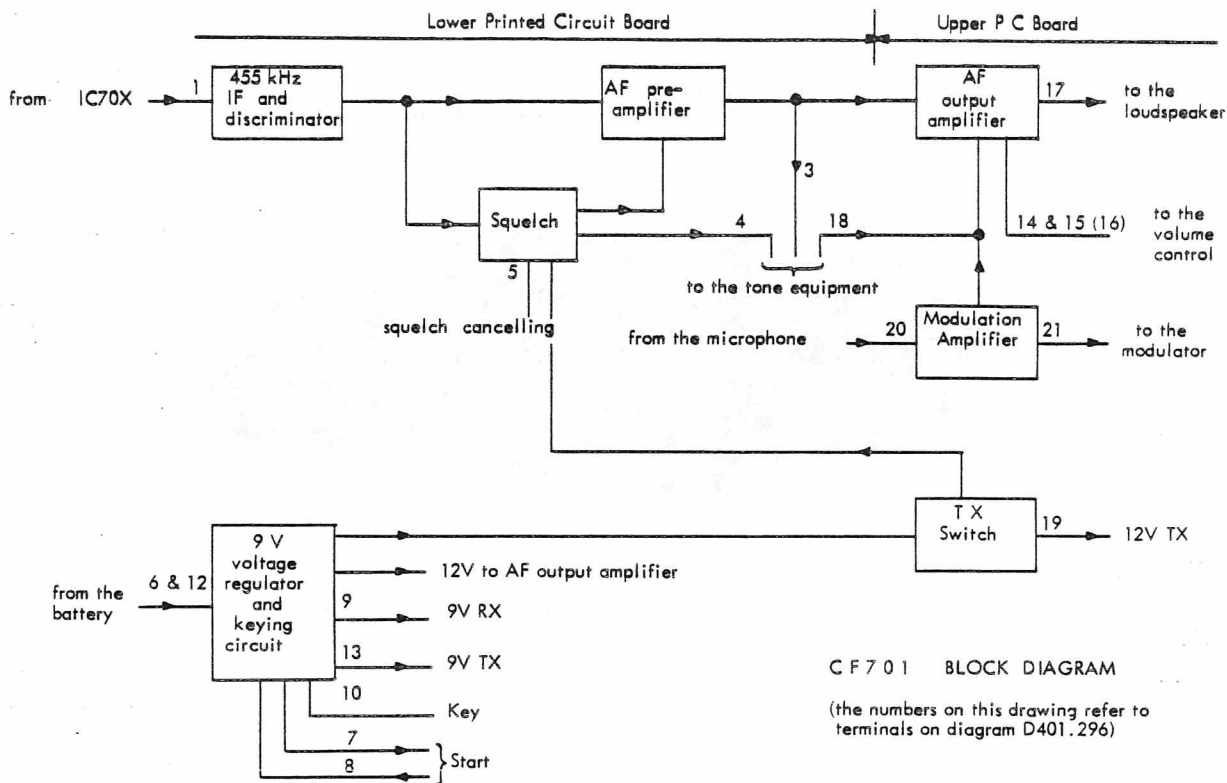
To aid heat dissipation, the AF amplifier output transistors and the drive resistor for Q29 in the TX switch, all on the upper p-c board, as well as the series regulator transistors in the voltage regulators on the lower board all have good thermal contact to the chassis.

The 455 kHz signal from IC700 passes through the IF stages to the integrated circuit discriminator, IC-1. From there the audio signal divides between the squelch circuit input and the de-emphasis filter at the input to the audio preamplifier.

The squelch circuit opens and closes the signal path through the preamp according to the noise content in the demodulated signal. Also, control voltages for use with tone equipment are obtained from the squelch circuit.

The audio signal is taken from the 600 Ω output of the preamplifier to the AF amplifier. When transmitting, the signal path through the output amplifier becomes automatically blocked. The tone equipment can also block the signal path here.

The signal from the microphone is amplified and limited in the modulation amplifier, which is designed around a dual, integrated operational amplifier. Both amplifiers, IC2a and IC2b, are contained in the same housing.



CF 701 BLOCK DIAGRAM
(the numbers on this drawing refer to terminals on diagram D401.296)

To avoid adjacent channel interference, the high-frequency component of the modulating signal is filtered out and the signal is also amplitude limited in order to keep the carrier frequency swing within the established maximum excursions for which ever channel separation is employed.

As mentioned previously, the CF unit also contains two voltage regulators; one supplies the receiver section and the other, the transmitter. The AF output amplifier and the PA stage are supplied through a filter choke directly from the battery and are therefore unregulated.

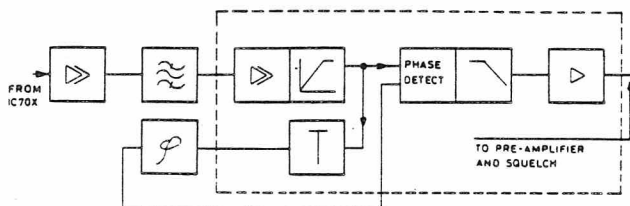
Switching between transmit and receive is accomplished without relays. The transmitter key electronically switches one or the other of the voltage regulators on so that both do not function at the same time. Terminal 10 is grounded during transmission and otherwise floats when the key is not activated.

12 V TX is taken off before the on/off switch in order to avoid any voltage drop

in the start cable when employing extended local control. 12 V TX is applied to the PA stage through a transistor switching arrangement, the TX switch, which is driven by the 9 V TX regulator. When the key is activated the TX switch blocks the audio preamplifier as a precaution against the possibility that any transients in the squelch circuit might open the receiver during transmission, since the supply voltage to the AF output amplifier is always on whenever the on/off switch is turned on.

The 455 kHz IF Amplifier and Discriminator

This circuit amplifies, selects, limits and detects the receiver's second IF signal of 455 kHz, allowing a deviation of up to ± 15 kHz from centre frequency.



The amplifier has five stages; the first two, Q1 and Q2, are made up of discrete components while the last three are a part of the integrated circuit, IC1, along with the phase detector.

The only resonant circuits employed in the 2nd IF stage are those between the collector of Q2 and the input to IC1. Resistors R9 and R12 load T1 and T2 enough to achieve sufficiently broad bandwidth.

Inductive coupling between circuits is less than critical, R11 in the coupling link determining the coupling factor. Q2 operates with its collector-emitter voltage held low to prevent overdriving IC1.

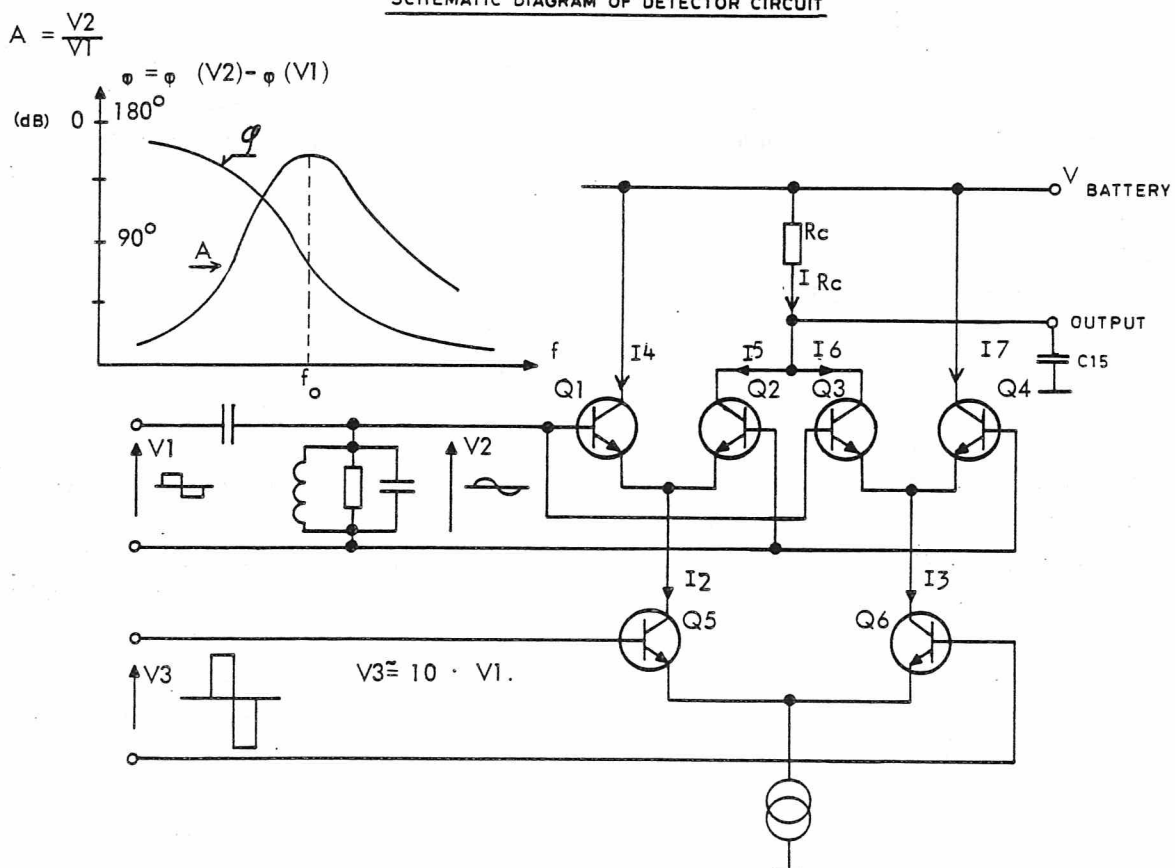
The three amplifier stages in IC1 are differential amplifiers, which configuration approaches ideal symmetrical limiting. The stages are DC coupled and stability is assured through strong negative feedback. Capacitor C12 eliminates the feedback as far as AC voltages are concerned.

Via an emitter follower within the IC housing, the signal is fed to the phase detector. The IF signal, with its amplitude peaks clipped, is applied directly to one of the phase detector inputs.

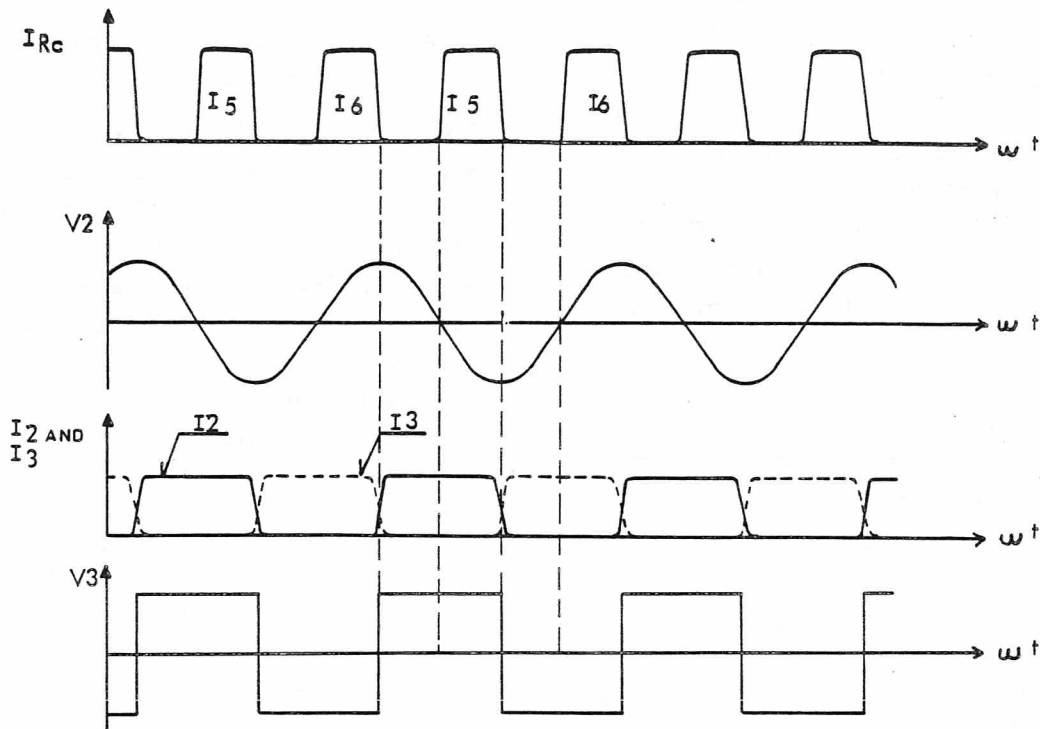
The other input is fed the same signal, attenuated and approximately 90° out of phase (at f_0). Phase shift is accomplished with discrete components: C13, C14, L1 and R14. The following diagram shows the detector circuit schematic and the amplitude and phase characteristics of the phase shifting network. A graph of the detector current and voltage relationships is also included here.

The phase detector is designed around three differential amplifiers, all supplied through a constant-current source. In addition to the components shown in the detector schematic, IC1 also contains an emitter follower after the detector output, another emitter follower between the phase shifting network and one of the detector inputs, and various biasing networks.

SCHEMATIC DIAGRAM OF DETECTOR CIRCUIT



GRAPH OF VOLTAGE AND CURRENT RELATIONSHIPS
IN THE PHASE DETECTOR WHEN $f = f_0$



As long as voltage V_2 is high enough to drive the two differential stages - $Q_1 + Q_2$, and $Q_3 + Q_4$ - as switches, the collector current pulses, I_5 and I_6 , will appear as a constant amplitude value and the average value of current through R_C remains independent of the amplitude of the input voltage.

As seen on the schematic, current pulses through R_C only appear when V_2 and V_3 are of opposite polarities and I_5 appears only when V_3 is positive while I_6 appears when V_3 is negative. Supposing that $f > f_0$, then the difference in phase ($V_2 - V_1$) is reduced (the V_2 pulse a little to the right in relation to V_3), causing the width of current pulses I_5 and I_6 to decrease. In other words, the average current through R_C will decrease. When $f < f_0$, the opposite will occur.

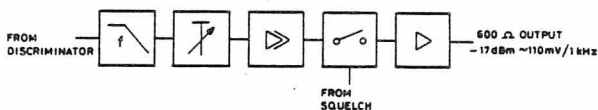
The width of I_5 and I_6 is therefore seen to be a measurement of the phase difference between V_2 and V_3 . By integrating

the output voltage (via R_C and C_{15}) a voltage that is directly proportional to the phase shift is obtained.

Making use of both the negative and positive excursions of the signals, as in the detector configuration employed here, gives excellent suppression of noise and other undesired effects of inherent nonsymmetry in the clipped IF signal. For example, if the positive going half of V_3 is wider than the negative half, I_6 will be narrower and I_5 wider with the result that the average current through R_C will remain unchanged.

An "S" curve similar to those known from conventional FM detectors will be present at the output (directly on pin 1 of IC_1). However, the mid-point of this "S" curve will be around 3.5 V instead of 0 V. Circuit Q is designed low enough to enable the detector to handle frequency deviations of up to ± 15 kHz.

The De-emphasis Filter, AF Preamplifier and Electronic Squelching Switch



Network R15 and C19 take care of de-emphasising the demodulated signal at the rate of -6 dB pr. octave.

The three stages of the preamplifier, Q3, Q4 and Q6, must then amplify the AF signal and match it to the nominal 600 Ω load. In addition, Q5 is inserted between Q4 and Q6. Q5, which is a field-effect transistor, operates as an electronic switch, interrupting the signal path on command from the squelch circuit.

The nominal output voltage of the preamp is -17 dBm into the 600 Ω output line. R16 is the adjustment used for setting the correct output level.

The collector of Q3 is directly coupled to the base of Q4; resistors R21, R22 and R23 provide the feedback necessary to stabilise the two stages.

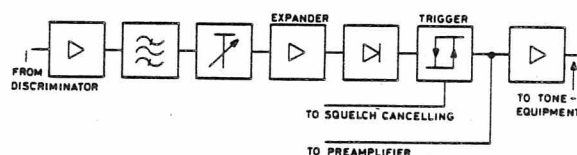
The signal path between the second and third amplifier stages is through the FET transistor, which acts like a relay contact, or switch. A gate-to-source potential of 4 V, at most, will "break" the path between source and drain. Since the collector of Q4 is at approx. 4.7 V, a gate voltage at Q5 under 0.7 V "breaks" the connection and "makes" the connection between Q4 and Q6 again when gate voltage rises above 4.7 V.

The Squelch

The squelch circuit opens or closes the audio signal path through the AF preamp according to the noise content of the incoming signal. The squelch circuit also provides a signal voltage for use in tone signalling.

An internal adjustment, potentiometer R38, is provided for setting the squelch level. The squelch function can be cancelled altogether by grounding terminal 5 via the squelch cancelling button on the control panel.

By altering only a few passive component values, the squelch section can operate on any of the three channel bandwidths normally employed.



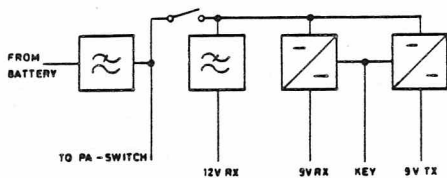
The squelch section includes a frequency selective noise amplifier, Q7, an expander stage, Q8, a noise detector, A Schmitt trigger, Q9 and Q10, and an emitter follower amplifier, Q11.

The operating principle is as follows:

Some of the AF signal from the discriminator is fed to the noise amplifier whose collector load is made up of a parallel resonant circuit tuned to some frequency well above the voice range, and depending upon the channel bandwidth employed. The selected noise is then fed to Q8 which is biased in such a way that only positive going pulses of a certain minimum amplitude cause the transistor to conduct. Since only pulses of a certain amplitude can become amplified, the result is that a given relative change in noise amplitude at the base of Q8 appears as a larger relative change at the collector. The noise pulses are then rectified and filtered to a DC potential that, in turn, controls the Schmitt trigger, Q9 and Q10. The collector voltage on Q10 is used partly to drive the emitter follower, Q11, and partly, through an R-C network, to switch the FET transistor in the AF preamplifier.

Keying the transmitter interrupts the power to the receiver. At the same time, diodes E2 and E6 in the squelch are grounded through Q30 to prevent any false signals that might appear in the squelch circuitry from effecting the AF amplifier or Q11 during this condition.

The 9 V Voltage Regulators and Keying Circuits



The two 9 V voltage regulators supply the receiver and the transmitter sections, respectively. They are intended for use with a 12 volt auto battery.

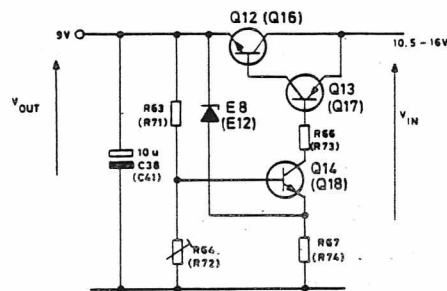
The battery connects to the regulators through the transient and ripple filter, L3a and C39, and through the vehicle's start switch via terminals 7 and 8. The AF output amplifier is supplied with unregulated, filtered battery power via the other filter winding, L3b, and C56 in the AF amplifier circuit.

To protect the equipment against incorrect battery polarity or excess voltage, a properly dimensioned zener diode is placed across the supply. If the power supply is connected wrong the zener diode will act as a short circuit at the input, blowing the fuses in the battery leads. In case of excess supply voltage, the zener diode will not allow more than about 20 volts to be present at the input to the regulators.

The voltage regulators are protected against short circuits; with shorted output the current through Q12 will be < 0.5 A and through Q16, < 0.1 A. The power transistors are mechanically mounted so as to be in good thermal contact with the chassis.

The two regulators are principally identical as shown on the simplified diagram as follows:

Q12 is driven by Q13, which is controlled by amplifier Q14. Transistor Q14 compares the zener reference voltage across E8 with a portion of the output voltage through dividing resistors R63 and R64. R64 sets the output voltage.



The operating principle is as follows:

If V_{out} drops (due to a decrease in input voltage or an increase in load current), V_{BE} for Q14 will increase, also increasing base current for Q13 and Q12. When base current to Q12 increases, more current flows through the output load, cancelling the original drop in output voltage.

If the load current increases to a certain value, Q14 goes into saturation. If the load current increases still more, the zener diode will act as an open circuit and V_{BE} for Q14 decreases whereby base current for Q14, Q13 and Q12 decreases, too. Finally, Q14 will be cut off and base current in Q12 and Q13 will be zero. Thus Q12 is protected against destruction by short circuits at its output. Resistors R66 and R67 determine the saturation current through Q14 and, of course, the short circuit current.

A regulator built exactly like the simplified diagram would not be self-starting, however. Therefore, the regulators in the CF701 are provided with starting circuits;

9 V RX employs R61, R62 and E9 in its starting circuit and 9 V TX employs R70 and E11. Since 9 V RX and 9 V TX must not operate simultaneously, the regulators are also mutually coupled through a keying circuit that blocks, or cuts off, one regulator while allowing the other to operate. This function is controlled via terminal 10.

Operation of Keying and Starting Circuits

When terminal 10 is floating and the power is turned on, 9 V RX will build up voltage since Q12 gets base current through R58, E9, R61 and R62. When 9 V RX reaches its final value the starting circuit will have no effect on the regulator because diode E9 will then be nonconducting (the unloaded voltage at terminal 10 is approx. 8.2 V at nominal battery voltage).

Transistors Q15 and Q19 are both heavily saturated, so the 9 V RX regulator will operate undisturbed while 9 V TX will be blocked because Q18 is completely cut-off by Q19.

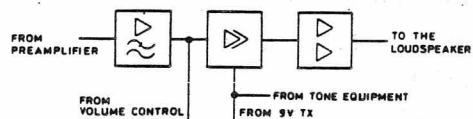
Grounding terminal 10 immediately cuts off Q15 and Q19. 9 V RX falls towards 0 V as there is now no base current to Q13. 9 V RX falls off at a rate determined by the time constant of R38 and the load on terminal 9. Under all operating conditions within factory specifications for the radio-telephone, the time constant will easily be long enough that the current through starting circuit R70 and E11 can turn on Q18, whereby a voltage builds up on 9 V TX that finally reaches a level where diode E11 becomes nonconducting.

Diode E10 and resistor R68 ensure that keying the transmitter cuts off base current to Q13 effectively, even at high temperatures. Diode E7 ensures effective keying even if terminal 10 is not brought all the way down to 0 V potential.

Note that 9 V TX cannot begin to build up a voltage by itself after a short circuit. Since - as just explained - it is 9 V RX that starts 9 V TX, it is necessary to activate the transmitter key again. Even with 9 V RX shorted, Q12 still gets its base current through the starting circuit where one of the resistors, R62, is a PTC resistor that will limit base current to the transistor at high ambient temperatures or when Q12 heats up.

The AF Output Amplifier

The output amplifier amplifies the audio signal from the preamplifier and powers the loudspeaker.



Frequencies below 250 Hz are very sharply cut off in the first amplifier stage, transistor Q20. Included in the collector of Q20 is a variable resistor which allows for adjustment of the amplifier gain above the nominal amount in order to compensate for weak modulation of the incoming signal.

The signal passes from the 1st stage to the volume control whose arm connects to terminal 15 in the case of local control or to terminal 16 in case of extended local control. An isolation resistor is placed between the two terminals, allowing for extended local control without necessitating the removal of the local control connections.

The 2nd amplifier stage, Q21, is an emitter follower whose base voltage is the essential factor in determining the symmetry of the drive signal to the loudspeaker output.

From Q21, the signal is fed via two R-C low-pass filter networks to the 3rd ampli-

fier stage, Q22. The primary purpose of the two low-pass networks is to stabilise the amplifier in regard to AC when employing extended local control.

In Q22, which in principle is coupled in the grounded emitter configuration, the signal is amplified and passes directly to the next amplifier stage which, in turn, is coupled directly to the driver transistors, Q25 and Q26. Transistor Q23 and resistors R98, R99 and R100 provide temperature compensated biasing for the driver transistors. As far as AC is concerned, the circuit appears as a short circuit between the bases of the two driver transistors. The complementary output transistors operate in class AB push-pull. Strong negative DC feedback is introduced in order to stabilise the operating point for the output stages. The feedback network is from the output, over R106 to the emitter of Q22. The AC feedback network is formed by R106 in conjunction with R96.

The power transistors employ aluminium heat sinks fastened to the radio chassis for good thermal contact.

During transmission a "muting signal" grounds the base of Q24 via terminal 18 and an R-C network, blocking the output amplifier. This network also functions as the blocking gate for the tone equipment

The Modulation Amplifier

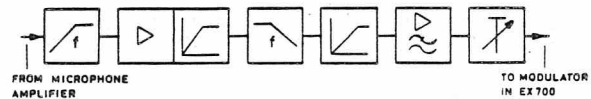
General

The modulation amplifier differentiates, amplifies, limits and integrates the microphone signal. It also suppresses undesired high frequencies with an active filter designed for either 20, 25 or 50 kHz channel separation or, with a few resistor values changed, 12.5 kHz channel spacing.

Both amplifiers are contained in a single integrated circuit made up of dual opera-

tional amplifiers. The modulation amplifier contains additional passive differentiating and integrating circuits as well as diode clippers to prevent overmodulation.

The following block diagram shows the operating principle for the amplifier:



Input

The input circuit, which is also the collector return for the microphone amplifier output stage through resistor R112, is asymmetric.

The Differentiating Circuit

The differentiation network is made up of C64 and R113 (the input impedance of the op amp is negligible due to the feedback through R116). It differentiates at the rate of +6 dB pr. octave over the entire audio range of 300 to 3000 Hz.

The Amplifier - Clipper

The 1st amplifier stage has a very accurately determined gain due to its feedback. Clipping action begins as soon as the amplifier is driven to where the collector excursions approximate the battery voltage. This level will be about 6.8 V peak-to-peak. The amplifier can be driven up to 25 dB above its nominal input level. Symmetry of the clipping is determined by bias network R114 and R115 and therefore is fixed.

The Integration Circuit

Integrating takes place from 230 Hz at 6 dB pr. octave. The passive integrating network consists of R118 and C67. The lower limit for integration is determined solely by these two components as the pre-

vious amplifier's feedback makes its output impedance negligible, and because the loading of the network by the filter that follows is very light as long as the signal remains below the frequency limit of that filter.

The 2nd Clipper (or Phase Clipper)

This extra clipper is inserted to prevent strong input signals at low frequencies from overdriving the modulator stage. For signal levels corresponding to the nominal frequency swing, the clipper has no effect. Two 1.5 V diodes and capacitor C69 make up this circuit. The clipping level is only approx. 1.2 V at maximum due to the comparatively large impedance of R118.

The Splatter Filter

The purpose of this filter is to cut off frequencies that lie above the voice range in order to avoid undesirable sideband noise. It is an active filter consisting of the second operational amplifier and its associated components. Its response approaches that of a Chebishev filter. The circuit arrangement is the so-called voltage follower, where the voltage gain is very near unity (1). The significant passive filter components are resistors R119,

R120 and R121 and capacitors C70, C71, C72, C75, C76 and C77. The filter cannot be overdriven because the input signal level is subject to limiting by the diode clipper.

Adjusting the Frequency Swing

The amount of signal to the modulator input, and thus the frequency swing, is set by potentiometer R124 which forms a voltage divider with the modulator input impedance.

The TX Switch.

The PA keying circuit operates an electronic switch in the path of the 12 V TX supply voltage to the PA unit. The circuit consists of Q29 and Q30 along with the associated resistor networks at their bases. The transistors operate in saturation when transmitting and are cut-off during standby, or receive. The circuit is controlled from 9 V TX.

In addition, Q30 grounds out spurious squelch signals whenever the transmitter is activated.

TECHNICAL SPECIFICATIONS

Nominal Supply Voltage

13.6 V

Current Drain for CF701 (at nominal supply voltage)

Transmit: 220 mA

Receive : 65 mA

12 dB SINAD Sensitivity (where 1.75 kHz deviation of the 455 kHz IF results in a 1 kHz audio signal)

1.2 μ V input signal at antenna termination

AF Line Out (terminal 3)

-17 dBm / 600 Ω

Regulated Voltages

Receiver (terminal 9) : 9 V

Transmitter (terminal 13): 9 V

Unregulated, Filtered Voltages

AF output amplifier : 13.6 V

PA stage (terminal 19): 13.6 V

AF Output Power (terminal 17)

2 W

Modulation Amplifier Sensitivity (for normal frequency swing of 1 kHz)

110 mV +1/ -0 dB

The following, more detailed specifications for the seven CF701 functions are all typical values measured at 25°C ambient temperature, unless otherwise stated.

455 kHz IF AMPLIFIER and DISCRIMINATOR

Current Drain (at nominal 9 V supply)

18 mA

Maximum Frequency Deviation

\pm 15 kHz

IF Bandwidth (3 dB attenuation)

\pm 17 kHz

Input Impedance

1 k Ω // 15 pF

Gain

from input (terminal 1) to pin 4 of IC1: 55 dB

from IC1 input (pin 4) to IC1 amplifier

high output, pin 10: 55 dB

Discriminator Conversion Efficiency

50 mV / kHz

AF Output Voltage ($f_m = 1$ kHz, $\Delta f = 3.5$ kHz)

110 mV

Measured at test point 2, terminated with 2.2 k Ω load.

Discriminator Linearity (relative to 1000 Hz)

Pass-Band 100 - 3500 Hz: +0 / -1 dB

Measured at test point 2, terminated with 2.2 k Ω load.

Discriminator Output Resistance

200 Ω

Minimum Load Resistance

2 k Ω

Harmonic Distortion

$\Delta f = 15$ kHz : 4.5 %

$\Delta f = 3.5$ kHz: 1.0 %

AF PREAMPLIFIER and SQUELCH-CONTROLLED SWITCH

Current Drain (at nominal 9 V supply)

8 mA

Input Impedance (at 1 kHz)

2.2 k Ω

Output Impedance

$R_{OUT} = 680 \Omega$

Gain (gain control at highest setting)

$R_L = 560 \Omega$, $f = 1 \text{ kHz}$: 12.5 dB

Harmonic Distortion ($R_L = 560 \Omega$, $f = 1 \text{ kHz}$)

$V_{OUT} = 110 \text{ mV}$ (nominal): 0.2 %

$V_{OUT} = 500 \text{ mV}$: 0.5 %

Required Turn-on Potential (at gate of Q5)

To ensure normal signal path: $\geq 4.7 \text{ V}$

Required Turn-off Potential (at gate of Q5)

To ensure 70 dB attenuation of signal: $\leq 0.7 \text{ V}$

Measured with 110 mV, 1 kHz signal applied to circuit input, test point 2, and gain control set at max., V_{OUT} (terminal 3) = approx. 500 mV.

De-emphasis Cut-off Frequency

90 Hz

Frequency Response (relative to -6 dB/octave characteristic)

Pass-Band linearity (300 - 3000 Hz): +0/-1 dB
50 - 100 Hz : +15 dB

SQUELCH CIRCUITCurrent Drain (at nominal 9 V supply)

12 mA

Measured with unloaded Squelch Signalling (terminal 4).

Input Impedance (at 1 kHz)

20 k Ω

Noise Filter Resonant Frequency

12.5 kHz channel spacing : 7.1 kHz

20/25 kHz channel spacing: 7.1 kHz

50 kHz channel spacing : 10 kHz

Output Voltage

Squelched condition : $\leq 100 \text{ mV}$

Un-squelched condition: $> 5.7 \text{ V}$

Measured at test point 1. DC.

Squelch Signalling (terminal 4)

R_{LOAD} minimum: 680 Ω

V_{OUT} (with $R_L = 680 \Omega$)

Squelched condition $\leq 100 \text{ mV}$

Un-squelched condition $\geq 4.0 \text{ V}$

Transition Time (gain control set for nominal V_{OUT})

6 ms

Delay measured from the time that the voltage at test point 1 switches state until the AF signal at terminal 3 increases from 10% to 90% of its nominal amplitude.

Turn-off delay (signal decrease from 90% to 10%) is also 6 ms.

Overall Receiver Squelch Response

Turn-on delay: 30 ms

Turn-off delay: 25 ms

Measured with receiver adjusted for 12 dB SINAD.

9V VOLTAGE REGULATORS and KEYING CIRCUITSNominal Supply Voltage

13.6 V

Operating Range

10.5 V to 16 V

Regulated Output Voltages

Receiver supply 9V RX: $9.0 \text{ V} \pm 0.2 \text{ V}$

Transmitter supply 9V TX: $9.0 \text{ V} \pm 0.2 \text{ V}$

 V_{REG} vs. Temperature

3.6 mV/pr. $^{\circ}\text{C}$

Suppression of $\Delta V_{BATTERY}$ in V_{REG}
(at nominal load)

DC : 46 dB

1 kHz: 50 dB

Internal Resistance of Regulators

$R_I = 0.5 \Omega$

Regulator Output Current

Maximum 250 mA

12 V-RX to AF Output Amplifier (filtered, un-regulated voltage)

ripple suppression at 1 kHz, no load condition: 36 dB
voltage drop over filter when $P_{OUT} = 2W$: 0.25 V
maximum output current: 500 mA

Keying Termination

Maximum allowable resistance of wiring : 180 Ω
Alternatively, V_{MAX} at terminal 10: 1.0 V

Regulator Switching Time ($V_{BATT.} = 13.6 V$)

9V RX turn-on delay, $t_{0-90\%}$: 0.4 ms
9V RX turn-off delay, $t_{100-10\%}$: 100 ms
9V TX turn-on delay, $t_{0-90\%}$: 0.1 ms
9V TX turn-off delay, $t_{100-10\%}$: 25 ms

Measured under normal load conditions.

AF OUTPUT AMPLIFIERNominal Supply Voltage

13.6 V

Operating Range

10.5 to 16.0 V

Current Drain (at nominal supply voltage)

no-signal condition: 20 mA
at 2 W output: : 300 mA
blocked : 20 mA

Output Power (at nominal supply voltage)

maximum 2 W

Loudspeaker Impedance

Nominal / minimum: 5 Ω

Input Impedance (at 1 kHz)

560 Ω

Nominal Gain

Input signal (1 kHz) required for 2 W output: 110 mV

Measured with volume control (5 k Ω potentiometer) connected to terminals 14, 15 and chassis ground, and turned fully up.

Where the connections are to terminals 14, 16 and chassis, as with extended local control, the gain increases by 2 dB.

Adjustment of R83 can increase sensitivity 12 dB.

Gain vs. $\Delta V_{BATT.}$

13.6 V +2.4 / -3.1 V: 0.2 dB

Harmonic Distortion

$P_{OUT} = 2 W$: 1 %
 $P_{OUT} = 0.2 W$: 0.5 %

Frequency Response (relative to 1 kHz)

100 Hz -22 dB
300 Hz 0 dB
2700 Hz -0.5 dB
6 Hz -2 dB

Measured at 0.2 W output power.

AF Muting

Required DC at terminal 18 to attenuate the output signal by 60 dB: 8.0 V

MODULATION AMPLIFIERCurrent Drain (at nominal 9 V supply)

2 mA

Input Impedance (at 1 kHz)

560 Ω

Limiting

Signal clipping begins to occur with an input signal (1000 Hz) of: 110 mV

Output signal level observed at pin 2 of IC2 when clipping occurs: 7.0 V p.p.

Phase Limiting

Phase clipping level (at 300 Hz): 2.1 V p.p.

Measured immediately after the integration network, with an input signal of 1.1 V (nominal 110 mV + 20 dB).

Output Voltage (1000 Hz)

560 mV

Measured at Modulation Output (terminal 21) with potentiometer R124 fully up, and load impedance = 1 kΩ.

Input level = 110 mV

Harmonic Distortion (at 1000 Hz)

for 110 mV input signal: 0.8 %

Frequency Response (relative to 1 kHz)

	channel spacing	
	<u>20/25/50 kHz</u>	<u>12.5 kHz</u>
300 Hz	- 0.5 dB	- 0.5 dB
3 kHz	- 1 dB	- 4 dB
6 kHz	- 19 dB	- 25 dB
10 kHz	- 32 dB	- 37 dB

Measured for 15 mV input signal, and with a resistive output load.

PA KEYING CIRCUIT

Nominal Supply Voltage

13.6 V

Operating Range

10.5 to 16 V

Maximum Load Current

3 A

TX Switch

Voltage drop across transistor switch when ON, at 2 A load current: 0.2 V

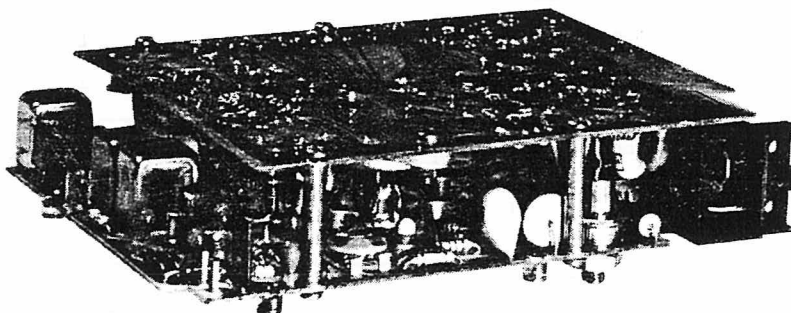
Transistor collector current when OFF:

T_{AMB} = 25°C : 0.2 mA

T_{AMB} = 60°C : 10 mA

COMMON FUNCTIONS UNIT

CF701 & CF702



Description

The CF unit module contains all the circuitry for the CQM700 series radiotelephones that is not dependent upon frequency or channel separation. CF701 is designed for simplex operation and CF702 for duplex. The unit includes the following functions:

- a 455 kHz intermediate frequency amplifier and discriminator
- a de-emphasis network and an audio frequency preamplifier, including an electronic squelching switch
- a squelch circuit
- two 9 V voltage regulators and keying circuitry
- an audio output amplifier
- a modulation amplifier
- a keying circuit for the power amplifier stage

The CF unit is constructed on two printed circuit boards mounted in a sandwich assembly. The two p-c boards are held in place with spacers, a small sewn cable taking care of internal connections. The conductive sides of the printed wiring boards face outwards, with the board containing the IF, the AF preamp, the squelch and the voltage regulators fastened to the chassis. External connections to the CF unit are all solder connections with the exception of the battery connection, which is through a plug.

Operating Principle

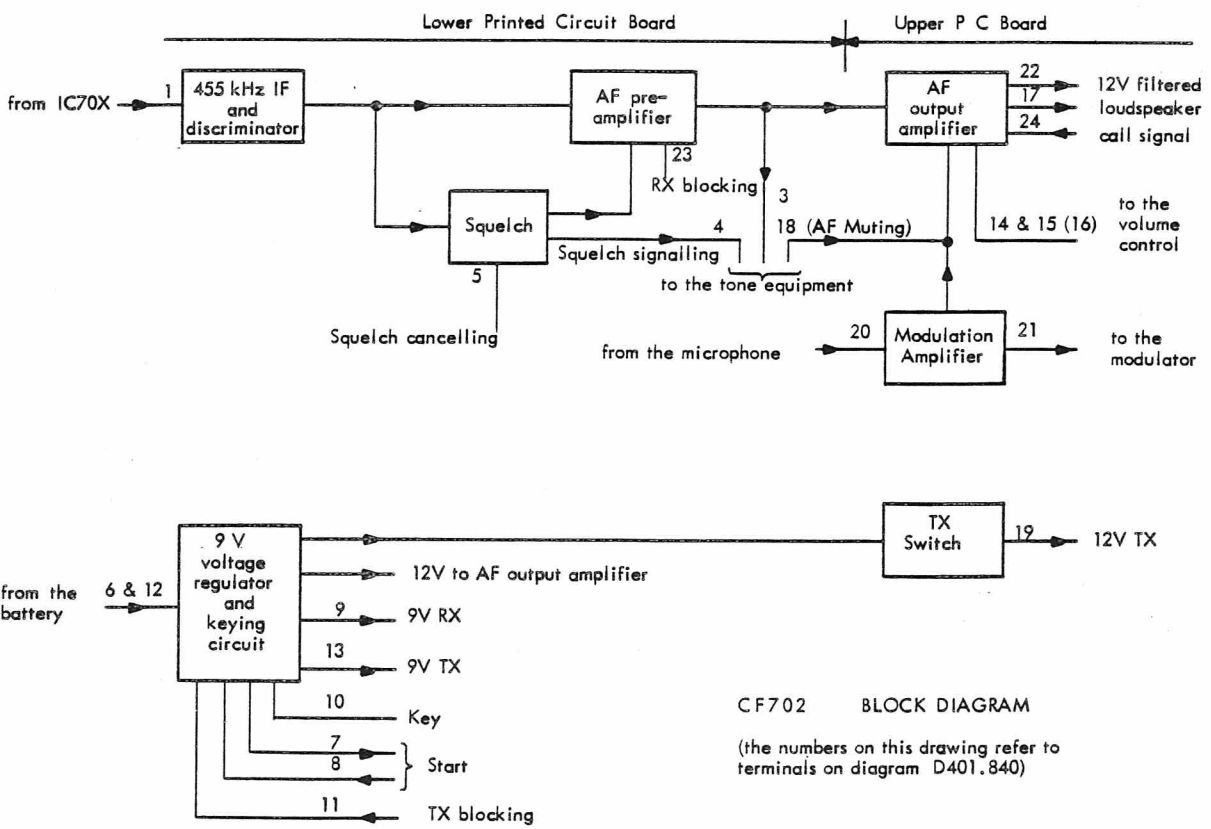
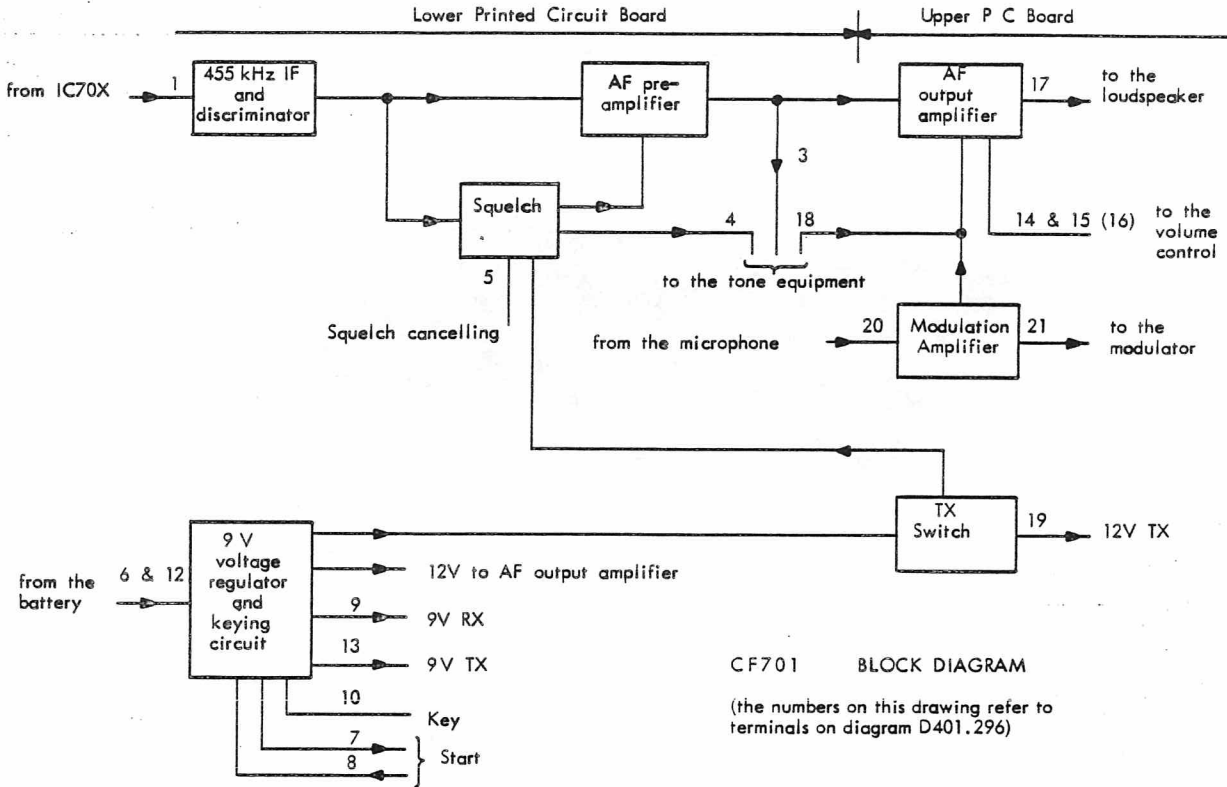
To aid heat dissipation, the AF amplifier output transistors and the drive resistor for Q29 in the TX switch, all on the upper p-c board, as well as the series regulator transistors in the voltage regulators on the lower board all have good thermal contact to the chassis.

The 455 kHz signal from IC700 passes through the IF stages to the integrated circuit discriminator, IC-1. From there the audio signal divides between the squelch circuit input and the de-emphasis filter at the input to the audio preamplifier.

The squelch circuit opens and closes the signal path through the preamp according to the noise content in the demodulated signal. Also, control voltages for use with tone equipment are obtained from the squelch circuit.

The audio signal is taken from the 600 Ω output of the preamplifier to the AF amplifier. When transmitting in the simplex mode (CF701), the signal path through the output amplifier becomes automatically blocked. The tone equipment can also block the signal path here.

The signal from the microphone is amplified and limited in the modulation amplifier, which is designed around a dual, integrated operation-



al amplifier. Both amplifiers, IC2a and IC2b, are contained in the same housing.

To avoid adjacent channel interference, the high-frequency component of the modulating signal is filtered out and the signal is also amplitude limited in order to keep the carrier frequency swing within the established maximum excursions for whichever channel separation is employed.

As mentioned previously, the CF unit also contains two voltage regulators; one supplies the receiver section and the other, the transmitter. The AF output amplifier and the PA stage are supplied through a filter choke directly from the battery and are therefore unregulated.

Switching between transmit and receive is accomplished without relays. In CF701 the transmitter key electronically switches one or the other of the voltage regulators on so that both do not function at the same time. Terminal 10 is grounded during transmission and otherwise floats when the key is not activated.

Likewise, in the case of CF702, switching between the duplex and the receive conditions is accomplished without relays. Whenever the equipment is turned on the 9 V RX voltage regulator will always be on.

The PA stage is controlled by the 9 V TX regulator which turns on when terminal 10 is grounded (via the transmit key). Thus when transmitting, both the 9 V TX and the 9 V RX regulators are on.

12 V TX is taken off before the on/off switch in order to avoid any voltage drop in the start cable when employing extended local control. 12 V TX is applied to the PA stage through a transistor switching arrangement, the TX switch, which is driven by 9 V TX regulator.

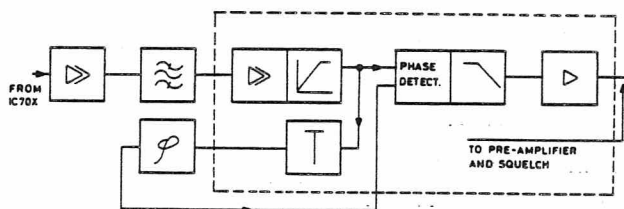
The 12 V supply voltage to the AF output amplifier is always on whenever the on/off switch is turned on. Therefore, in simplex equipment (CF701), the TX switch is designed to block the audio preamplifier when the transmitter is keyed. This is a precaution against any transients in the

scquelch circuit that might be applied to the receiver output during transmission.

As just explained, the receiver section in duplex equipment (CF702) is always on whenever power is applied to the set.

The 455 kHz IF Amplifier and Discriminator

This circuit amplifies, selects, limits and detects the receiver's second IF signal of 455 kHz, allowing a deviation of up to ± 15 kHz from centre frequency.



The amplifier has five stages; the first two, Q1 and Q2, are made up of discrete components while the last three are a part of the integrated circuit, IC1, along with the phase detector.

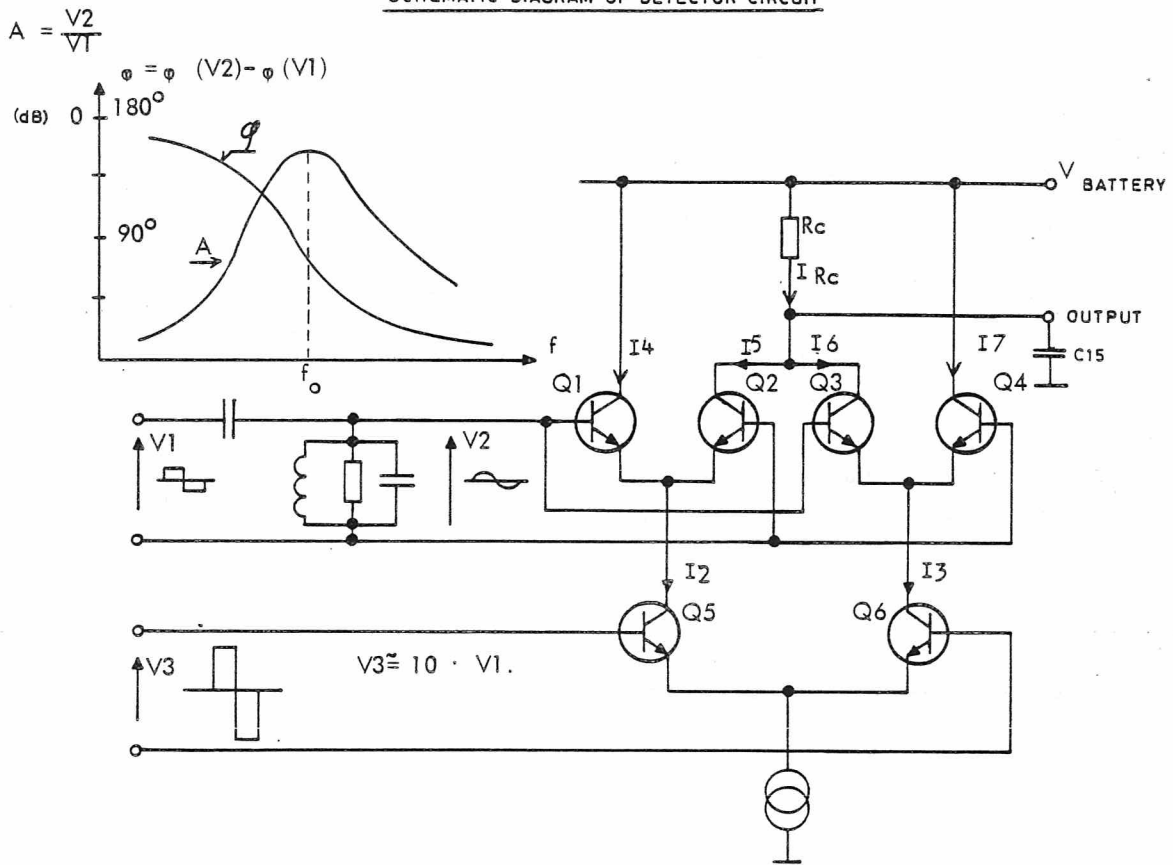
The only resonant circuits employed in the 2nd IF stage are those between the collector of Q2 and the input to IC1. Resistors R9 and R12 load T1 and T2 enough to achieve sufficiently broad bandwidth.

Inductive coupling between circuits is less than critical, R11 in the coupling link determining the coupling factor. Q2 operates with its collector-emitter voltage held low to prevent overdriving IC1.

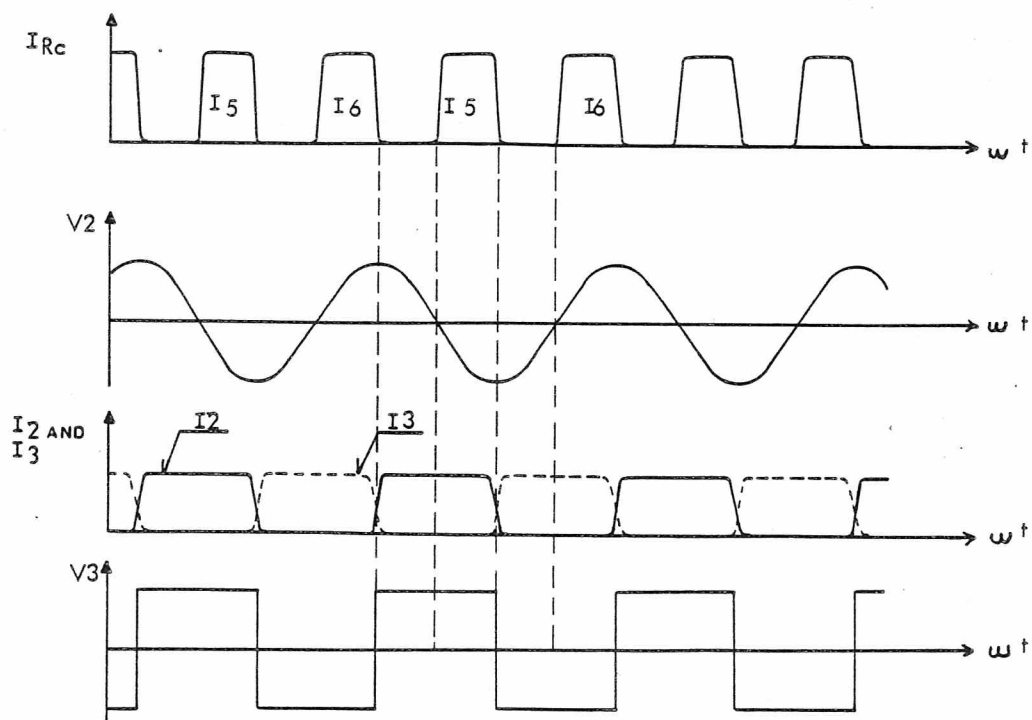
The three amplifier stages in IC1 are differential amplifiers, which configuration approaches ideal symmetrical limiting. The stages are DC coupled and stability is assured through strong negative feedback. Capacitor C12 eliminates the feedback as far as AC voltages are concerned.

Via an emitter follower within the IC housing, the signal is fed to the phase detector. The IF signal, with its amplitude peaks clipped, is applied directly to one of the phase detector inputs.

SCHMATIC DIAGRAM OF DETECTOR CIRCUIT



GRAPH OF VOLTAGE AND CURRENT RELATIONSHIPS IN THE PHASE DETECTOR WHEN $f = f_0$



The other input is fed the same signal, attenuated and approximately 90° out of phase (at f_0). Phase shift is accomplished with discrete components: C13, C14, L1 and R14. The following diagram shows the detector circuit schematic and the amplitude and phase characteristics of the phase shifting network. A graph of the detector current and voltage relationships is also included here.

The phase detector is designed around three differential amplifiers, all supplied through a constant-current source. In addition to the components shown in the detector schematic, IC1 also contains an emitter follower after the detector output, another emitter follower between the phase shifting network and one of the detector inputs, and various biasing networks.

As long as voltage V2 is high enough to drive the two differential stages - Q1 + Q2, and Q3 + Q4 - as switches, the collector current pulses, I5 and I6, will appear as a constant amplitude value and the average value of current through R_C remains independent of the amplitude of the input voltage.

As seen on the schematic, current pulses through R_C only appear when V2 and V3 are of opposite polarities and I5 appears only when V3 is positive while I6 appears when V3 is negative. Supposing that $f > f_0$, then the difference in phase (V2 - V1) is reduced (the V2 pulse a little to the right in relation to V3), causing the width of current pulses I5 and I6 to decrease. In other words, the average current through R_C will decrease. When $f < f_0$, the opposite will occur.

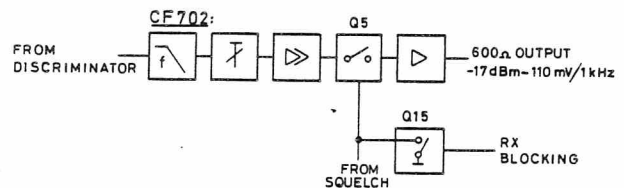
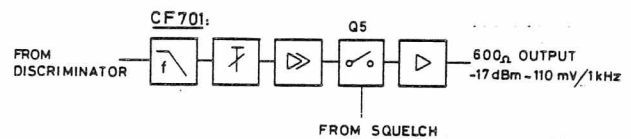
The width of I5 and I6 is therefore seen to be a measurement of the phase difference between V2 and V3. By integrating the output voltage (via R_C and C15) a voltage that is directly proportional to the phase shift is obtained.

Making use of both the negative and positive excursions of the signals, as in the detector configuration employed here, gives excellent suppression of noise and other undesired effects of inherent nonsymmetry in the clipped IF sig-

nal. For example, if the positive going half of V3 is wider than the negative half, I6 will be narrower and I5 wider with the result that the average current through R_C will remain unchanged.

An "S" curve similar to those known from conventional FM detectors will be present at the output (directly on pin 1 of IC1). However, the midpoint of this "S" curve will be around 3.5 V instead of 0 V. Circuit Q is designed low enough to enable the detector to handle frequency deviations of up to ± 15 kHz.

The De-emphasis Filter, AF Preamplifier and Electronic Squelching Switch



Network R15 and C19 take care of de-emphasizing the demodulated signal at the rate of -6 dB pr. octave.

The three stages of the preamplifier, Q3, Q4 and Q6, must then amplify the AF signal and match it to the nominal 600 Ω load. In addition, Q5 is inserted between Q4 and Q6. Q5, which is a field-effect transistor, operates as an electronic switch, interrupting the signal path on command from the squelch circuit.

CF702 includes an additional transistor, Q15. With a DC potential of ≥ 3 V at terminal 23 (RX Blocking) Q15 will be driven on, turning the AF switch, Q5, off. With the gate of Q5 held at ground by Q15, the condition of the squelch circuit will have no effect on the preamplifier.

The nominal output voltage of the preamplifier is -17 dBm into the 600 Ω output line. R16 is the adjustment used for setting the correct output level.

The collector of Q3 is directly coupled to the base of Q4; resistors R21, R22 and R23 provide the feedback necessary to stabilize the two stages.

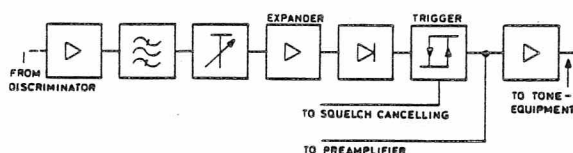
The signal path between the second and third amplifier stages is through the FET transistor, which acts like a relay contact, or switch. A gate-to-source potential of 4 V, at most, will "break" the path between source and drain. Since the collector of Q4 is at approx. 4.7 V, a gate voltage at Q5 under 0.7 V "breaks" the connection and "makes" the connection between Q4 and Q6 again when gate voltage rises above 4.7 V.

The Squelch

The squelch circuit opens or closes the audio signal path through the AF preamplifier according to the noise content of the incoming signal. The squelch circuit also provides a signal voltage for use in tone signalling.

An internal adjustment, potentiometer R38, is provided for setting the squelch level. The squelch function can be cancelled altogether by grounding terminal 5 via the squelch cancelling button on the control panel.

By altering only a few passive component values, the squelch section can operate on any of the three channel bandwidths normally employed.



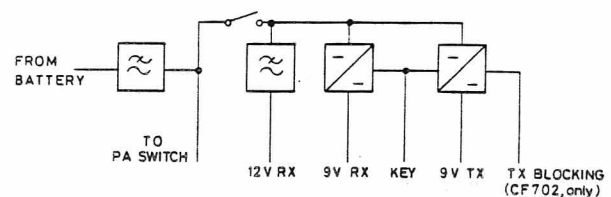
The squelch section includes a frequency selective noise amplifier, Q7, an expander stage, Q8, a noise detector, A Schmitt trigger, Q9 and Q10, and an emitter follower amplifier, Q11.

The operating principle is as follows:

Some of the AF signal from the discriminator is fed to the noise amplifier whose collector load is made up of a parallel resonant circuit tuned to some frequency well above the voice range, and depending upon the channel bandwidth employed. The selected noise is then fed to Q8 which is biased in such a way that only positive going pulses of a certain minimum amplitude cause the transistor to conduct. Since only pulses of a certain amplitude can become amplified, the result is that a given relative change in noise amplitude at the base of Q8 appears as a larger relative change at the collector. The noise pulses are then rectified and filtered to a DC potential that, in turn, controls the Schmitt trigger, Q9 and Q10. The collector voltage on Q10 is used partly to drive the emitter follower, Q11, and partly, through an R-C network, to switch the FET transistor in the AF preamplifier.

Where CF701 is used, keying the transmitter also interrupts the power to the receiver. At the same time, diodes E2 and E6 in the squelch are grounded through Q30 to prevent any false signals that might appear in the squelch circuitry from affecting the AF amplifier or Q11 during this condition. This does not apply to CF702.

The 9 V Voltage Regulators and Keying Circuits



The two 9 V voltage regulators supply the receiver and the transmitter sections, respectively. They are intended for use with a 12 volt auto battery.

The battery connects to the regulators through the transient and ripple filter, L3a and C39,

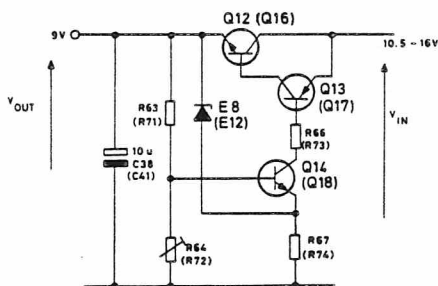
and through the vehicle's start switch via terminals 7 and 8. The AF output amplifier is supplied with unregulated, filtered battery power via the other filter winding, L3b, and C56 in the AF amplifier circuit.

To protect the equipment against incorrect battery polarity or excess voltage, a properly dimensioned zener diode is placed across the supply. If the power supply is connected wrong the zener diode will act as a short circuit at the input, blowing the fuses in the battery leads. In case of excess supply voltage, the zener diode will not allow more than about 20 volts to be present at the input to the regulators.

The voltage regulators are protected against short circuits; with shorted output the current through Q12 will be < 0.5 A and through Q16, < 0.1 A. The power transistors are mechanically mounted so as to be in good thermal contact with the chassis.

The two regulators are principally identical as shown on the simplified diagram as follows:

Q12 is driven by Q13, which is controlled by amplifier Q14. Transistor Q14 compares the zener reference voltage across E8 with a portion of the output voltage through dividing resistors R63 and R64. R64 sets the output voltage.



The operating principle is as follows:

If V_{OUT} drops (due to a decrease in input voltage or an increase in load current), V_{BE} for Q14 will increase, also increasing base current for Q13 and Q12. When base current to Q12 increases, more current flows through

the output load, cancelling the original drop in output voltage.

If the load current increases to a certain value, Q14 goes into saturation. If the load current increases still more, the zener diode will act as an open circuit and V_{BE} for Q14 decreases whereby base current for Q14, Q13 and Q12 decreases, too. Finally, Q14 will be cut off and base current in Q12 and Q13 will be zero. Thus is Q12 protected against destruction by short circuits at its output. Resistors R66 - and R67 - determine the saturation current through Q14 and, of course, the short circuit current.

A regulator built exactly like the simplified diagram would not be self-starting, however. Therefore, the regulators in the CF701 are provided with starting circuits;

9 V RX employs R61, R62 and E9 in its starting circuit and 9 V TX employs R70 and E11. Since 9 V RX and 9 V TX must not operate simultaneously, the regulators are also mutually coupled through a keying circuit that blocks, or cuts off, one regulator while allowing the other to operate. This function is controlled via terminal 10,

CF702 is arranged in a slightly different manner since 9 V RX must always operate when the equipment is turned on. While the 9 V RX and 9 V TX regulators employ the same starting circuits as just explained for CF701, the difference here is that keying the transmitter (which grounds terminal 10) does not turn the CF702 9 V RX regulator off.

Operation of Keying and Starting Circuits

For CF701:

When terminal 10 is floating and the power is turned on, 9 V RX will build up voltage since Q12 gets base current through R58, E9, R61 and R62. When 9 V RX reaches its final value the starting circuit will have no effect on the regulator because diode E9 will then be nonconducting (the unloaded voltage at terminal 10 is approx. 8.2 V at nominal battery voltage).

Transistors Q15 and Q19 are both heavily saturated, so the 9 V RX regulator will operate un-

disturbed while 9 V TX will be blocked because Q18 is completely cut off by Q19.

Grounding terminal 10 immediately cuts off Q15 and Q19. 9 V RX falls towards 0 V as there is now no base current to Q13. 9 V RX falls off at a rate determined by the time constant of C38 and the load on terminal 9. Under all operating conditions within factory specifications for the radiotelephone, the time constant will easily be long enough that the current through starting circuit R70 and E11 can turn on Q18, whereby a voltage builds up on 9 V TX that finally reaches a level where diode E11 becomes nonconducting.

Diode E10 and resistor R68 ensure that keying the transmitter cuts off base current to Q13 effectively, even at high temperatures. Diode E7 ensures effective keying even if terminal 10 is not brought all the way down to 0 V potential.

Note that 9 V TX cannot begin to build up a voltage by itself after a short circuit. Since - as just explained - it is 9 V RX that starts 9 V TX, it is necessary to activate the transmitter key again. Even with 9 V RX shorted, Q12 still gets its base current through the starting circuit where one of the resistors, R62, is a PTC resistor that will limit base current to the transistor at high ambient temperatures or when Q12 heats up.

For CF702

When terminal 10 is floating and the power is turned on, 9 V RX will build up voltage since Q12 gets base current through R58, E9, R61 and R62. When 9 V RX reaches its final value the starting circuit will have no effect on the regulator because diode E9 will then be nonconducting (the unloaded voltage at terminal 10 is approx. 8.2 V at nominal battery voltage).

Transistor Q19 is heavily saturated, completely cutting off Q18 and thus blocking the 9 V TX voltage regulator.

When the transmit key grounds terminal 10, two things happen:

1.) Q19 loses its forward bias and immediately cuts off. Now, instead of acting as a short circuit between the base of Q18 and ground, Q19 can now be considered a large resistance.

2.) C45, which has been charging through diode E10, has accumulated a charge of about 6.6 V. With terminal 10 grounded the charge on C45 reverse biases E10. Now C45 will discharge.

There are two discharge paths available to C45, one through the bleeder resistor, R59, and one through R70 and E11 to the base of Q18. Remember that the base of Q18 is no longer grounded by Q19.

The discharge current to the base of Q18 drives this transistor on. Once Q18 turns on its base assumes a potential of approx. 5 V. By now C45 has discharged so much that E11 becomes reverse biased by the 5 V on the base of Q18, and C45 continues to discharge through its other path (R59).

As long as terminal 10 is kept at chassis potential by the transmit key the 9 V TX regulator continues to operate.

When the key is released and terminal 10 resumes its unloaded potential of approx. 7.3 V, Q19 is driven on and short circuits the base of Q18 again. The 9 V TX regulator then turns off.

C45 charges again through E10.

Diode E7 ensures effective keying even if terminal 10 is not brought all the way down to 0 V potential.

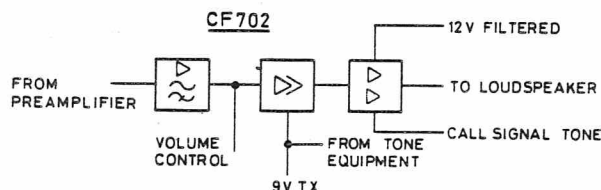
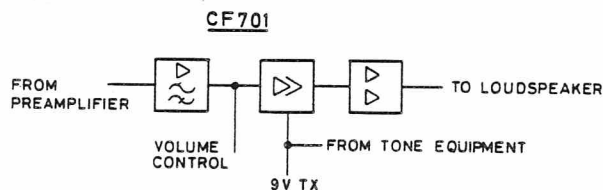
Note that 9 V TX cannot begin to build up a voltage by itself after a short circuit but must be started again by keying the transmitter.

Even with 9 V RX shorted, Q12 still gets its base current through the starting circuit where one of the resistors, R62, is a PTC resistor

that will limit base current to the transistor at high ambient temperatures or when Q12 heats up.

The AF Output Amplifier

The output amplifier amplifies the audio signal from the preamplifier and powers the loudspeaker.



Frequencies below 250 Hz are very sharply cut off in the first amplifier stage, transistor Q20. Included in the collector of Q20 is a variable resistor which allows for adjustment of the amplifier gain above the nominal amount in order to compensate for weak modulation of the incoming signal.

The signal passes from the 1st stage to the volume control whose arm connects to terminal 15 in the case of local control or to terminal 16 in case of extended local control. An isolation resistor is placed between the two terminals, allowing for extended local control without necessitating the removal of the local control connections.

The 2nd amplifier stage, Q21, is an emitter follower whose base voltage is the essential factor in determining the symmetry of the drive signal to the loudspeaker output.

From Q21, the signal is fed via two R-C low-pass filter networks to the 3rd amplifier stage, Q22. The primary purpose of the two low-pass networks is to stabilize the amplifier in regard to AC when employing extended local control.

In Q22, which in principle is coupled in the grounded emitter configuration, the signal is amplified and passes directly to the next amplifier stage which, in turn, is coupled directly to the driver transistors, Q25 and Q26. Transistor Q23 and resistors R98, R99 and R100 provide temperature compensated biasing for the driver transistors. As far as AC is concerned, the circuit appears as a short circuit between the bases of the two driver transistors. The complementary output transistors operate in class AB push-pull. Strong negative DC feedback is introduced in order to stabilize the operating point for the output stages. The feedback network is from the output, over R106 to the emitter of Q22. The AC feedback network is formed by R106 in conjunction with R96.

The power transistors employ aluminium heat sinks fastened to the radio chassis for good thermal contact.

During transmission a "muting signal" grounds the base of Q24 via terminal 18 and an R-C network, blocking the output amplifier. This network also functions as the blocking gate for the tone equipment.

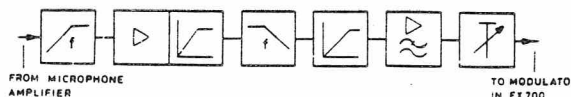
The Modulation Amplifier

General

The modulation amplifier differentiates, amplifies, limits and integrates the microphone signal. It also suppresses undesired high frequencies with an active filter designed for either 20, 25 or 50 kHz channel separation or, with a few resistor values changed, 12.5 kHz channel spacing.

Both amplifiers are contained in a single integrated circuit made up of dual operational amplifiers. The modulation amplifier contains additional passive differentiating and integrating circuits as well as diode clippers to prevent overmodulation.

The following block diagram shows the operating principle for the amplifier:



Input

The input circuit, which is also the collector return for the microphone amplifier output stage through resistor R112, is asymmetric.

The Differentiating Circuit

The differentiation network is made up of C64 and R113 (the input impedance of the op amp is negligible due to the feedback through R116). It differentiates at the rate of +6 dB pr. octave over the entire audio range of 300 to 3000 Hz.

The Amplifier - Clipper

The gain of the first amplifier stage, IC2a, is determined by the amount of feedback introduced. Circuit gain can be varied by about 10 dB by adjusting potentiometer R133.

Clipping action begins as soon as the amplifier is driven to where the collector excursions approximate the battery voltage. This level will be about 6.8 V peak-to-peak. The amplifier can be driven up to 25 dB above its nominal input level. Symmetry of the clipping is determined by bias network R114 and R115 and therefore is fixed.

The Integration Circuit

Integrating takes place from 230 Hz at 6 dB pr. octave. The passive integrating network consists of R118 and C67. The lower limit for integration is determined solely by these two components as the previous amplifier's feedback makes its output impedance negligible, and because the loading of the network by the filter that follows is very light as long as the signal remains below the frequency limit of that filter.

The 2nd Clipper (or Phase Clipper)

This extra clipper is inserted to prevent strong input signals at low frequencies from overdriving the modulator stage. For signal levels corresponding to the nominal frequency swing, the clipper has no effect. Two 1.5 V diodes and

capacitor C69 make up this circuit. These two diodes are connected to the junction of voltage divider R131 and R132 in order to have the same potential on both sides of C69, thus avoiding the time constant $R118 \times C69$ when keying the transmitter. The clipping level is only approx. 1.2 V at maximum due to the comparatively large impedance of R118.

The Splatter Filter

The purpose of this filter is to cut off frequencies that lie above the voice range in order to avoid undesirable sideband noise. It is an active filter consisting of the second operational amplifier and its associated components. Its response approaches that of a Chebishev filter. The circuit arrangement is the so-called voltage follower, where the voltage gain is very near unity (1). The significant passive filter components are resistors R119, R120 and R121 and capacitors C70, C71, C72, C75, C76 and C77. The filter cannot be overdriven because the input signal level is subject to limiting by the diode clipper.

Adjusting the Frequency Swing

The amount of signal to the modulator input, and thus the frequency swing, is set by potentiometer R124. R133 sets the modulation sensitivity.

The TX Switch.

The PA keying circuit operates an electronic switch in the path of the 12 V TX supply voltage to the PA unit. The circuit consists of Q29 and Q30 along with the associated resistor networks at their bases. The transistors operate in saturation when transmitting and are cut-off during standby, or receive. The circuit is controlled from 9 V TX.

For CF701, Q30 has the additional function of grounding out any spurious squelch signals whenever the transmitter is activated.

TECHNICAL SPECIFICATIONS

Nominal Supply Voltage

13.6 V

Current Drain for CF701 (at nominal supply voltage)

Transmit: 220 mA

Receive : 65 mA

Current Drain for CF702 (at nominal supply voltage)

Transmit: 285 mA

Receive : 65 mA

12 dB SINAD Sensitivity (where 1.75 kHz deviation of the 455 kHz IF results in a 1 kHz audio signal)

1.2 μ V input signal at antenna terminationAF Line Out (terminal 3)-17 dBm/ 600 Ω Regulated Voltages

Receiver (terminal 9) : 9 V

Transmitter (terminal 13): 9 V

Unregulated, Filtered Voltages

AF output amplifier : 13.6 V

PA stage (terminal 19) : 13.6 V

AF Output Power (terminal 17)

2 W

Modulation Amplifier Sensitivity (for normal frequency swing of 1 kHz)

110 mV +1/ -0 dB

The following, more detailed specifications for the several CF701 and CF702 functions are all typical values measured at 25^o C ambient temperature, unless otherwise stated.

455 kHz IF AMPLIFIER and DISCRIMINATORCurrent Drain (at nominal 9 V supply)

18 mA

Maximum Frequency Deviation \pm 15 kHzIF Bandwidth (3 dB attenuation) \pm 17 kHzInput Impedance1 k Ω // 15 pFGain

from input (terminal 1) to pin 4 of IC1: 55 dB

from IC1 input (pin 4) to IC1 amplifier

high output, pin 10: 55 dB

Discriminator Conversion Efficiency

50 mV / kHz

AF Output Voltage ($f_m = 1$ kHz, $\Delta f = 3.5$ kHz)

110 mV

Measured at test point 2, terminated with 2.2 k Ω load.

Discriminator Linearity (relative to 1000 Hz)

Pass-Band 100 - 3500 Hz: +0/ -1 dB

Measured at test point 2, terminated with 2.2 k Ω load.

Discriminator Output Resistance200 Ω

Minimum Load Resistance2 k Ω Harmonic Distortion $\Delta f = 15 \text{ kHz} : 4.5\%$ $\Delta f = 3.5 \text{ kHz} : 1.0\%$ AF PREAMPLIFIER and
SQUELCH-CONTROLLED SWITCHCurrent Drain (at nominal 9 V supply)

8 mA

Input Impedance (at 1 kHz)2.2 k Ω Output Impedance $R_{OUT} = 680 \Omega$ Gain (gain control at highest setting) $R_L = 560 \Omega, f = 1 \text{ kHz} : 12.5 \text{ dB}$ Harmonic Distortion ($R_L = 560 \Omega, f = 1 \text{ kHz}$) $V_{OUT} = 110 \text{ mV (nominal)} : 0.2 \%$ $V_{OUT} = 500 \text{ mV} : 0.5 \%$ Required Turn-on Potential for CF701

(at gate of Q5)

To ensure normal signal path: $\geq 4.7 \text{ V}$ Required Turn-off Potential for CF701

(at gate of Q5)

To ensure 70 dB attenuation of signal: $\leq 0.7 \text{ V}$

Measured with 110 mV, 1 kHz signal applied to circuit input, test point 2, and gain control set at max., V_{OUT} (terminal 3) = approx. 500 mV.

Required Turn-on Potential for CF702

a. at gate of Q5, to ensure normal signal path: $\geq 4.7 \text{ V}$

b. at terminal 23 (RX Blocking), to allow normal operation of squelch command: $\leq 0.8 \text{ V}$

Required Turn-off Potential for CF702

a. at gate of Q5, to ensure 70 dB attenuation of signal: $\leq 0.7 \text{ V}$

b. at terminal 23 (RX Blocking), for same result: $\geq 3 \text{ V}$

Measured with 110 mV, 1 kHz signal applied to circuit input, test point 2, and gain control set at max., V_{OUT} (at terminal 3) = approx. 500 mV.

De-emphasis Cut-off Frequency

90 Hz

Frequency Response (relative to -6 dB/octave characteristic)

Pass-Band linearity (300 - 3000 Hz): $+0/-1 \text{ dB}$
50 - 100 Hz : $+15 \text{ dB}$

SQUELCH CIRCUITCurrent Drain (at nominal 9 V supply)

12 mA

Measured with unloaded Squelch Signalling (terminal 4).

Input Impedance (at 1 kHz)20 k Ω Noise Filter Resonant Frequency

12.5 kHz channel spacing : 7.1 kHz

20/25 kHz channel spacing : 7.1 kHz

50 kHz channel spacing : 10 kHz

Output VoltageSquelched condition : $\leq 100 \text{ mV}$ Un-squelched condition: $> 5.7 \text{ V}$ Measured at test point 1. DC.Squelch Signalling (terminal 4) R_{LOAD} minimum: 680 Ω V_{OUT} (with $R_L = 680\Omega$)Squelched condition $\leq 100 \text{ mV}$ Un-squelched condition $\geq 4.0 \text{ V}$

Transition Time (gain control set for nominal V_{OUT})

6 ms

Delay measured from the time that the voltage at test point (1) switches state until the AF signal at terminal 3 increases from 10% to 90% of its nominal amplitude.

Turn-off delay (signal decrease from 90% to 10%) is also 6 ms.

Overall Receiver Squelch Response

Turn-on delay: 30 ms

Turn-off delay: 25 ms

Measured with receiver adjusted for 12 dB SINAD.

AF OUTPUT AMPLIFIER

Nominal Supply Voltage

13.6 V

Operating Range

10.5 to 16.0 V

Current Drain (at nominal supply voltage)

no-signal condition : 20 mA

at 2 W output : 300 mA

blocked : 20 mA

Output Power (at nominal supply voltage)

maximum 2 W

Loudspeaker Impedance

Nominal / minimum: 5 Ω

Input Impedance (at 1 kHz)

560 Ω

Nominal Gain

Input signal (1 kHz) required for 2 W output: 110 mV

Measured with volume control (5 k Ω potentiometer) connected to terminals 14, 15 and chassis ground, and turned fully up.

Where the connections are to terminals 14, 16 and chassis, as with extended local control, the gain increases by 2 dB.

Adjustment of R83 can increase sensitivity 12 dB.

Gain vs. $\Delta V_{BATT.}$

13.6 V +2.4 / -3.1 V: 0.2 dB

Harmonic Distortion

$P_{OUT} = 2 W$: 1%

$P_{OUT} = 0.2 W$: 0.5%

Frequency Response (relative to 1 kHz)

100 Hz -22 dB

300 Hz 0 dB

2700 Hz -0.5 dB

6 Hz -2 dB

Measured at 0.2 W output power.

AF Muting

Required DC at terminal 18 to attenuate the output signal by 60 dB: 8.0 V

MODULATION AMPLIFIER

Current Drain, CF701 (at nominal 9 V supply)

2 mA

Current Drain, CF702 (at nominal 9 V supply)

5 mA

Input Impedance (at 1 kHz)

560 Ω

Limiting

Signal clipping begins to occur with an input signal (1000 Hz) of: 110 mV

Output signal level observed at pin 2 of IC2 when clipping occurs: 7.0 V p.p.

Phase Limiting, CF701

Phase clipping level (at 300 Hz): 2.1 V p.p.

Measured immediately after the integration network, with an input signal of 1.1 V (nominal 110 mV + 20 dB).

Phase Limiting, CF702

Phase clipping level (at 300 Hz): 2.5 V p.p.

Measured immediately after the integration network, with an input signal of 1.1 V (nominal 110 mV + 20 dB).

Output Voltage (1000 Hz)

560 mV

Measured at Modulation Output (terminal 21) with potentiometer R124 fully up, and load impedance = 1 kΩ.

Input level = 110 mV

Harmonic Distortion (at 1000 Hz)

for 110 mV input signal : 0.8%

Frequency Response (relative to 1 kHz)

	channel spacing	
	20/25/50 kHz	12.5 kHz
300 Hz	-0.5 dB	-0.5 dB
3 kHz	-1 dB	-4 dB
6 kHz	-19 dB	-25 dB
10 kHz	-32 dB	-37 dB

Measured for 15 mV input signal, and with a resistive output load.

12 V RX to AF Output Amplifier (filtered, unregulated voltage)

ripple suppression at 1 kHz, no load condition: 36 dB
 voltage drop over filter when $P_{OUT} = 2 W$: 0.25 V
 maximum output current: 500 mA

Keying Termination

Maximum allowable resistance of wiring : 180 Ω
 Alternatively, V_{MAX} at terminal 10 : 1.0 V

Regulator Switching Time ($V_{BATT.} = 13.6 V$)

9V RX turn-on delay, $t_{0-90\%}$: 0.4 ms
 9V RX turn-off delay, $t_{100-10\%}$: 100 ms
 9V TX turn-on delay, $t_{0-90\%}$: 0.1 ms
 9V TX turn-off delay, $t_{100-10\%}$: 25 ms

Measured under normal load conditions.

Regulator Output Current

Maximum 150 mA

Internal Resistance of Regulators

$R_I = 0.5 \Omega$

Suppression of $\Delta V_{BATTERY}$ in V_{REG}

(at nominal load)

DC : 46 dB

1 kHz : 50 dB

9V VOLTAGE REGULATORS and KEYING CIRCUITS

Nominal Supply Voltage

13.6 V

Operating Range

10.5 V to 16 V

Regulated Output Voltages

Receiver supply 9V RX: 9.0 V ± 0.2 V

Transmitter supply 9V TX: 9.0 V ± 0.2 V

V_{REG} vs. Temperature

3.6 mV / pr. °C

PA KEYING CIRCUIT

Nominal Supply Voltage

13.6 V

Operating Range

10.5 to 16 V

Maximum Load Current

3 A

TX Switch

Voltage drop across transistor switch when ON, at 2 A load current: 0.2 V

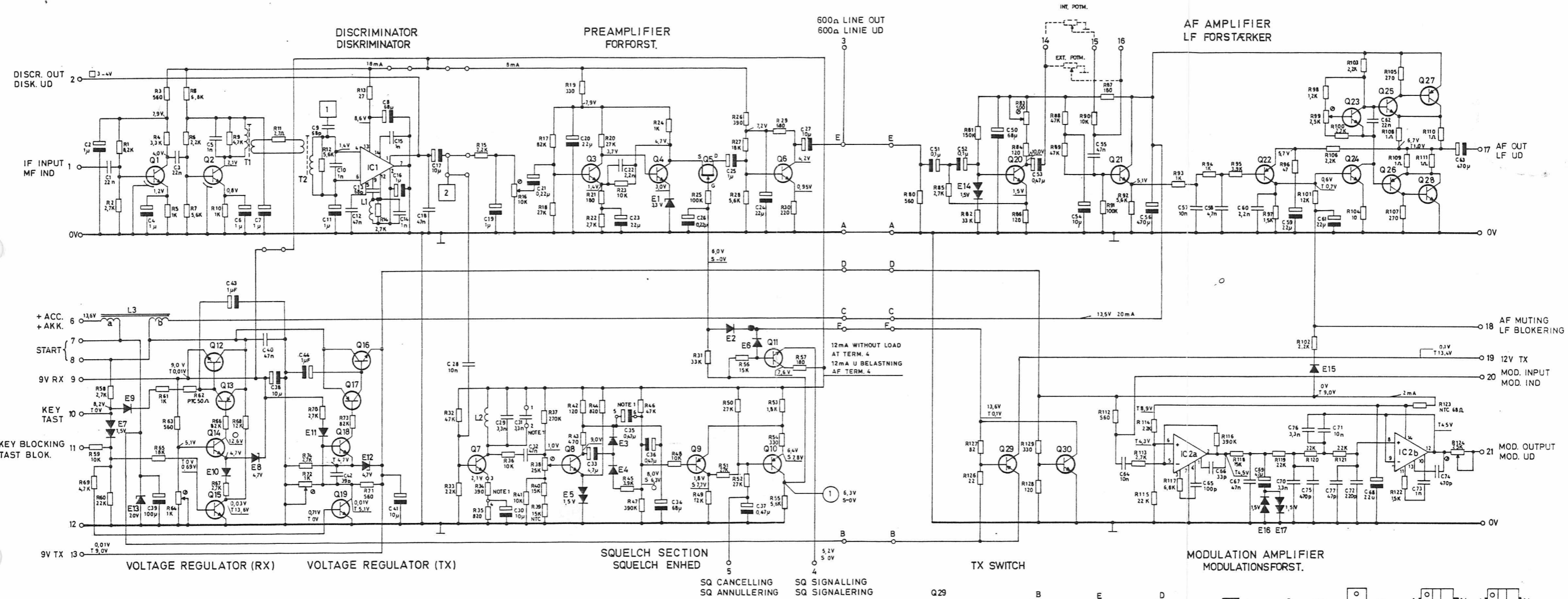
Transistor collector current when OFF:

$T_{AMB} = 25^{\circ}C$: 0.2 mA

$T_{AMB} = 60^{\circ}C$: 10 mA

LOWER PRINTED WIRING BOARD

UPPER PRINTED WIRING BOARD

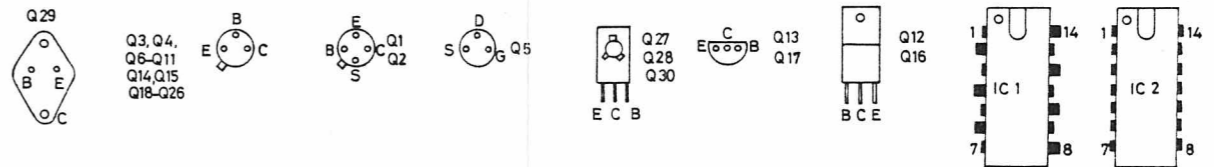


DEPENDENT ON THE CHANNEL SEPARATION EMPLOYED
MAKE THE FOLLOWING ALTERATIONS:

CH. SEP.	POINTS	1-2	3-4	5-6	
12.5 kHz		3.3nF	150Ω	0.47μF	REPLACE R119, R120, R121, BY 27KΩ
20/25 kHz		3.3nF	390Ω	0.47μF	
50 kHz	OPEN		820Ω	OPEN	

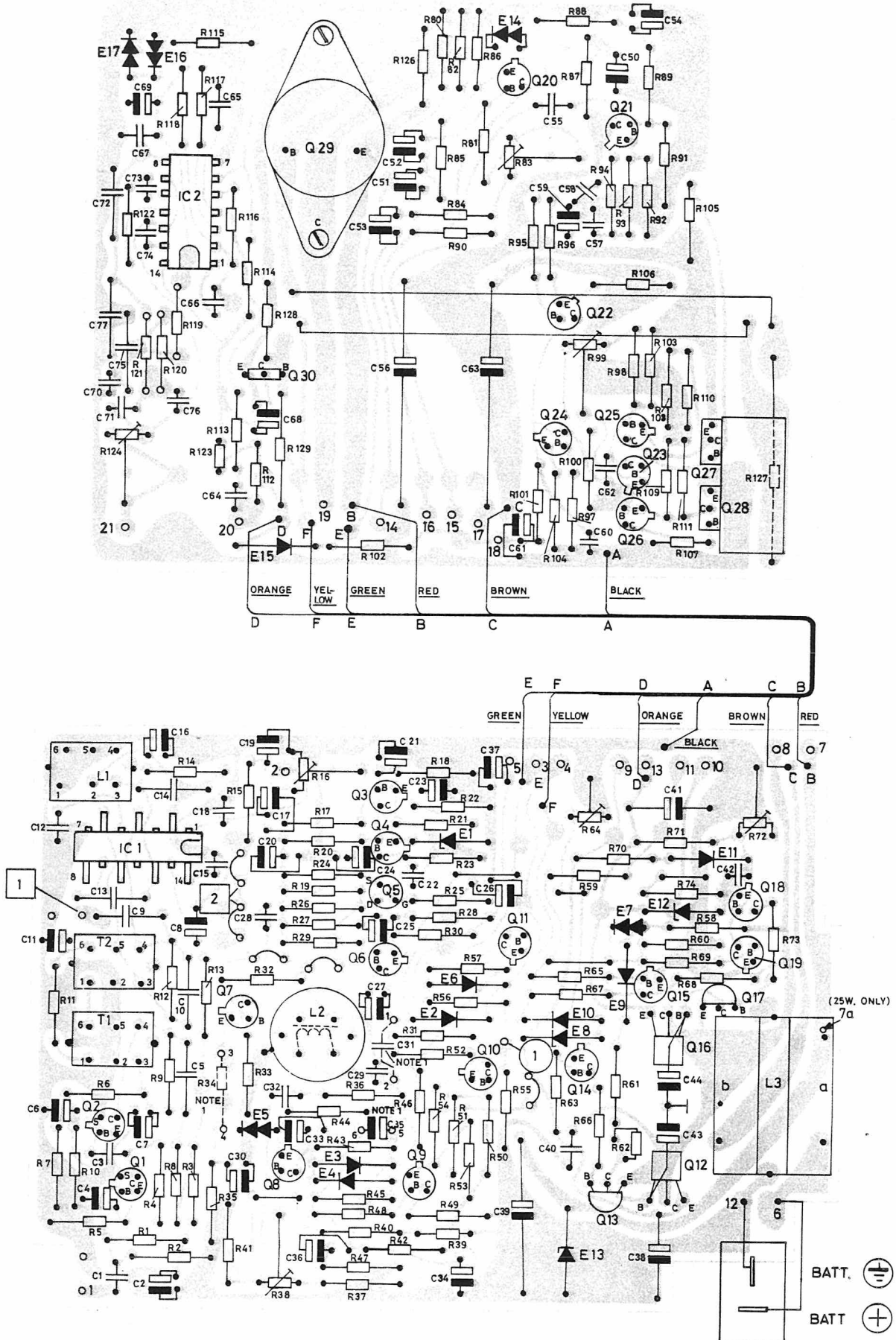
CONDITIONS OF MEASUREMENTS

- MEASURED AT $\Delta f = 0$ kHz
- Δ RESISTOR R83 SHORT-CIRCUITED
- S SQUELCHED CONDITION
- T TRANSMITTER KEYED CONDITION
- USE A HIGH-RESISTANCE VOLTMETER (2MΩ)



COMMON FUNCTION UNIT
FÆLLESENHED CF701

D401.296/2



COMMON FUNCTION UNIT CF701

D401.515

TYPE	NO.	CODE	DATA
CF701		10.2433	Common Functions Unit
	C1	76.5071	22 nF 10% polyester, FL
	C2	73.5114	1 μF 20% tantal
	C3	76.5071	22 nF 10% polyester, FL
	C4	73.5114	1 μF 20% tantal
	C5	76.5109	1 nF 2.5% polyester, TB
	C6	73.5114	1 μF 20% tantal
	C7	73.5114	1 μF 20% tantal
	C8	73.5106	68 μF 20% tantal
	C9	76.5101	68 pF 2.5% polystyr TB
	C10	76.5109	1 nF 2.5% polystyr TB
	C11	73.5114	1 μF 20% tantal
	C12	76.5072	47 nF 10% polyester, FL
	C13	76.5101	68 pF 2.5% polystyr TB
	C14	76.5109	1 nF 2.5% polystyr TB
	C15	76.5069	1 nF 10% polyester FL
	C16	73.5114	1 μF 20% tantal
	C17	73.5109	10 μF 20% tantal
	C18	76.5072	47 nF 10% polyester FL
	C19	73.5114	1 μF 20% tantal
	C20	73.5127	22 μF 20% tantal
	C21	73.5118	0.22 μF 20% tantal
	C22	76.5059	2.2 nF 10% polyester FL
	C23	73.5127	22 μF 20% tantal
	C24	73.5127	22 μF 20% tantal
	C25	73.5114	1 μF 20% tantal
	C26	73.5118	0.22 μF 20% tantal
	C27	73.5109	10 μF 20% tantal
	C28	76.5070	10 nF 10% polyester FL
	C29	76.5060	3.3 nF 10% polyester, FL
	C30	73.5109	10 μF 20% tantal
	C31	76.5060	3.3 nF 10% polyester, FL
	C32	76.5072	47 nF 10% polyester FL
	C33	73.5126	4.7 μF 20% tantal
	C34	73.5106	68 μF 20% tantal
	C35	73.5125	0.47 μF 20% tantal
	C36	73.5125	0.47 μF 20% tantal
	C37	73.5125	0.47 μF 20% tantal
	C38	73.5011	10 μF -10/+100% elco
	C39	73.5071	100 μF -10/+100% elco
	C40	76.5072	47nF 10% polyester FL
	C41	73.5011	10 μF -10/+100% elco
	C42	74.5187	39pF 10% ceram N750 PL
	C43	73.5114	1 μF 20% tantal
	C44	73.5114	1 μF 20% tantal
	C50	73.5106	68 μF 20% tantal
	C51	73.5089	0.1 μF 20% tantal

TYPE	NO.	CODE	DATA
	C52	73.5089	0.1 μF 20% tantal
	C53	73.5125	0.47 μF 20% tantal
	C54	73.5109	10 μF 20% tantal
	C55	76.5072	47 nF 10% polyester FL
	C56	73.5138	470 μF -10/+50% elco
	C57	76.5070	10 nF 10% polyester, FL
	C58	76.5061	4.7 nF 10% polyester FL
	C59	73.5127	22 μF 20% tantal
	C60	76.5059	2.2 nF 10% polyester FL
	C61	73.5127	22 μF 20% tantal
	C62	76.5071	22 nF 10% polyester FL
	C63	73.5137	470 μF -10/+50% elco
	C64	76.5070	10 nF 10% polyester FL
	C65	74.5165	100 pF 10% ceram PL
	C66	74.5116	33 pF 5% ceram TB
	C67	76.5072	47 nF 10% polyester FL
	C68	73.5127	22 μF 20% tantal
	C69	73.5126	4.7 μF 20% tantal
	C70	76.5060	3.3 nF 10% polyester, FL
	C71	76.5070	10 nF 10% polyester FL
	C72	76.5104	220 pF 5% polystyr TB
	C73	76.5069	1 nF 10% polyester FL
	C74	74.5161	470 pF -20/+80% ceram PL
	C75	76.5106	470 pF 5% polystyr TB
	C76	76.5060	3.3 nF 10% polyester FL
	C77	76.5090	47 pF 5% polystyr
	R1	80.5260	8.2 kΩ 5% carbon film
	R2	80.5254	2.7 kΩ 5% "
	R3	80.5246	560 Ω 5% "
	R4	80.5255	3.3 kΩ 5% "
	R5	80.5249	1 kΩ 5% "
	R6	80.5253	2.2 kΩ 5% "
	R7	80.5258	5.6 kΩ 5% "
	R8	80.5259	6.8 kΩ 5% "
	R9	80.5257	4.7 kΩ 5% "
	R10	80.5249	1 kΩ 5% "
	R11	80.5218	2.7 Ω 5% "
	R12	80.5258	5.6 kΩ 5% "
	R13	80.5258	27 Ω 5% "
	R14	80.5254	2.7 kΩ 5% "
	R15	80.5253	2.2 kΩ 5% "

COMMON FUNCTIONS UNIT CF701

TYPE	NO.	CODE	DATA
	R16	86. 5039	10 k Ω 20% potentiometer
	R17	80. 5276	82 k Ω 5% carbon film
	R18	80. 5266	27 k Ω 5% "
	R19	80. 5243	330 Ω 5% "
	R20	80. 5266	27 k Ω 5% "
	R21	80. 5240	180 Ω 5% "
	R22	80. 5254	2. 7 k Ω 5% "
	R23	80. 5261	10 k Ω 5% "
	R24	80. 5249	1 k Ω 5% "
	R25	80. 5273	0. 1 M Ω 5% "
	R26	80. 5244	390 Ω 5% "
	R27	80. 5264	18 k Ω 5% "
	R28	80. 5258	5. 6 k Ω 5% "
	R29	80. 5247	680 Ω 5% "
	R30	80. 5241	220 Ω 5% "
	R31	80. 5267	33 k Ω 5% "
	R32	80. 5269	47 k Ω 5% "
	R33	80. 5265	22 k Ω 5% "
	R34	80. 5244	390 Ω 5% "
	R35	80. 5248	820 Ω 5% "
	R36	80. 5261	10 k Ω 5% "
	R37	80. 5278	0. 27 M Ω 5% "
	R38	86. 5044	25 k Ω 20% potentiometer
	R39	89. 5010	15 k Ω 2% NTC
	R40	80. 5263	15 k Ω 5% carbon film
	R41	80. 5261	10 k Ω 5% "
	R42	80. 5238	120 Ω 5% "
	R43	80. 5245	470 Ω 5% "
	R44	80. 5248	820 Ω 5% "
	R45	80. 5256	3. 9 k Ω 5% "
	R46	80. 5269	47 k Ω 5% "
	R47	80. 5280	0. 39 M Ω 5% "
	R48	80. 5261	10 k Ω 5% "
	R49	80. 5262	12 k Ω 5% "
	R50	80. 5266	27 k Ω 5% "
	R51	80. 5266	27 k Ω 5% "
	R52	80. 5266	27 k Ω 5% "
	R53	80. 5252	1. 8 k Ω 5% "
	R54	80. 5243	330 Ω 5% "
	R55	80. 5258	5. 6 k Ω 5% "
	R56	80. 5263	15k Ω 5% "
	R57	80. 5240	180 Ω 5% "
	R58	80. 5254	2. 7 k Ω 5% "
	R59	80. 5261	10 k Ω 5% "
	R60	80. 5265	22 k Ω 5% "
	R61	80. 5249	1 k Ω 5% "
	R62	89. 5046	50 Ω PTC
	R63	80. 5246	560 Ω 5% "

TYPE	NO.	CODE	DATA
	R64	86. 5068	1 k Ω 20% potentiometer
	R65	80. 5264	18 k Ω 5% carbon film
	R66	80. 5272	82 k Ω 5% "
	R67	80. 5254	2. 7 k Ω 5% "
	R68	80. 5262	12 k Ω 5% "
	R69	80. 5257	4. 7 k Ω 5% "
	R70	80. 5254	2. 7 k Ω 5% "
	R71	80. 5246	560 Ω 5% "
	R72	86. 5058	1 k Ω 20% potentiometer
	R73	80. 5272	82 k Ω 5% carbon film
	R74	80. 5254	2. 7 k Ω 5% "
	R80	80. 5246	560 Ω 5% "
	R81	80. 5275	0. 15 M Ω 5% "
	R82	80. 5267	33 k Ω 5% "
	R83	86. 5042	500 Ω 20% potentiometer
	R84	80. 5238	120 Ω 5% carbon film
	R85	80. 5254	2. 7 k Ω 5% "
	R86	80. 5238	120 Ω 5% "
	R87	80. 5240	180 Ω 5% "
	R88	80. 5269	47 k Ω 5% "
	R89	80. 5269	47 k Ω 5% "
	R90	80. 5261	10 k Ω 5% "
	R91	80. 5273	0. 1 M Ω 5% "
	R92	80. 5258	5. 6 k Ω 5% "
	R93	80. 5249	1 k Ω 5% "
	R94	80. 5249	1 k Ω 5% "
	R95	80. 5256	3. 9 k Ω 5% "
	R96	80. 5233	47 Ω 5% "
	R97	80. 5251	1. 5 k Ω 5% "
	R98	80. 5250	1. 2 k Ω 5% "
	R99	86. 5043	2. 5 k Ω 20% potentiometer
	R100	80. 5254	2. 7 k Ω 5% carbon film
	R101	80. 5262	12 k Ω 5% "
	R102	80. 5253	2. 2k Ω 5% "
	R103	80. 5253	2. 2 k Ω 5% "
	R104	80. 5225	10 Ω 5% "
	R105	80. 5242	270 Ω 5% "
	R106	80. 5253	2. 2 k Ω 5% "
	R107	80. 5242	270 Ω 5% "
	R108	80. 5213	1 Ω 5% "
	R109	80. 5213	1 Ω 5% "
	R110	80. 5213	1 Ω 5% "

COMMON FUNCTIONS UNIT CF701

X401. 322/ 2

TYPE	NO.	CODE	DATA
	R111	80.5213	1 Ω 5% carbon film
	R112	80.5246	560 Ω 5% " "
	R113	80.5254	2.7 kΩ 5% " "
	R114	89.5062	22 kΩ 1% metal film
	R115	89.5062	22 kΩ 1% metal film
	R116	80.5280	0.39 MΩ 5% carbon film
	R117	80.5259	6.8 kΩ 5% " "
	R118	80.5263	15 kΩ 5% " "
	R119	89.5062	22 kΩ 1% metal film
	R120	89.5062	22 kΩ 1% metal film
	R121	89.5062	22 kΩ 1% metal film
	R122	80.5251	1.5 kΩ 5% carbon film
	R123	89.5061	68 Ω 20% NTC
	R124	86.5044	25 kΩ 20% potentiometer
	R126	80.5229	22 Ω 5% carbon film
	R127	84.5224	82 Ω 5% wire wound
	R128	80.5238	120 Ω 5% carbon film
	R129	80.5443	330 Ω 5% " "
	L1	61.1131	IF coil 455 kHz
	L2	61.1132	Coil 75 mH
	L3	60.5158	Cnoke
	T1	61.1130	IF Transformer 455 kHz
	T2	61.1130	IF Transformer 455 kHz
	E1	99.5210	Zenerdiode 3.3V 5%
	E2	99.5237	1N4148 Diode
	E3	99.5237	1N4148 Diode
	E4	99.5237	1N4148 Diode
	E5	99.5209	Stab. diode 1.5V
	E6	99.5237	1N4148 Diode
	E7	99.5209	Stab. diode 1.5V
	E8	99.5224	Zenerdiode 4.7V 5%
	E9	99.5237	1N4148 Diode
	E10	99.5237	1N4148 Diode
	E11	99.5237	1N4148 Diode
	E12	99.5224	Zenerdiode 4.7V 5%
	E13	99.5249	Zenerdiode BZY93/C20R
	E14	99.5209	Stab. diode 1.5V
	E15	99.5237	1N4148 Diode
	E16	99.5209	Stab. diode 1.5V
	E17	99.5209	Stab. diode 1.5V
	Q1	99.5166	BF167 Transistor
	Q2	99.5166	BF167 Transistor
	Q3	99.5143	BC108 Transistor
	Q4	99.5143	BC108 Transistor

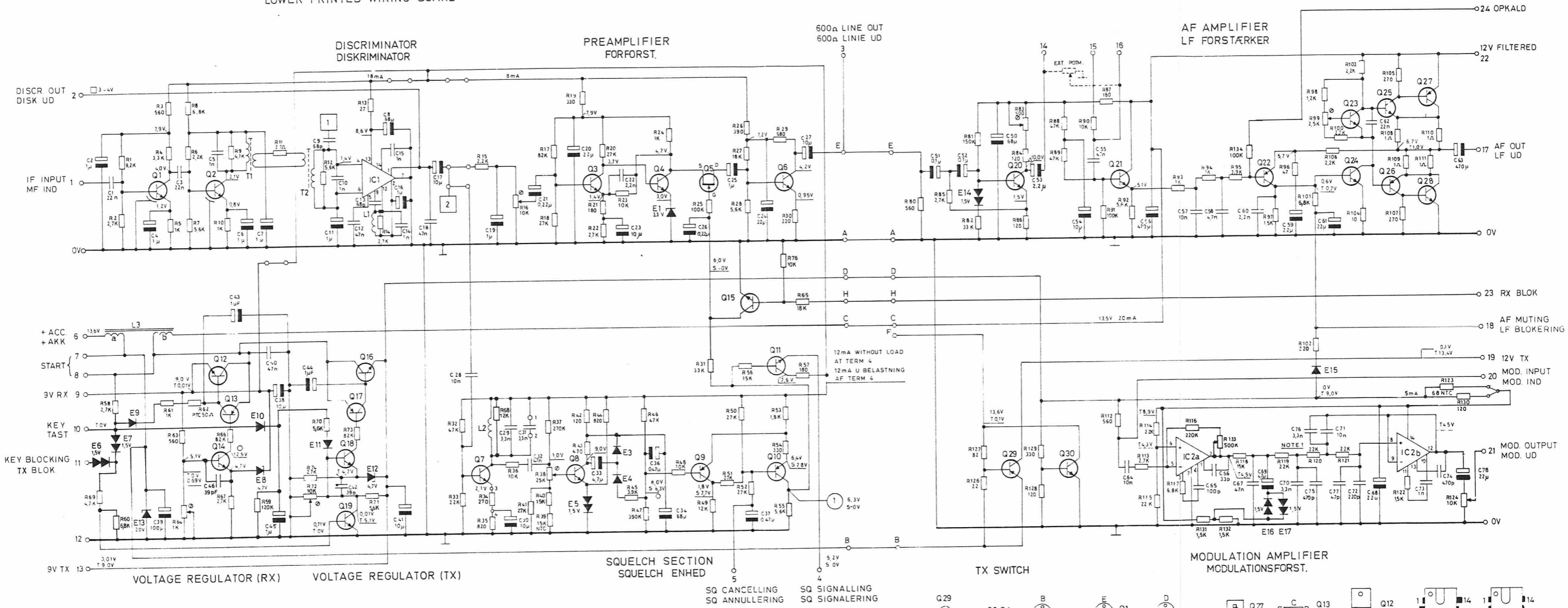
TYPE	NO.	CODE	DATA
	Q5	99.5247	2N4302 Transistor FET
	Q6	99.5143	BC108 Transistor
	Q7	99.5143	BC108 Transistor
	Q8	99.5143	BC108 Transistor
	Q9	99.5115	BC179 Transistor
	Q10	99.5115	BC179 Transistor
	Q11	99.5143	BC108 Transistor
	Q12	99.5246	TIP 31 Transistor
	Q13	99.5144-01	BC214L Transistor
	Q14	99.5243	BC108 Transistor
	Q15	99.5243	BC108 Transistor
	Q16	99.5246	TIP 31 Transistor
	Q17	99.5144-01	BC214L Transistor
	Q18	99.5143	BC108 Transistor
	Q19	99.5143	BC108 Transistor
	Q20	99.5201	BC109 Transistor
	Q21	99.5201	BC109 Transistor
	Q22	99.5115	BC179 Transistor
	Q23	99.5143	BC108 Transistor
	Q24	99.5143	BC108 Transistor
	Q25	99.5143	BC108 Transistor
	Q26	99.5115	BC179 Transistor
	Q27	99.5236	BD136 Transistor
	Q28	99.5235	BD135 Transistor
	Q29	99.5248	SP2629 Transistor
	Q30	99.5235	BD135 Transistor
	IC1	14.5010	IF ampl./discr.
	IC2	14.5006	MCI437P dual OP amp.

COMMON FUNCTIONS UNIT CF701

X401.322/2

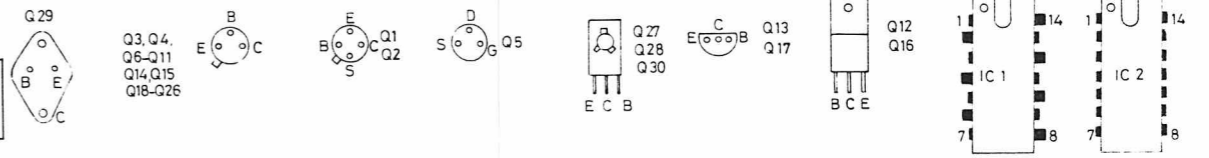
LOWER PRINTED WIRING BOARD

UPPER PRINTED WIRING BOARD

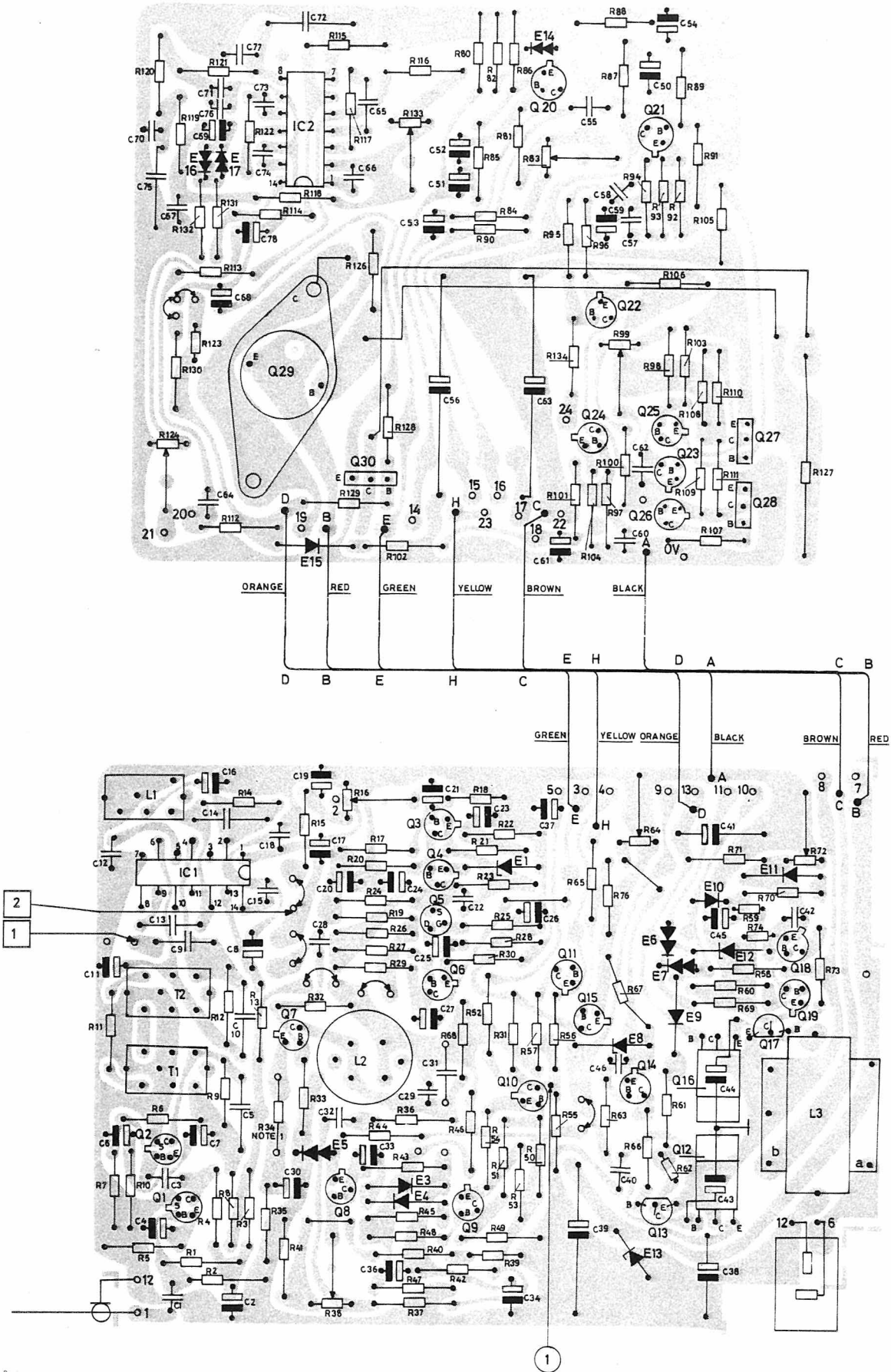


- CONDITIONS OF MEASUREMENTS**
- MEASURED AT $\Delta f = 0 \text{ kHz}$
 - △ RESISTOR R83 SHORT-CIRCUITED
 - S SQUELCHED CONDITION
 - T TRANSMITTER KEYED CONDITION
 - USE A HIGH-RESISTANCE VOLTMETER (2M Ω)

NOTE 1
 1 ANLÆG TIL SVERIGE SKAL R119, R120 OG R121 ERSTATTES MED 27K Ω .



COMMON FUNCTION UNIT
 FÆLLESENHED
 D401.840 CF702



COMMON FUNCTIONS UNIT CF702

TYPE	NO.	CODE	DATA
	R13	80.5230	27 Ω 5% carbon film
	R14	80.5254	2.7 KΩ 5%
	R15	80.5253	2.2 KΩ 5%
	R16	86.5039	10 KΩ 20% potentiometer
	R17	80.5272	82 KΩ 5% carbon film
	R18	80.5266	27 KΩ 5%
	R19	80.5243	330 Ω 5%
	R20	80.5266	27 KΩ 5%
	R21	80.5240	180 Ω 5%
	R22	80.5254	2.7 KΩ 5%
	R23	80.5261	10 KΩ 5%
	R24	80.5249	1 KΩ 5%
	R25	80.5273	0.1 MΩ 5%
	R26	80.5244	390 Ω 5%
	R27	80.5264	18 KΩ 5%
	R28	80.5258	5.6 KΩ 5%
	R29	80.5247	680 Ω 5%
	R30	80.5241	220 Ω 5%
	R31	80.5267	33 KΩ 5%
	R32	80.5269	47 KΩ 5%
	R33	80.5265	22 KΩ 5%
	R34	80.5244	390 Ω 5%
	R35	80.5248	820 Ω 5%
	R36	80.5261	10 KΩ 5%
	R37	80.5278	0.27 MΩ 5%
	R38	86.5044	25 KΩ 20% potentiometer
	R39	89.5010	15 KΩ 2% NTC
	R40	80.5263	15 KΩ 5% carbon film
	R41	80.5266	27 KΩ 5%
	R42	80.5238	120 Ω 5%
	R43	80.5245	470 Ω 5%
	R44	80.5248	820 Ω 5%
	R45	80.5256	3.9 KΩ 5%
	R46	80.5269	47 KΩ 5%
	R47	80.5280	0.39 MΩ 5%
	R48	80.5261	10 KΩ 5%
	R49	80.5262	12 KΩ 5%
	R50	80.5266	27 KΩ 5%
	R51	80.5266	27 KΩ 5%
	R52	80.5266	27 KΩ 5%
	R53	80.5252	1.8 KΩ
	R54	80.5243	330 Ω 5%
	R55	80.5258	5.6 KΩ 5%
	R56	80.5263	15 KΩ 5%
	R57	80.5240	180 Ω 5%
	R58	80.5254	2.7 KΩ 5%
	R59	80.5274	120 KΩ 5%
	R60	80.5259	6.8 KΩ 5%

TYPE	NO.	CODE	DATA
	R61	80.5249	1 KΩ 5% carbon film
	R62	89.5046	50Ω PTC
	R63	80.5246	560 Ω 5%
	R64	86.5068	1 KΩ 20% potentiometer
	R65	80.5264	18 KΩ 5% carbon film
	R66	80.5272	82 KΩ 5%
	R67	80.5254	2.7 KΩ 5%
	R68	80.5262	12 KΩ 5%
	R69	80.5257	4.7 KΩ 5%
	R70	80.5258	5.6 KΩ 5%
	R71	80.5258	5.6 KΩ 5%
	R72	86.5039	10 KΩ 20% potentiometer
	R73	80.5272	82 KΩ 5% carbon film
	R74	80.5254	2.7 KΩ 5%
	R76	80.5261	10 KΩ 5%
	R80	80.5246	560 Ω 5%
	R81	80.5275	0.15 MΩ 5%
	R82	80.5267	33 KΩ 5%
	R83	86.5042	500 Ω 20% potentiometer
	R84	80.5238	120 Ω 5% carbon film
	R85	80.5254	2.7 KΩ 5%
	R86	80.5238	120 Ω 5%
	R87	80.5240	180 Ω 5%
	R88	80.5269	47 KΩ 5%
	R89	80.5269	47 KΩ 5%
	R90	80.5261	10 KΩ 5%
	R91	80.5273	0.1 MΩ 5%
	R92	80.5258	5.6 KΩ 5%
	R93	80.5249	1 KΩ 5%
	R94	80.5249	1 KΩ 5%
	R95	80.5256	3.9 KΩ 5%
	R96	80.5233	47 Ω 5%
	R97	80.5251	1.5 KΩ 5%
	R98	80.5250	1.2 KΩ 5%
	R99	86.5043	2.5 KΩ 20% potentiometer
	R100	80.5254	2.7 KΩ 5% carbon film
	R101	80.5259	6.8 KΩ 5%
	R102	80.5253	2.2 KΩ 5%
	R103	80.5253	2.2 KΩ 5%
	R104	80.5225	10 Ω 5%
	R105	80.5242	270 Ω 5%
	R106	80.5253	2.2 KΩ 5%

COMMON FUNCTIONS UNIT CF702

X 401.868

TYPE	NO.	CODE	DATA
	R107	80.5242	270 Ω 5% carbon film
	R108	80.5213	1 Ω 5%
	R109	80.5213	1 Ω 5%
	R110	80.5213	1 Ω 5%
	R111	80.5213	1 Ω 5%
	R112	80.5246	560 Ω 5%
	R113	80.5254	2.7 KΩ 5%
	R114	89.5062	22 KΩ 1% metal film
	R115	89.5062	22 KΩ 1% metal film
	R116	80.5277	0.22 MΩ 5% carbon film
	R117	80.5259	6.8 KΩ 5%
	R118	80.5263	15 KΩ 5%
	R119	89.5062	22 KΩ 1% metal film
	R120	89.5062	22 KΩ 1% metal film
	R121	89.5062	22 KΩ 1% metal film
	R122	80.5251	1.5 KΩ 5% carbon film
	R123	89.5061	68 Ω 20% NTC
	R124	86.5053	10 KΩ 20% potentiometer
	R126	80.5229	22 Ω 5% carbon film
	R127	84.5224	82 Ω 5% wire wound
	R128	80.5238	120 Ω 5% carbon film
	R129	80.5443	330 Ω 5%
	R130	80.5238	120 Ω 5%
	R131	80.5251	1.5 KΩ 5%
	R132	80.5251	1.5 KΩ 5%
	R133	86.5038	500 KΩ 20% potentiometer
	R134	80.5273	100 KΩ 5% carbon film
	L1	61.1131	IF coil 455 kHz
	L2	61.1132	Coil 75 mH
	L3	60.5158	Choke
	T1	61.1130	IF Transformer 455 kHz
	T2	61.1130	IF Transformer 455 kHz
	E1	99.5210	Zenerdiode 3.3 V 5%
	E3	99.5237	1N4148 Diode
	E4	99.5237	1N4148 Diode
	E5	99.5209	Stab. diode 1.5 V
	E6	99.5209	Stab. diode 1.5 V
	E7	99.5209	Stab. diode 1.5 V
	E8	99.5224	Zenerdiode 4.7 V 5%
	E9	99.5237	1N4148 Diode
	E10	99.5237	1N4148 Diode
	E11	99.5237	1 N4148 Diode
	E12	99.5224	Zenerdiode 4.7 V 5%
	E13	99.5249	Zenerdiode BZY93/C20R
	E14	99.5209	Stab. diode 1.5 V
	E15		

TYPE	NO.	CODE	DATA
	E15	99.5237	1N4148 Diode
	E16	99.5209	Stab. diode 1.5 V
	E17	99.5209	Stab. diode 1.5 V
	Q1	99.5166	BF167 Transistor
	Q2	99.5166	BF167 Transistor
	Q3	99.5143	BC108 Transistor
	Q4	99.5143	BC108 Transistor
	Q5	99.5247	2N4302 Transistor FET
	Q6	99.5143	BC108 Transistor
	Q7	99.5143	BC108 Transistor
	Q8	99.5143	BC108 Transistor
	Q9	99.5115	BC179 Transistor
	Q10	99.5115	BC179 Transistor
	Q11	99.5143	BC108 Transistor
	Q12	99.5246	TIP 31 Transistor
	Q13	99.5144-01	BC214L Transistor
	Q14	99.5243	BC108 Transistor
	Q15	99.5243	BC108 Transistor
	Q16	99.5246	TIP 31 Transistor
	Q17	99.5144-01	BC214L Transistor
	Q18	99.5143	BC108 Transistor
	Q19	99.5143	BC108 Transistor
	Q20	99.5201	BC109 Transistor
	Q21	99.5201	BC109 Transistor
	Q22	99.5115	BC179 Transistor
	Q23	99.5143	BC108 Transistor
	Q24	99.5143	BC108 Transistor
	Q25	99.5143	BC108 Transistor
	Q26	99.5115	BC179 Transistor
	Q27	99.5236	BD136 Transistor
	Q28	99.5235	BD135 Transistor
	Q29	99.5248	SP2629 Transistor
	Q30	99.5235	BD135 Transistor
	IC1	14.5010	IF ampl./discr.
	IC2	14.5006	MC1437P dual OP amp.

COMMON FUNCTIONS UNIT CF702

X 401.868

COMMON FUNCTION UNIT

CF703 - CF704

Description

The CF subunit contains all circuitry for the CQM700 radiotelephone that is not dependent upon frequency or channel separation.

CF703 is designed for simplex operation and CF704 for duplex.

The unit includes the following functions:

- a 455 kHz intermediate frequency amplifier and discriminator.
- two 9 V voltage regulators and keying circuitry.
- an audio output amplifier.
- a de-emphasis network and an audio frequency preamplifier, including an electronic squelching circuit.
- a squelch circuit
- a modulation amplifier.

The CF subunit is constructed on two printed circuit boards mounted in a sandwich assembly. The two p. c. boards are held in place with spacers, a small sewn cable taking care of the internal connections. The conductive sides of the p. c. boards face outwards, with the board containing the IF, the AF output amplifier, and the voltage regulators fastened to the chassis. External connections to the CF subunit are all solder connection with the exception of the battery connection, which is through a plug.

Operating Principle

To aid heat dissipation, the integrated AF output amplifier and the series regulator transistors in the voltage regulators on the lower board all have good thermal contact to the chassis.

The 455 kHz signal from IC700 passes through the IF stages to the integrated circuit discriminator, IC3. From there the audio signal divides between the squelch circuit input and the de-emphasis filter at the input to the audio preamplifier.

The squelch circuit opens and closes the signal path through the preamplifier according to the noise content in the demodulated signal. Also, control voltages for use with tone equipment are obtained from the squelch circuit.

The audio signal is taken from the 600 Ω output of the preamplifier to the AF output amplifier. When transmitting in the simplex mode (CF703), the signal path through the output amplifier becomes automatically blocked. The tone equipment can also block the signal path here.

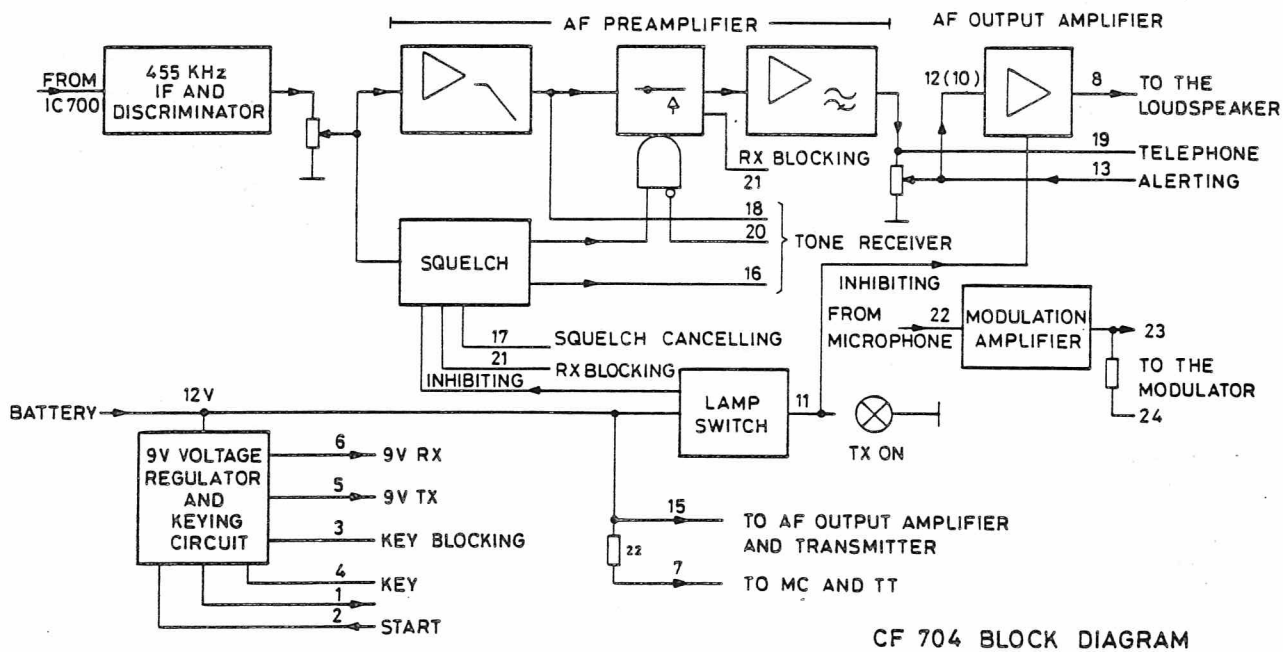
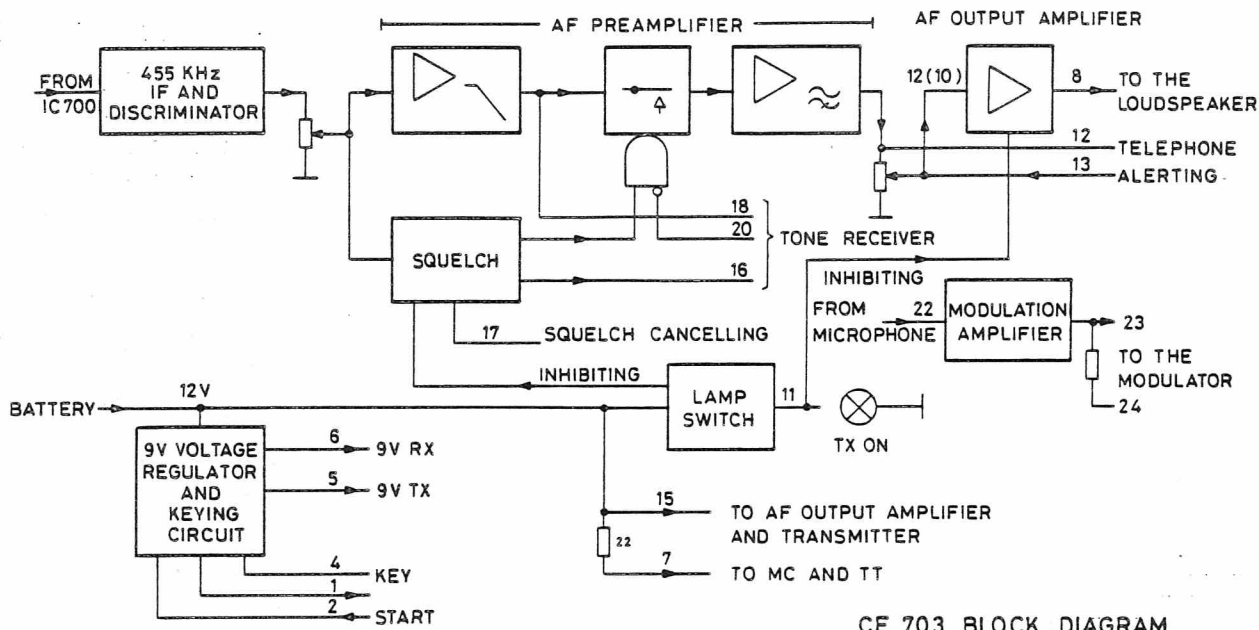
The signal from the microphone is amplified and limited in the modulation amplifier, which is designed around a dual, integrated operational amplifier. Both amplifiers, IC1a and IC1b, are contained in the same housing.

To avoid adjacent channel interference, the high-frequency component of the modulating signal is filtered out and the signal is also amplitude limited in order to keep the carrier frequency deviation within the established maximum excursions for whichever channel separation is employed.

As mentioned previously, the CF subunit also contains two voltage regulators; one supplies the receiver section and the other the transmitter. The AF output amplifier and the PA stage are supplied directly from the battery and are therefore unregulated.

Switching between transmit and receive is accomplished without relays. In CF703 the transmitter key electronically switches one or the other of the voltage regulators on so that both do not function at the same time. Terminal 4 is grounded during transmission and otherwise floats when the key is not activated.

Likewise, in the case of CF704, switching between the duplex and the receive conditions is accomplished without relays. Whenever the equipment is turned on the 9 V RX voltage regulator will always be on.



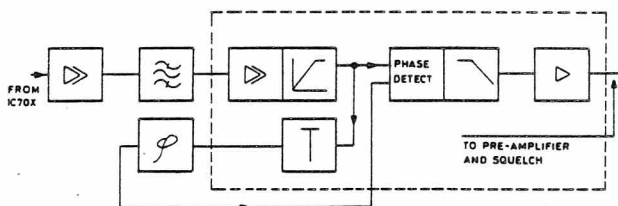
The 12 V supply voltage to the AF output amplifier and the TX power amplifier is always on whenever the on/off switch is turned on. Therefore the TX lamp switch circuit is designed to inhibit the audio preamplifier and audio output amplifier when the transmitter is keyed. This is a precaution against any transients in the squelch circuit that might be able to open the receiver output during transmission.

As explained, the receiver section in duplex equipment (CF704) is always on whenever the power is applied to the set.

455 kHz IF Amplifier and Discriminator

This circuit amplifies, selects, limits, and detects the receiver's second IF signal of 455 kHz, allowing a deviation of up to ± 15 kHz from centre frequency.

The amplifier has five stages; the first two, Q30 and Q31, are made up of discrete components while the last three are a part of the integrated circuit, IC3, along with the phase detector.



The only resonant circuits employed in the 2nd IF stage are those between the collector of Q31 and the input to IC3. Resistors R111 and R114 load T1 and T2 enough to achieve sufficiently broad bandwidth.

Inductive coupling between circuits is less than critical, R113 in the coupling link determining the coupling factor. Q31 operates with its collector-emitter voltage held low to prevent over-driving IC3.

The three amplifier stages in IC3 are differential amplifiers, which configuration approaches ideal symmetrical limiting. The stages are DC coupled and stability is assured through strong negative feedback. Capacitor C53 eliminates the feedback as far as AC voltages are concerned.

Via an emitter follower within the IC housing, the signal is fed to the phase detector. The IF signal, with its amplitude peaks clipped, is applied directly to one of the phase detector inputs.

The other input is fed the same signal, attenuated and approximately 90° out of phase (at f_0). Phase shift is accomplished with discrete components: C50, C51, L2 and R115. The following diagram shows the detector circuit schematic and the amplitude and phase characteristics of the phase shifting network. A graph of the detector current and voltage relationships is also included here.

The phase detector is designed around three differential amplifiers, all supplied through a constant-current source. In addition to the components shown in the detector schematic, IC3 also contains an emitter follower after the detector output, another emitter follower between the phase shifting network and one of the detector inputs, and various biasing networks.

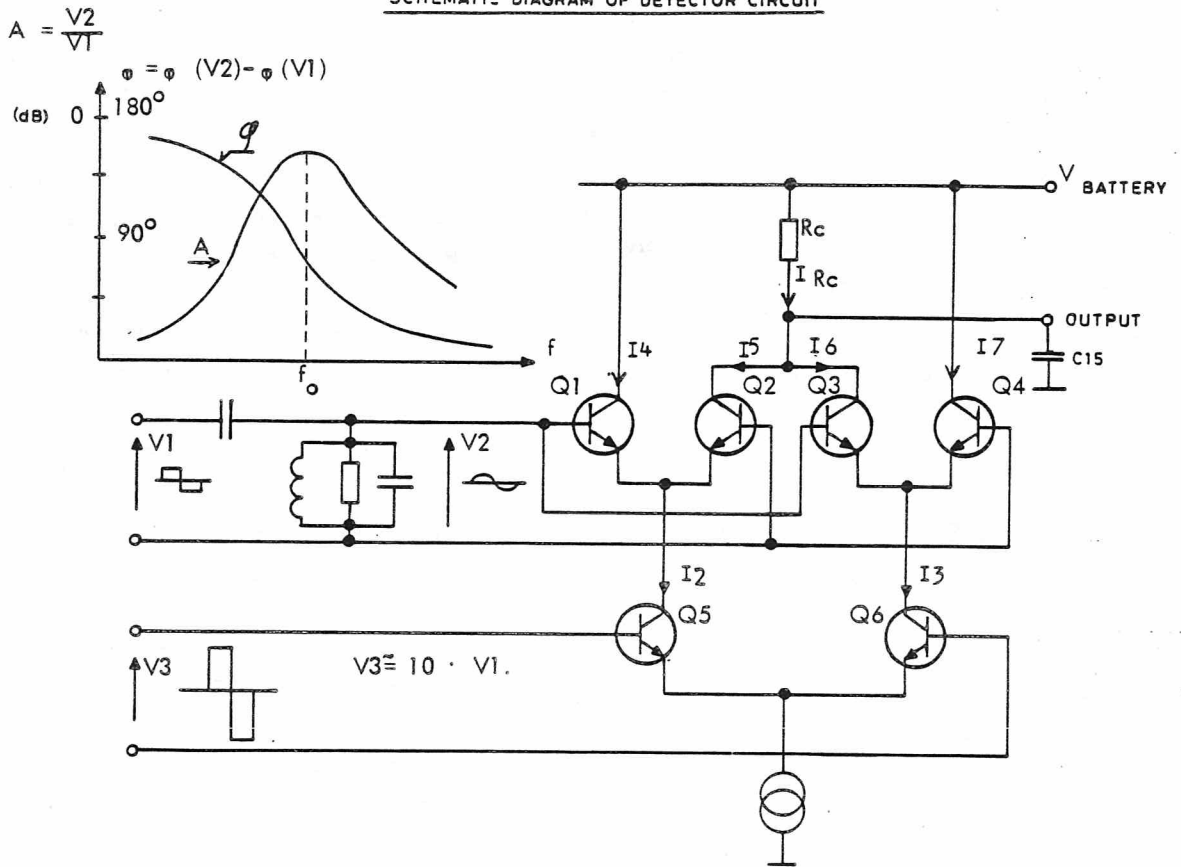
As long as voltage V2 is high enough to drive the two differential stages - Q1 + Q2, and Q3 + Q4 - as switches, the collector current pulses, I5 and I6, will appear as a constant amplitude value and the average value of current through R_C remains independent of the amplitude of the input voltage.

As seen on the schematic, current pulses through R_C only appear when V2 and V3 are of opposite polarities and I5 appears only when V3 is positive while I6 appears when V3 is negative. Supposing that $f > f_0$, then the difference in phase (V2 - V1) is reduced (the V2 pulse a little to the right in relation to V3), causing the width of current pulses I5 and I6 to decrease. In other words, the average current through R_C will decrease. When $f < f_0$, the opposite will occur.

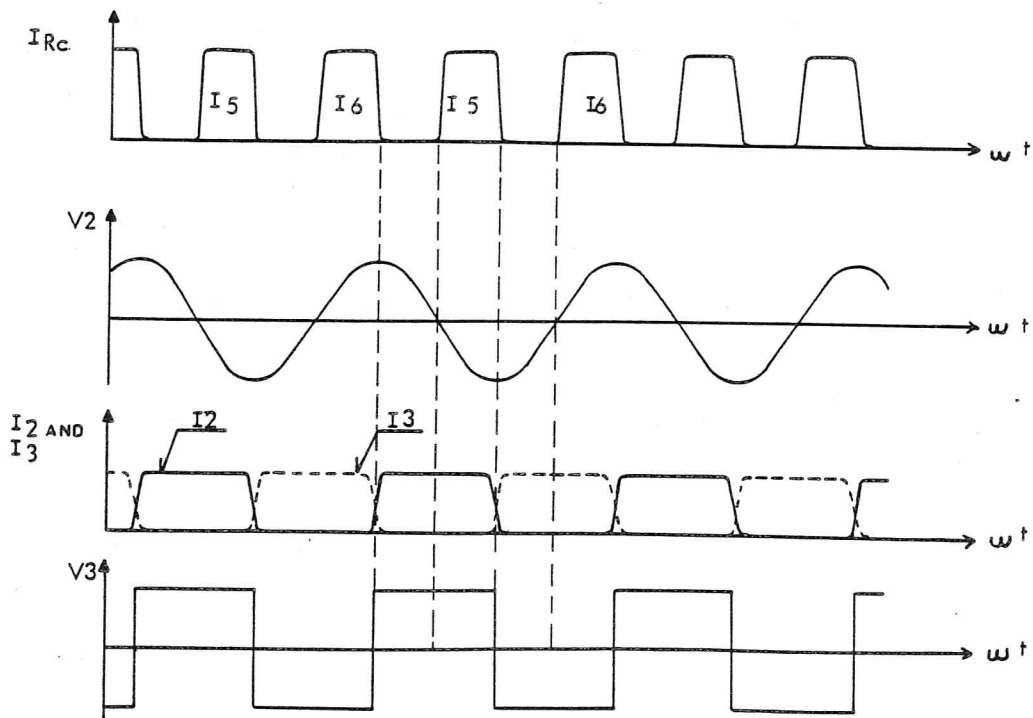
The width of I5 and I6 is therefore seen to be a measurement of the phase difference between V2 and V3. By integrating the output voltage (via R_C and C54) a voltage that is directly proportional to the phase shift is obtained.

Making use of both the negative and positive excursions of the signals, as in the detector con-

SCHEMATIC DIAGRAM OF DETECTOR CIRCUIT



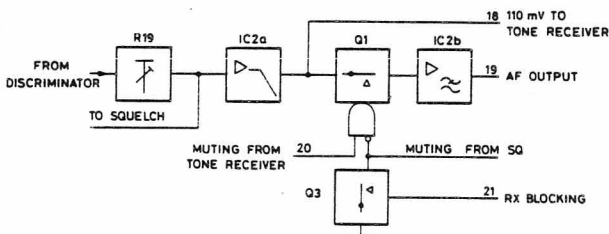
GRAPH OF VOLTAGE AND CURRENT RELATIONSHIPS IN THE PHASE DETECTOR WHEN $f = f_0$



figuration employed here, gives excellent suppression of noise and other undesired effects of inherent nonsymmetry in the clipped IF signal. For example, if the positive going half of V3 is wider than the negative half, I6 will be narrower and I5 wider with the result that the average current through R_C will remain unchanged.

An "S" curve similar to those known from conventional FM detectors will be present at the output (directly on pin 1 of IC3). However, the midpoint of this "S" curve will be around 3.5 V instead of 0 V. Circuit Q is designed low enough to enable the detector to handle frequency deviations of up to ± 15 kHz.

The De-emphasis Filter, AF Preamp and Electronic Squelching Switch



Network R14/C12 and IC2a take care of de-emphasizing the demodulated signal at the rate of 6 dB/octave and the required gain of 15 dB at 1000 Hz.

The integrated preamplifier, IC2, amplifies the AF signal and match it to the nominal 600 Ω load. In addition Q1 is inserted between IC2a and IC2b. Transistor Q1 operates as an electronic switch, interrupting the signal path on command from the squelch circuit.

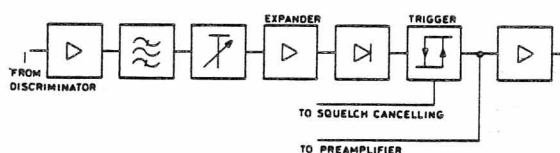
CF704 includes an additional transistor, Q3. With a d. c. potential of ≥ 2.5 V at terminal 21 (RX Blocking)- Q3 will be driven on, turning the AF switch, Q1, off. With the base of Q2 held at ground by Q3, the condition of the squelch circuit will have no effect on the preamplifier. Potentiometer R19 adjusts the level to the preamplifier, and to the squelch as well.

The second half of the integrated amplifier, IC2b, and C14 - C15 - R29 - R28 constitute a filter, which strongly attenuates low frequencies (< 250 Hz).

R32 - C 16 introduce a suitable roll-off at high frequencies (> 6 kHz). Preamplifier IC2b is, like IC2a, biased via R28.

The signal path between the first and second amplifier stages is through a transistor, which acts like a switch controlled by both the squelch and the tone receiver.

The Squelch



The squelch circuit opens and closes the audio signal path through the AF preamplifier according to the noise content of the incoming signal. The squelch circuit also provides a signal voltage for use in tone signalling.

An internal adjustment, potentiometer R46, is provided for setting the squelch level. The squelch function can be cancelled altogether by grounding terminal 17 via the squelch cancelling button on the control panel.

The squelch section includes a frequency selective noise amplifier, Q4 - Q5, an expander stage, Q6, a noise detector, a Schmitt trigger, Q7 and Q8, and an emitter follower amplifier, Q9.

The operating principle is as follows:

Some of the AF signal from the discriminator is fed to the noise amplifier whose collector load is made up of a parallel resonant circuit tuned to approximately 7 kHz. The selected noise is then fed to Q6 which is biased in such a way that only positive going pulses of a certain minimum amplitude cause the transistor to conduct. Since only pulses of a certain amplitude can become amplified, the result is that a given relative change in noise amplitude at the base of Q6 appears as a larger relative change at the collector. The noise pulses are then rectified and filtered to a d. c. potential that, in turn, controls the Schmitt trig-

ger, Q7 and Q8. The collector voltage on Q8 is used partly to drive the emitter follower, Q9, and partly to switch the transistor, Q1, in the AF preamplifier.

Where CF703 is used, keying the transmitter also interrupts the power to the receiver. At the same time, diodes E7 and E8 in the squelch are grounded through Q28 to prevent any false signals that might appear in the squelch circuitry from affecting the AF amplifier or Q9 during this condition.

This does not apply to CF704.

The 9 V Voltage Regulators and Keying Circuits

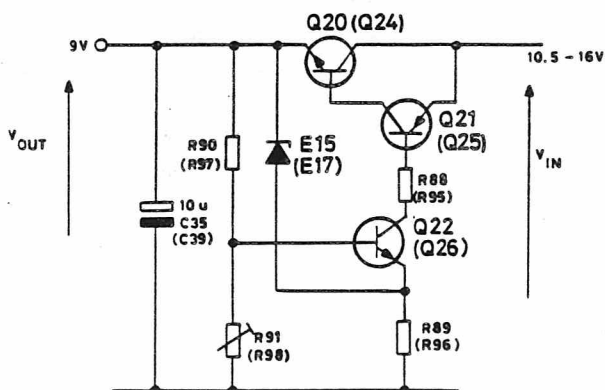
The two 9 V voltage regulators supply the receiver and the transmitter sections, respectively. They are intended for use with a 12 V storage battery.

The battery connects to the regulators through the start relay switches.

To protect the equipment against incorrect battery polarity a diode, E9, is placed in series with the start relay. If the power supply is connected wrong the diode will not conduct and the start relay thus refuses to operate.

The voltage regulators are protected against short circuits; with shorted output the current through Q20 will be less than 0.5 A and through Q24 less than 0.1 A. The power series transistors are mechanical mounted so as to be in good thermal contact with the chassis.

The two regulators are principally identical as shown on the simplified diagram as follows:



Q20 is driven by Q21, which is controlled by amplifier Q22. Transistor Q22 compares the zener reference voltage across E15 with a portion of the output voltage through dividing resistors R90 and R91. R91 sets the output voltage.

The operating principle is as follows:

If V_{out} drops (due to a decrease in input voltage or an increase in load current), V_{BE} for Q22 will increase, also increasing base current for Q21 and Q20. When base current to Q20 increases, more current flows through the output load, cancelling the original drop in output voltage.

If the load current increases to a certain value, Q22 goes into saturation. If the load current increases still more, the zener diode will act as an open circuit and V_{BE} for Q22 decreases whereby base current for Q22, Q21, and Q20 decreases, too. Finally, Q22 will be cut off and base current in Q20 and Q21 will be zero. Thus is Q20 protected against destruction by short circuits at its output. Resistors R88 - and R89 - determine the saturation current through Q22 and, of course, the short circuit current.

A regulator built exactly like the simplified diagram would not be self-starting, however. Therefore, the regulators in the CF703 are provided with starting circuits; 9 V RX employs R82, R83, and E13 in its starting circuit and 9 V TX employs R92 and E16. Since 9 V RX and 9 V TX must not operate simultaneously, the regulators are also mutually coupled through a keying circuit that blocks, or cuts off, one regulator while allowing the other to operate. This function is controlled via terminal 4.

CF704 is arranged in a slightly different manner since 9 V RX must always operate when the equipment is turned on. While the 9 V RX and 9 V TX regulators employ the same starting circuit as just explained for CF703, the difference here is that keying the transmitter (which grounds terminal 4) does not turn the CF704 9 V RX regulator off.

Operation of Keying and Starting Circuits

For CF703:

When terminal 4 is floating and the power is turned on, 9 V RX will build up voltage since Q20

gets base current through R82, R83, and E13. When 9 V RX reaches its final value the starting circuit will have no effect on the regulator because diode E13 will then be nonconducting (the unloaded voltage at terminal 4 is approx. 8.1 V at nominal battery voltage).

Transistors Q23 and Q27 are both heavily saturated, so the 9 V RX regulator will operate undisturbed while 9 V TX will be blocked because Q26 is completely cut off by Q27.

Grounding terminal 4 immediately cuts off Q23 and Q27. 9 V RX falls towards 0 V as there is now no base current to Q21. 9 V RX falls off at a rate determined by the time constant of C35 and the load on terminal 6. Under all operating conditions within factory specifications for the radiotelephone, the time constant will easily be long enough that the current through starting circuit R92 and E16 can turn on Q26, whereby a voltage builds up on 9 V TX that finally reaches a level where diode E16 becomes nonconducting.

Diode E12 and resistor R87 ensures that keying the transmitter cuts off base current to Q21 effectively, even at high temperatures. Diode E11 ensures effective keying even if terminal 4 is not brought all the way down to 0 V potential.

Note that 9 V TX cannot begin to build up a voltage by itself after a short circuit. Since - as just explained - it is 9 V RX that starts 9 V TX, it is necessary to activate the transmitter key again.

For CF704:

When terminal 4 is floating and the power is turned on, 9 V RX will build up voltage since Q20 gets base current through R82, R83, and E13. When 9 V RX reaches its final value the starting circuit will have no effect on the regulator because diode E13 will then be nonconducting (the unloaded voltage at terminal 4 is approx. 7.0 V at nominal battery voltage).

When the transmit key grounds terminal 4, two things happen:

1. Q27 loses its forward bias and immediately cuts off. Now, instead of acting as a short circuit between the base of Q26 and ground,

Q27 can now be considered a large resistance.

2. C36, which has been charging through diode E14, has accumulated a charge of about 6.4 V. With terminal 4 grounded the charge on C36 reverse biases E14. Now C36 will discharge.

There are two discharge paths available to C36, one through the bleeder resistor, R94, and one through R93 and E16 to the base of Q26. Remember that the base of Q26 is no longer grounded.

The discharge current to the base of Q26 drives this transistor on. Once Q26 turns on its base assumes a potential of approx. 4.6 V. By now C36 has discharged so much that E16 becomes reverse biased by the 5.1 V on the base of Q26, and C36 continues to discharge through its other path (R94).

As long as terminal 4 is kept at chassis potential by the transmit key the 9 V TX regulator continues to operate.

When the key is released and terminal 4 resumes its unloaded potential of approx. 7.0 V, Q27 is driven on and short circuits the base of Q26 again. The 9 V TX regulator then turns off.

C36 charges again through E14.

Diode E11 ensures effective keying even if terminal 4 is not brought all the way down to 0 V potential.

Note that 9 V TX cannot begin to build up a voltage by itself after a short circuit but must be started again by keying the transmitter.

The operations described above presume the key blocking terminal to be at approx. 0 V potential.

The TX Lamp Switch

The TX lamp switch supplies 12 V to the transmit lamp, when transmitting, and also submit inhibit voltages to the squelch (CF703 only) and to the AF output amplifier. The lamp switch includes Q28/Q29 and is controlled by 9 V TX.

The AF Output Amplifier

The output amplifier amplifies the audio signal from the preamplifier and powers the loudspeaker.

The amplifier is built around an integrated AF power module mounted on stand-offs, which are fastened to the chassis and act as heat sink. The amplification factor is determined by a suitable amount of feedback. In order to compensate variations in gain the internal feedback resistor (approx. 4 k Ω) is shunted by R127. Besides the normal input, the amplifier has an input for an Alerting tone from the tone receiver, when called. As the Alerting tone is to be heard from the loudspeaker when the volume control is turned down an isolating resistor, R120 is inserted.

In order to provide, optionally, a remote control for a locally controlled equipment, resistor R119 is serving to separate the two volume controls. Also note that the amplifier inputs (terminal 10 or 12) must have a d. c. path to chassis in order to bias the amplifier properly. C60/R125 increase the maximum achievable output power (bootstrapping) and C58/C59 together with R126/C23 constitute the frequency compensation.

Supply voltage ripple is suppressed by C57, and R117/R118 reduce the current spike through the start relay switches when the equipment is turned on.

During transmit the amplifier is totally inhibited via Q32.

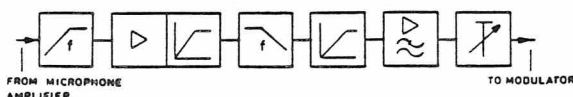
The Modulation Amplifier

General

The modulation amplifier differentiates, amplifies, limits and integrates the microphone signal. It also suppresses undesired high frequencies with an active filter designed for either 20, 25 or 50 kHz channel separation or, with a few resistor values changed, 12.5 kHz channel spacing.

Both amplifiers are contained in a single integrated circuit made up of dual operational amplifiers. The modulation amplifier contains additional passive differentiation and integrating circuits as well as diode clippers to prevent overmodulation.

The following block diagram shows the operating principle for the amplifier:



Input

The input circuit, which is also the collector return for the microphone amplifier output stage through resistor R2, is asymmetric.

The Differentiating Circuit

The differentiation network is made up of C1 and R3 (the input impedance of the operational amplifier is negligible due to the feedback through R8).

It differentiates at the rate of +6 dB pr. octave over the entire audio range of 300 - 3000 Hz.

The AF Amplifier - Clipper

The gain of the first amplifier stage, IC1a, is determined by the amount of feedback introduced.

Clipping action begins as soon as the amplifier is driven to where the collector excursions approximate the battery voltage. This level will be about 6.5 V peak-to-peak. The amplifier can be driven up to 25 dB above its nominal input level. Symmetry of the clipping is determined by bias network R6 and R7 and therefore is fixed.

The Integration Circuit

Integrating takes place from 150 Hz at -6 dB pr. octave. The passive integrating network consists of R11 and C4. The lower limit for integration is determined solely by these two components as the previous amplifier's feedback makes its output impedance negligible, and because the loading of the network by the filter that follows is very light as long as the signal remains below the frequency limit of that filter.

The 2nd Clipper (or Phase Clipper)

This extra clipper is inserted to prevent strong input signals at low frequencies from overdriving the modulator stage. For signal levels corresponding to the nominal frequency swing, the clipper has no effect. Two 1.5 V diodes and capacitor C3 make up this circuit.

The Splatter Filter

The purpose of this filter is to cut off frequencies that lie above the voice range in order to avoid undesirable sideband noise. It is an active filter consisting of the second operational amplifier and its associated components. Its response approaches that of a Chebishev filter. The circuit arrangement is the so-called voltage follower, where the voltage gain is very near unity (1).

The filter cannot be overdriven because the input signal level is subject to limiting by the diode clipper.

Adjusting the Frequency Swing

The amount of signal to the modulator input, and thus the frequency swing, is set by the voltage divider formed by R18 and the input impedance of the modulator. If the frequency swing cannot be reduced sufficiently an additional resistor can be inserted by using terminal 24 instead of terminal 23.

TECHNICAL SPECIFICATIONS

Nominal Supply Voltage

13.6 V

Current Drain for CF703

(at nominal supply voltage)

Transmit: 22 mA

Receive : 100 mA

Current Drain for CF704

(at nominal supply voltage)

Transmit: 120 mA

Receive : 100 mA

12 dB SINAD Sensitivity

(where 1.75 kHz deviation of the 455 kHz IF results in a 1 kHz audio signal)

1.2 μ V input signal at antenna termination

AF Line Out (terminal 18)

-17 dBm/600 Ω (110 mV)

AF Telephone Output (terminal 16)

90 mV

Regulated Voltages

Receiver (terminal 6): 9 V

Transmitter (terminal 5): 9 V

Unregulated Voltages

AF output amplifier: 13.6 V

PA stage (terminal 15): 13.6 V

Tone transmitter and
microphone (terminal 7): 13.6 V

AF Output Power (terminal 8)

3 W

Modulation Amplifier Sensitivity

(for normal frequency swing of 1 kHz)

110 mV +1/-3 dB

TX Inhibit CF704

Voltage/current: \geq 6 V/2 mA

RX Inhibit CF703

Voltage/current: \geq 2.5 V/0.1 mA

Temperature Range

Working range: -25 $^{\circ}$ C - +60 $^{\circ}$ C

Function range: -30 $^{\circ}$ C - +75 $^{\circ}$ C

The following, more detailed specifications for the several CF703 and CF704 functions are all typical values measured at 25 $^{\circ}$ C ambient temperature, unless otherwise stated.

455 kHz IF Amplifier and DiscriminatorCurrent Drain (at nominal 9 V supply)

18 mA

Maximum Frequency Deviation ± 15 kHzIF Bandwidth (3 dB attenuation) ± 17 kHzInput Impedance1 k Ω // 15 pFGain

from input (terminal 1) to pin 4 of IC3: 55 dB

from IC3 input (pin 4) to IC3 amplifier

high output, pin 10: 55 dB

Discriminator Conversion Efficiency

50 mV / kHz

AF Output Voltage ($f_m = 1$ kHz, $\Delta f = 3.5$ kHz)

110 mV

Measured at test point 2, terminated with 2.2 k Ω load.Discriminator Linearity (relative to 1000 Hz)

Pass-Band 100 - 3500 Hz: +0/-1 dB

Measured at test point 2, terminated with 2.2 k Ω load.Discriminator Output Resistance200 Ω Minimum Load Resistance2 k Ω Harmonic Distortion $\Delta f = 15$ kHz : 4.5% $\Delta f = 3.5$ kHz : 1.0%AF PREAMPLIFIER and SQUELCH-CONTROLLED SWITCHCurrent Drain (at nominal 9 V supply)

1.5 mA

Input Impedance (at 1 kHz)2.2 k Ω Output Impedance $R_{OUT} = \sim 0 \Omega$ Gain (gain control at highest setting) $R_L = 1.8$ k Ω , $f = 1$ kHz;

Tone output: 15 dB

Telephone output: 13 dB

Harmonic Distortion ($R_L = 1.8$ k Ω , $f = 1$ kHz) $V_{OUT} = 110$ mV (nominal): 0.2% $V_{OUT} = 500$ mV : 0.5%Required Turn-on Potential

(between R30 and R65)

To ensure normal signal path: ≥ 2.3 V

Terminal 20 must float.

Deemphasis Cut-off Frequency

60 Hz

Frequency Response at Tone Receiver Output

(relative to -6 dB/octave characteristic)

Pass -Band linearity (300 - 3000 Hz): +0/-1 dB

Frequency Response at Telephone Output

(relative to -6 dB/octave characteristic)

Pass-Band linearity (300 - 3000 Hz) : +0/-1.5 dB

100 Hz rel. to 1000 Hz : +6 dB

6 kHz rel. to 1000 Hz : -17 dB

SQUELCH CIRCUITCurrent Drain (at nominal 9 V supply)

16 mA

Measured with unloaded Squelch Signalling
(terminal 16)

Input Impedance15 k Ω Noise Filter Resonant Frequency

12.5 kHz channel spacing: 7.2 kHz
20/25 kHz " " : 7.2 kHz
(50 kHz " " : 10 kHz

Output VoltageSquelched condition: ≤ 100 mVUn-squelched condition: > 5.6 V

measured at Q8's collector.

Squelch Signalling (terminal 16) R_{LOAD} minimum = 680 Ω V_{OUT} (with $R_L = 680 \Omega$)Squelched condition: ≤ 100 mVUn-squelched condition: ≥ 4.0 V**AF OUTPUT AMPLIFIER**Nominal Supply Voltage

13.6 V

Operating Range

10.5 to 16 V

Current Drain (at nominal supply voltage)

no-signal condition: 12 mA

at 4 W output : 520 mA

inhibited : 6 mA

Output Power (at nominal supply voltage)

Maximum 4 W

Loudspeaker ImpedanceNominal/minimum: 4 Ω Input Impedance (at 1 kHz)100 k Ω Nominal Gain

32 dB (at 1 kHz)

Harmonic Distortion $P_{OUT} = 2$ W: 1% $P_{OUT} = 0.2$ W: 0.5%Frequency Response (relative to 1 kHz)

80 Hz -3 dB

300 Hz 0 dB

3000 Hz -0.5 dB

15 kHz -3 dB

Measured at 0.2 W output power.

Alerting Tone Input

Voltage gain: 3.5 dB

Input impedance: 100 k Ω **MODULATION AMPLIFIER**Current Drain, (at nominal 9 V supply)

7 mA

Input Impedance (at 1 kHz)540 Ω Limiting

Signal clipping begins to occur with an input
signal (1000 Hz) of: 110 mV

Output signal level observed at pin 2 of IC1
when clipping occurs: 7.0 V p.p.

Phase Limiting

Phase clipping level (at 300 Hz): 2.1 V p.p.

Measured immediately after the integration
network, with an input signal of 1.1 V (nominal
110 mV + 20 dB).

Output Voltage (1 kHz)

560 mV

Measured at modulation output (terminal 23) with potentiometer R18 fully up, and load impedance = 1 kΩ.
Input level = 110 mV.

Harmonic Distortion (at 1 kHz)

for 110 mV input signal: 0.8%

Frequency Response (relative to 1 kHz)

	Channel spacing	
	20/25/50 kHz	12.5 kHz
300 Hz	-1.5 dB	-1.5 dB
3 kHz	0 dB	-4 dB
6 kHz	-19 dB	-25 dB
10 kHz	-32 dB	-37 dB

Measured for 15 mV input signal, and with a resistive output load.

9 V VOLTAGE REGULATORS and KEYING CIRCUITS

Nominal Supply Voltage

13.6 V

Operating Range

10.5 V to 16 V

Regulated Output Voltages

Receiver supply 9 V RX: 9.0 V ± 0.2 V
Transmitter supply 9 V TX: 9.0 V ± 0.2 V

V_{REG} vs. Temperature

3.6 mV / pr. °C

Suppression of Δ V_{BATTERY} in V_{REG}

(at nominal load)

DC : 46 dB
1 kHz : 50 dB

Internal Resistance of Regulators

R_I = 0.5 Ω

Regulator Output Current

Maximum 250 mA

Maximum Load

on terminal 7 (MC-MT-TT) : 100 mA
on terminal 15 (PA) : 6 A
on terminal 11 (TX lamp) : 100 mA

Keying Termination

Maximum allowable resistance of wiring : 180 Ω
Alternatively, V_{MAX} at terminal 4 : 1.0 V

Regulator Switching Time

(V_{BATTERY} = 13.6 V)

9 V RX turn-on delay, t_{0 - 90%} : 0.4 ms
9 V RX turn-off delay, t_{100 - 10%} : 100 ms
9 V TX turn-on delay, t_{0 - 90%} : 0.1 ms
9 V TX turn-off delay, t_{100 - 10%} : 25 ms

Measured under normal load conditions.

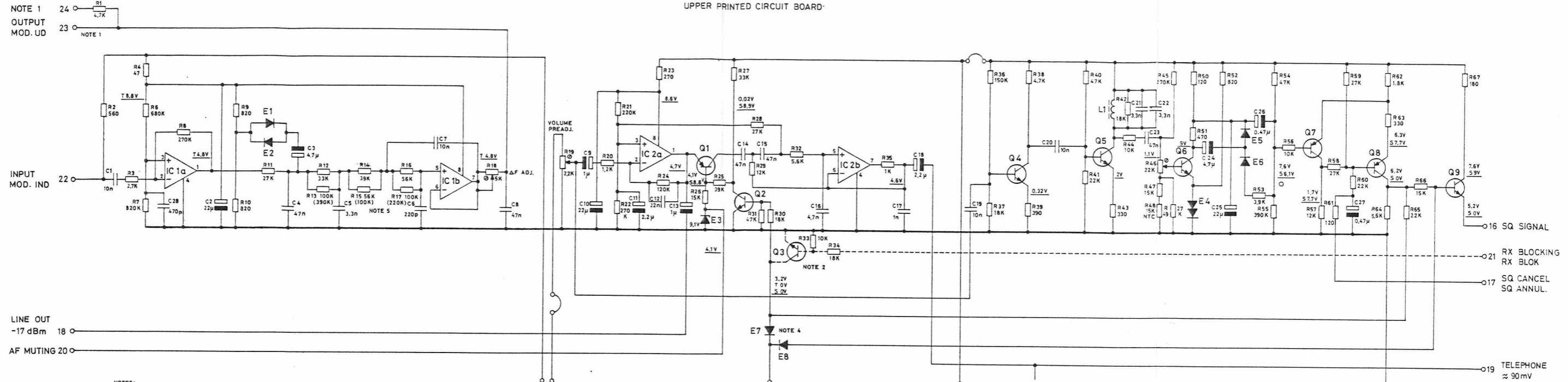
TX Inhibit (terminal 3)

Voltage/current : ≥ 6 V / 2 mA

MODULATION AMPLIFIER
MODULATIONSFORSTÆRKER

PREAMPLIFIER
FORSTÆRKER
UPPER PRINTED CIRCUIT BOARD

SQUELCH



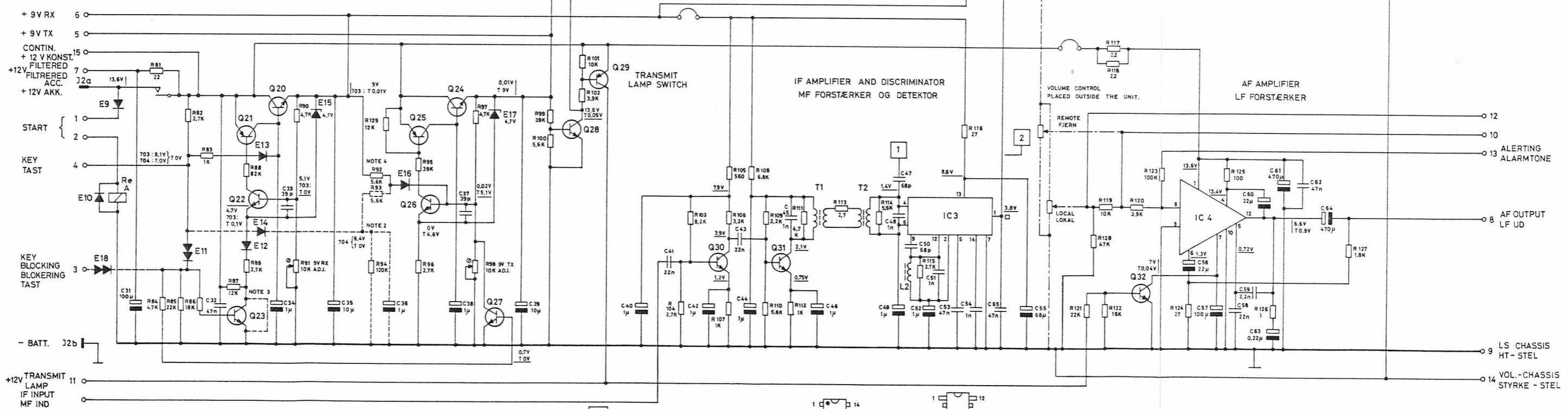
- NOTES:
- 1 : 23 IS NORMAL OUTPUT. IF A.F IS NOT ADJUSTABLE USE 24 AND REMOVE C8.
 - 2 : COMPONENTS SHOWN IN DOTTED LINE APPLY TO CF 704 ONLY.
 - 3 : REMOVE Q 23 IN 704 AND STRAP THE EMITTER - COLLECTOR TERMINALS.
 - 4 : CF 703 ONLY.
 - 5 : VALUES IN PARENTHESES ARE VALID FOR 12,5 KHZ EQUIPMENT AND SWEDISH EQUIPMENT ONLY.

- CONDITIONS OF MEASUREMENTS :
- T ~ TRANSMITTER KEYED CONDITION.
 - S ~ SQUELCHED CONDITION.
 - ~ USE A HIGH-RESISTANCE VOLTMETER (2 M.Ω)
 - ~ MEASURED AT ΔF = 0KHZ

RX VOLTAGE REGULATOR
SPÆNDINGSREGULATOR RX

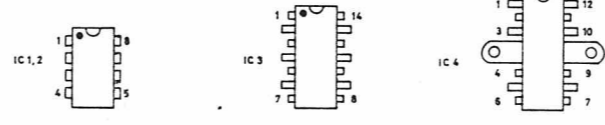
TX VOLTAGE REGULATOR
SPÆNDINGSREGULATOR TX

LOWER PRINTED CIRCUIT BOARD



- Q2,3,4,5,6,7,8
Q9,22,23,26,27
Q28,29,32

- Q1,21,25
Q30,31



COMMON FUNCTIONS
CF 703 / CF 704

TYPE	Nº	CODE	DATA
CF703 CF704	C1	10. 3364-00	Common Functions
	C2	10. 3499	Common Functions
	C3	76. 5070	10 nF 50 V
	C4	73. 5127	22 µF 16 V
	C5	73. 5126	4.7 µF 35 V
	C6	76. 5072	47 nF 50 V
	C7	76. 5060	3.3 nF 50 V
	C8	76. 5063	220 pF 160 V
	C9	76. 5070	10 nF 50 V
	C10	73. 5114	1 µF 35 V
	C11	73. 5127	22 µF 16 V
	C12	73. 5102	2.2 µF 35 V
	C13	76. 5071	22 nF 50 V
	C14	73. 5114	1 µF 35 V
	C15	76. 5072	47 nF 50 V
	C16	76. 5072	47 nF 50 V
	C17	76. 5061	4.7 nF 50 V
	C18	74. 5155	1 nF -20 + 80% ceram PL
	C19	73. 5102	2.2 µF 35 V
	C20	76. 5070	10 nF 50 V
	C21	76. 5070	10 nF 50 V
	C22	76. 5060	3.3 nF 50 V
	C23	76. 5072	3.3 nF 50 V
	C24	73. 5126	4.7 µF 50 V
	C25	73. 5127	22 µF 35 V
	C26	73. 5125	22 µF 16 V
	C27	73. 5125	0.47 µF 35 V
	C28	74. 5161	470 pF 35 V
	C31	73. 5071	100 µF 40 V
	C32	76. 5072	47 nF 50 V
CF704	C33	74. 5187	39 pF 25 V
	C34	73. 5114	1 µF 35 V
CF704	C35	73. 5011	10 µF 16 V
	C36	73. 5114	1 µF 35 V
	C37	74. 5187	39 pF 25 V
	C38	73. 5114	1 µF 35 V
	C39	73. 5011	10 µF 16 V
	C40	73. 5114	1 µF 35 V
	C41	76. 5071	22 nF 50 V
	C42	73. 5114	1 µF 35 V
	C43	76. 5071	22 nF 50 V
	C44	73. 5115	1 µF 35 V
	C45	76. 5067	1 nF 160 V
	C46	73. 5114	1 µF 35 V
C47	74. 5341	68 pF 63 V	
C48	76. 5067	1 nF 160 V	

TYPE	Nº	CODE	DATA
	C49	73. 5114	1 µF 20%
	C50	74. 5341	68 pF ceram
	C51	76. 5067	1 nF polystyr TB
	C52	73. 5114	1 µF 20%
	C53	76. 5072	47 nF 10% polyester FL
	C54	76. 5069	1 nF 10% polyester FL
	C55	73. 5106	68 µF 20% tantal
	C56	73. 5127	22 µF 20%
	C57	73. 5151	100 µF -10 + 50% elko
	C58	76. 5071	22 nF 10% polyester FL
	C59	76. 5059	2.2 nF 10% polyester FL
	C60	73. 5127	22 µF 20% tantal
	C61	73. 5138	470 µF -10 + 100% elko
	C62	76. 5072	47 nF 10% polyester FL
	C63	76. 5072	47 nF 10% polyester FL
	C64	73. 5137	470 µF -10 + 50% elko
	C65	76. 5072	47 nF 10% polyester FL
	R1	80. 5257	4.7 KΩ carbon film
	R2	80. 5246	560 Ω "
	R3	80. 5254	2.7 KΩ "
	R4	80. 5233	47 Ω "
	R6	80. 5283	680 KΩ carbon film
	R7	80. 5284	820 KΩ trim. carbon
	R8	80. 5280	390 KΩ carbon film
	R9	80. 5248	820 Ω "
	R10	80. 5248	820 Ω "
	R11	80. 5266	27 KΩ "
	R12	80. 5267	33 KΩ "
	R13	80. 5273	100 KΩ "
	R14	80. 5278	39 KΩ "
	R15	80. 5270	56 KΩ "
	R16	80. 5270	56 KΩ "
	R17	80. 5273	100 KΩ "
	R18	86. 5050	5 KΩ trim carbon
	R19	86. 5043	2.2 KΩ 20%
	R20	80. 5250	1.2 KΩ 5%
	R21	80. 5277	220 KΩ 5%
	R22	80. 5278	270 KΩ 5%
	R23	80. 5242	270 Ω 5%
	R24	80. 5242	270 Ω 5%

COMMON FUNCTIONS CF703, CF704

X402. 429/2

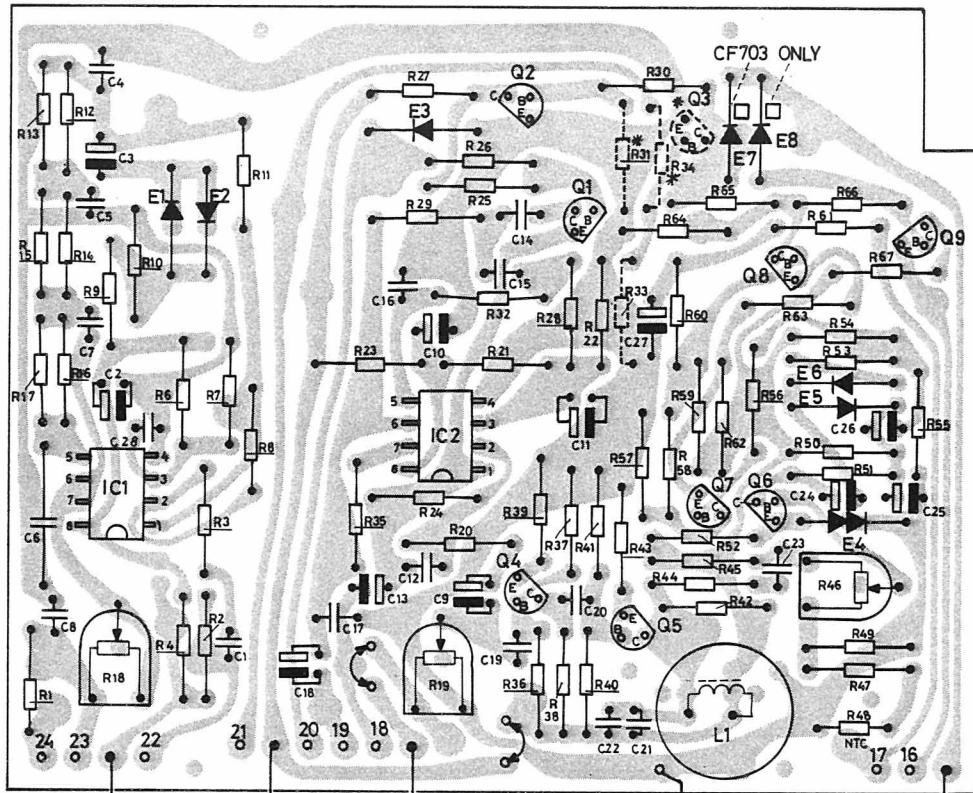
TYPE	Nº	CODE	DATA
	R124	80.5230	27 Ω
	R125	80.5237	100 Ω
	R126	80.5213	1 Ω
	R127	80.5252	1.8 KΩ
	L1	61.1132	Squelch coil 75 mH
	L2	61.1131	IA coil 455 kHz
	E1	99.5237	1 N 4148 Diode
	E2	99.5237	1 N 4148 "
	E3	99.5042	Zenerdiode 9.1 V 5%
	E4	99.5209	Stabilizerdiode 1.5 V
	E5	99.5237	1 N 4148 Diode
	E6	99.5237	1 N 4148 "
	E7	99.5237	1 N 4148 "
	E8	99.5237	1 N 4148 "
	E9	99.5020	1 N 4004 "
	E10	99.5237	1 N 4148 "
	E11	99.5209	Stabilizerdiode 1.5 V
	E12	99.5237	1 N 4148 Diode
	E13 E14	99.5237	1 N 4148 "
	E15	99.5224	Zenerdiode 4.7 V 5%
	E16	99.5237	1 N 4148 Diode
	E17	99.5224	Zenerdiode 4.7 V 5%
	E18	99.5209	1.5 V Stab. diode
	Q1	99.5144	Transistor
	Q2	99.5143	"
	Q3	99.5143	"
	Q4	99.5143	"
	Q5	99.5143	"
	Q6	99.5201	"
	Q7	99.5115	"
	Q8	99.5115	"
	Q9	99.5143	"
	Q20	99.5246	"
	Q21	99.5144	"
	Q22	99.5143	"
	Q23	99.5143	"
	Q24	99.5246	"
	Q25	99.5144	"
	Q26	99.5143	"
	Q27	99.5143	"
	Q28	99.5143	"
	Q29	99.5115	"
	Q30	99.5326	"
	Q31	99.5326	"
	Q32	99.5143	"
	T1	61.1130	IA transformer

CF704

TYPE	Nº	CODE	DATA
	T2	61.1130	IA transformer 455 kHz
	IC1	14.5105	MC1458 Dual OP-amp.
	IC2	14.5105	MC1458 Dual OP-amp.
	IC3	14.5010	IF Amplifier/Discr. ULN 2111 N
	IC4	14.5104	Audio Power Amplifier TBA 810 AS
	ReA	58.5084	Relay 330 Ω 12 V

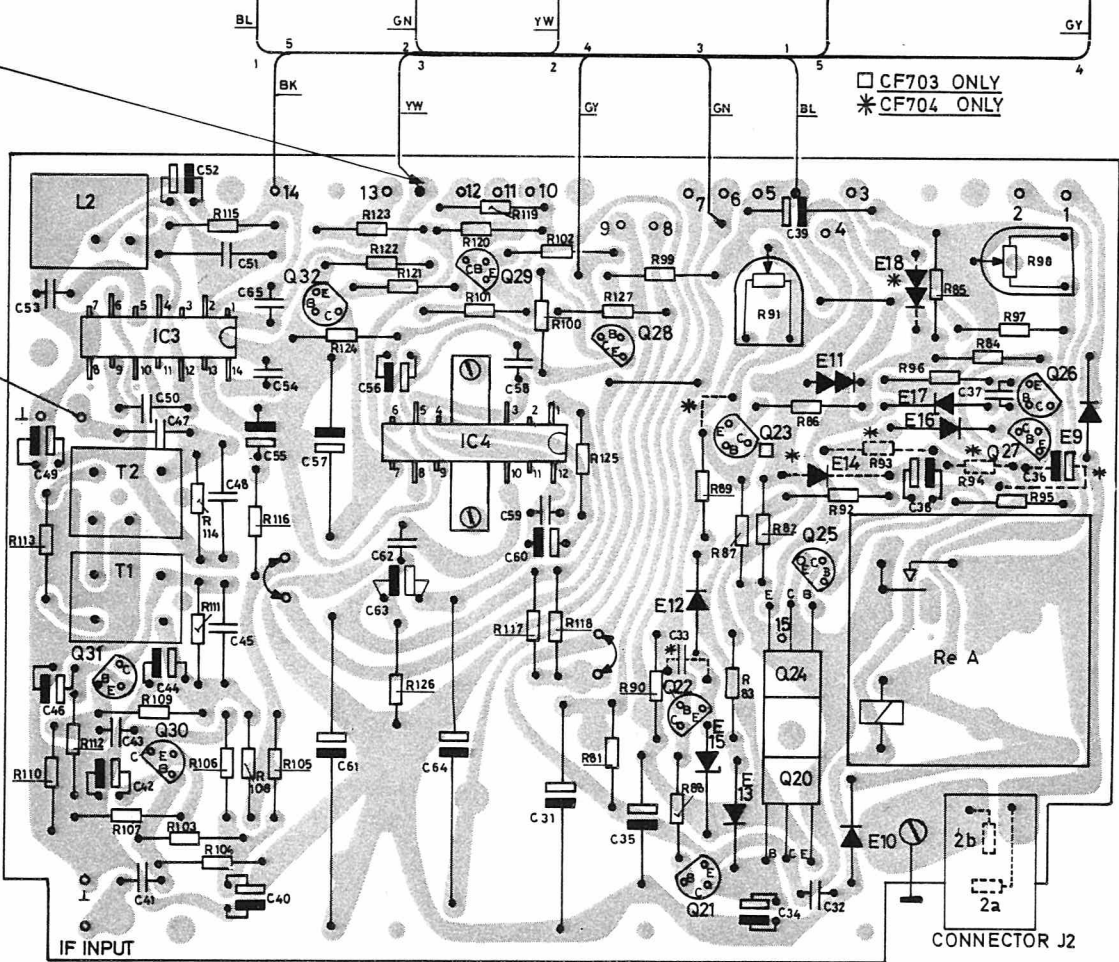
COMMON FUNCTIONS CF703, CF704

X 402.429/2



2

1



COMMON FUNCTIONS UNIT CF703, CF704

COMMON FUNCTIONS UNIT

CF705

Description

The CF subunit contains all circuitry for the CQM713 P3 radiotelephone that is not dependent upon frequency or channel separation.

The unit includes the following functions:

- a 455 kHz intermediate frequency amplifier and discriminator.
- two 9 V voltage regulators and keying circuitry.
- an audio output amplifier.
- a de-emphasis network and an audio frequency preamplifier, including an electronic squelching circuit.
- a squelch circuit.
- a modulation amplifier.

The CF subunit is constructed on two printed circuit boards mounted in a sandwich assembly. The two p. c. boards are held in place with spacers, a small sewn cable taking care of the internal connections. The conductive sides of the p. c. boards face outwards, with the board containing the IF, the AF output amplifier, and the voltage regulators fastened to the chassis. External connections to the CF subunit are all solder connection with the exception of the battery connection, which is through a plug.

Operating Principle

To aid heat dissipation, the integrated AF output amplifier and the series regulator transistors in the voltage regulators on the lower board all have good thermal contact to the chassis.

The 455 kHz signal from IC700 passes through the IF stages to the integrated circuit discriminator, IC3. From there the audio signal divides between the squelch circuit input and the de-emphasis filter at the input to the audio preamplifier.

The squelch circuit opens and closes the signal path through the preamplifier according to the noise content in the demodulated signal. Also, control voltages for use with tone equipment are obtained from the squelch circuit.

The audio signal is taken from the 600 Ω output of the preamplifier to the AF output amplifier. When transmitting, the signal path through the output amplifier becomes automatically blocked.

The signal from the microphone is amplified and limited in the modulation amplifier, which is designed around a dual, integrated operational amplifier. Both amplifiers, IC1a and IC1b, are contained in the same housing.

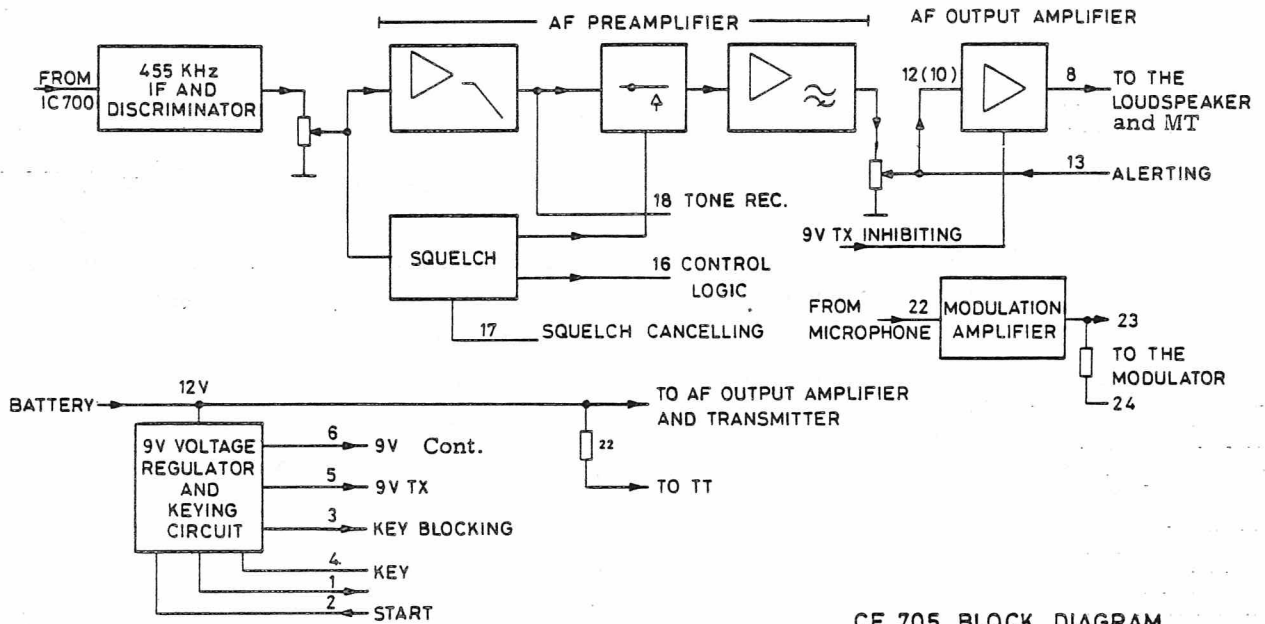
To avoid adjacent channel interference, the high-frequency component of the modulating signal is filtered out and the signal is also amplitude limited in order to keep the carrier frequency deviation within the established maximum excursions for whichever channel separation is employed.

As mentioned previously, the CF subunit also contains two voltage regulators; one supplies the receiver section and the other the transmitter. The AF output amplifier and the PA stage are supplied directly from the battery and are therefore unregulated.

Switching between transmit and receive is accomplished without relays. The transmitter key electronically switches TX voltage regulator on.

Terminal 4 is grounded during transmission and otherwise floats when the key is not activated.

The 12 V supply voltage to the AF output amplifier and the TX power amplifier is always on whenever the on/off switch is turned on. Therefore the 9 V TX circuit is designed to inhibit the audio preamplifier and audio output amplifier

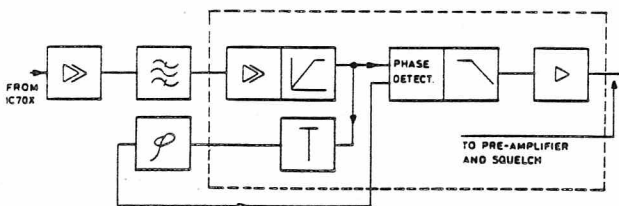


CF 705 BLOCK DIAGRAM

when the transmitter is keyed. This is a precaution against any transients in the squelch circuit that might be able to open the receiver output during transmission.

455 kHz IF Amplifier and Discriminator

This circuit amplifies, selects, limits, and detects the receiver's second IF signal of 455 kHz, allowing a deviation of up to ± 15 kHz from centre frequency.



The amplifier has five stages; the first two, Q30 and Q31, are made up of discrete components while the last three are a part of the integrated circuit, IC3, along with the phase detector.

The only resonant circuits employed in the 2nd IF stage are those between the collector of Q31 and the input to IC3. Resistors R111 and R114

load T1 and T2 enough to achieve sufficiently broad bandwidth.

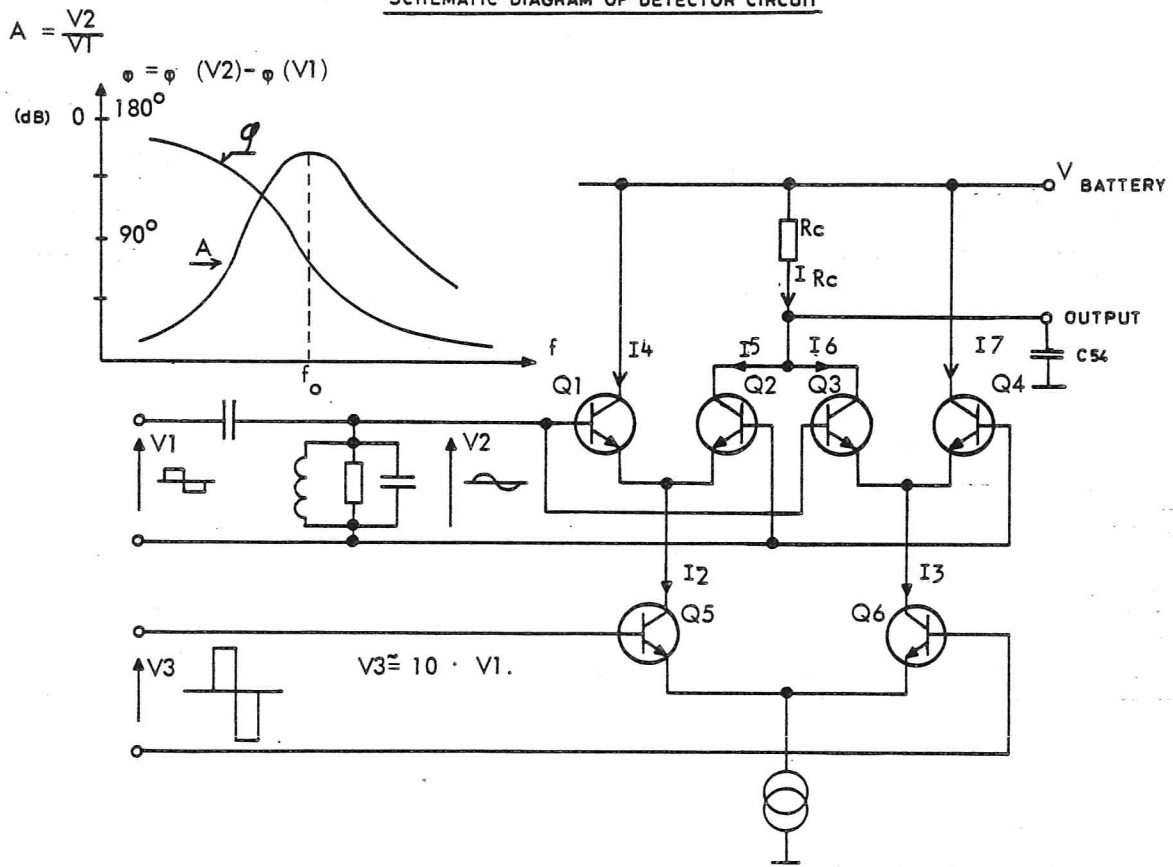
Inductive coupling between circuits is less than critical, R113 in the coupling link determining the coupling factor. Q31 operates with its collector-emitter voltage held low to prevent over-driving IC3.

The three amplifier stages in IC3 are differential amplifiers, which configuration approaches ideal symmetrical limiting. The stages are DC coupled and stability is assured through strong negative feedback. Capacitor C53 eliminates the feedback as far as AC voltages are concerned.

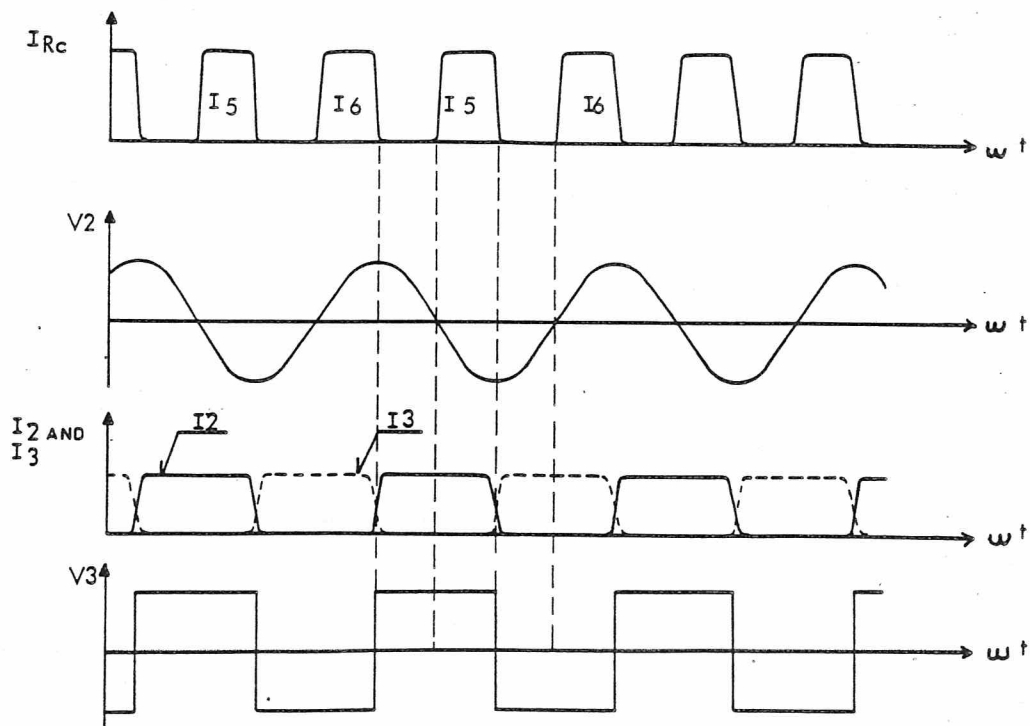
Via an emitter follower within the IC housing, the signal is fed to the phase detector. The IF signal, with its amplitude peaks clipped, is applied directly to one of the phase detector inputs.

The other input is fed the same signal, attenuated and approximately 90° out of phase (at f_0). Phase shift is accomplished with discrete components: C50, C51, L2 and R115. The following diagram shows the detector circuit schematic and the amplitude and phase characteristics of the phase shifting network. A graph of the de-

SCHEMATIC DIAGRAM OF DETECTOR CIRCUIT



GRAPH OF VOLTAGE AND CURRENT RELATIONSHIPS IN THE PHASE DETECTOR WHEN $f = f_0$



detector current and voltage relationships is also included here.

The phase detector is designed around three differential amplifiers, all supplied through a constant-current source. In addition to the components shown in the detector schematic, IC3 also contains an emitter follower after the detector output, another emitter follower between the phase shifting network and one of the detector inputs, and various biasing networks.

As long as voltage V 2 is high enough to drive the two differential stages - Q1 + Q2, and Q3 + Q4 - as switches, the collector current pulses, I5 and I6, will appear as a constant amplitude value and the average value of current through R_C remains independent of the amplitude of the input voltage.

As seen on the schematic, current pulses through R_C only appear when V2 and V3 are of opposite polarities and I5 appears only when V3 is positive while I6 appears when V3 is negative. Supposing that $f > f_0$, then the difference in phase (V2 - V1) is reduced (the V2 pulse a little to the right in relation to V3), causing the width of current pulses I5 and I6 to decrease. In other words, the average current through R_C will decrease. When $f < f_0$, the opposite will occur.

The width of I5 and I6 is therefore seen to be a measurement of the phase difference between V2 and V3. By integrating the output voltage (via R_C and C54) a voltage that is directly proportional to the phase shift is obtained.

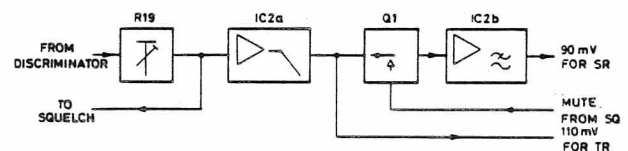
Making use of both the negative and positive excursions of the signals, as in the detector configuration employed here, gives excellent suppression of noise and other undesired effects of inherent nonsymmetry in the clipped IF signal. For example, if the positive going half of V3 is wider than the negative half, I6 will be narrower and I5 wider with the result that the average current through R_C will remain unchanged.

An "S" curve similar to those known from conventional FM detectors will be present at the output (directly on pin 1 of IC3). However, the midpoint of this "S" curve will be around 3.5 V instead of 0 V. Circuit Q is designed low enough

to enable the detector to handle frequency deviations of up to ± 15 kHz.

The De-emphasis Filter, AF Preamp and Electronic Squelching Switch

Network R14/C12 and IC2a take care of de-emphasizing the demodulated signal at the rate of 6 dB/octave and the required gain of 8.5 dB at 1000 Hz.



The integrated preamplifier, IC2, amplifies the AF signal and match it to the nominal 600 Ω load. In addition Q1 is inserted between IC2a and IC2b. Transistor Q1 operates as an electronic switch, interrupting the signal path on command from the squelch circuit.

Potentiometer R19 adjusts the level to the preamplifier, and to the squelch as well.

The second half of the integrated amplifier, IC2b, and C14 - C15 - R29 - R28 constitute a filter, which strongly attenuates low frequencies (< 250 Hz).

R32 - C 16 introduce a suitable roll-off at high frequencies (> 6 kHz). Preamplifier IC2b is, like IC2a, biased via R28.

The signal path between the first and second amplifier stages is through a transistor, which acts like a switch controlled by the squelch.

The Squelch

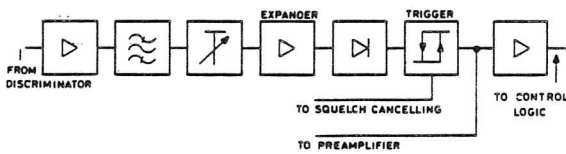
The squelch circuit opens and closes the audio signal path through the AF preamplifier according to the noise content of the incoming signal. The squelch circuit also provides a signal voltage for use in tone signalling.

An internal adjustment, potentiometer R46, is provided for setting the squelch level. The squelch function can during test be cancelled altogether by grounding terminal 17 via squelch cancelling button.

The squelch section includes a frequency selective noise amplifier, Q4 - Q5, an expander stage, Q6, a noise detector, a Schmitt trigger, Q7 and Q8, and an emitter follower amplifier, Q9.

The operating principle is as follows:

Some of the AF signal from the discriminator is fed to the noise amplifier whose collector load is made up of a parallel resonant circuit tuned to approximately 7.5 kHz. The selected noise is then fed to Q6 which is biased in such a way that only



positive going pulses of a certain minimum amplitude cause the transistor to conduct. Since only pulses of a certain amplitude can become amplified, the result is that a given relative change in noise amplitude at the base of Q6 appears as a larger relative change at the collector. The noise pulses are then rectified and filtered to a d. c. potential that, in turn, controls the Schmitt trigger, Q7 and Q8. The collector voltage on Q8 is used partly to drive the emitter follower, Q9, and partly to switch the transistor, Q1, in the AF preamplifier.

The 9 V Voltage Regulators and Keying Circuits

The two 9 V voltage regulators supply the receiver and the transmitter sections, respectively. They are intended for use with a 12 V storage battery.

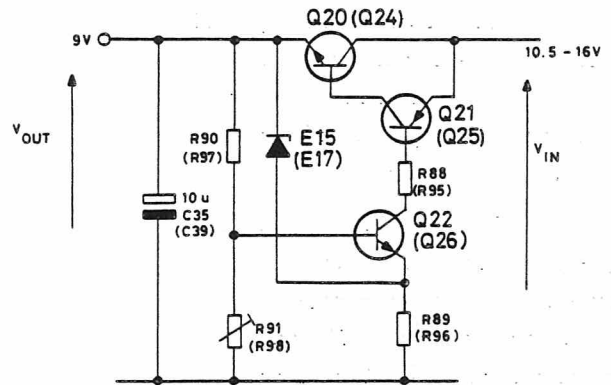
The battery connects to the regulators through the start relay switches.

To protect the equipment against incorrect battery polarity a diode, E9, is placed in series with the start relay. If the power supply is connected wrong the diode will not conduct and the start relay thus refuses to operate.

The voltage regulators are protected against short circuits; with shorted output the current through Q20 will be less than 0.5 A and through Q24 less than 0.1 A. The power series transistors are me-

chanical mounted so as to be in good thermal contact with the chassis.

The two regulators are principally identical as shown on the simplified diagram as follows:



Q20 is driven by Q21, which is controlled by amplifier Q22. Transistor Q22 compares the zener reference voltage across E15 with a portion of the output voltage through dividing resistors R90 and R91. R91 sets the output voltage.

The operating principle is as follows:

If V_{out} drops (due to a decrease in input voltage or an increase in load current), V_{BE} for Q22 will increase, also increasing base current for Q21 and Q20. When base current to Q20 increases, more current flows through the output load, cancelling the original drop in output voltage.

If the load current increases to a certain value, Q22 goes into saturation. If the load current increases still more, the zener diode will act as an open circuit and V_{BE} for Q22 decreases whereby base current for Q22, Q21, and Q20 decreases, too. Finally, Q22 will be cut off and base current in Q20 and Q21 will be zero. Thus is Q20 protected against destruction by short circuits at its output. Resistors R88 - and R89 - determine the saturation current through Q22 and, of course, the short circuit current.

A regulator built exactly like the simplified diagram would not be self-starting, however. Therefore, the regulators are provided with starting circuits; 9V RX employs R82, R83, and E13 in its starting circuit and 9V TX employs R93 and E16.

Operation of Keying and Starting Circuits

When terminal 4 is floating and the power is turned on, 9 V RX will build up voltage since Q 20 gets base current through R82, R83 and E13. When 9 V RX reaches its final value the starting circuit will have no effect on the regulator because diode E13 will then be nonconducting (the unloaded voltage at terminal 4 is approx. 8.2V at nominal battery voltage).

Transistor Q27 is heavily saturated, so the 9V RX regulator will operate undisturbed while 9V TX will be blocked because Q26 is completely cut off by Q27.

When the transmit key grounds terminal 4, two things happen:

1. Q27 loses its forward bias and immediately cuts off. Now, instead of acting as a short circuit between the base of Q26 and ground, Q27 can now be considered a large resistance.
2. C36, which has been charging through diode E14, has accumulated a charge of about 6.4 V. With terminal 4 grounded the charge on C36 reverse biases E14. Now C36 will discharge.

There are two discharge paths available to C36, one through the bleeder resistor, R94, and one through R93 and E16 to the base of Q26. Remember that the base of Q26 is no longer grounded.

The discharge current to the base of Q26 drives this transistor on. Once Q26 turns on its base assumes a potential of approx. 5.1 V. By now

C36 has discharged so much that E16 becomes reverse biased by the 5.1 V on the base of Q26, and C36 continues to discharge through its other path (R94).

As long as terminal 4 is kept at chassis potential by the transmit key the 9 V TX regulator continues to operate.

When the key is released and terminal 4 resumes its unloaded potential of approx. 7.0 V, Q27 is driven on and short circuits the base of Q26 again. The 9 V TX regulator then turns off.

C36 charges again through E14.

Diode E11 ensures effective keying even if terminal 4 is not brought all the way down to 0 V potential.

Note that 9 V TX cannot begin to build up a voltage by itself after a short circuit but must be started again by keying the transmitter.

The operations described above presume the key blocking terminal to be at approx. 0 V potential.

The AF Output Amplifier

The output amplifier amplifies the audio signal from the preamplifier and powers the loudspeaker.

The amplifier is built around an integrated AF power module mounted on stand-offs, which are fastened to the chassis and act as heat sink. The amplification factor is determined by a suitable amount of feedback. In order to compensate variations in gain the internal feedback resistor (approx. 4 k Ω) is shunted by R127. Besides the normal input, the amplifier has an input for an Alerting tone from the tone receiver, when called. As the Alerting tone is to be heard from the loudspeaker when the volume control is turned down an isolating resistor, R120 is inserted.

In order to provide, optionally, a remote control for a locally controlled equipment, resistor R119 is serving to separate the two volume controls. Also note that the amplifier inputs (terminal 10

or 12) must have a d. c. path to chassis in order to bias the amplifier properly. C60/R125 increase the maximum achievable output power (bootstrapping) and C58/C59 together with R126/C63 constitute the frequency compensation.

Supply voltage ripple is suppressed by C57, and R117/R118 reduce the current spike through the start relay switches when the equipment is turned on.

During transmit the amplifier is totally inhibited via Q32.

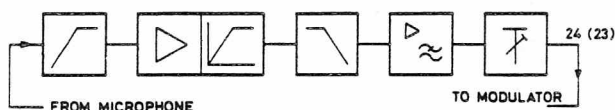
The Modulation Amplifier

General

The modulation amplifier differentiates, amplifies, limits and integrates the microphone signal. It also suppresses undesired high frequencies with an active filter designed for 25 kHz channel spacing.

Both amplifiers are contained in a single integrated circuit made up of dual operational amplifiers. The modulation amplifier contains additional passive differentiation and integrating circuits to prevent overmodulation.

The following block diagram shows the operating principle for the amplifier:



Input

The input circuit, which is also the collector return for the microphone amplifier output stage through resistor R2, is asymmetric.

The Differentiating Circuit

The differentiation network is made up of C1 and R3 (the input impedance of the operational amplifier is negligible due to the feedback through R8).

It differentiates at the rate of +6 dB pr. octave over the entire audio range of 300 - 3000 Hz.

The AF Amplifier - Clipper

The gain of the first amplifier stage, IC1a, is determined by the amount of feedback introduced.

Clipping action begins as soon as the amplifier is driven to where the output excursions approximate the battery voltage. This level will be about 6.5 V peak-to-peak. The amplifier can be driven up to 25 dB above its nominal input level. Symmetry of the clipping is determined by bias network R5, R6, and R7 and therefore is fixed.

The Integration Circuit

Integrating takes place from 30 Hz at -6 dB pr. octave. The passive integrating network consists of R11 and C4. The lower limit for integration is determined solely by these two components as the previous amplifier's feedback makes its output impedance negligible, and because the loading of the network by the filter that follows is very light as long as the signal remains below the frequency limit of that filter.

The Splatter Filter

The purpose of this filter is to cut off frequencies that lie above the voice range in order to avoid undesirable sideband noise. It is an active filter consisting of the second operational amplifier and its associated components. Its response approaches that of a Chebishev filter. The circuit arrangement is the so-called voltage follower, where the voltage gain is very near unity (1).

Adjusting the Frequency Swing

The amount of signal to the modulator input, and thus the frequency swing, is set by the voltage divider formed by R18 and the input impedance of the modulator. If the frequency swing cannot be set sufficiently high, terminal 23 can be used instead of terminal 24.

TECHNICAL SPECIFICATIONS

Nominal Supply Voltage

13.6 V

Current Drain

(at nominal supply voltage)

Transmit: 120 mA

Receive : 100 mA

12 dB SINAD Sensitivity

(where 1.75 kHz deviation of the 455 kHz IF results in a 1 kHz audio signal)

1.2 μ V input signal at input terminationLine Output (terminal 19)-17 dBm/600 Ω (110 mV)AF Telephone Output (terminal 16)

90 mV

Regulated Voltages

Receiver (terminal 6): 9 V

Transmitter (terminal 5): 9 V

Unregulated filtered Voltages

AF output amplifier: 13.6 V

PA stage (terminal 15): 13.6 V

Tone transmitter

(terminal 7): 13.6 V

AF Output Power (terminal 8)

3 W

Modulation Amplifier Sensitivity

(for normal frequency swing at 1 kHz)

110 mV +1/-3 dB

TX InhibitVoltage/current: \geq 6 V/2 mATemperature Range

Working range: -25°C - +60°C

Function range: -30°C - +75°C

The following, more detailed specifications for the several CF705 functions are all typical values measured at 25°C ambient temperature, unless otherwise stated.

455 kHz IF Amplifier and DiscriminatorCurrent Drain (at nominal 9 V supply)

18 mA

Maximum Frequency Deviation \pm 15 kHzIF Bandwidth (3 dB attenuation) \pm 17 kHzInput Impedance1 k Ω // 15 pFGain

from input (terminal 1) to pin 4 of IC3: 55 dB

from IC3 input (pin 4) to IC3 amplifier

high output, pin 10: 55 dB

Discriminator Conversion Efficiency

50 mV / kHz

AF Output Voltage ($f_m = 1$ kHz, $\Delta f = 3.5$ kHz)

110 mV

Measured at test point 2, terminated with 2.2 k Ω load.

Discriminator Linearity (relative to 1000 Hz)

Pass-Band 100 - 3500 Hz: +0/-1 dB

Measured at test point 2, terminated with 2.2 k Ω load.

Discriminator Output Resistance200 Ω Minimum Load Resistance2 k Ω Harmonic Distortion $\Delta f = 15 \text{ kHz} : 4.5\%$ $\Delta f = 3.5 \text{ kHz} : 1.0\%$ AF PREAMPLIFIER and SQUELCH-CONTROLLED SWITCHCurrent Drain (at nominal 9 V supply)

1.5 mA

Input Impedance (at 1 kHz)2.2 k Ω Output Impedance $R_{\text{OUT}} = \sim 0 \Omega$ Gain (gain control at highest setting) $R_L = 1.8 \text{ k}\Omega, f = 1 \text{ kHz};$

Terminal 19: 6.5 dB

Terminal 18: 8.5 dB

Harmonic Distortion ($R_L = 1.8 \text{ k}\Omega, f = 1 \text{ kHz}$)

(terminal 18 and 19)

 $V_{\text{OUT}} = 110 \text{ mV}$ (nominal): 0.2% $V_{\text{OUT}} = 500 \text{ mV} : 0.5\%$ Required Turn-on Potential

(between R30 and R65)

To ensure normal signal path: $\geq 2.3 \text{ V}$ To close signal path: $< 0.7 \text{ V}$ Deemphasis Cut-off Frequency

60 Hz

Frequency Response at Tone Receiver Output

(terminal 18)

(relative to -6 dB/octave characteristic)

Pass -Band linearity (300 - 3000 Hz): +0/-1 dB

Frequency Response at Output for AF Amplifier and Tone Receiver

(terminal 19)

(relative to -6 dB/octave characteristic)

Pass-Band linearity (300 - 3000 Hz) : +0/-1.5 dB

100 Hz rel. to 1000 Hz : +6 dB

6 kHz rel. to 1000 Hz : -17 dB

SQUELCH CIRCUITCurrent Drain (at nominal 9 V supply)

21 mA

Measured with unloaded Squelch Signalling (terminal 16)

Input Impedance15 k Ω Noise Filter Resonant Frequency

7.5 kHz

Output VoltageSquelched condition: $\leq 100 \text{ mV}$ Un-squelched condition: $> 5.6 \text{ V}$
measured at Q8's collector.Squelch Signalling (terminal 16) R_{LOAD} minimum = 680 Ω V_{OUT} (with $R_L = 680 \Omega$)Squelched condition: $\leq 100 \text{ mV}$ Un-squelched condition: $\geq 4.0 \text{ V}$ AF OUTPUT AMPLIFIERNominal Supply Voltage

13.6 V

Operating Range

10.5 to 16 V

Current Drain (at nominal supply voltage)

no-signal condition: 12 mA

at 4 W output : 520 mA

inhibited : 6 mA

Output Power (at nominal supply voltage)

Maximum 4 W

Loudspeaker ImpedanceNominal/minimum: 4 Ω Input Impedance (at 1 kHz)100 k Ω Nominal Gain

32 dB (at 1 kHz)

Harmonic Distortion (at 1kHz) $P_{OUT} = 2 \text{ W}: 1\%$ $P_{OUT} = 0.2 \text{ W}: 0.5\%$ Frequency Response (relative to 1 kHz)

80 Hz	-3 dB
300 Hz	0 dB
3000 Hz	-0.5 dB
15 kHz	-3 dB

Measured at 0.2 W output power.

Alerting Tone Input

Voltage gain: 1.5 dB

Input impedance: 270 k Ω

MODULATION AMPLIFIER

Current Drain, (at nominal 9 V supply)

1.5 mA

Input Impedance (at 1 kHz)540 Ω Limiting

Signal clipping begins to occur with an input signal (1000 Hz) of: 160 mV

Output signal level observed at pin 1 of IC1 when clipping occurs: 7.0 V p.p.

Output Voltage (1 kHz)

12 mV

Measured at modulation output (terminal 24) with potentiometer R18 fully up, and load impedance = 1 k Ω .
Input level = 160 mV.Harmonic Distortion (at 1 kHz)

for 160 mV input signal: 0.8%

Frequency Response (relative to 1 kHz)

300 Hz	- 0 dB
3 kHz	- 0 dB
6 kHz	- 19 dB
10 kHz	- 32 dB

Measured for 15 mV input signal, and with a resistive output load.

9 V VOLTAGE REGULATORS and
KEYING CIRCUITSNominal Supply Voltage

13.6 V

Operating Range

10.5 V to 16 V

Regulated Output VoltagesReceiver supply 9 V RX: 9.0 V \pm 0.2 VTransmitter supply 9 V TX: 9.0 V \pm 0.2 V V_{REG} vs. Temperature3.6 mV / pr. $^{\circ}\text{C}$ Suppression of $\Delta V_{BATTERY}$ in V_{REG}

(at nominal load)

DC : 46 dB

1 kHz : 50 dB

Internal Resistance of Regulators $R_I = 0.5 \Omega$ Regulator Output Current

Maximum 250 mA

Maximum Load

on terminal 7 (TT) : 100 mA
on terminal 15 (PA) : 6 A

Keying Termination

Maximum allowable resistance of
wiring : 180 Ω
Alternatively, V_{MAX} at terminal 4 : 1.0 V

Regulator Switching Time $(V_{BATTERY} = 13.6 \text{ V})$

9 V TX turn-on delay, $t_0 - 90\%$: 0.1 ms
9 V TX turn-off delay, $t_{100 - 10\%}$: 25 ms

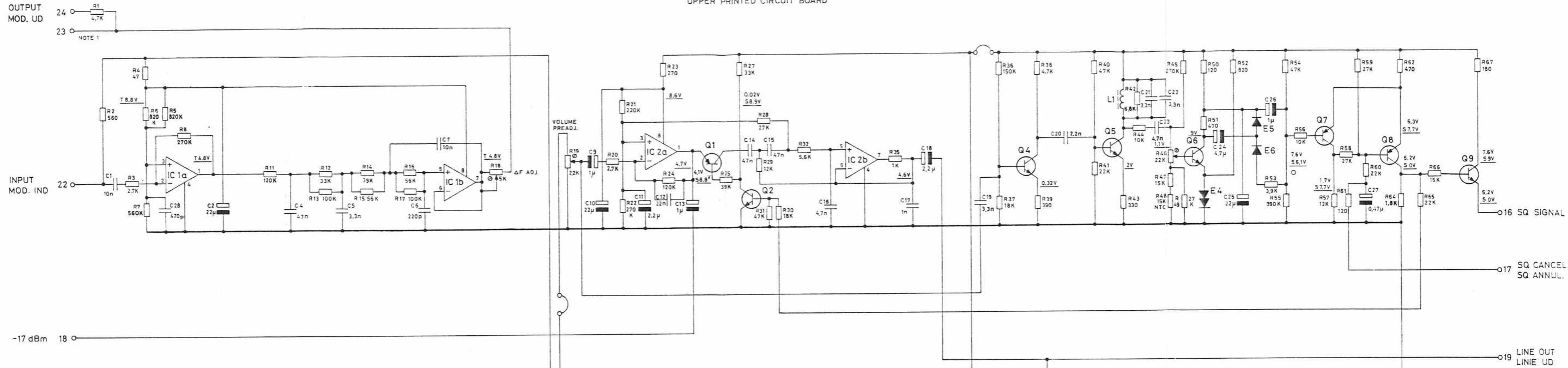
Measured under normal load conditions.

TX Inhibit (terminal 3)Voltage/current : $\geq 6 \text{ V} / 2 \text{ mA}$

MODULATION AMPLIFIER
MODULATIONSFORSTÆRKER

PREAMPLIFIER
FORSTÆRKER
UPPER PRINTED CIRCUIT BOARD

SQUELCH



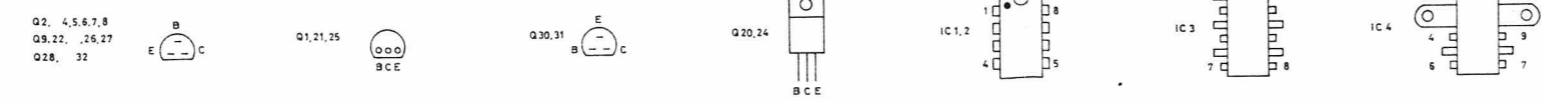
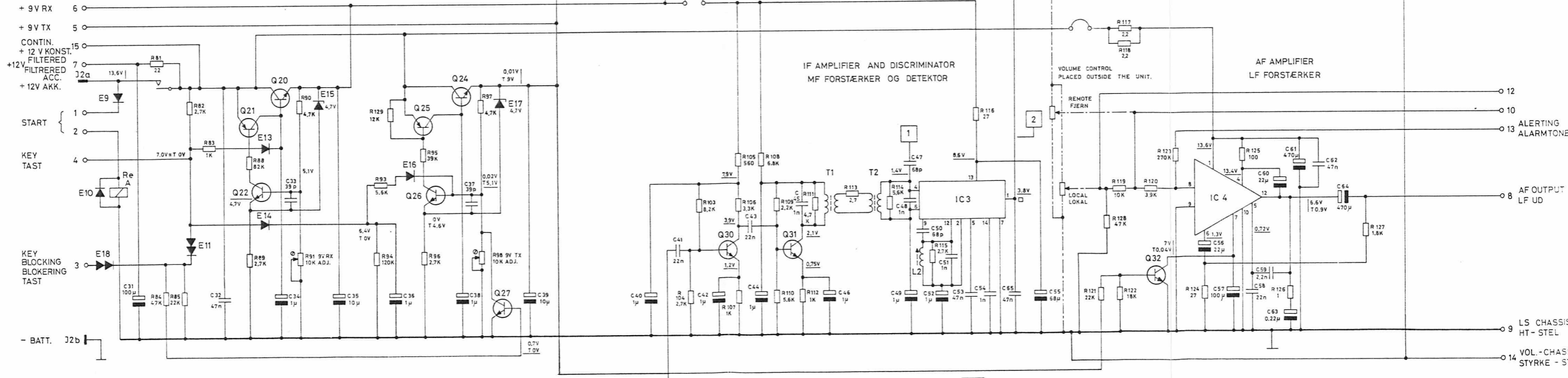
RX VOLTAGE REGULATOR
SPENDINGSREGULATOR RX

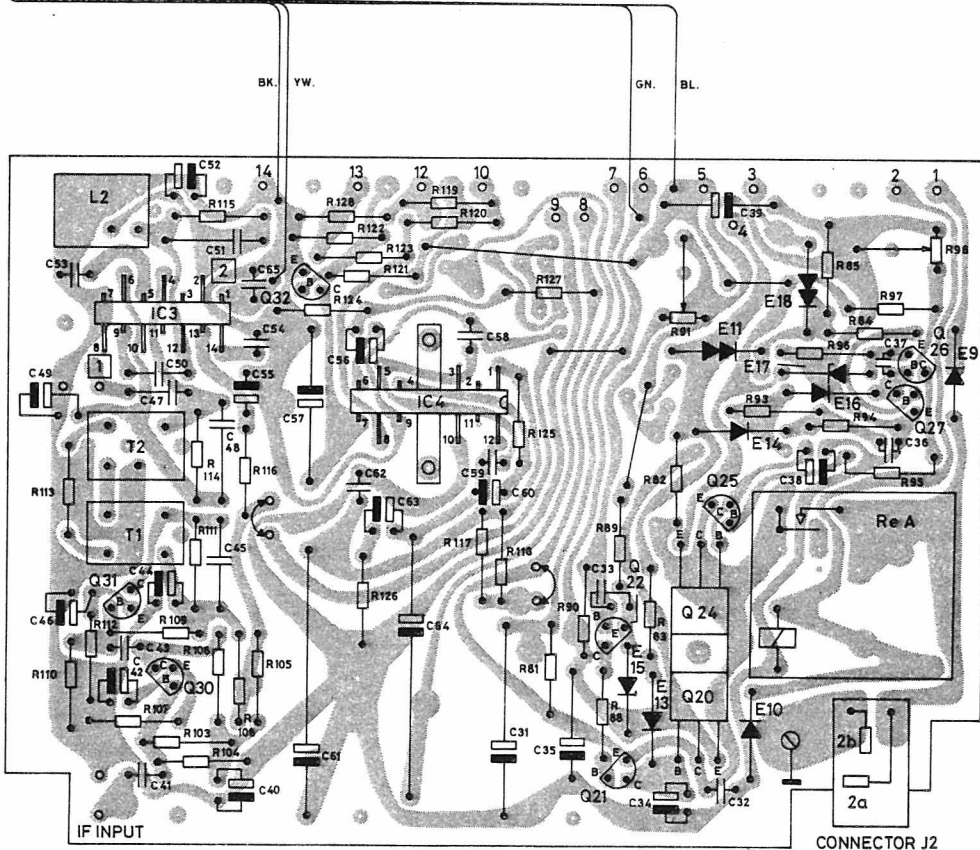
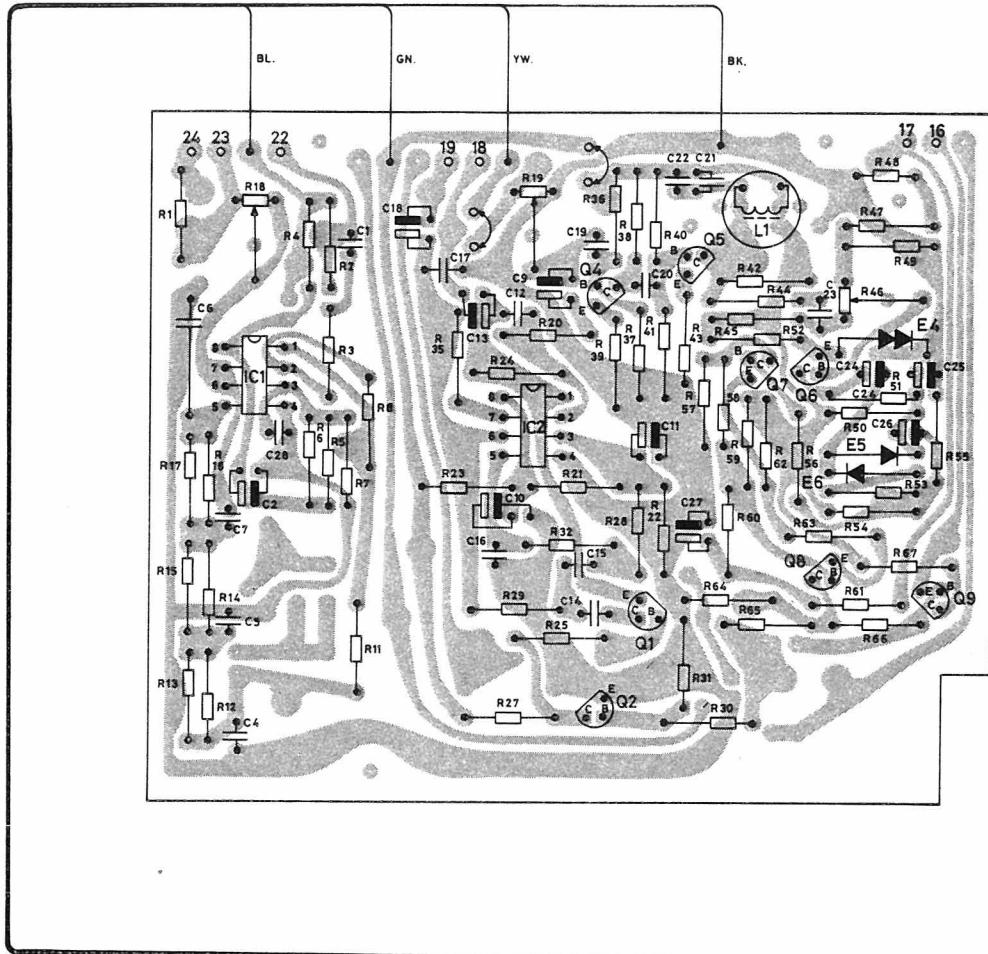
TX VOLTAGE REGULATOR
SPENDINGSREGULATOR TX

LOWER PRINTED CIRCUIT BOARD

IF AMPLIFIER AND DISCRIMINATOR
MF FORSTÆRKER OG DETEKTOR

AF AMPLIFIER
LF FORSTÆRKER





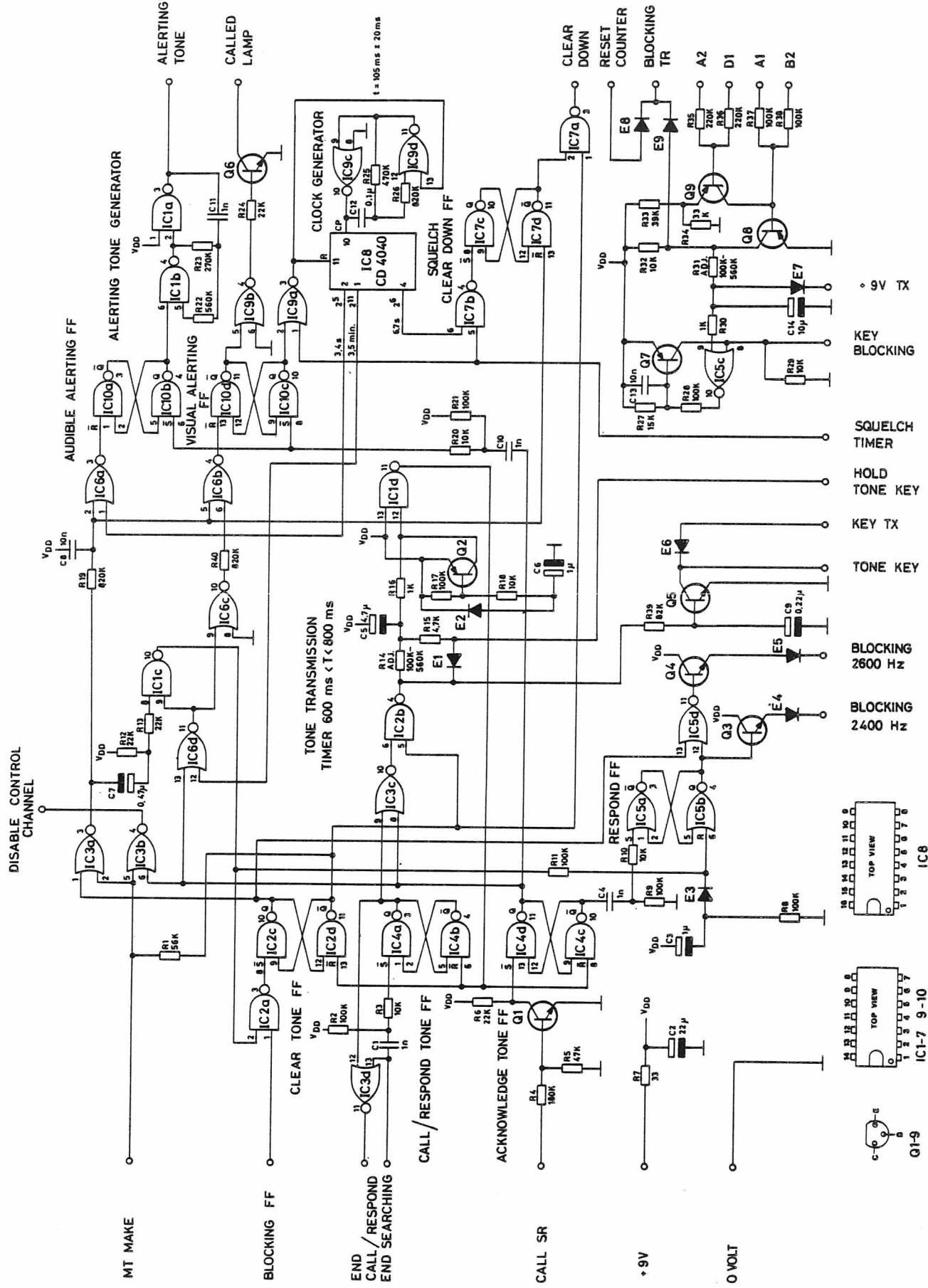
COMMON FUNCTIONS UNIT CF 705

TYPE	Nº	CODE	DATA
CF705		10. 3502-00	Common Functions
	C1	76. 5070	10 nF 50 V
	C2	73. 5127	22 µF 16 V
	C4	76. 5072	47 nF 50 V
	C5	76. 5060	3.3 nF 10%
	C6	76. 5063	220 pF 5%
	C7	76. 5070	10 nF 10%
	C9	73. 5114	1 µF 20%
	C10	73. 5127	22 µF 20%
	C11	73. 5102	2.2 µF 20%
	C12	76. 5071	22 nF 10%
	C13	73. 5114	1 µF 20%
	C14	76. 5072	47 nF 10%
	C15	76. 5072	47 nF 10%
	C16	76. 5061	4.7 nF 10%
	C17	74. 5155	1 nF -20/+80%
	C18	73. 5102	2.2 µF 20%
	C19	76. 5060	3.3 nF 10%
	C20	76. 5059	2.2 nF 10%
	C21	76. 5060	3.3 nF 10%
	C22	76. 5060	3.3 nF 10%
	C23	76. 5061	4.7 nF 10%
	C24	73. 5126	4.7 µF 20%
	C25	73. 5127	22 µF 20%
	C26	73. 5114	1 µF 20%
	C27	73. 5125	0.47 µF 20%
	C28	74. 5161	470 pF -20/+80%
	C31	73. 5071	100 µF -10/+50%
	C32	76. 5072	47 nF 10%
	C33	74. 5338	39 pF 2%
	C34	73. 5114	1 µF 20%
	C35	73. 5011	10 µF -10/+100%
	C36	73. 5114	1 µF 20%
	C37	74. 5338	39 pF 2%
	C38	73. 5114	1 µF 20%
	C39	73. 5011	10 µF -10/+100%
	C40	73. 5114	1 µF 20%
	C41	76. 5071	22 nF 10%
	C42	73. 5114	1 µF 20%
	C43	76. 5071	22 nF 10%
	C44	73. 5114	1 µF 20%
	C45	76. 5067	1 nF 5%
	C46	73. 5114	1 µF 20%
	C47	74. 5341	68 pF 2%
	C48	76. 5067	1 nF 5%
	C49	73. 5114	1 µF 20%
	C50	74. 5341	68 pF 2%

TYPE	Nº	CODE	DATA
	C51	76. 5067	1 nF 5%
	C52	73. 5114	1 µF 20%
	C53	76. 5072	47 nF 10%
	C54	76. 5069	1 nF 10%
	C55	73. 5106	68 µF 20%
	C56	73. 5127	22 µF 20%
	C57	73. 5151	100 µF -10/+50%
	C58	76. 5071	2.2 nF 10%
	C59	76. 5059	2.2 nF 10%
	C60	73. 5127	22 µF 20%
	C61	73. 5138	470 µF -10/+100%
	C62	76. 5072	47 nF 10%
	C63	73. 5118	0.22 µF 20%
	C64	73. 5137	470 µF -10/+50%
	C65	76. 5072	47 nF 10%
	R1	80. 5257	4.7 k Ω 5%
	R2	80. 5246	560 Ω 5%
	R3	80. 5254	2.7 k Ω 5%
	R4	80. 5233	47 Ω 5%
	R5	80. 5284	820 k Ω 5%
	R6	80. 5284	820 k Ω 5%
	R7	80. 5282	560 k Ω 5%
	R8	80. 5278	270 k Ω 5%
	R11	80. 5274	120 k Ω 5%
	R12	80. 5267	33 k Ω 5%
	R13	80. 5273	100 k Ω 5%
	R14	80. 5268	39 k Ω 5%
	R15	80. 5270	56 k Ω 5%
	R16	80. 5270	56 k Ω 5%
	R17	80. 5273	100 k Ω 5%
	R18	86. 5050	5 k Ω 20%
	R19	86. 5043	2.2 k Ω 20%
	R20	80. 5254	2.7 k Ω 5%
	R21	80. 5277	220 k Ω 5%
	R22	80. 5278	270 k Ω 5%
	R23	80. 5242	270 Ω 5%
	R24	80. 5274	120 k Ω 5%
	R25	80. 5268	39 k Ω 5%
	R27	80. 5267	33 k Ω 5%
	R28	80. 5266	27 k Ω 5%
	R29	80. 5262	12 k Ω 5%
	R1		carbon film
	R2		"
	R3		"
	R4		"
	R5		"
	R6		"
	R7		"
	R8		"
	R11		"
	R12		"
	R13		"
	R14		"
	R15		"
	R16		"
	R17		"
	R18		trim carbon
	R19		"
	R20		carbon film
	R21		"
	R22		"
	R23		"
	R24		"
	R25		"
	R27		"
	R28		"
	R29		"

COMMON FUNCTIONS CF705

X402.554



CONTROL LOGIC CL701

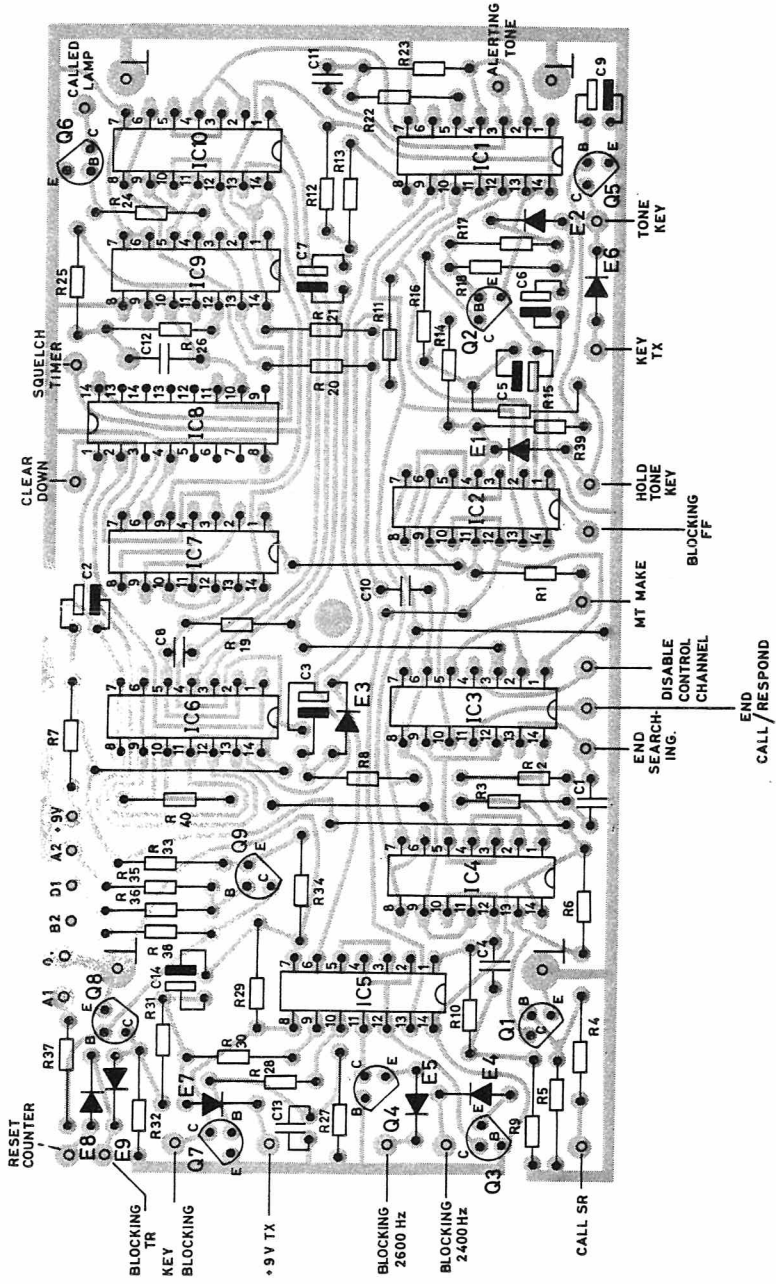
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TYPE	Nº	CODE	DATA
CL701		10. 3369-00	Control Logic
	C1	74. 5155	63 V
	C2	73. 5127	16 V
	C3	73. 5114	35 V
	C4	74. 5155	63 V
	C5	73. 5126	35 V
	C6	73. 5114	35 V
	C7	73. 5125	35 V
	C8	76. 5070	50 V
	C9	73. 5118	35 V
	C10	74. 5155	63 V
	C11	76. 5069	50 V
	C12	76. 5125	100 V
	C13	76. 5070	50 V
	C14	73. 5109	16 V
	R1	80. 5270	5% 1/8 W
	R2	80. 5273	5% 1/8 W
	R3	80. 5261	5% 1/8 W
	R4	80. 5276	5% 1/8 W
	R5	80. 5269	5% 1/8 W
	R6	80. 5265	5% 1/8 W
	R7	80. 5231	5% 1/8 W
	R8	80. 5273	5% 1/8 W
	R9	80. 5273	5% 1/8 W
	R10	80. 5261	5% 1/8 W
	R11	80. 5273	5% 1/8 W
	R12	80. 5265	5% 1/8 W
	R13	80. 5265	5% 1/8 W
	R14	80. 52xx	5% 1/8 W
	R15	80. 5257	5% 1/8 W
	R16	80. 5249	5% 1/8 W
	R17	80. 5273	5% 1/8 W
	R18	80. 5261	5% 1/8 W
	R19	80. 5284	5% 1/8 W
	R20	80. 5261	5% 1/8 W
	R21	80. 5273	5% 1/8 W
	R22	80. 5282	5% 1/8 W
	R23	80. 5278	5% 1/8 W
	R24	80. 5265	5% 1/8 W
	R25	80. 5281	5% 1/8 W
	R26	80. 5284	5% 1/8 W
	R27	80. 5263	5% 1/8 W
	R28	80. 5273	5% 1/8 W
	R29	80. 5261	5% 1/8 W
	R30	80. 5249	5% 1/8 W
	R31	80. 52xx	5% 1/8 W
		ADJ	5%
		ADJ	5%

TYPE	Nº	CODE	DATA
	R32	80. 5261	10 kΩ 5%
	R33	80. 5268	39 kΩ 5%
	R34	80. 5267	33 kΩ 5%
	R35	80. 5277	220 kΩ 5%
	R36	80. 5277	220 kΩ 5%
	R37	80. 5273	100 kΩ 5%
	R38	80. 5273	100 kΩ 5%
	R39	80. 5272	82 kΩ 5%
	R40	80. 5284	820 kΩ 5%
	E1-E9	99. 5237	1 N 4148 Diode
	Q1	99. 5143	BC 238 Transistor
	Q2	99. 5230	BC 308 Transistor
	Q3-Q6	99. 5143	BC 238 Transistor
	Q7	99. 5230	BC 308 Transistor
	Q8	99. 5143	BC 238 Transistor
	Q9	99. 5230	BC 308 Transistor
	IC1-2	14. 5051	CD 4011 AE quadr. 2 input NAND
	IC3	14. 5074	SD 4001 AE quadr. 2 input NOR
	IC4	14. 5051	CD 4011 AE quadr. 2 input NAND
	IC5-6	14. 5074	SD 4001 AE quadr. 2 input NOR
	IC7	14. 5051	CD 4011 AE quadr. 2 input NAND
	IC8	14. 5111	CD 4040 AE 12 stage binary counter
	IC9	14. 5074	CD 4001 AE quadr. 2 input NOR
	IC10	14. 5051	CD 4011 AE quadr. 2 input NAND

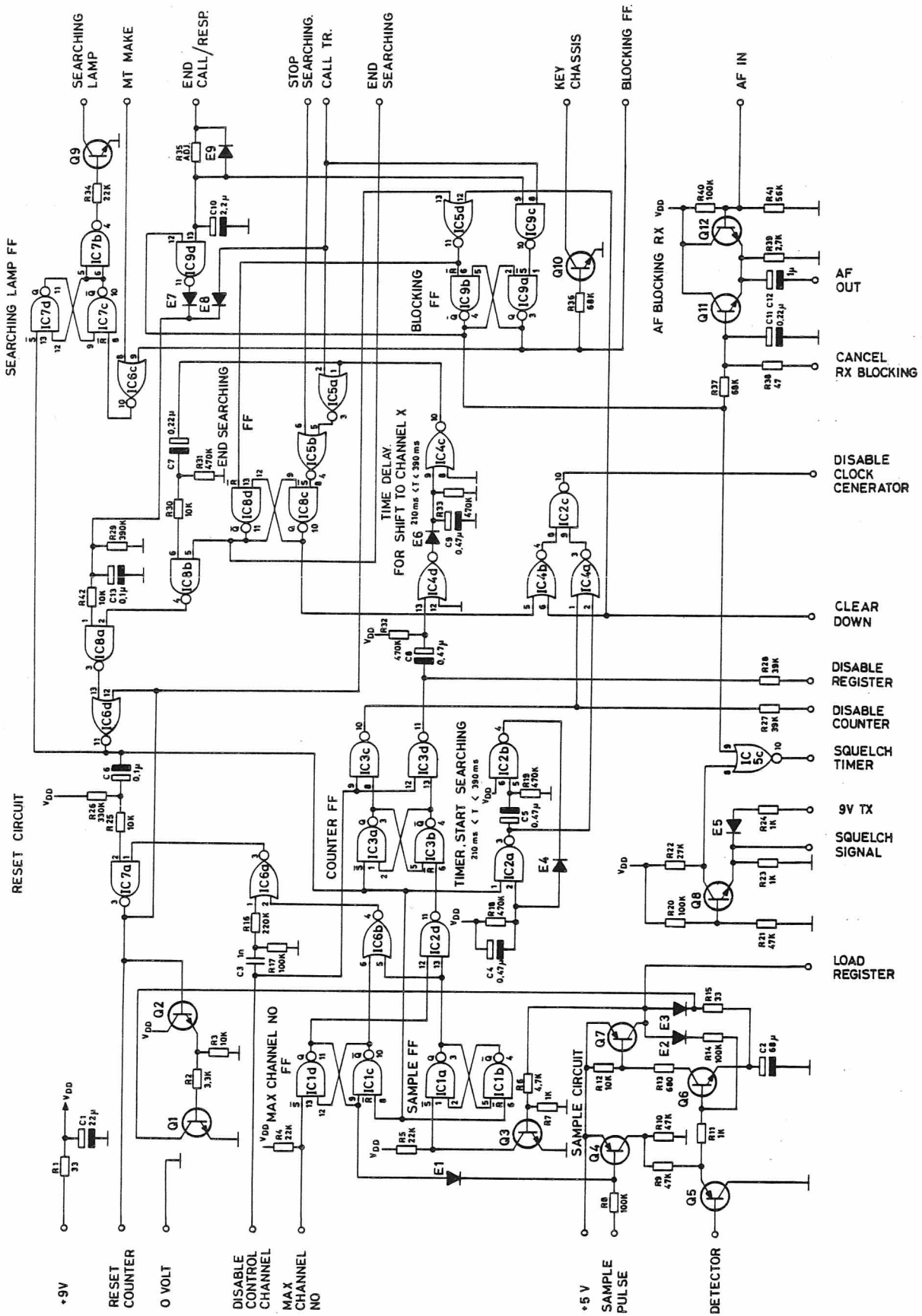
CONTROL LOGIC UNIT CL701

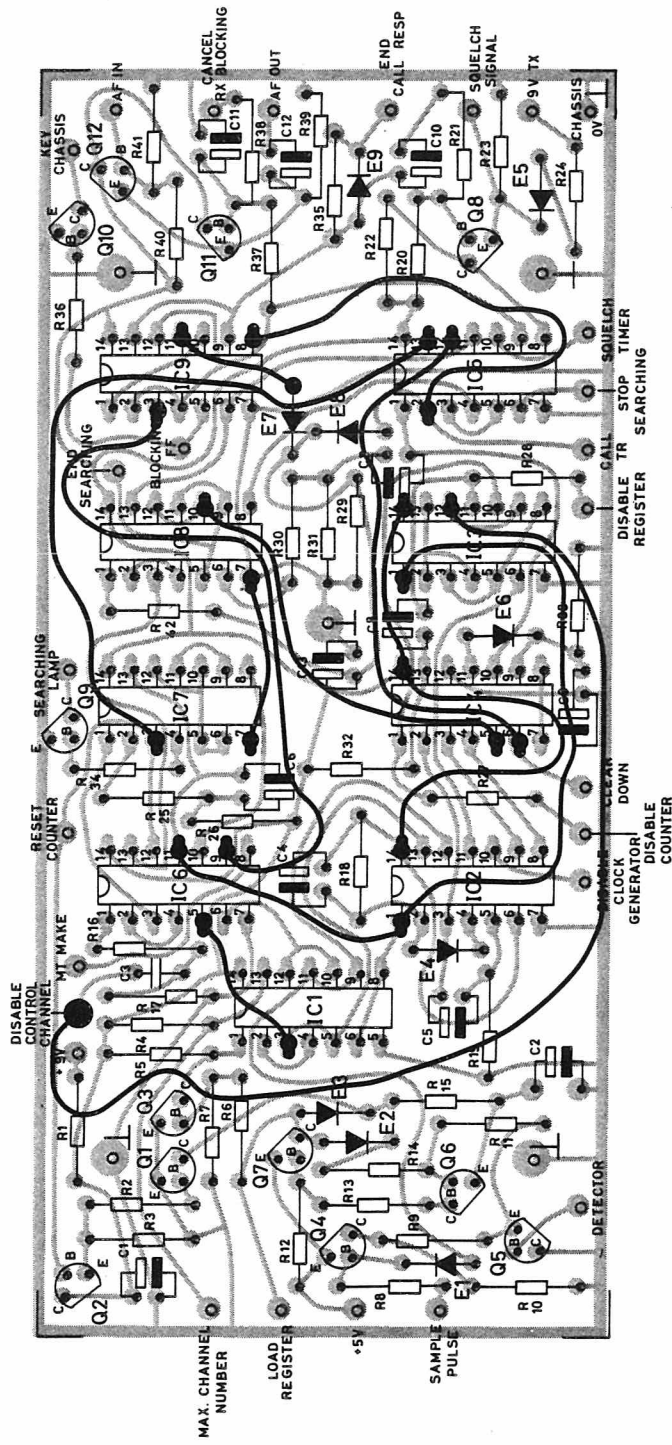
X402. 464



CONTROL LOGIC CL701

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PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE.

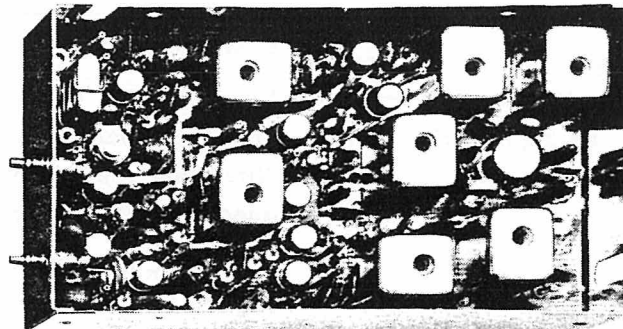
STORNOPHONE 700
 MAINTENANCE MANUAL
 VOLUME II
 Section 3

TITLE		Code
EX711	Description 1 - 3	60. 179-E1
	Schematic	D401. 361/2
	Component Lay-out	D401. 521/2
	Part List 1 - 2	X401. 371/2
EX712	Schematic	D401. 847
	Part List 1 - 2	X401. 945
EX731	Description 1 - 3	60. 180-E1
	Schematic	D401. 524/2
	Component Lay-out	D401. 524/3
	Part List 1 - 3	X401. 786
EX761	Description 1 - 3	60. 181-E1
	Schematic	D401. 312/2
	Component Lay-out	D401. 519
	Part List 1 - 2	X401. 321/2
EX762	Schematic	D401. 805
	Component Lay-out	D401. 892
	Part List 1 - 2	X401. 867
FC701 & FC702	Schematic	D401. 819/2
	Part List	X401. 964
FC703	Schematic	D401. 832
	Part List	X401. 864
FC704	Schematic	D402. 145
	Part List	X402. 365
	Component Lay-out	D402. 431
FC705	Schematic	D402. 383/2
	Part List	X402. 463/2
	Component Lay-out	D402. 508

STORNOPHONE 700
MAINTENANCE MANUAL
VOLUME II
Section 3

FS701	Schematic	D401. 714/3
	Component Lay-out	D401. 891/3
	Part List	X401. 863/2
FS702	Schematic	D402. 406
	Component Lay-out	D402. 550
	Part List	X402. 467

EXCITER EX711



Description

General

The exciter must modulate and convert the signal from the transmitter oscillator so the frequency and amplitude are suitable for driving the power amplifier, PA711.

EX 711 contains the following stages:

- an oscillator (for single channel service)
- a phase modulator with associated buffer stages
- a frequency tripler
- two frequency doublers
- an amplifier

After passing through the buffer stage, the oscillator signal becomes phase modulated, goes through another buffer, then is multiplied 12 times, being first tripled then doubled and finally doubled once more. The result is a signal at the transmitter antenna frequency (146 to 174 MHz.)

For multichannel service the built-in oscillator can be switched out and another oscillator (and frequency) switched in from the oscillator switching unit, XS701.

Oscillator

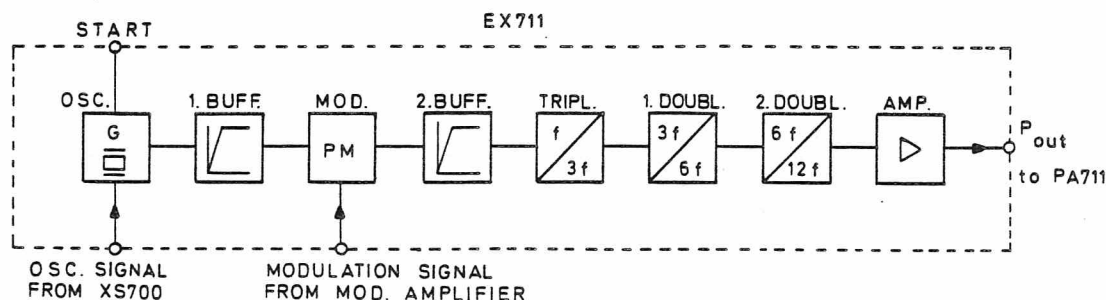
To start the oscillator, the emitter circuit of Q1 must be returned to ground via terminal 1. For single channel service the terminal is tied to ground right in the EX unit.

In the case of multichannel service the emitter of Q1 is grounded through the control panel. When one of the oscillators in the XS unit is functioning, the emitter connection to Q1 is open and the signal from XS is applied to the exciter at terminal 2. R5 in EX711 serves as a collector resistor common to all of the oscillators.

Buffer Stages

Buffer Q2 keeps the RF input signal to the modulator at a constant level while Q4 presents a constant load impedance to the modulator.

The output signals from the different oscillators can vary slightly and since the correct functioning of the modulator depends upon a constant input signal, Q2 is inserted between the oscillator output and the modulator input. The signal is led from the collector of Q2 via a low-pass filter, L1 and C14, which suppresses any har-



monics of the fundamental oscillator frequency. From there the signal is introduced to the base of the modulator, Q3.

Since proper functioning of the modulator likewise depends upon the load impedance, buffer Q4 is inserted between the modulator output and the multiplier chain. Q4 also limits any amplitude modulation present in the signal before it is applied to the first multiplier.

Modulator

The phase modulator stage is built around transistor Q3 and can be considered as a voltage divider consisting of the two identical capacitors, C13 and C15, and transistor Q3, over which the output signal is taken off.

Base voltage for Q3 is applied from the joint of C13 and C15, whereby Q3 appears as an inductance having the same reactance as one of the capacitors. In addition to the reactive current in the transistor there is also a resistive component which is determined by the transistor's operating point; this resistive component can be considered as a resistor in series with the inductance.

The phase shift between the modulator input signal applied to C13 and the modulator output signal taken off across Q3 is therefore dependent upon the transistor's operating point.

Applying a modulation signal to the emitter of Q3 will shift the operating point (transfer characteristic) coincident with the modulating signal, thus achieving the desired phase modulation.

Frequency Multiplication Stages

The frequency multiplier chain is composed of a tripler and two doublers, giving a multiplication factor of 12, resulting in the required antenna frequency of 146 to 174 MHz. The first multiplier, Q5 and Q6, is a balanced tripler configuration where the even-numbered harmonics of the fundamental frequency are suppressed. The signal from the second buffer stage, Q4, is applied to the base of Q5 through

C20. The base of Q6 is grounded, as far as the signal is concerned, through C21 and C22. Since R23 is common to both transistor emitters, any signal through Q5 will also be across the emitter-base circuit of Q6 with the proper polarity to drive the stage in push-pull.

Two tuned LC circuits, L4 and C26, and L5 and C31, form a capacitive coupled band-pass filter tuned to the third harmonic of the frequency at the tripler input.

C32 and C33 pass the signal on to the succeeding multiplier, Q7 and Q8. This stage is a balanced doubler, suppressing the odd harmonics of the input signal frequency. Tuned circuits L6 and C36, and L7 and C39 in the collector path also make up a capacitive coupled band-pass filter, this time tuned to the second harmonic of the frequency at its input. The signal is fed on through C38 and C40 to the second doubler, Q9 and Q10, also operating as a balanced frequency doubler.

The collector circuit consisting of L8, C44 and C42 is, of course, tuned to the second harmonic of the input frequency. The collector circuit and the tuned circuit L9 and C46 in the base circuit of the following amplifier stage form another capacitive coupled band-pass filter. C45 is a coupling capacitor. L9 and C46 make up a series resonant circuit as seen from the base of Q11.

The output stage, Q11, amplifies the approx. 20 mW output signal from the final frequency multiplier to the required exciter output level of approx. 80 mW. Finally, the signal is fed from the collector of the transistor through the resonant circuit consisting of L10, C50, C52 and C53 to the output terminals. The output transistor collector impedance is transformed down to an output impedance of 50 Ω by capacitively tapping the resonant circuit.

The bandpass filters determine the over-all bandwidth of the exciter, just as they also suppress undesired harmonics generated during frequency multiplication. They all employ close-to-critical coupling.

Technical Specifications

Supply Voltage

9 V

Current Consumption

80 mA

Frequency Range

146 to 174 MHz

Frequency Multiplication Factor

3 x 2 x 2 = 12

Crystal Frequency Band

12.166 - 14.500 MHz

Bandwidth (3 dB)

5 MHz

Output Power

100 mW

Load Impedance

50 Ω

AF Input Impedance

1 k Ω

Modulation Sensitivity

Required e.m.f. from a 600 Ω generator:
(for $\Delta f = 3.5$ kHz at 1 kHz) : 210 mV

Modulation Distortion

Measured without de-emphasis,
at $f = 3.5$ kHz / 1 kHz : 2.5 %

Oscillator Frequency Adjustable by

$$\frac{\Delta f}{f} \geq \pm 30 \times 10^{-6}$$

Frequency Stability

for voltage variations of 2.5 %

$$\frac{\Delta f}{f} \leq \pm 0.1 \times 10^{-6}$$

for temperatures between -25° and $+75^{\circ}$ C

$$\frac{\Delta f}{f} \leq \pm 2 \times 10^{-6}$$

Input Impedance for External Oscillators

470 Ω // 22 pF

Sensitivity at Input for External Oscillators

(required input voltage) : 100 mV

Crystal Types

98-12, 98-20, 98-26

Temperature Range

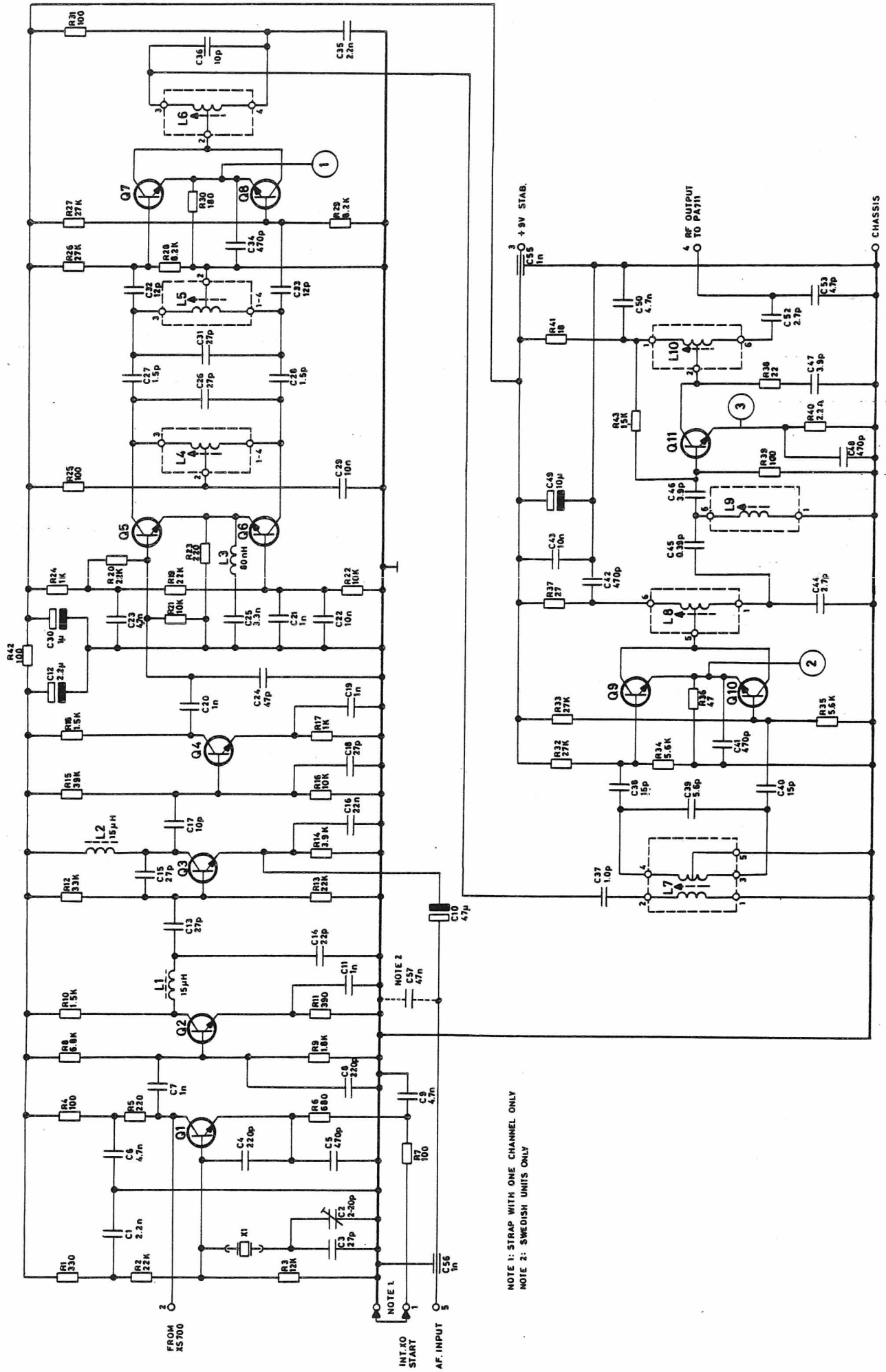
operating range -25° to $+70^{\circ}$ C

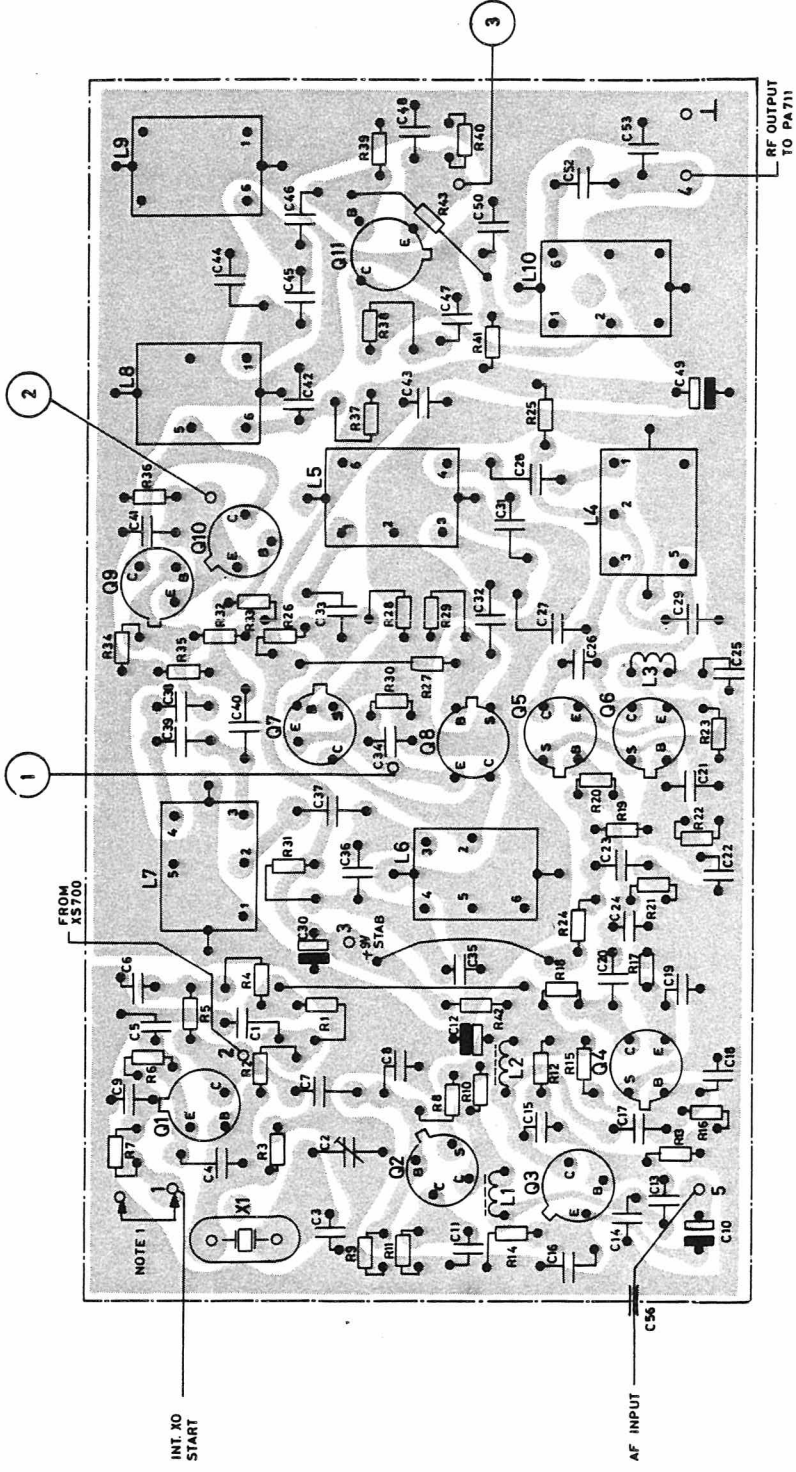
functioning range -30° to $+80^{\circ}$ C

Mechanical Dimensions

Metal enclosure: 24.7 x 50.8 x 91.5 mm

Printed circuit board: 48.3 x 88.9 mm





PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE

EXCITER EX711

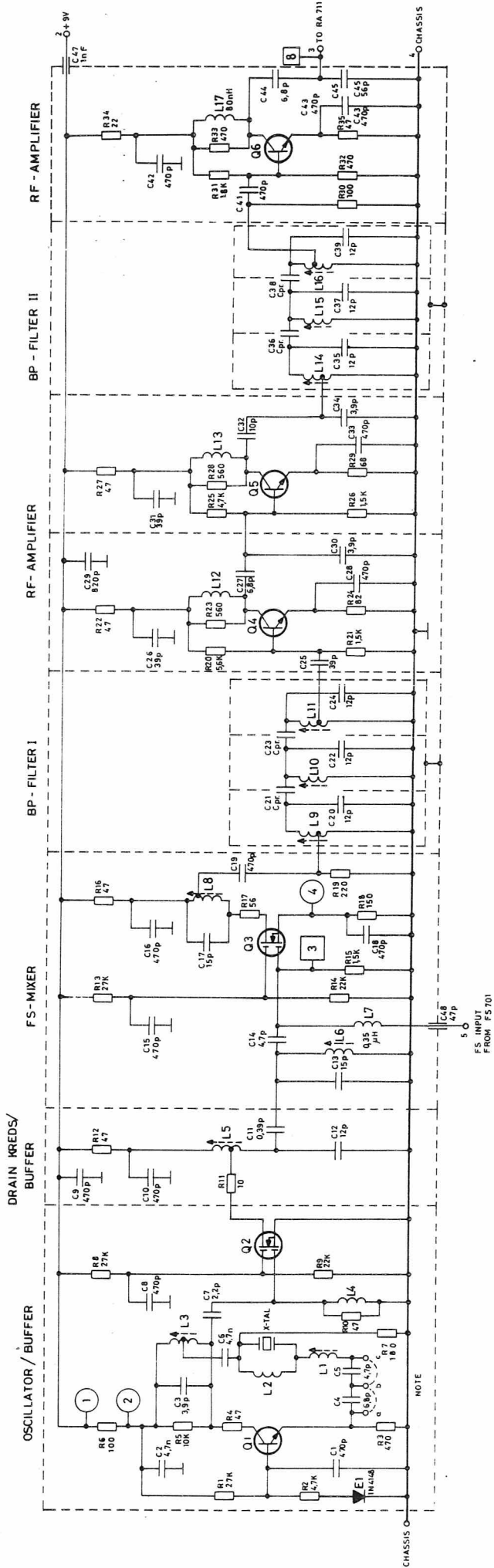
D401.521/2

TYPE	NO.	CODE	DATA
EX711		10.2570	Exciter Unit
	C1	76.5059	2.2 nF 10% polyester, FL
	C2	78.5046	2-20 pF trimmer
	C3	74.5192	27 pF 5% ceram TB
	C4	76.5104	220 pF 2.5% polystyr TB
	C5	76.5106	470 pF 2.5% polystyr TB
	C6	76.5061	4.7 nF 10% polyester FL
	C7	74.5155	1 nF -20 +80% ceram PL
	C8	76.5104	220 pF 2.5% polystyr TB
	C9	76.5061	4.7 nF 10% polyester, FL
	C10	73.5124	47 μ F 20% tantal
	C11	76.5069	1 nF 10% polyester, FL
	C12	73.5129	2.2 μ F -20 +50% tantal
	C13	74.5107	27 pF 5% ceram
	C14	74.5106	22 pF 5% ceram
	C15	74.5107	27 pF 5% ceram
	C16	76.5071	22 nF 10% polyester, FL
	C17	74.5135	10 pF 5% ceram DI
	C18	74.5107	27 pF 5% ceram
	C19	76.5069	1 nF 10% polyester, FL
	C20	74.5155	1 nF -20 +80% ceram PL
	C21	74.5155	1 nF -20 +80% ceram PL
	C22	76.5070	10 nF 10% polyester FL
	C23	76.5061	4.7 nF 10% polyester, FL
	C24	74.5186	47 pF 10% ceram PL
	C25	76.5060	3.3 nF 10% polyester, FL
	C26	74.5107	27 pF 5% ceram
	C27	74.5125	1.5 pF \pm 0.25 pF ceram BD
	C28	74.5125	1.5 pF \pm 0.25 pF ceram BD
	C29	76.5070	10 nF 10% polyester, FL
	C30	73.5135	1 μ F -20 +50% tantal
	C31	74.5107	27 pF 5% ceram DI
	C32	74.5136	12 pF 5% ceram DI
	C33	74.5136	12 pF 5% ceram DI
	C34	74.5161	470 pF -20 +80% ceram PL
	C35	76.5059	2.2 nF 10% polyester FL
	C36	74.5135	10 pF 5% ceram DI
	C37	74.5123	1.0 pF \pm 0.25 pF ceram BD
	C38	74.5137	15 pF 5% ceram DI
	C39	74.5132	5.6 pF \pm 0.25 pF ceram DI
	C40	74.5137	15 pF 5% ceram DI
	C41	74.5161	470 pF -20 +80% ceram PL
	C42	74.5161	470 pF -20 +80% ceram PL
	C43	76.5070	10 nF 10% polyester, PL
	C44	74.5128	2.7 pF \pm 0.25 pF ceram DI
	C45	74.5120	0.39 pF \pm 0.1 pF ceram BD
	C46	74.5130	3.9 \pm 0.25 pF ceram DI

TYPE	NO.	CODE	DATA
	C47	74.5130	3.9 pF \pm 0.25 pF ceram DI
	C48	74.5161	470 pF -20 +80% ceram PL
	C49	73.5109	10 μ F 20% tantal
	C50	76.5061	4.7 nF 10% polyester, FL
	C51		
	C52	74.5128	2.7 pF \pm 0.25 pF ceram DI
	C53	74.5131	4.7 pF \pm 0.25 pF ceram DI
	C54		
	C55	74.5167	1 nF -20 +80% ceram FT
	C56	74.5167	1 nF -20 +80% ceram FT
	C57	76.5072	47nF 10% Polyester, FL (Swedish units only)
	R1	80.5243	330 Ω 5% carbon film
	R2	80.5265	22 k Ω 5% "
	R3	80.5262	12 k Ω 5% "
	R4	80.5237	100 Ω 5% "
	R5	80.5241	220 Ω 5% "
	R6	80.5247	680 Ω 5% "
	R7	80.5237	100 Ω 5% "
	R8	80.5259	6.8 k Ω 5% "
	R9	80.5252	1.8 k Ω 5% "
	R10	80.5251	1.5 k Ω 5% "
	R11	80.5244	390 Ω 5% "
	R12	80.5267	33 k Ω 5% "
	R13	80.5265	22 k Ω 5% "
	R14	80.5256	3.9 k Ω 5% "
	R15	80.5268	39 k Ω 5% "
	R16	80.5261	10 k Ω 5% "
	R17	80.5249	1 k Ω 5% "
	R18	80.5251	1.5 k Ω 5% "
	R19	80.5265	22 k Ω 5% "
	R20	80.5265	22 k Ω 5% "
	R21	80.5261	10 k Ω 5% "
	R22	80.5261	10 k Ω 5% "
	R23	80.5241	220 Ω 5% "
	R24	80.5249	1 k Ω 5% "
	R25	80.5237	100 Ω 5% "
	R26	80.5266	27 k Ω 5% "
	R27	80.5266	27 k Ω 5% "
	R28	80.5260	8.2 k Ω 5% "
	R29	80.5260	8.2 k Ω 5% "
	R30	80.5240	180 Ω 5% "
	R31	80.5237	100 Ω 5% "
	R32	80.5266	27 k Ω 5% "

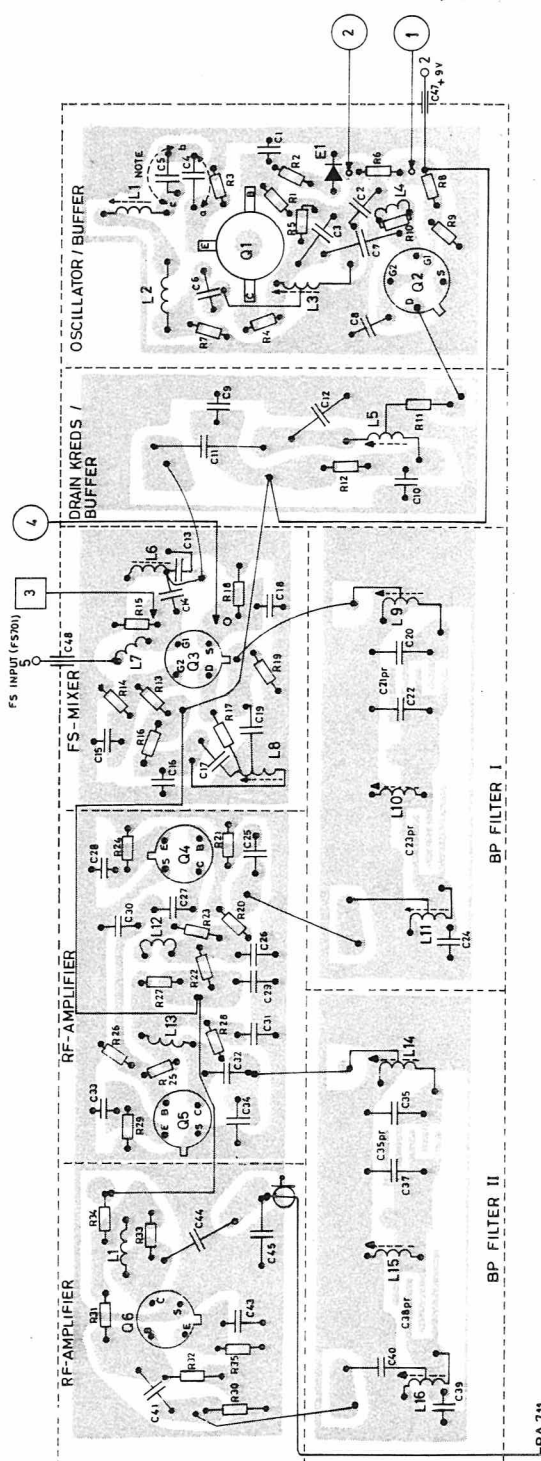
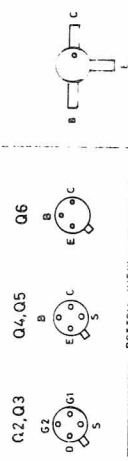
EXCITER UNIT
STYRESENDER
EX711

X401.371/2



NOTE:

FREQUENCY FREKVENNS	STRAP STRÄPNING
UP / OP	NONE / INGEN
NORMAL	a - b
DOWN / NED	b - c



EXCITER
STYRESENDER

EX 712

D.4.01.B.471

TYPE	NO.	CODE	DATA
EX712		10. 2936	Exciter
	C1	74. 5162	ceram DI 400V
	C2	74. 5108	ceram PL 20V
	C3	74. 5302	ceram PL 63V
	C4	74. 5321	ceram PL 100V
	C5	74. 5318	ceram PL 100V
	C6	74. 5108	ceram PL 20V
	C7	74. 5299	ceram PL 63V
	C8	74. 5161	ceram PL 63V
	C9	74. 5162	ceram DI 400V
	C10	74. 5162	ceram DI 400V
	C11	74. 5129	ceram BD 250V
	C12	74. 5135	ceram DI 125V
	C13	74. 5136	ceram DI 125V
	C14	74. 5131	ceram DI 250V
	C15	74. 5162	ceram DI 400V
	C16	74. 5162	ceram DI 400V
	C17	74. 5136	ceram DI 125V
	C18	74. 5162	ceram DI 400V
	C19	74. 5161	ceram PL 63V
	C20	74. 5308	ceram PL 63V
	C21	74. 5308	ceram PL 63V
	C22	74. 5308	ceram PL 63V
	C23	74. 5308	ceram PL 63V
	C24	74. 5308	ceram PL 63V
	C25	74. 5316	ceram PL 63V
	C26	74. 5316	ceram PL 63V
	C27	74. 5305	ceram PL 63V
	C28	74. 5162	ceram DI 400V
	C29	74. 5314	ceram PL 63V
	C30	74. 5302	ceram PL 63V
	C31	74. 5316	ceram PL 63V
	C32	74. 5307	ceram PL 63V
	C33	74. 5162	ceram PL 63V
	C34	74. 5302	ceram DI 400V
	C35	74. 5308	ceram PL 63V
	C36	74. 5308	ceram PL 63V
	C37	74. 5308	ceram PL 63V
	C38	74. 5308	ceram PL 63V
	C39	74. 5308	ceram PL 63V
	C40	74. 5161	ceram PL 63V
	C41	74. 5161	ceram PL 63V
	C42	74. 5162	ceram DI 400V
	C43	74. 5133	ceram DI 250V
	C44	74. 5132	ceram DI 250V
	C45	74. 5132	ceram DI 250V

TYPE	NO.	CODE	DATA
	C46	74. 5198	Not used
	C47	74. 5323	1nF -20/+80%
	C48		47pF 20%
	R1	80. 5066	27 K Ω 5%
	R2	80. 5057	4.7 K Ω 5%
	R3	80. 5045	470 Ω 5%
	R4	80. 5033	47 Ω 5%
	R5	80. 5061	10 K Ω 5%
	R6	80. 5237	100 Ω 5%
	R7	80. 5040	180 Ω 5%
	R8	80. 5066	27 K Ω 5%
	R9	80. 5065	22 K Ω 5%
	R10	80. 5033	47 Ω 5%
	R11	80. 5025	10 Ω 5%
	R12	80. 5233	47 Ω 5%
	R13	80. 5066	27 K Ω 5%
	R14	80. 5065	22 K Ω 5%
	R15	80. 5051	1.5 K Ω 5%
	R16	80. 5033	47 Ω 5%
	R17	80. 5034	56 Ω 5%
	R18	80. 5039	150 Ω 5%
	R19	80. 5041	220 Ω 5%
	R20	80. 5058	5.6 K Ω 5%
	R21	80. 5051	1.5 K Ω 5%
	R22	80. 5033	47 Ω 5%
	R23	80. 5054	560 Ω 5%
	R24	80. 5036	82 Ω 5%
	R25	80. 5057	4.7 K Ω 5%
	R26	80. 5051	1.5 K Ω 5%
	R27	80. 5033	47 Ω 5%
	R28	80. 5046	560 Ω 5%
	R29	80. 5035	68 Ω 5%
	R30	80. 5037	100 Ω 5%
	R31	80. 5052	1.8 K Ω 5%
	R32	80. 5045	470 Ω 5%
	R33	80. 5045	470 Ω 5%
	R34	80. 5029	22 Ω 5%
	R35	80. 5033	47 Ω 5%
	L1	61. 1234	RF coil

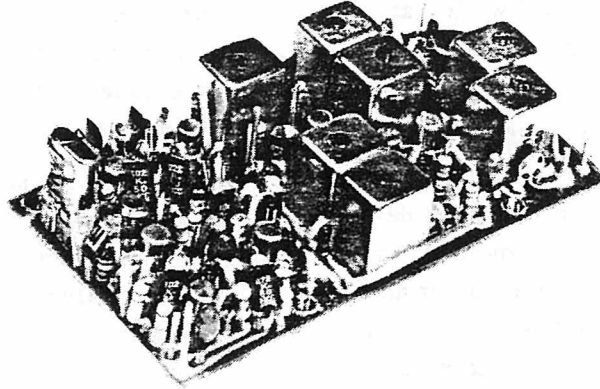
EXCITER

STYRESENDER

EX712

X401.945

EXCITER EX731



Description

General

The exciter must modulate and convert the signal from the transmitter oscillator so the frequency and amplitude are suitable for driving the power amplifier, PA731.

EX731 contains the following stages:

- an oscillator (for single channel service)
- a phase modulator with associated buffer stages
- a frequency tripler
- a frequency doubler
- an amplifier.

The oscillator signal is sent through the modulators and buffers and is next tripled and finally doubled. The result is a signal at the transmitter antenna frequency (68 to 88 MHz).

The amplifier stage in the output of the exciter raises the signal to the level required to drive the power amplifier (80 mW).

While in the phase modulators the oscillator signal, still at its fundamental frequen-

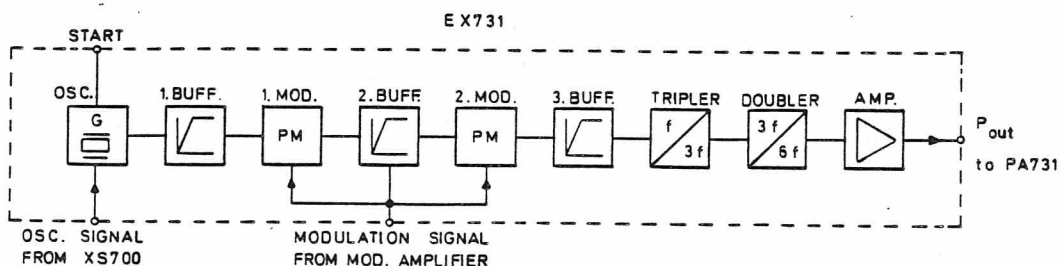
cy, is phase modulated with the audio frequency signal from the modulation amplifier in CF701.

For multichannel service the built-in oscillator can be switched out and another oscillator (and frequency) switched in from the oscillator switching unit, XS701.

Oscillator.

To start the oscillator, the emitter circuit of Q1 must be returned to ground via terminal 1. For single channel service the terminal is tied to ground right in the EX unit.

In the case of multichannel service the emitter of Q1 is grounded through the control panel. When one of the oscillators in the XS unit is functioning, the emitter connection to Q1 is open and the signal from XS is applied to the exciter at terminal 2. R5 in EX731 serves as a collector resistor common to all of the oscillators.



Modulator and Buffer Stages

Buffer amplifiers Q2, Q4 and Q6 are required to keep the RF input signal to the modulators at a constant level while, at the same time, presenting a constant load impedance to the modulators.

The output signals from the different oscillators can vary slightly and since the correct functioning of the modulators depends upon a constant input signal, Q2 is inserted between the oscillator output and the modulators. The signal is led from the collector of Q2 via a low-pass filter, L1 and C11, which suppresses any harmonics of the fundamental oscillator frequency. From there the signal is introduced to the base of the modulator, Q3.

Buffer amplifier stage Q4 is identical to Q2. Its purpose is to isolate the two modulators from each other.

Since proper functioning of the modulator likewise depends upon the load impedance, buffer Q6 is inserted between the modulator output and the multiplier chain. Q6 also limits any amplitude modulation present in the signal before it is applied to the first multiplier.

In order to achieve sufficient phase deviation with minimum distortion the phase modulator is designed as two identical modulator stages (Q3 and Q5) in series. The modulation signal is fed to both transistor emitters at the same time.

Since the two modulators are identical we will consider only Q3 here.

The phase modulator can be considered as a voltage divider consisting of the two identical capacitors, C12 and C13, and transistor Q3, over which the output signal is taken off.

Base voltage for Q3 is applied from the joint of C12 and C13, whereby Q3 appears as an inductance having the same reactance as one of the capacitors. In addition to the reactive current in the transistor there is also a resistive component which is determined by the transistor's operating point;

this resistive component can be considered as a resistor in series with the inductance.

The phase shift between the modulator input signal applied to C12 and the modulator output signal taken off across Q3 is therefore dependent upon the transistor's operating point.

Applying a modulation signal to the emitter of Q3 will shift the operating point (transfer characteristic) coincident with the modulating signal, thus achieving the desired phase modulation.

Frequency Multiplication Stages

The frequency multiplier chain is composed of a tripler and a doubler, giving a multiplication factor of 6, resulting in the required antenna frequency of 68 to 88 MHz. The first multiplier, Q5 and Q6, is a balanced tripler figuration where the even-numbered harmonics of the fundamental frequency are suppressed. The signal from the third buffer stage, Q6, is applied to the balanced tripler, Q7 and Q8, through transformer L5.

Two tuned LC circuits, L6 and C35, and L7 and C38, form a capacitive coupled band-pass filter tuned to the third harmonic of the frequency at the tripler input.

C39 and C40 pass the signal on to the succeeding multiplier, Q9 and Q10. This stage is a balanced doubler, suppressing the odd harmonics of the input signal frequency.

Tuned circuits L8, C43 and L9, and C45 and C46 in the collector path also make up a capacitive coupled band-pass filter, this time tuned to the second harmonic of the frequency at its input. The signal has now reached the final antenna frequency of 68 to 88 MHz and is applied to the output transistor, Q11.

The output stage, Q11, amplifies the approx. 15 mW output signal from the final frequency multiplier to the required exciter output level of approx. 80 mW. Finally, the signal is fed from the collector of the transistor through the resonant circuit consisting of

L10 and C49, and L11 and C51 and C52 to the output terminals. The output transistor collector impedance is transformed down to an output impedance of 50Ω by capacitively tapping the resonant circuit.

The band-pass filters determine the over-all bandwidth of the exciter, and they also suppress undesired harmonics generated during frequency multiplication. All of the band-pass filters employ close-to-critical coupling.

Technical Specifications

Supply Voltage

+9 V

Current Consumption

60 mA

Frequency Range

68 to 88 MHz

Frequency Multiplication Factor

6

Crystal Frequency Band

11.33 to 14.67

Band Width (3 dB)

3 MHz

Output Power

80 mW

Load Impedance

50Ω

AF Input Impedance

1 k Ω

Modulation Sensitivity

Required EMF from a 600Ω generator
(for $\Delta f = 3.5$ kHz at 1 kHz): 350 mV

Modulation Distortion

Measured without de-emphasis,
at $f = 3.5$ kHz / 1 kHz : 2.5%.

Oscillator frequency adjustable by:

$$\frac{\Delta f}{f} \geq \pm 30 \times 10^{-6}$$

Frequency Stability

for voltage variations of 2.5%:

$$\frac{\Delta f}{f} \leq \pm 0.1 \times 10^{-6}$$

for temperatures between -25° and $+75^{\circ}$ C:

$$\frac{\Delta f}{f} \leq \pm 2 \times 10^{-6}$$

Input Impedance for External Oscillators

$470 \Omega // 22$ pF

Sensitivity at Input for Ext. Oscillators

(required input voltage) : 100 mV

Crystal Types

98-12, 98-20, 98-26

Temperature Range

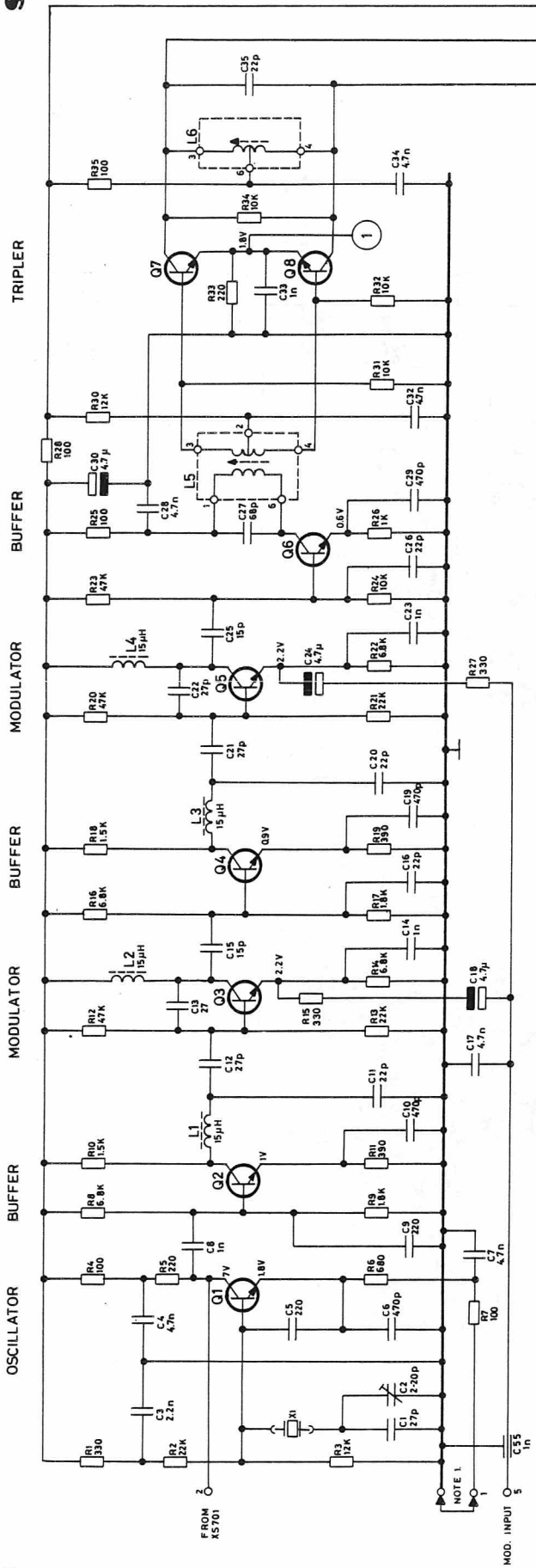
Operating range: -25° to $+70^{\circ}$ C

Functioning range: -30° to $+80^{\circ}$ C

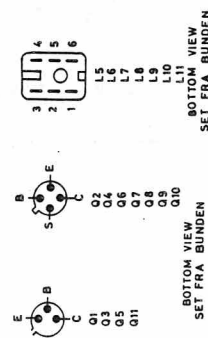
Mechanical Dimensions

Metal enclosure: 24.7 x 50.8 x 91.5 mm

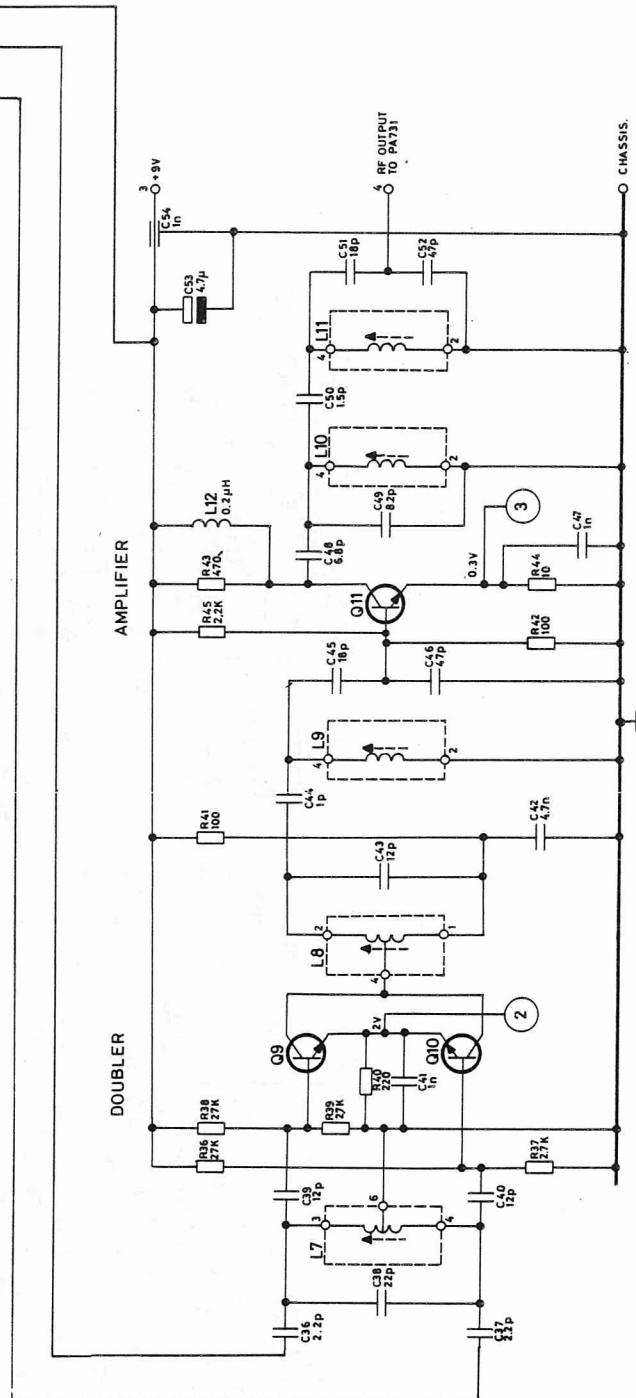
Printed circuit board: 48.3 x 88.9 mm



NOTE 1 - CONNECTION FOR 1 CHANNEL EQUIPMENT
 FORBIDENSE 11 KANAL UDSTRYR



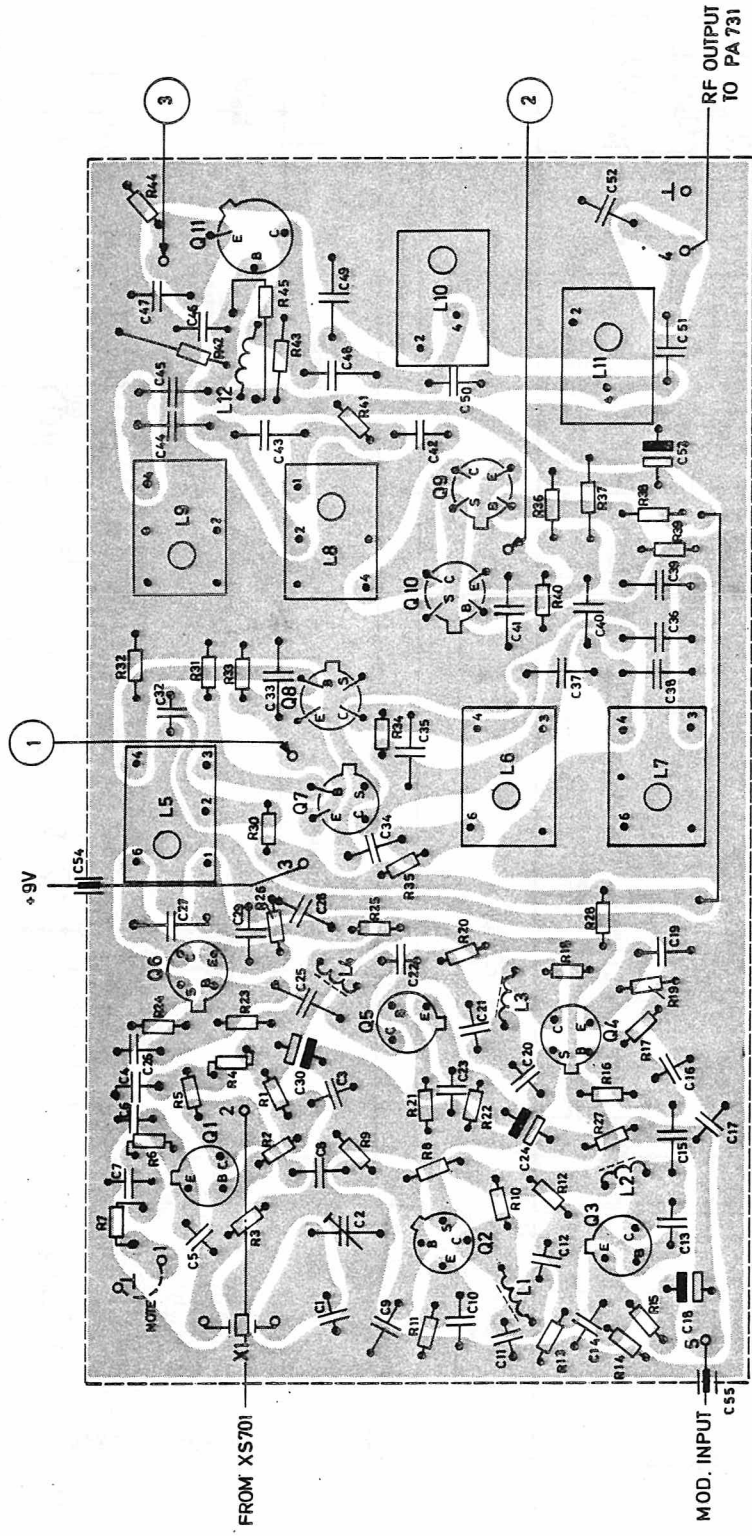
BOTTOM VIEW
 SET FRA BUNDEN.



EXCITER
 STYRESENDER

EX 731

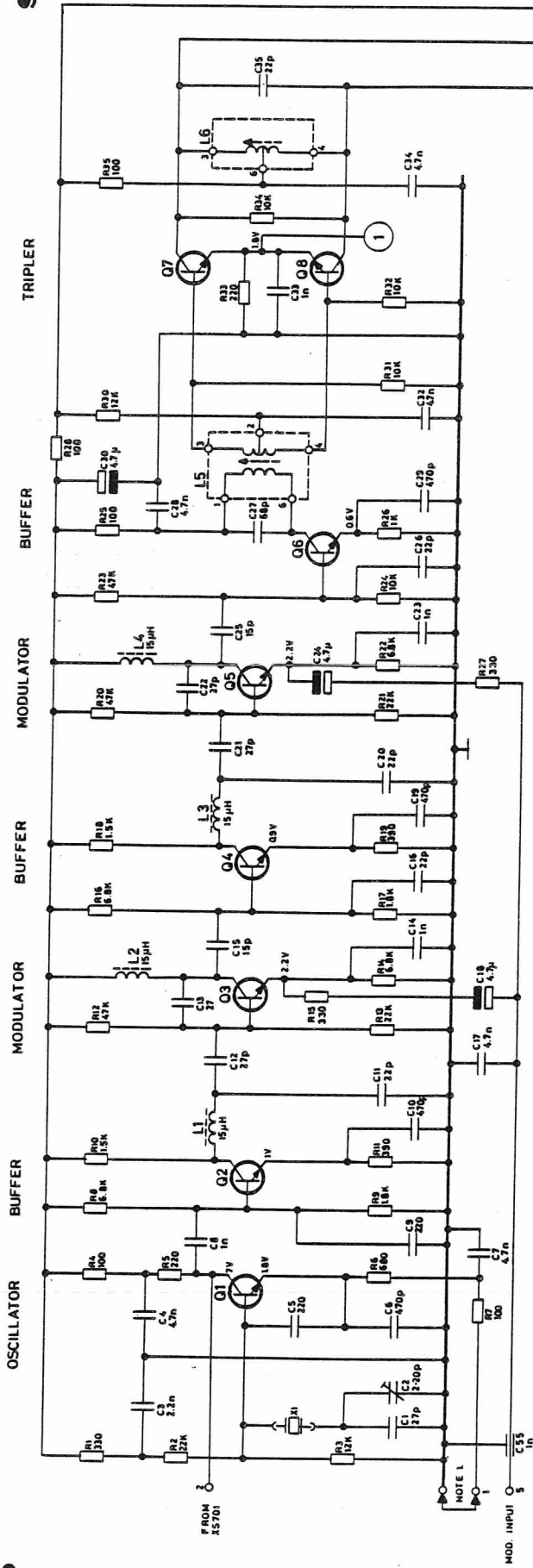
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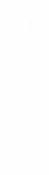
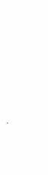
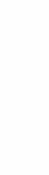
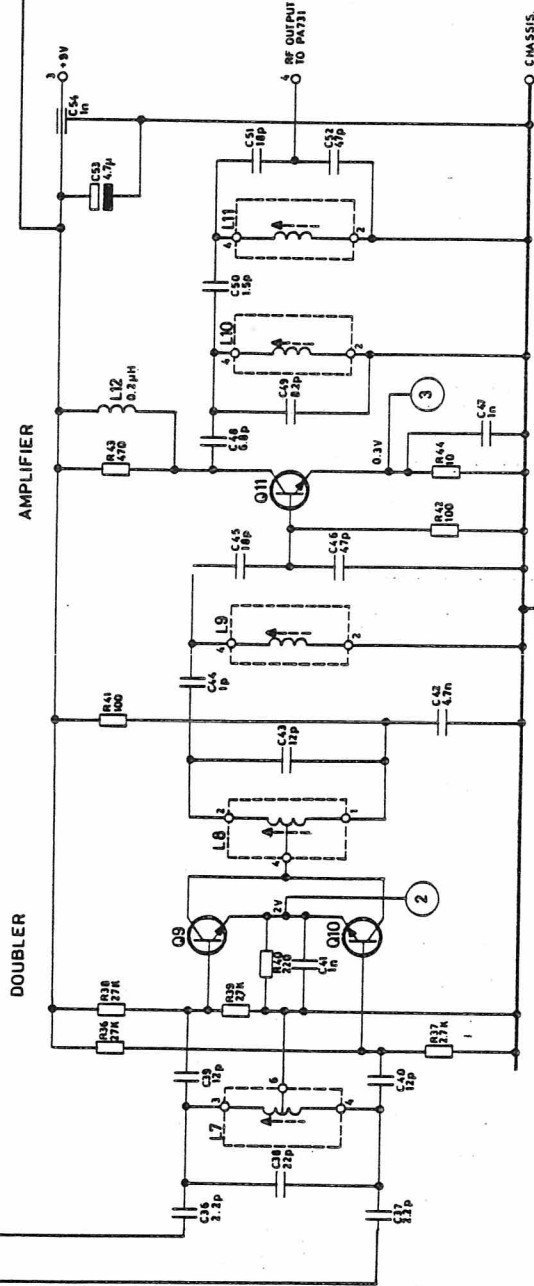
EXCITER
STYRESENDER

EX 731

D 401.524/3

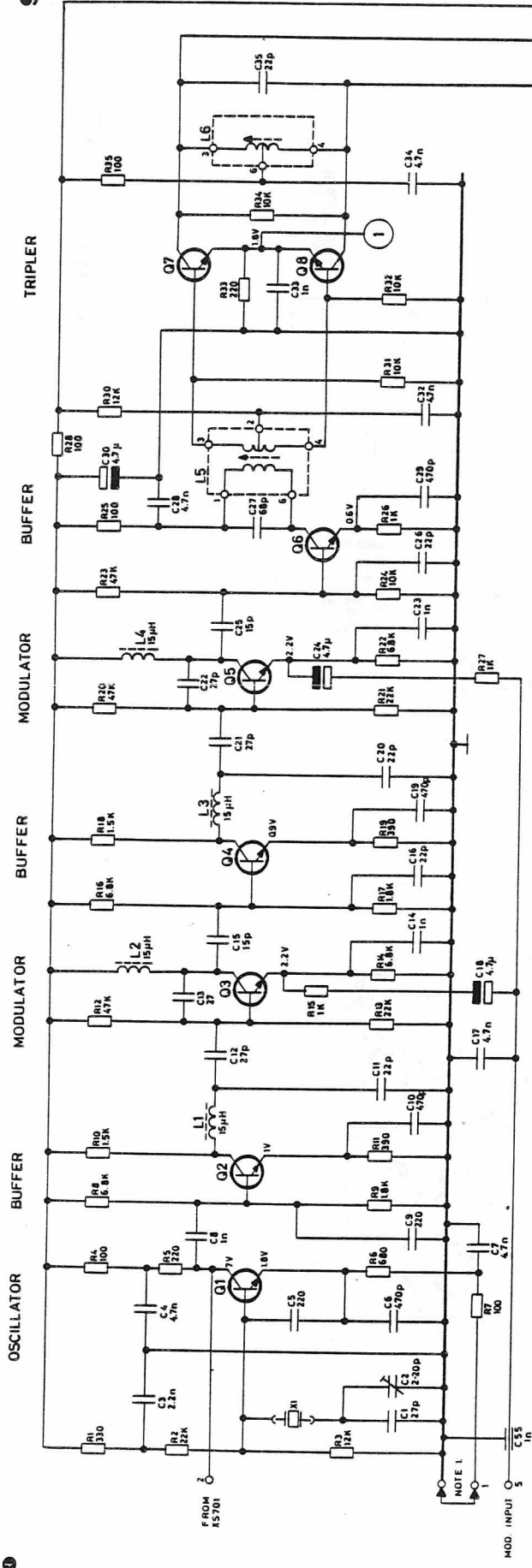


NOTE 1: CONNECTION FOR 1 CHANNEL EQUIPMENT FORBINOISE 11 MANAL UDSTRK

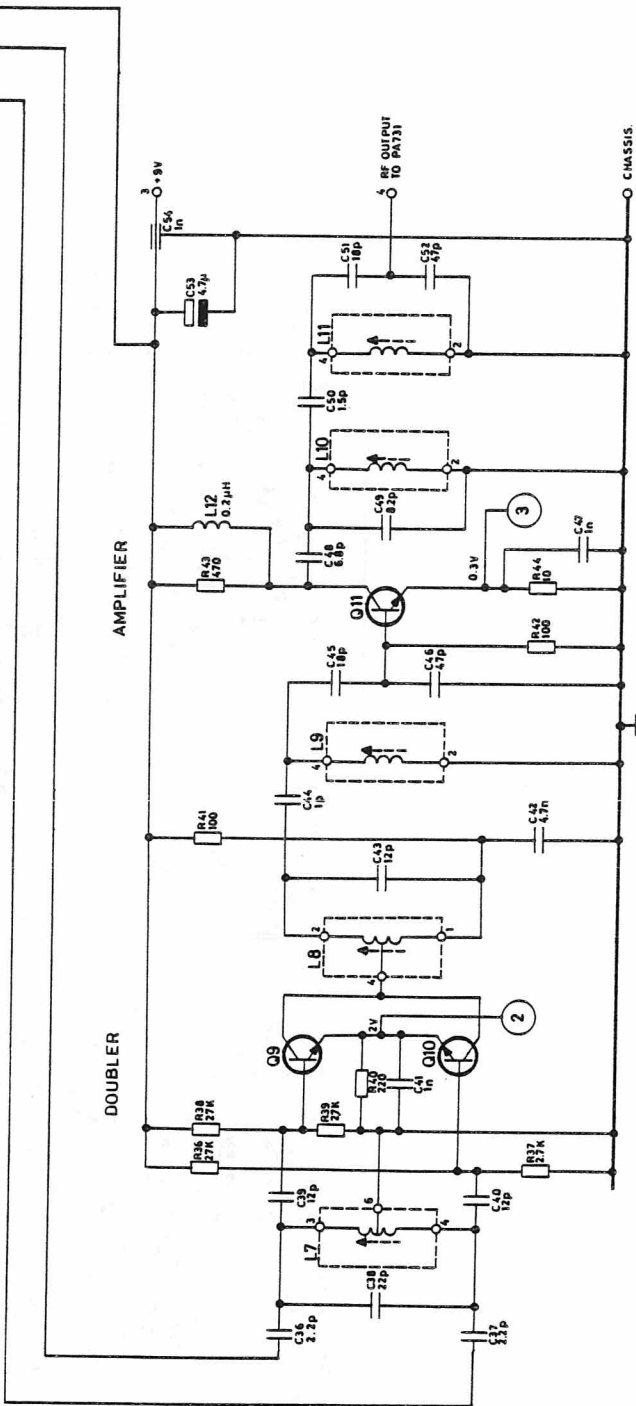


BOTTOM VIEW SET FRA BUNDEN

BOTTOM VIEW SET FRA BUNDEN



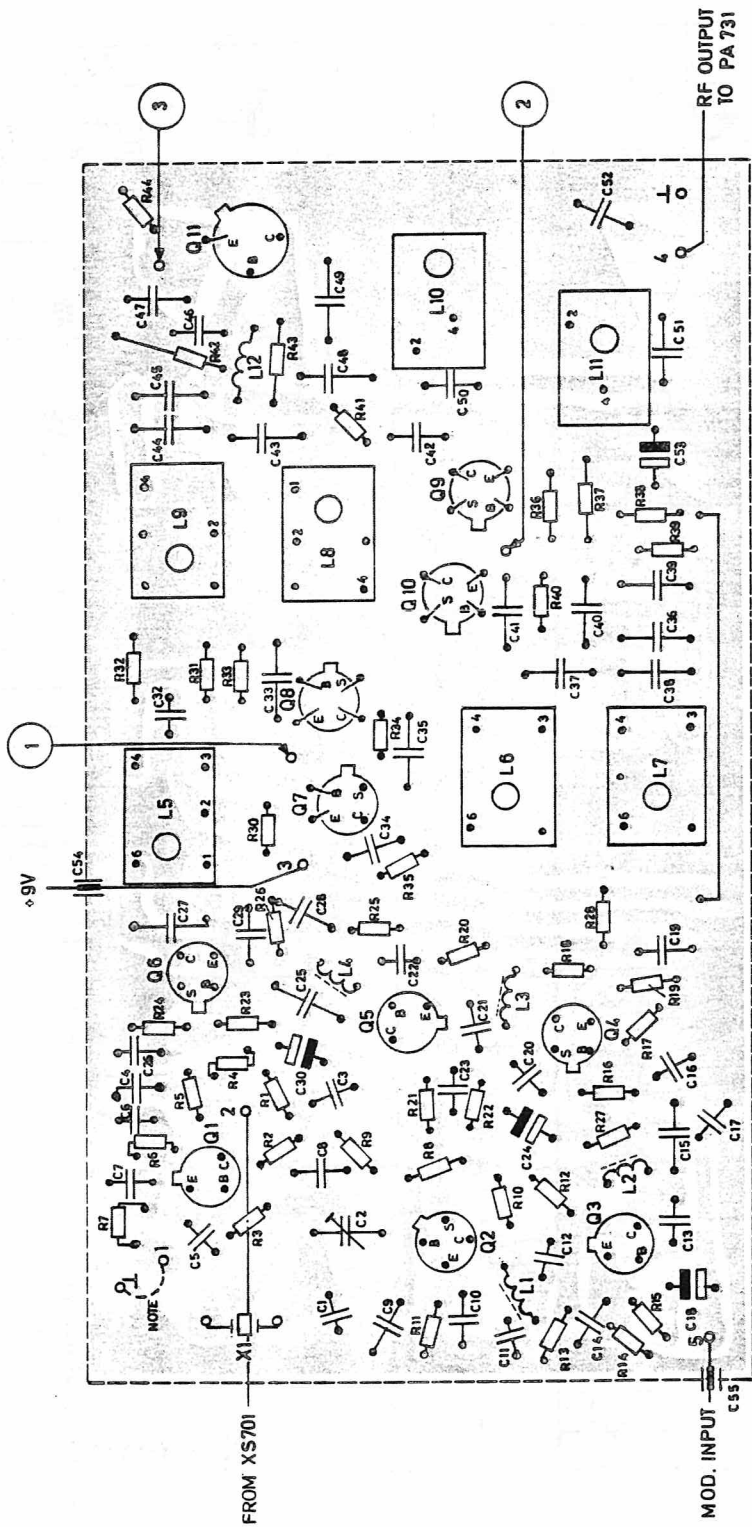
NOTE 1: CONNECTION FOR 1 CHANNEL EQUIPMENT
FORBINDELSE I 1 KANAL UDSTYR



EXCITER
STYRESENDER

EX 731

D401524



EXCITER
STYRESENDER

EX 731

D 401.524/2

TYPE	NO.	CODE	DATA
EX731		10.2673	Exciter Unit
	C1	74.5192	27pF 5% ceram TB 160V
	C2	78.5040	2-2pF trimmer 300V
	C3	76.5059	2.2nF 10% polyest. FL 50V
	C4	76.5061	4.7 nF 10% polyest 50V
	C5	76.5104	220 pF 2.5% polystyr TB 25V
	C6	76.5106	470pF 2.5% polystyr TB 25V
	C7	76.5061	4.7nF 10% polyest. FL 50V
	C8	76.5069	1nF 10% polyest. 50V
	C9	76.5104	220 pF 2.5% polystyr TB 25V
	C10	74.5161	470pF - 20+ 80% ceram PL 63V
	C11	74.5106	22pF 5% ceram TB 160V
	C12	74.5107	27pF 5% ceram TB 160V
	C13	74.5107	27pF 5% ceram TB 160V
	C14	76.5069	1nF 10% polyest. FL 50V
	C15	74.5137	15pF 5% ceram DI 125V
	C16	74.5106	22pF 5% ceram TB 160V
	C17	76.5061	4.7nF 10% polyest. FL 50V
	C18	73.5126	4.7μF 20% tantal 35V
	C19	74.5161	470pF - 20+80% ceram PL 63V
	C20	74.5106	22pF 5% ceram TB 160V
	C21	74.5107	27pF 5% ceram TB 160V
	C22	74.5107	27pF 5% ceram TB 160V
	C23	76.5069	1nF 10% polyest. FL 50V
	C24	73.5126	4.7μF 20% tantal 35V
	C25	74.5137	15pF 5% ceram DI 125V
	C26	74.5106	22pF 5% ceram TB 160V
	C27	76.5101	68pF 2.5% polystyr TB 30V
	C28	76.5061	4.7nF 10% polyest FL 50V

**EXCITER
STYRESENDER**

EX731

X 401.786

page 1 of 3

TYPE	NO.	CODE	DATA
	C29	74.5161	470pF - 20+80% ceram PL 63V
	C30	73.5126	4.7μF 20% tantal 35V
	C31		
	C32	76.5061	4.7nF 10% polyest 35V
	C33	74.5155	1nF - 20+80% ceram PL 63V
	C34	76.5061	4.7nF 10% polyest FL 50V
	C35	74.5106	22pF 5% ceram TB 160V
	C36	74.5127	2.2pF± 0.25pF ceram DI 250V
	C37	74.5127	2.2pF± 0.25pF ceram DI 250V
	C38	74.5106	22pF 5% ceram TB 160V
	C39	74.5136	12pF 5% ceram DI 250V
	C40	74.5136	12pF 5% ceram DI 250V
	C41	74.5155	1nF - 20+80% ceram PL 63V
	C42	76.5061	4.7nF 10% polyest. FL 50V
	C43	74.5136	12pF 5% ceram DI 250V
	C44	74.5123	1.0pF± 0.25pF ceram BD 250V
	C45	74.5138	18pF 5% ceram DI 125V
	C46	76.5090	47pF 2.5% polyest TB 63V
	C47	74.5155	1nF - 20+ 80% ceram PL 63V
	C48	74.5133	6.8pF ± 0.25pF ceram DI 250V
	C49	74.5134	8.2pF ± 0.25pF ceram DI 250V
	C50	74.5125	1.5pF ± 0.25pF ceram BD 250V
	C51	74.5138	18pF 5% ceram DI 125V
	C52	76.5090	47pF 2.5% polystyr TB 63V
	C53	73.5126	4.7μF 20% tantal 35V
	C54	74.5167	1nF - 20+80% ceram FT 300V

Storno**Storno**

TYPE	NO.	CODE	DATA
	C55	74.5167	1nF - 20+80% ceram FT 300V
	R1	80.5243	330k 5% carbon film 1/8W
	R2	80.5265	22k 5% carbon film 1/8W
	R3	80.5262	12k 5% carbon film 1/8W
	R4	80.5237	100k 5% carbon film 1/8W
	R5	80.5241	220k 5% carbon film 1/8W
	R6	80.5247	680k 5% carbon film 1/8W
	R7	80.5237	100k 5% carbon film 1/8W
	R8	80.5259	6.8k 5% carbon film 1/8W
	R9	80.5252	1.8k 5% carbon film 1/8W
	R10	80.5251	1.5k 5% carbon film 1/8W
	R11	80.5244	390k 5% carbon film 1/8W
	R12	80.5269	47k 5% carbon film 1/8W
	R13	80.5265	22k 5% carbon film 1/8W
	R14	80.5259	6.8k 5% carbon film 1/8W
	R15	80.5249	1k 5% carbon film 1/8W
	R16	80.5259	6.8k 5% carbon film 1/8W
	R17	80.5252	1.8k 5% carbon film 1/8W
	R18	80.5251	1.5k 5% carbon film 1/8W
	R19	80.5244	390k 5% carbon film 1/8W
	R20	80.5269	47k 5% carbon film 1/8W
	R21	80.5265	22k 5% carbon film 1/8W
	R22	80.5259	6.8k 5% carbon film 1/8W
	R23	80.5269	47k 5% carbon film 1/8W
	R24	80.5261	10k 5% carbon film 1/8W
	R25	80.5237	100k 5% carbon film 1/8W
	R26	80.5249	1k 5% carbon film 1/8W
	R27	80.5249	1k 5% carbon film 1/8W
	R28	80.5237	100k 5% carbon film 1/8W

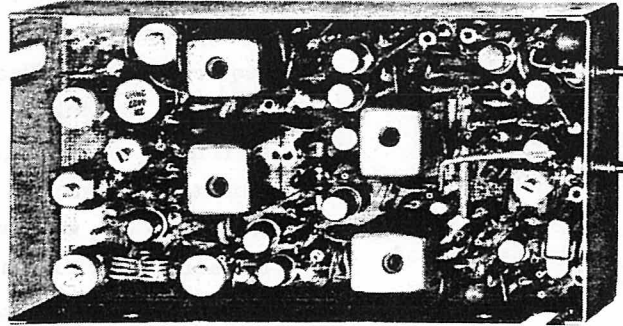
TYPE	NO.	CODE	DATA
	R29	80.5262	12k 5% carbon film 1/8W
	R30	80.5261	10k 5% carbon film 1/8W
	R31	80.5261	10k 5% carbon film 1/8W
	R32	80.5241	220k 5% carbon film 1/8W
	R33	80.5261	10k 5% carbon film 1/8W
	R34	80.5237	100k 5% carbon film 1/8W
	R35	80.5266	27k 5% carbon film 1/8W
	R36	80.5254	2.7k 5% carbon film 1/8W
	R37	80.5266	27k 5% carbon film 1/8W
	R38	80.5254	2.7k 5% carbon film 1/8W
	R39	80.5241	220k 5% carbon film 1/8W
	R40	80.5237	100k 5% carbon film 1/8W
	R41	80.5237	100k 5% carbon film 1/8W
	R42	80.5245	470k 5% carbon film 1/8W
	R43	80.5225	10k 5% carbon film 1/8W
	R44	80.5225	10k 5% carbon film 1/8W
	L1	63.5007	15μH 10% RF choke 0.5A
	L2	63.5007	15μH 10% RF choke 0.5A
	L3	63.5007	15μH 10% RF choke 0.5A
	L4	63.5007	15μH 10% RF choke 0.5A
	L5	61.1169	RF coil 11.3 - 14.7MHz
	L6	61.1168	RF coil 34 - 44MHz
	L7	61.1168	RF coil 34 - 44 MHz
	L8	61.1167	RF coil 68 - 88 MHz
	L9	61.1166	RF coil 68 - 88MHz

**EXCITER
STYRESENDER
EX731**

X401.786

page 2 of 3

EXCITER EX761



Description

General

The exciter must modulate and convert the signal from the transmitter oscillator so the frequency and amplitude are suitable for driving the power amplifier, PA761.

EX761 contains the following stages:

- an oscillator (for single channel service)
- a phase modulator with associated buffer stages
- two frequency triplers
- two frequency doublers
- an amplifier.

After passing through the buffer stage, the oscillator signal becomes phase modulated, goes through another buffer, then is multiplied 36 times, being first tripled, then doubled then tripled again, and finally doubled once more. The result is a signal at the transmitter antenna frequency (420 to 470 MHz.)

While in the phase modulator the oscillator signal, still at its fundamental frequency, is phase modulated with the audio frequency signal from the modulation amplifier in CF701.

For multichannel service the built-in oscillator can be switched out and another oscillator (and frequency) switched in from the oscillator switching unit, XS701 or XS702.

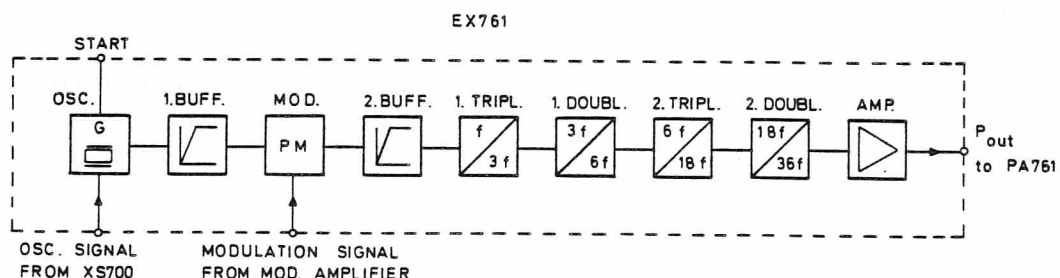
Oscillator

To start the oscillator, the emitter circuit of Q1 must be returned to ground via terminal 1. For single channel service the terminal is tied to ground right in the EX unit.

In the case of multichannel service the emitter of Q1 is grounded through the control panel. When one of the oscillators in the XS unit is functioning, the emitter connection to Q1 is open and the signal from XS is applied to the exciter at terminal 2. R5 in EX711 serves as a collector resistor common to all of the oscillators.

Buffer Stages

Buffer Q2 is required to keep the RF input signal to the modulator at a constant level while Q4 must present a constant load impedance to the modulator.



The output signals from the different oscillators can vary slightly and since the correct functioning of the modulator depends upon a constant input signal, Q2, is inserted between the oscillator output and the modulator input. The signal is led from the collector of Q2 via a low-pass filter, L1 and C11, which suppresses any harmonics of the fundamental oscillator frequency. From there the signal is introduced to the base of the modulator, Q3.

Since proper functioning of the modulator likewise depends upon the load impedance, buffer Q4 is inserted between the modulator output and the multiplier chain. Q4 also limits any amplitude modulation present in the signal before it is applied to the first multiplier.

Modulator

The phase modulator stage is built around transistor Q3 and can be considered as a voltage divider consisting of the two identical capacitors, C12 and C13, and transistor Q3, over which the output signal is taken off.

Base voltage for Q3 is applied from the joint of C12 and C13, whereby Q3 appears as an inductance having the same reactance as one of the capacitors. In addition to the reactive current in the transistor there is also a resistive component which is determined by the transistor's operating point; this resistive component can be considered as a resistor in series with the inductance.

The phase shift between the modulator input signal applied to C12 and the modulator output signal taken off across Q3 is therefore dependent upon the transistor's operating point.

Applying a modulation signal to emitter of Q3 will shift the operating point (transfer characteristic) coincident with the modulating signal, thus achieving the desired phase modulation.

Frequency Multiplication Stages

The frequency multiplier chain is composed of two triplers and two doublers, giving a multiplication factor of 36, resulting in the required antenna frequency of 420 to 470 MHz. The first multiplier, Q5 and Q6; is a balanced tripler configuration where the even-numbered harmonics of the fundamental frequency are suppressed. The signal from the second buffer stage, Q4, is applied to the base of Q5 through C18. The base of Q6 is grounded, as far as the signal is concerned, through C23 and C24. Since R23 is common to both transistor emitters, any signal through Q5 will also be across the emitter-base circuit of Q6 with the proper polarity to drive the stage in push-pull.

Two tuned LC circuits, L3 and C26, and L4 and C31, form a capacitive coupled band-pass filter tuned to the third harmonic of the frequency at the tripler input.

C29 and C30 pass the signal on the multiplier, Q7 and Q8. This stage is a balanced doubler, suppressing the odd harmonics of the input signal frequency. Tuned circuits L5 and C34, and L6 and C36 in the collector paths also make up a capacitive coupled band-pass filter, this time tuned to the second harmonic of the frequency at its input. The signal is fed on through C37 and C38 to the second tripler, Q9 and Q10, also operating as a balanced frequency tripler.

The collector circuit consisting of L7 and C40 is, of course, tuned to the second harmonic of the input frequency. The collector circuit and the tuned circuit L8 and C41 in the base circuit of the following amplifier stage form an inductively coupled band-pass filter.

The final multiplier stage (Q11), operating as a doubler, is designed around a single transistor. The tuned circuit of L10 and C46 in its collector is tuned to the second

harmonic of the frequency at the input to the doubler. The signal has now reached the antenna frequency (420 to 470 MHz) and is applied to the output transistor, Q12, via the series resonant circuit of L11 and C47.

The output stage, Q12, amplifies the approx. 20 mW signal from the second doubler to the output level required to drive the PA stage (approx. 80 mW). The signal from the collector of the output transistor passes through a band-pass filter consisting of L13 and C50, and L14 and C52 to the output terminals. The filter also transforms the collector impedance down to an output impedance of 50 Ω .

The band-pass filters determine the overall bandwidth of the exciter, and they also suppress undesired harmonics generated during frequency multiplication. All of the band-pass filters employ close-to-critical coupling.

Technical Specifications

Supply Voltage

9 V

Current Consumption

90 mA

Frequency Range

400 to 470 MHz

Frequency Multiplication Factor

36

Crystal Frequency Band

11.66 - 13.06 MHz

Band Width (3 dB)

15 MHz

Output Power

80 mW

Load Impedance

50 Ω

AF Input Impedance

1 k Ω

Modulation Sensitivity

Required EMF from a
600 generator: (for $\Delta f = 10.5$ kHz at 1 kHz):
210 mV

Modulation Distortion

Measured without de-emphasis,
at $f = 10.5$ kHz / 1 kHz: 2.5 %

Oscillator Frequency adjustable by:

$$\frac{\Delta f}{f} \geq \pm 30 \times 10^{-6}$$

Frequency Stability

for voltage variations of $\pm 2.5\%$:

$$\frac{\Delta f}{f} \leq \pm 0.1 \times 10^{-6}$$

for temperatures between -25 and $+75^{\circ}\text{C}$:

$$\frac{\Delta f}{f} \leq \pm 2 \times 10^{-6}$$

Input Impedance for External Oscillators

470 Ω / 22 pF

Sensitivity at Input for Ext. Oscillators

(required input voltage): 100 mV

Crystal Types

98-12, 98-20, 98-26

Temperature Range

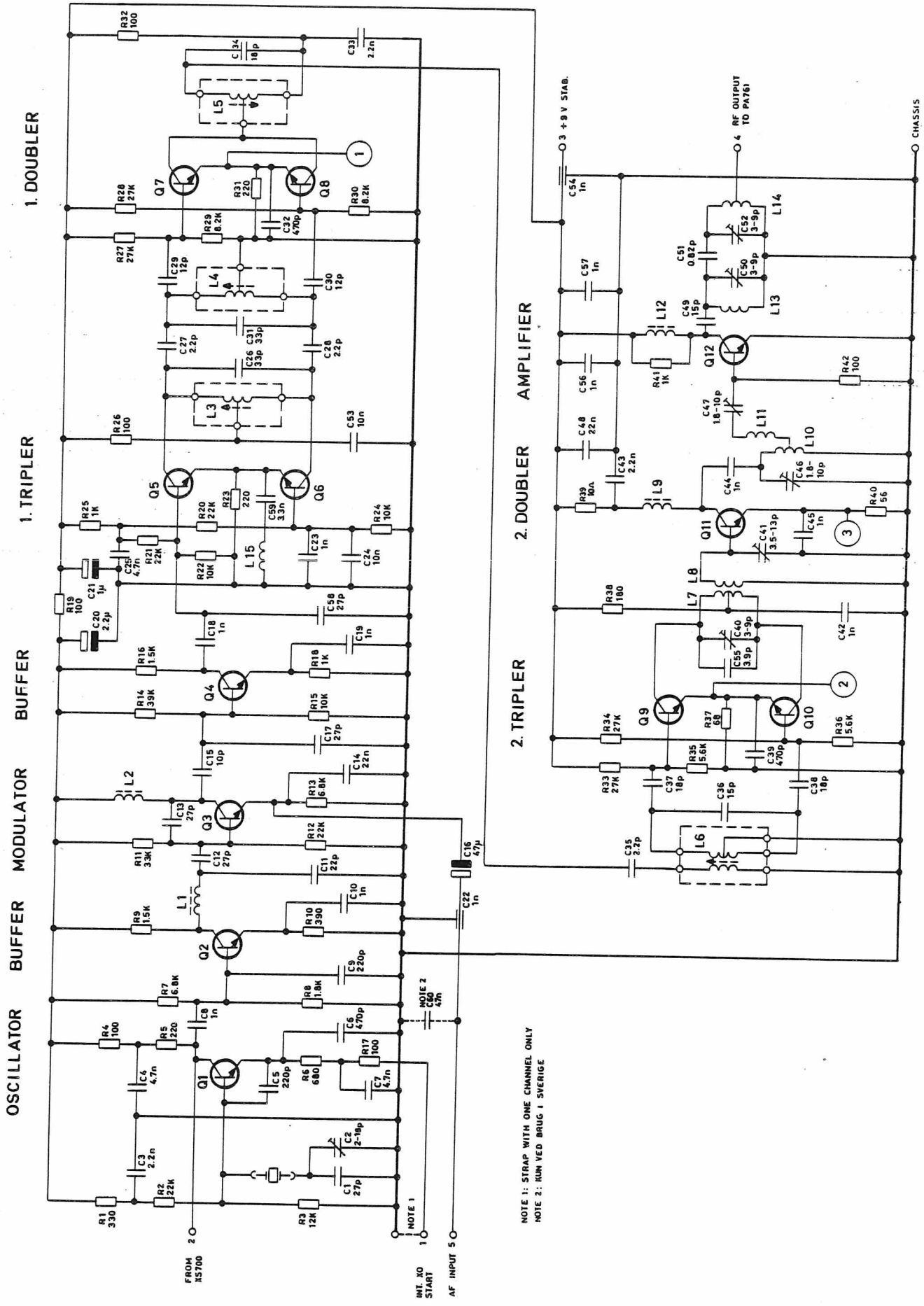
Operating range: -25° to $+70^{\circ}\text{C}$

Functioning range: -30° to $+80^{\circ}\text{C}$

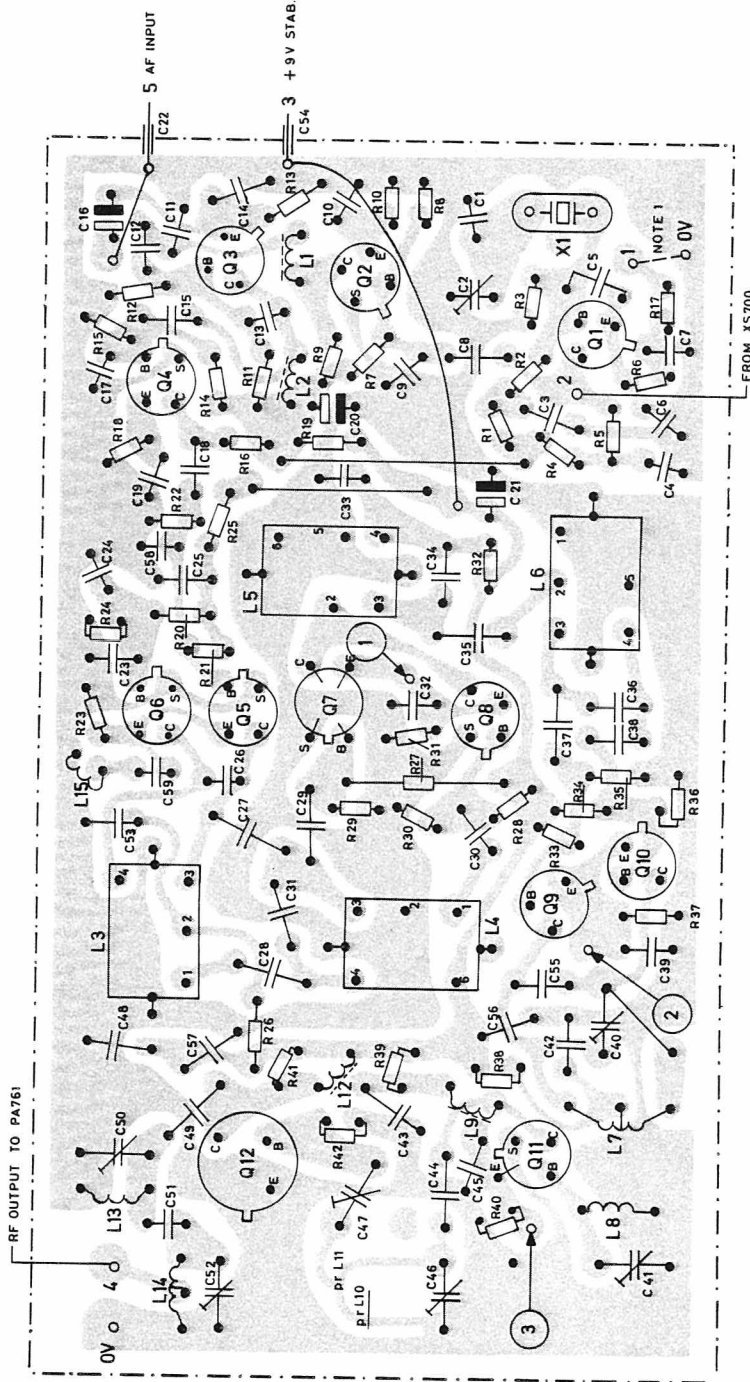
Mechanical Dimensions

Metal enclosure: 24.7 x 50.8 x 91.5 mm

Printed circuit board: 48.3 x 88.9 mm



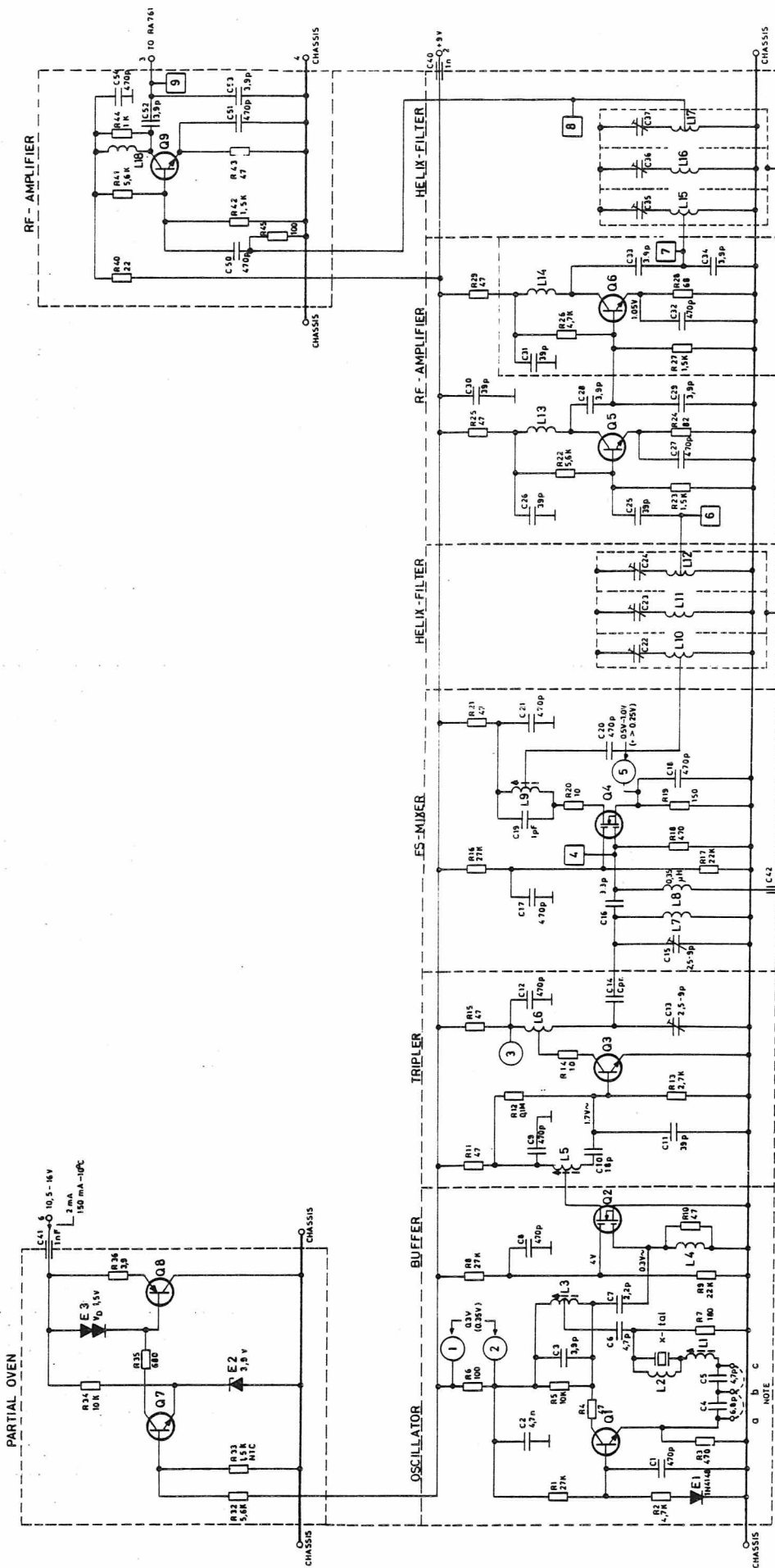
NOTE 1: STRAP WITH ONE CHANNEL ONLY
 NOTE 2: RUN VED BRUG I SVERIGE



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE

TYPE	NO.	CODE	DATA
EN761		10.2429	Exciter Unit
	C1	74.5192	160V 27 pF 5% ceram TB
	C2	78.5044	300V 2-18pF trimmer
	C3	76.5059	50V 2.2 nF 10% polyester FL
	C4	76.5061	50V 4.7 nF 10% polyester FL
	C5	76.5104	25V 220 pF 2.5% polystyr TB
	C6	76.5106	25V 470 pF 2.5% polyester TB
	C7	76.5061	50V 4.7 nF 10% polyester FL
	C8	74.5155	63V 1 nF -20/+50% ceram PL
	C9	76.5104	25V 220 pF 2.5% polystyr TB
	C10	76.5069	50V 1 nF 10% polyester FL
	C11	74.5106	160V 22 pF 5% ceram TB
	C12	74.5107	160V 27 pF 5% ceram TB
	C13	74.5107	160V 27 pF 5% ceram TB
	C14	76.5071	50V 22 pF 10% polyester FL
	C15	74.5135	125V 10 pF 5% ceram DI
	C16	73.5124	6.3V 47 μ F 20% tantal
	C17	74.5107	160V 27 pF 5% ceram TB
	C18	74.5155	50V 1 nF -20/+50% ceram PL
	C19	76.5069	63V 1 nF 10% polyester FL
	C20	73.5129	10V 2.2 μ F 20% tantal
	C21	73.5135	16V 1 μ F 20% tantal
	C22	74.5167	300V 1 nF -20/+80% ceram FT
	C23	74.5155	63V 1 nF -20/+50% ceram PL
	C24	76.5070	50V 10 nF 10% polyester FL
	C25	76.5061	50V 4.7 nF 10% polyester FL
	C26	74.5116	160V 33 pF 5% ceram TB
	C27	74.5127	250V 2.2 pF \pm 0.25 pF ceram BD
	C28	74.5127	250V 2.2 pF \pm 0.25 pF ceram BD
	C29	74.5136	125V 12 pF 5% ceram DI
	C30	74.5136	125V 12 pF 5% ceram DI
	C31	74.5116	160V 33 pF 5% ceram TB
	C32	74.5161	63V 470 pF -20/+50% ceram PL
	C33	76.5059	50V 2.2 nF 10% polyester FL
	C34	74.5138	18 pF 5% ceram DI
	C35	74.5127	250V 2.2 pF \pm 0.25pF ceram BD
	C36	74.5137	15 pF 5% ceram DI
	C37	74.5138	18 pF 5% ceram DI
	C38	74.5138	18 pF 5% ceram DI
	C39	74.5161	125V 470 pF -20/+50% ceram PL
	C40	78.5050	63V 3-9 pF trimmer
	C41	78.5025	160V 3.5 - 13 pF trimmer
	C42	74.5155	63V 1 nF -20/+50% ceram PL
	C43	74.5163	63V 2.2 nF -20/+50% ceram PL
	C44	74.5155	63V 1 nF -20/+50% ceram PL
	C45	74.5155	63V 1 nF -20/+50% ceram PL
	C46	78.5048	300V 1.8 - 10 pF trimmer

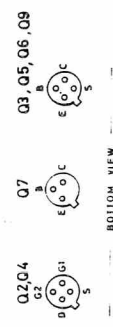
TYPE	NO.	CODE	DATA
	C47	78.5048	1.8 - 10 pF trimmer
	C48	76.5071	22 nF 10% polyester FL
	C49	74.5137	15 pF 5% ceram DI
	C50	78.5050	3-9 pF trimmer
	C51	74.5122	0.82 pF \pm 0.1 pF ceram BD
	C52	78.5050	3-9 pF trimmer
	C53	76.5070	10 nF 10% polyester FL
	C54	74.5167	1 nF -20/+80% ceram FT
	C55	74.5135	3.9 pF \pm 0.25 pF ceram DI
	C56	74.5155	1 nF -20/+50% ceram PL
	C57	74.5155	1 nF -20/+50% ceram PL
	C58	74.5107	27 pF 5% ceram TB
	C59	76.5060	3.3 nF 10% polyester FL
	R1	80.5243	330 Ω 5% carbon film
	R2	80.5265	22 k Ω 5% "
	R3	80.5262	12 k Ω 5% "
	R4	80.5237	100 Ω 5% "
	R5	80.5241	220 Ω 5% "
	R6	80.5247	680 Ω 5% "
	R7	80.5259	6.8 k Ω 5% "
	R8	80.5252	1.8 k Ω 5% "
	R9	80.5251	1.5 k Ω 5% "
	R10	80.5244	390 Ω 5% "
	R11	80.5267	33 k Ω 5% "
	R12	80.5265	22 k Ω 5% "
	R13	80.5259	6.8 k Ω 5% "
	R14	80.5268	39 k Ω 5% "
	R15	80.5261	10 k Ω 5% "
	R16	80.5251	1.5 k Ω 5% "
	R17	80.5237	100 Ω 5% "
	R18	80.5249	1 k Ω 5% "
	R19	80.5237	100 Ω 5% "
	R20	80.5265	22 k Ω 5% "
	R21	80.5265	22 k Ω 5% "
	R22	80.5261	10 k Ω 5% "
	R23	80.5241	220 Ω 5% "
	R24	80.5261	10 k Ω 5% "
	R25	80.5249	1 k Ω 5% "
	R26	80.5237	100 Ω 5% "
	R27	80.5266	27 k Ω 5% "
	R28	80.5266	27 k Ω 5% "



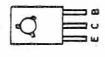
NOTE

FREQUENCY	STRAP
UP/OP	NONE/INGEN
NORMAL	a - b
DOWN/NEED	b - c

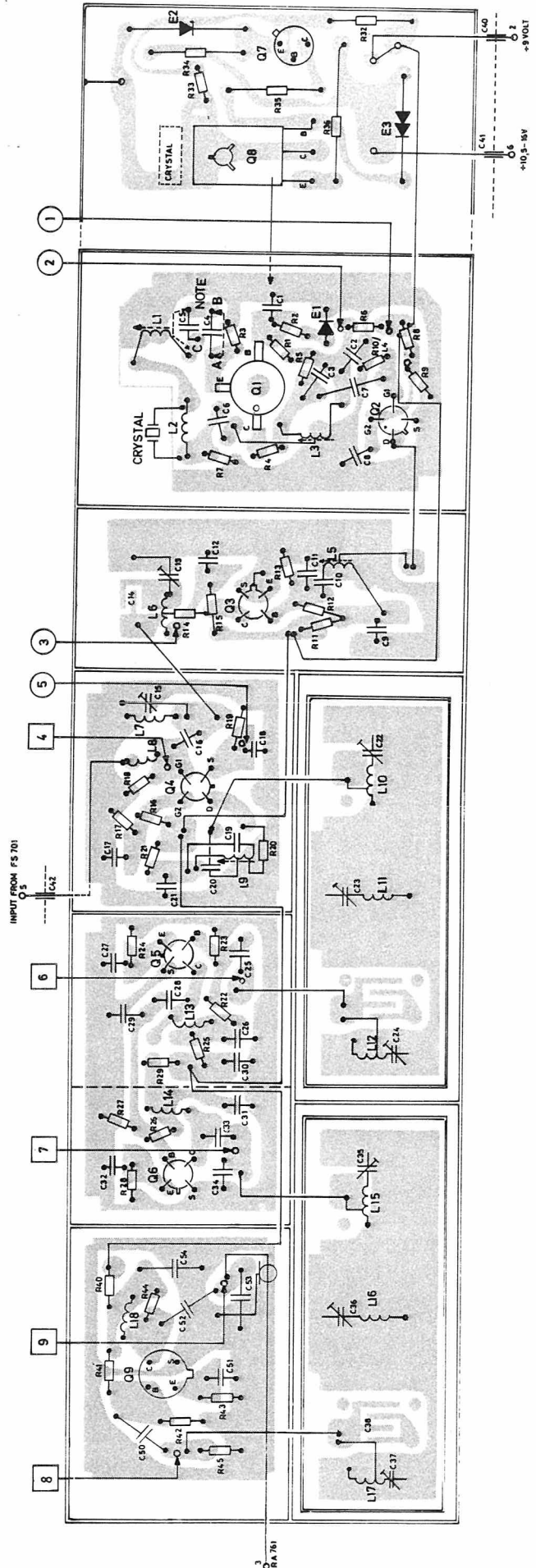
() MEASURED WITH DRIVE
MULTI MED USTYRING



BOTTOM VIEW



EXCITER
STYRESENDER EX762
D 401.805



EXCITER
STYRESENDER

EX 762

D401.892

Storno

TYPE	NO.	CODE	DATA
	L3	61.1229	RF Coil 119-159 MHz
	L4	61.1231	RF Choke, R10 incl.
	L5	61.1227	RF Coil
	L6	62.0876	RF Coil
	L7	62.0877	RF Coil
	L8	62.0659-01	RF Choke 0.35 μ H
	L9	61.1228	RF Coil
	L10	61.	Helix Coil 409.3-459.3 MHz
	L11	61.	Helix Coil 409.3-459.3 MHz
	L12	61.	Helix Coil 409.3-459.3 MHz
	L13	62.0875	RF Coil
	L14	62.0875	RF Coil
	L15	61.	Helix Coil 409.3-459.3 MHz
	L16	61.	Helix Coil 409.3-459.3 MHz
	L17	61.	Helix Coil 409.3-459.3 MHz
	L18	62.0875	RF Coil 420-470 MHz
	E1	99.5237	1N4148 Diode
	E2	99.5225	3.9 V Zenerdiode
	E3	99.5209	1.5 V Stab. diode
	Q1	99.5290	BFR90 Transistor
	Q2	99.5291	3N205 Transistor FET
	Q3	99.5240	BFX80 Transistor
	Q4	99.5291	3N205 Transistor FET
	Q5	99.5240	BFX89 Transistor
	Q6	99.5240	BFX89 Transistor
	Q7	99.5143	BC108 Transistor
	Q8	99.5236	BD136 Transistor
	Q9	99.5240	BFX89 Transistor

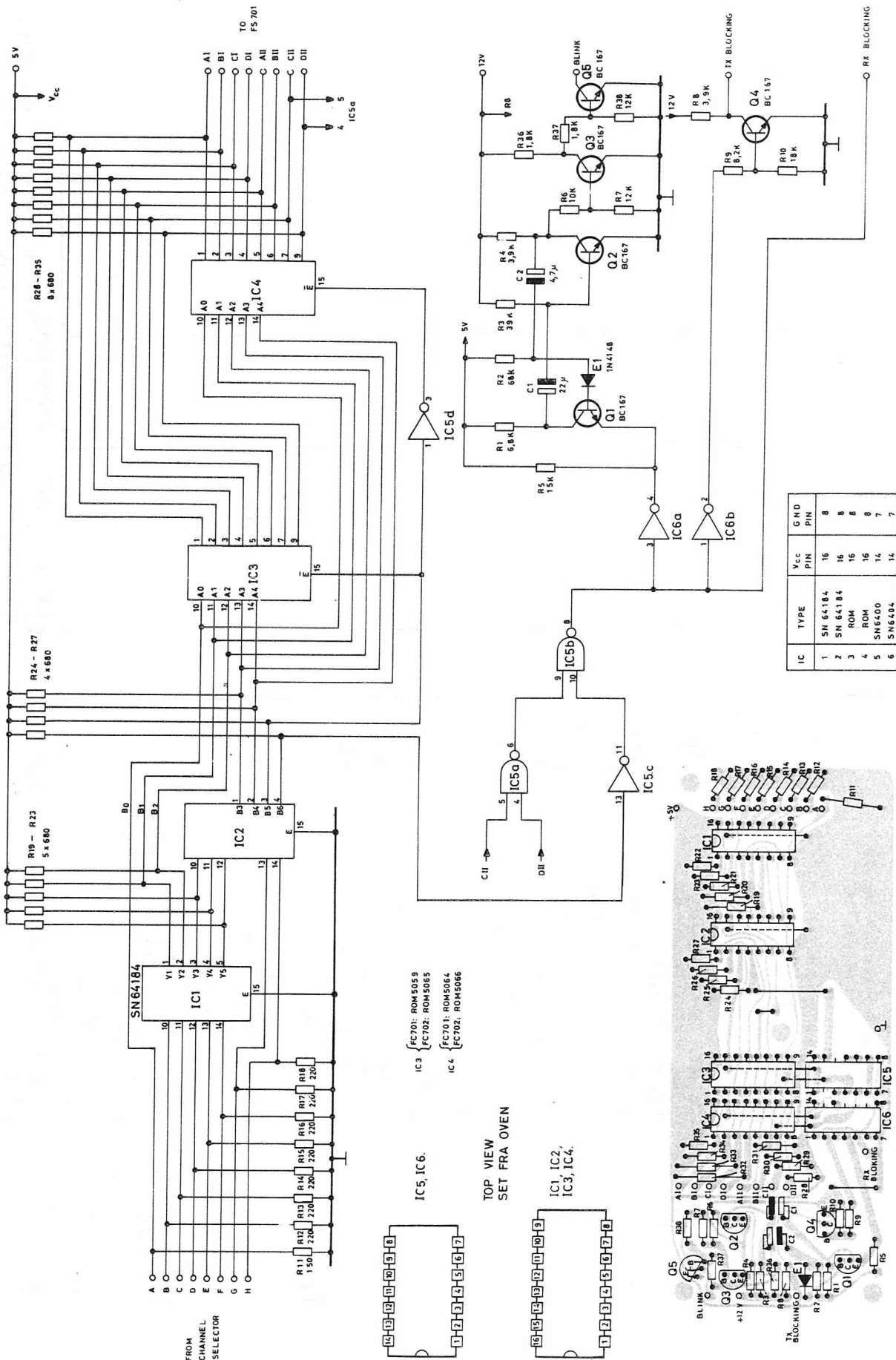
Storno

TYPE	NO.	CODE	DATA

EXCITER
STYRESENDER

EX 762

X401.867



FREQUENCY CONTROL UNIT
FREKVENSKONTROLLENHED

FC701, FC702

D.401.819/2

Storno

Storno

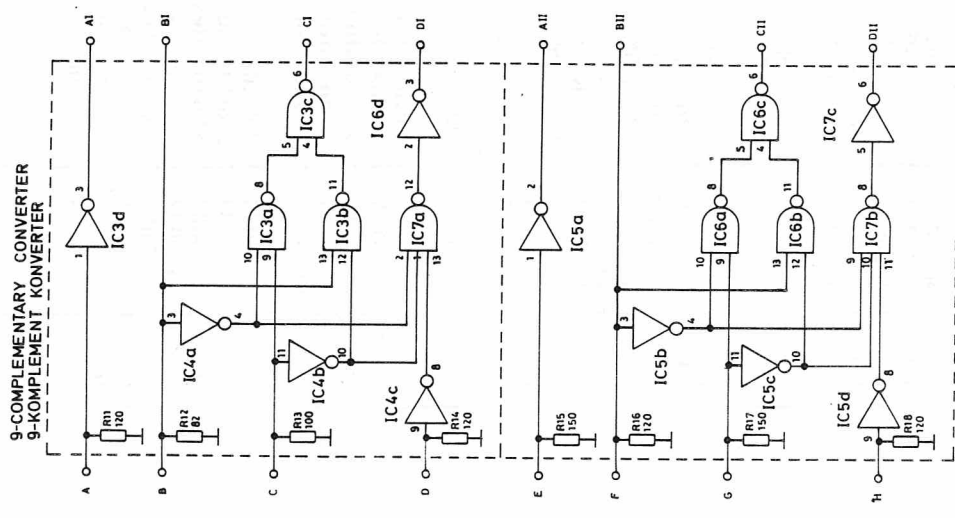
TYPE	NO.	CODE	DATA
FC701 FC702		10.2939	Frequency Control Unit DK
		10.2940	Frequency Control Unit N
	C1	73.5127	22μF 20% tantal 16V
	C2	73.5126	4.7μF 20% tantal 35V
	R1	80.5059	6.8kΩ 5% carbon film 1/10W
	R2	80.5071	68kΩ 5% carbon film 1/10W
	R3	80.5068	39kΩ 5% carbon film 1/10W
	R4	80.5056	3.9kΩ 5% carbon film 1/10W
	R5	80.5063	15kΩ 5% carbon film 1/10W
	R6	80.5061	10kΩ 5% carbon film 1/10W
	R7	80.5062	12kΩ 5% carbon film 1/10W
	R8	80.5056	3.9kΩ 5% carbon film 1/10W
	R9	80.5060	8.2kΩ 5% carbon film 1/10W
	R10	80.5064	18kΩ 5% carbon film 1/10W
	R11	80.5439	150Ω 5% carbon film 1/4W
	R12	80.5041	220Ω 5% carbon film 1/10W
	R13	80.5041	220Ω 5% carbon film 1/10W
	R14	80.5041	220Ω 5% carbon film 1/10W
	R15	80.5041	220Ω 5% carbon film 1/10W
	R16	80.5041	220Ω 5% carbon film 1/10W
	R17	80.5041	220Ω 5% carbon film 1/10W
	R18	80.5041	220Ω 5% carbon film 1/10W
	R19-35	80.5047	680Ω 5% carbon film 1/10W
	R36	80.5052	1.8kΩ 5% carbon film 1/10W
	R37	80.5052	1.8kΩ 5% carbon film 1/10W
	R38	80.5062	12kΩ 5% carbon film 1/10W
	E1	99.5237	1N4148 Diode
	Q1	99.5117	BC167 Transistor
	Q2	99.5117	BC167 Transistor
	Q3	99.5117	BC167 Transistor
	Q4	99.5117	BC167 Transistor
	Q5	99.5117	BC167 Transistor
	IC1	14.5063	SN64184 BCD to binary converter
	IC2	14.5063	SN64184 BCD to binary converter
	IC3	14.5059	5059 DK ROM
	IC3	14.5065	5065 N ROM
	IC4	14.5064	5064 DK ROM
	IC4	14.5066	5066 N ROM
	IC5	14.5024	SN6400 Quadruple 2-input NAND Gate
	IC6	14.5034	SN6404 Hex Inverter
FC701 FC702 FC701 FC702			

TYPE NO. CODE DATA

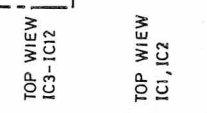
FREQUENCY CONTROL UNIT
FREKV ENSKONTROLLENHED

FC701, FC702

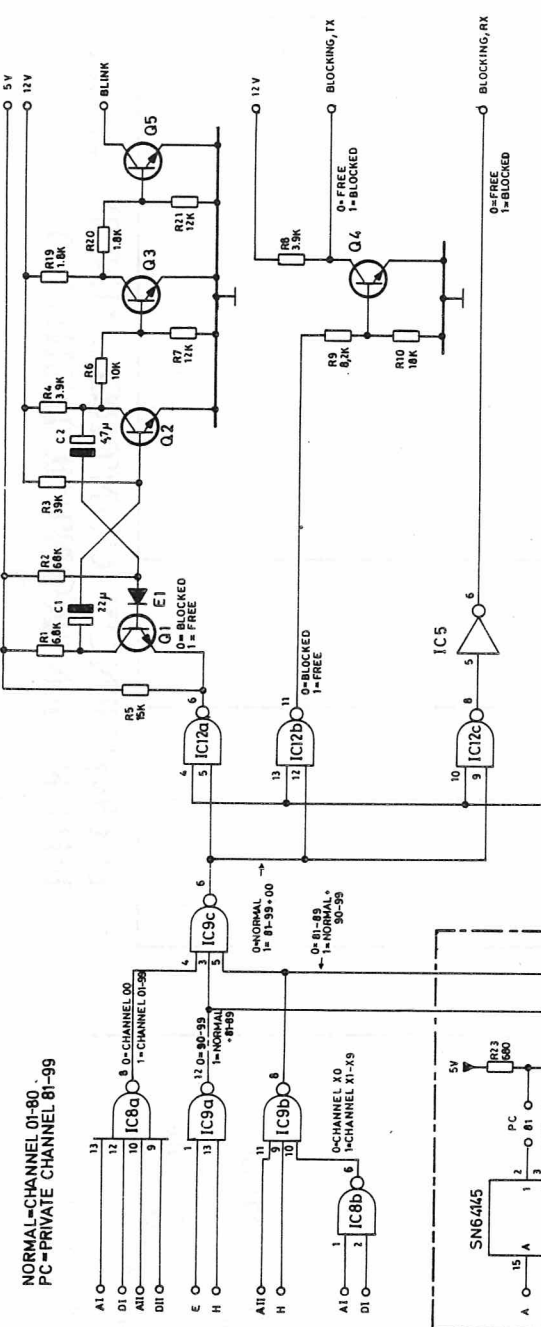
X401.964



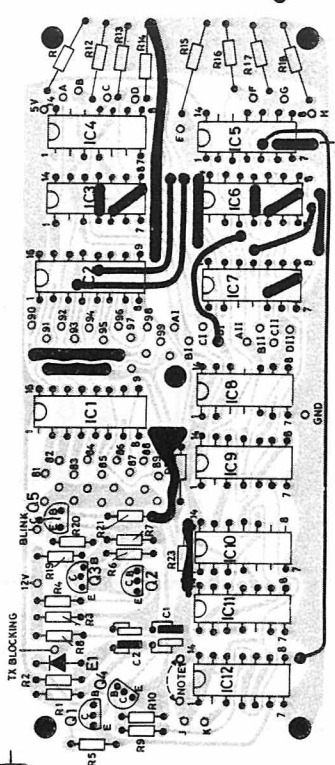
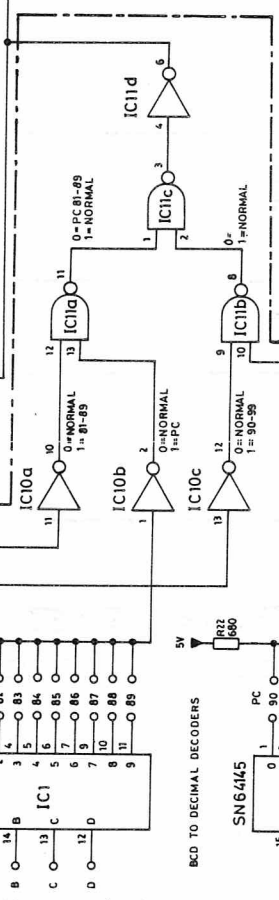
IC	Vcc	GND	PIN	PIN
IC1	SN64145	16	8	
IC2	SN64145	16	8	
IC3	SN6400	14	7	
IC4	SN6404	14	7	
IC5	SN6404	14	7	
IC6	SN6400	14	7	
IC7	SN6410	14	7	
IC8	SN6420	14	7	
IC9	SN6410	14	7	
IC10	SN6404	14	7	
IC11	SN6400	14	7	
IC12	SN6400	14	7	



NOTE1. TERMINAL J IS CONNECTED TO 5V IN UNITS WITHOUT PRIVATE CHANNEL CIRCUIT.



J	K
MTD	1 0
PC	0 1



FREQUENCY CONTROL UNIT
FREKVENSKONTROLLENHED

TYPE	NO.	CODE	DATA
FC703		10.2927	Frequency Control Unit
	C1	73.5127	22 μ F 20% tantal
	C2	73.5103	4.7 μ F 20% tantal
	R1	80.5059	6.8 K Ω 5% carbon film
	R2	80.5071	68 K Ω 5%
	R3	80.5068	39 K Ω 5%
	R4	80.5056	3.9 K Ω 5%
	R5	80.5063	15 K Ω 5%
	R6	80.5061	10 K Ω 5%
	R7	80.5062	12 K Ω 5%
	R8	80.5056	3.9 K Ω 5%
	R9	80.5060	8.2 K Ω 5%
	R10	80.5064	18 K Ω 5%
	R11	80.5438	120 Ω 5%
	R12	80.5436	82 Ω 5%
	R13	80.5437	100 Ω 5%
	R14	80.5438	120 Ω 5%
	R15	80.5439	150 Ω 5%
	R16	80.5438	120 Ω 5%
	R17	80.5439	150 Ω 5%
	R18	80.5438	120 Ω 5%
	R19	80.5052	1.8 K Ω 5%
	R20	80.5052	1.8 K Ω 5%
R21	80.5062	12 K Ω 5%	
R22	80.5247	680 Ω 5%	
R23	80.5247	680 Ω 5%	
E1	99.5237	Diode 1N4148	
Q1	99.5117	Transistor BC167	
Q2	99.5117	Transistor BC167	
Q3	99.5117	Transistor BC167	
Q4	99.5117	Transistor BC167	
Q5	99.5117	Transistor BC167	
IC3	14.5024	SN6400 Quadr. 2-input NAND gate	
IC4	14.5034	SN6404 Hex Inverter	
IC5	14.5034	SN6404 Hex Inverter	
IC6	14.5024	SN6400 Quadr. 2-input NAND gate	
IC7	14.5004	SN6410 Triple 3-input NAND gate	
IC8	14.5031	SN6420 Dual 4-input NAND gate	
IC9	14.5004	SN6410 Triple 3-input NAND gate	
IC12	14.5024	SN6400 Quadr. 2-input NAND gate	

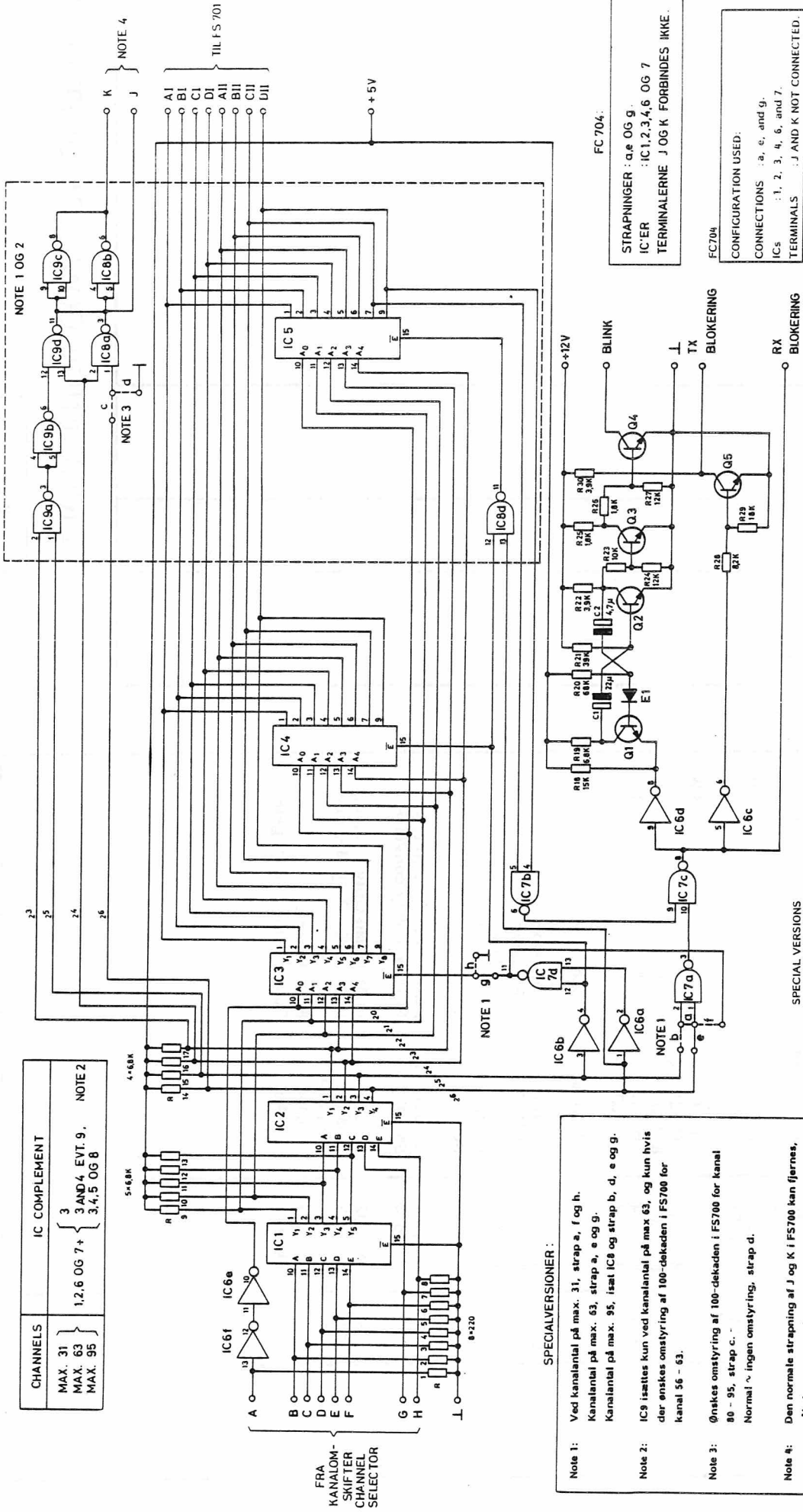
TYPE	NO.	CODE	DATA
	IC1	14.5071	SN64145 BCD to decimal decoder
	IC2	14.5071	SN64145 BCD to decimal decoder
	IC10	14.5034	SN6404 Hex Inverter
	IC11	14.5024	SN6400 Quadr. 2-input NAND gate
			Kit for Increasing Channels

FREQUENCY CONTROL UNIT
FREKV ENSKONTROLLENHED

FC703

X401.864

NOT USED IN STANDARD FC704
ANVENDES IKKE I FC704



CHANNELS	IC COMPLEMENT
MAX. 31	1, 2, 6 OG 7 + 3 AND/4 EVT. 9, 3, 4, 5 OG 8
MAX. 63	
MAX. 95	

NOTE 2

FRA
KANALOM-
SKIFTER
CHANNEL
SELECTOR

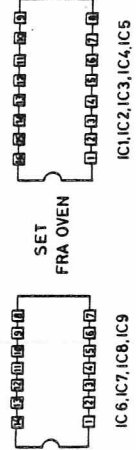
SPECIALVERSIONER:

- Note 1: Ved kanalantal på max. 31, strap a, f og h. Kanalantal på max. 63, strap a, e og g. Kanalantal på max. 95, isæt IC8 og strap b, d, e og g.
- Note 2: IC9 isættes kun ved kanalantal på max 63, og kun hvis der ønskes omstyring af 100-dekaden i FS700 for kanal 56 - 63.
- Note 3: Ønskes omstyring af 100-dekaden i FS700 for kanal 80 - 95, strap c. Normal ~ ingen omstyring, strap d.
- Note 4: Den normale strapning af J og K i FS700 kan fjernes, således, at omstyring af 100-dekaden kan indføres som nævnt i note 2 og 3. Deleforhold 6xx: J=1 og K=0 (NORMAL) Deleforhold 5xx: J=0 og K=1

SPECIAL VERSIONS

- NOTE 1: FOR MAXIMUM 31 CHANNELS, CONNECT a, f, and g. FOR MAXIMUM 63 CHANNELS, CONNECT b, e, and g. AND INSERT IC8.
- NOTE 2: IC9 IS ONLY INSERTED FOR A MAXIMUM OF 63 CHANNELS AND ONLY WHEN THE 100 DECADE CONTROL CODE IN FS700 IS TO BE REVERSED FOR CHANNEL 56 - 63.
- NOTE 3: FOR REVERSING OF THE 100 DECADE CONTROL CODE FOR CHANNEL 80 - 95, CONNECT c. NORMAL CONDITION, i. e. NO REVERSING, CONNECT d.
- NOTE 4: THE NORMAL CONNECTION OF J AND K IN FS700 CAN BE OMITTED IN ORDER TO REVERSE THE 100 DECADE AS STATED IN NOTE 2 AND 3.

IC	YCC PIN	GND PIN
1	SH64184	16 8
2	SH64184	16 8
3	PRON 5102	16 8
4	PRON 5102	16 8
5	PRON	16 8
6	SH6404	14 7
7	SH6400	14 7
8	SH6400	14 7
9	SH6400	14 7



FC704:

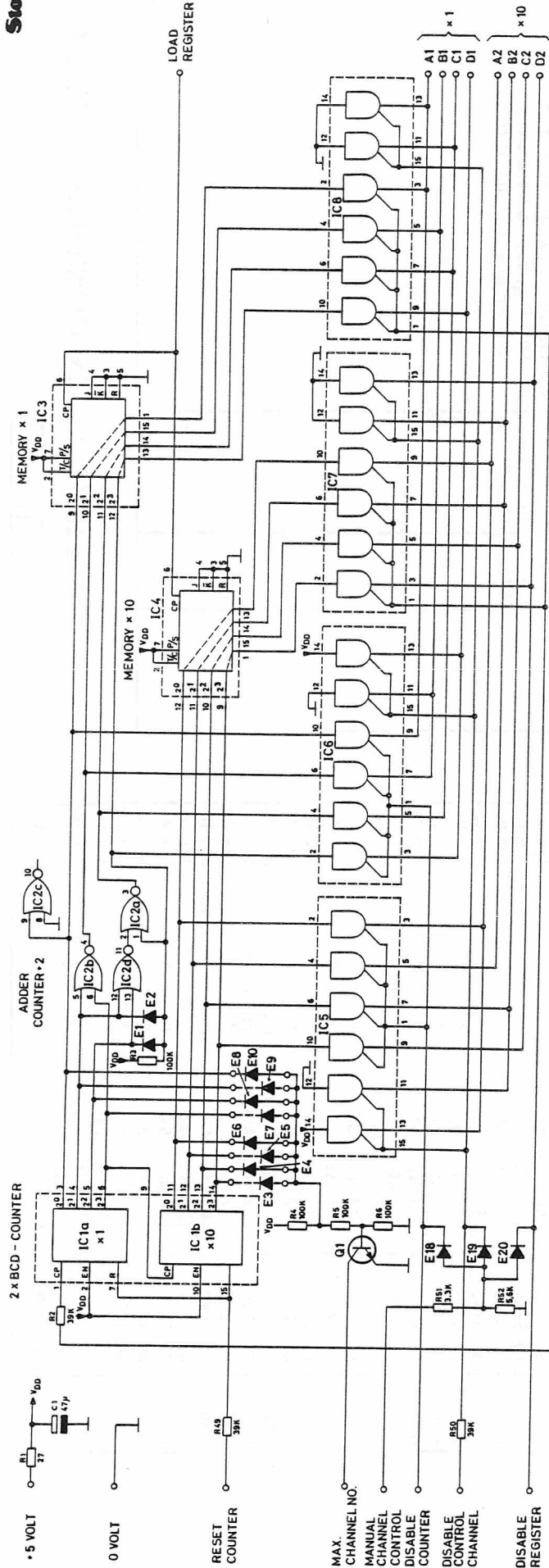
STRAPNINGER : a, e OG g.
IC'ER : IC1, 2, 3, 4, 6 OG 7
TERMINALERNE J OG K FORBINDES IKKE.

FC704:

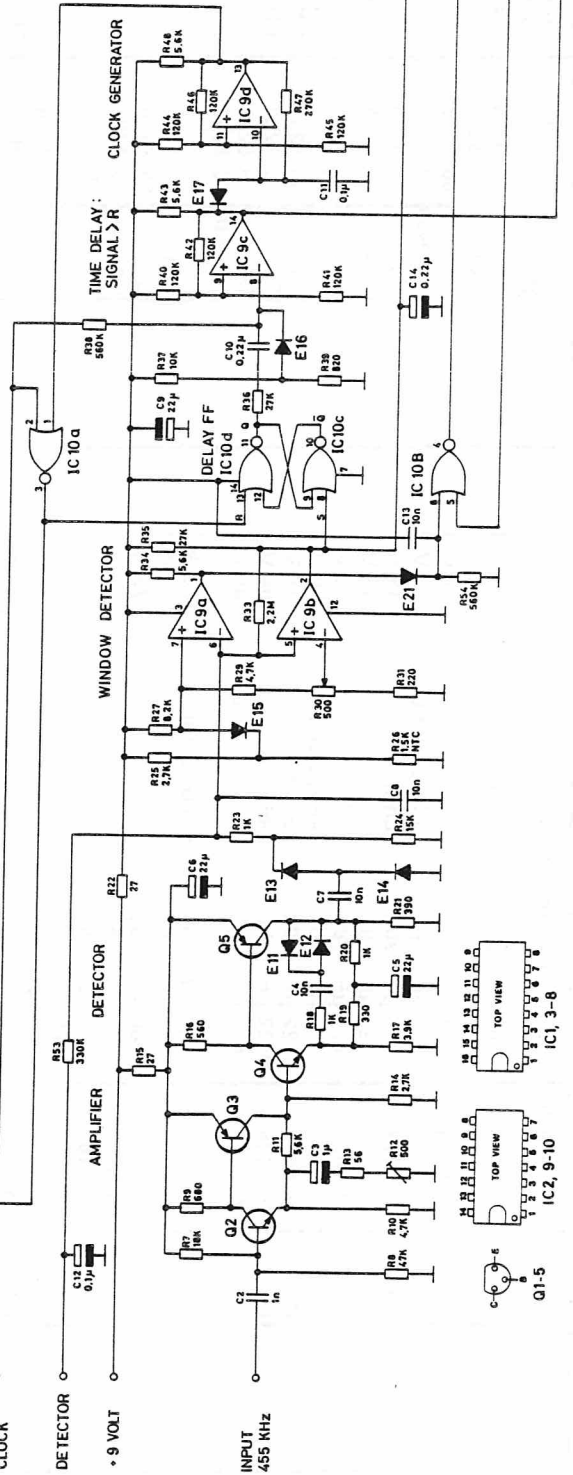
CONFIGURATION USED:
CONNECTIONS : a, e, and g.
ICs : 1, 2, 3, 4, 6, and 7.
TERMINALS : J AND K NOT CONNECTED.

FREQUENCY CONTROL UNIT FC 704
FREKVENSKONTROLLENHED

D402.145

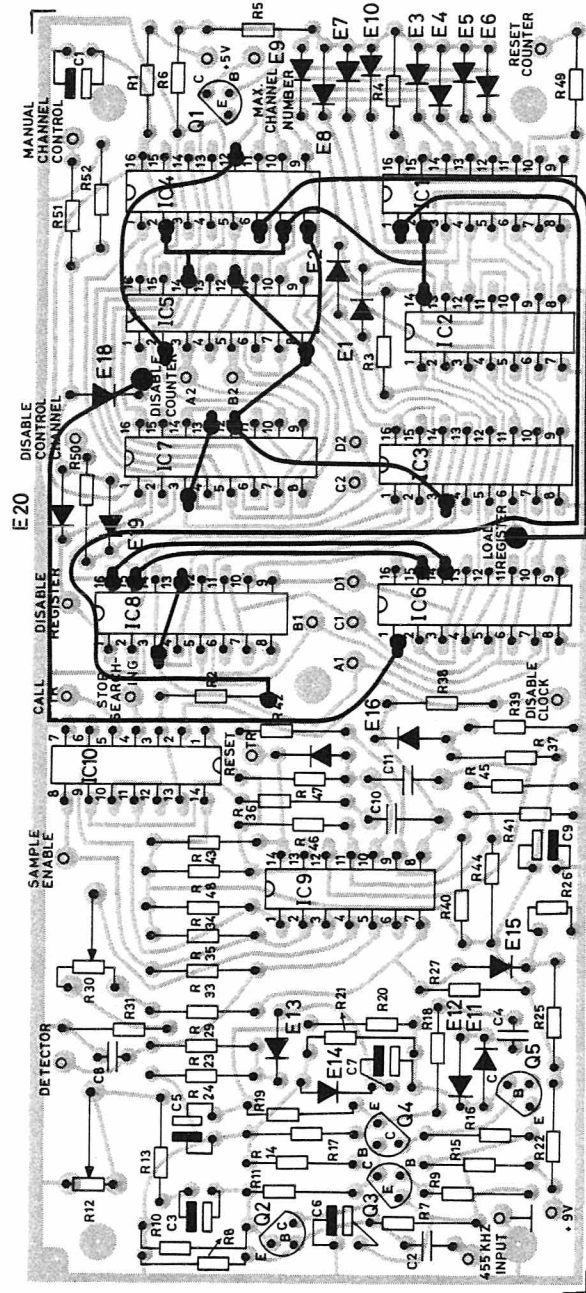


	VSS	VDD
IC1	8	16
IC2	7	14
IC3	8	16
IC4	8	16
IC5	8	16
IC6	8	16
IC7	8	16
IC8	8	16



FREQUENCY CONTROL UNIT FC705

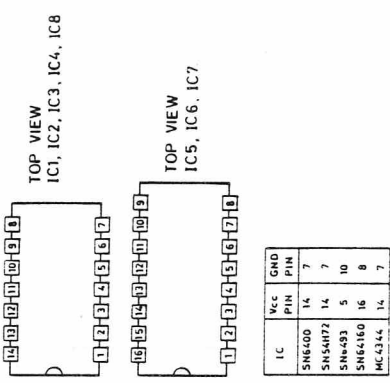
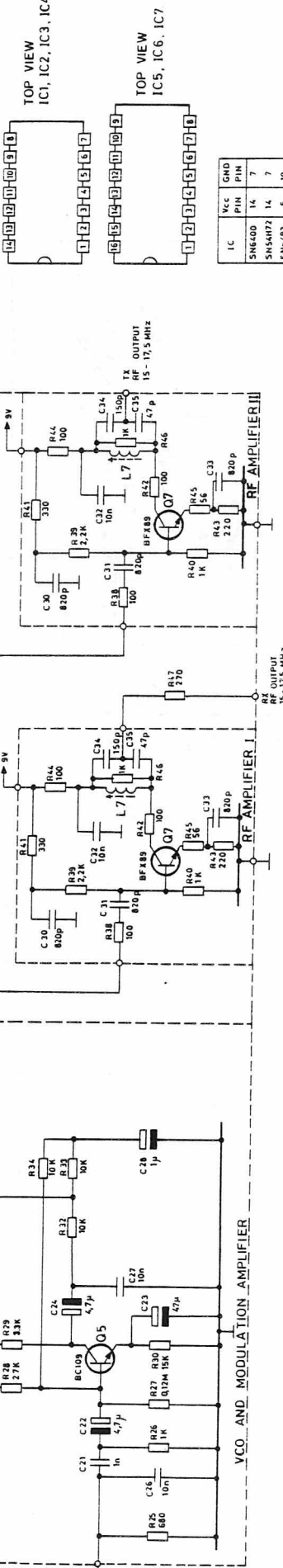
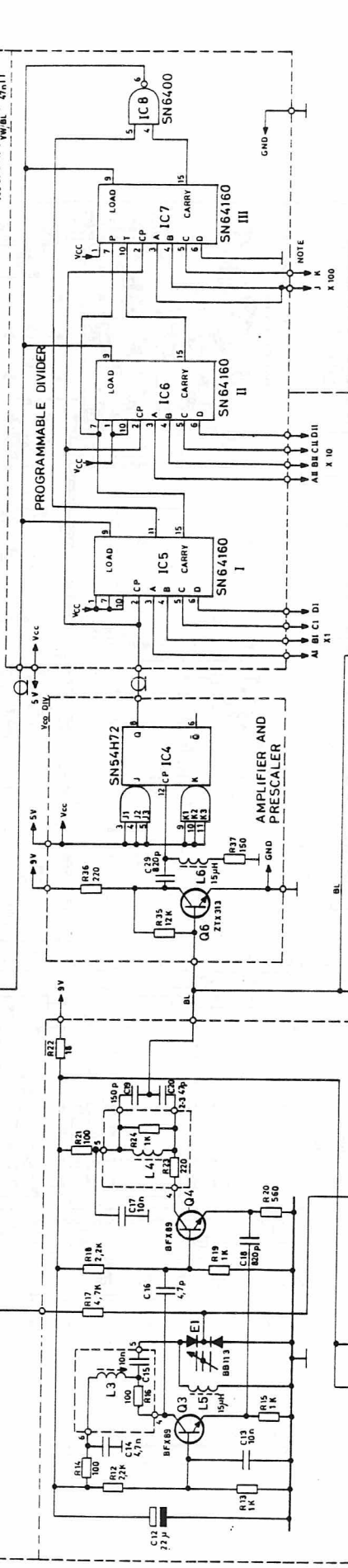
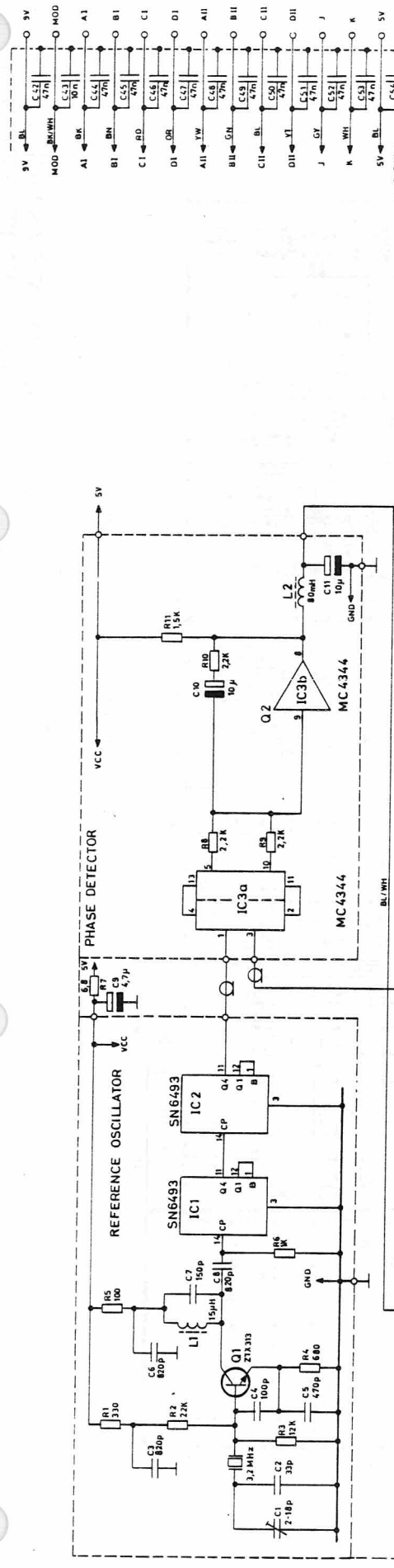
D 402.383/2



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE.

FREQUENCY CONTROL UNIT FC705

D 402.508



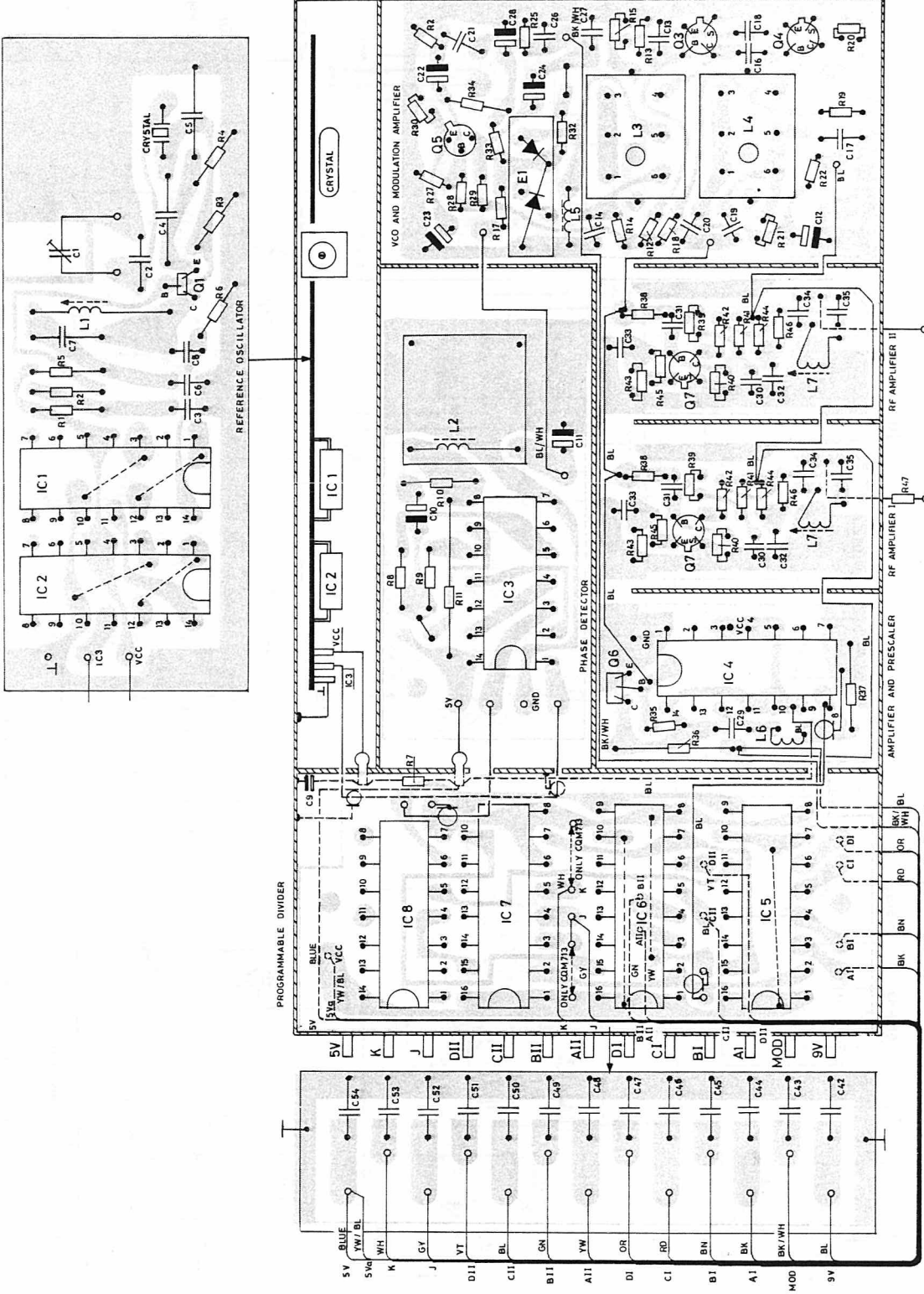
NOTE: IN COM713 (X450X AND X46N) J AND K ARE CONNECTED INTERNALLY IN THE PROGRAMMABLE DIVIDER TO 9 AND CARRY5, RESPECTIVELY. THESE CONNECTIONS ARE NOT MADE IN COM783D.

ICOM713D (X450X OG X46N) ER J OG K STRAPPET TIL H.V. 5V OG STEL INTERN I DEN PROGRAMMERBARE DELER.
ICOM783D ER OVENNAVTE STRAPPING INNE I DØBØTT.

FREQUENCY SYNTESENER
FREKVENSSYNTSEENHED

FS701

D40174/3



FREQUENCY SYNTESENER
FREKVENSSYNTESEENHED

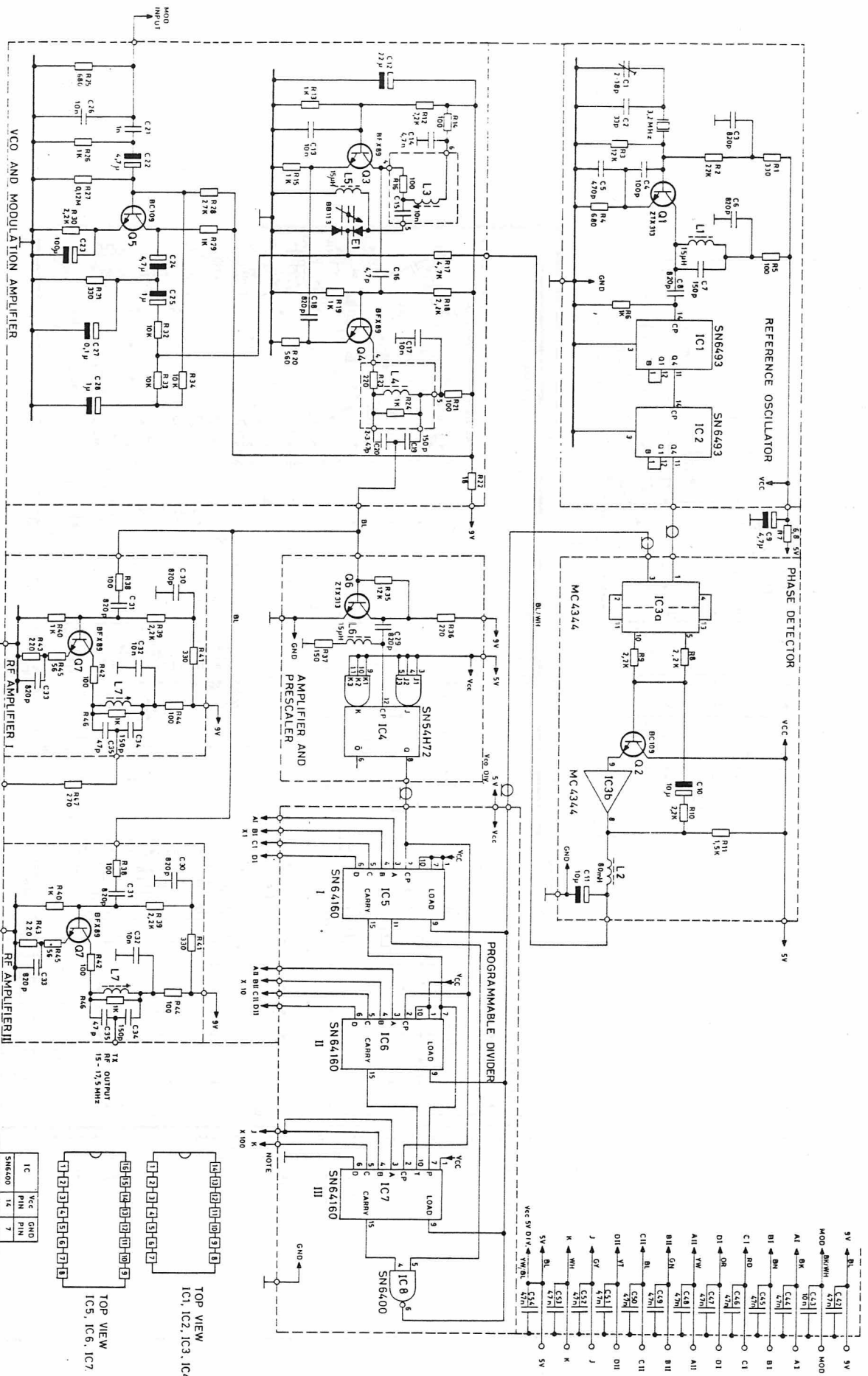
FS701

01.891/3

RX
RF OUTPUT
15-17,5 MHz

TX
RF OUTPUT
15-17,5 MHz

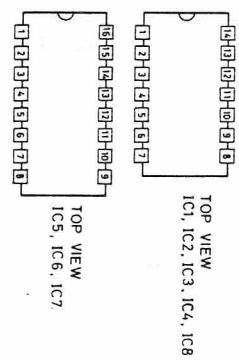
VIEWED FROM SOLDERING SIDE



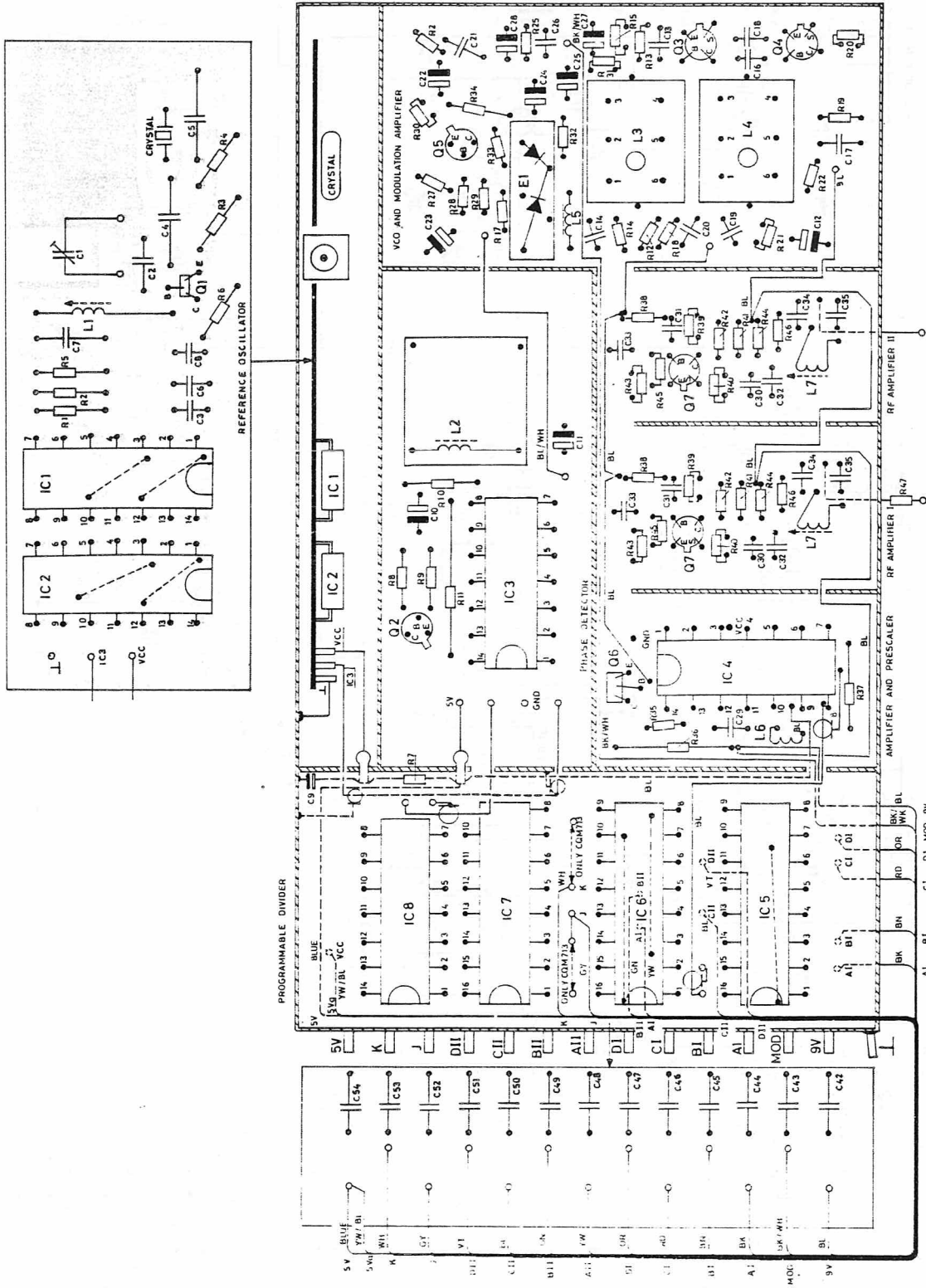
NOTE: IN COM113 (1490K AND 149N) J AND K ARE CONNECTED INTERNALLY IN THE PROGRAMMABLE DIVIDER TO 4.5V AND CHASSIS RESPECTIVELY. THESE CONNECTIONS ARE NOT MADE IN COM150.

ICOM113B (1490K AND 149N) EN J OG K STRAPPET TIL 4.5V SV OG STEL HENNAF DEG. HENNAF DEG STRAPPET TIL CHASSIS. I COM150 ER OVENSKRIVTE STRAPPINGER IKKE INDENBORT.

IC	Vcc	IC	GROUND
SN6493	14	7	
SN54H72	14	7	
SN64160	5	10	
SN64160	16	8	
MC4344	14	7	



FREQUENCY SYNTHESIZER
FREKVENSSYNTESSENERHED
FS701



RX
RF OUTPUT
15-17.5 MHz

TX
RF OUTPUT
15-17.5 MHz

VWED FROM SOLDERING SIDE

FREQUENCY SYNTESENER
FREKVENS SYNTESENERHED

FS701



TYPE	NO.	CODE	DATA
FS701		10.2923	Frequency Synthesizer
	C9	73.5126	35 V
	R7	80.5223	1/8W
	R17	80.5042	1/10W
			PC BOARD
			4.7 μ F 20% tantal
			6.8 Ω 5% carbon film
			270 Ω 5%
			CAPACITANCE BOARD
	C42	74.5283	47 nF 20% ceram CP
	C43	74.5281	10 nF 20% ceram CP
	C44 - C54	74.5283	47 nF 20% ceram CP
			REFERENCE OSCILLATOR
	C1	78.5044	2-18 pF trimmer
	C2	74.5116	33 pF 5% ceram TB
	C3	74.5314	820 pF -20+80% ceram PL
	C4	76.5102	100 pF 2.5 % polystyr TB
	C5	76.5065	470 pF 5% polystyr TB
	C6	74.5314	820 pF -20+80% ceram PL
	C7	76.5103	150 pF 2.5 % polystyr TB
	C8	74.5314	820 pF -20+80% ceram PL
	R1	80.5043	330 Ω 5% carbon film
	R2	80.5065	22 K Ω 5%
	R3	80.5062	12 K Ω 5%
	R4	80.5047	680 Ω 5%
	R5	80.5037	100 Ω 5%
	R6	80.5049	1 K Ω 5%
	L1	63.5007	15 μ H 20% choke
	Q1	99.5293	Transistor ZTX313
	IC1	14.5043	SN6493 4-bit binary counter
	IC2	14.5043	SN6493 4-bit binary counter
			PHASE DETECTOR
	C10	73.5109	10 μ F 20% tantal
	C11	73.5109	10 μ F 20% tantal
	R8	80.5053	2.2 K Ω 5% carbon film
	R9	80.5053	2.2 K Ω 5%
	R10	80.5053	2.2 K Ω 5%

TYPE	NO.	CODE	DATA
	R11	80.5051	1.5 K Ω 5% carbon film
	L2	61.1222	80 mH coil
	Q2	99.5201	Transistor BC109
	IC3	14.5060	MC4344 Phase/frequency detector
			VCO AND MODULATION AMPLIFIER
	C12	73.5127	22 μ F 20% tantal
	C13	76.5070	10 nF 10% polyester FL
	C14	76.5061	4.7 nF 10% polyester FL
	C15	76.5070	10 nF 10% polyester FL
	C16	74.5318	4.7 pF \pm 0.25 pF ceram PL
	C17	76.5070	10 nF 10% polyester FL
	C18	74.5314	820 pF -20+80% ceram PL
	C19	76.5103	150 pF 2.5 % polyester TB
	C20	74.5319	47 pF 2% ceram PL
	C21	76.5069	1 nF 10% polystyr FL
	C22	73.5126	4.7 μ F 20% tantal
	C23	73.5128	100 μ F 20% tantal
	C24	73.5126	4.7 μ F 20% tantal
	C25	73.5135	1 μ F -20+80% tantal
	C26	76.5070	10 nF 10% polyester FL
	C27	73.5089	0.1 μ F 20% tantal
	C28	73.5135	1 μ F -20+50% tantal
	R12	80.5053	2.2 K Ω 5% carbon film
	R13	80.5049	1 K Ω 5%
	R14	80.5037	100 Ω 5%
	R15	80.5049	1 K Ω 5%
	R16	80.5037	100 Ω 5%
	R17	80.5057	4.7 K Ω 5%
	R18	80.5053	2.2 K Ω 5%
	R19	80.5049	1K Ω 5%
	R20	80.5046	560 Ω 5%
	R21	80.5037	100 Ω 5%
	R22	80.5028	18 Ω 5%
	R23	80.5041	220 Ω 5%
	R24	80.5049	1 K Ω 5%
	R25	80.5047	120 K Ω 5%

FREQUENCY SYNTHESIZER
FREKVENS SYNTESSEHED

FS701

X401.863

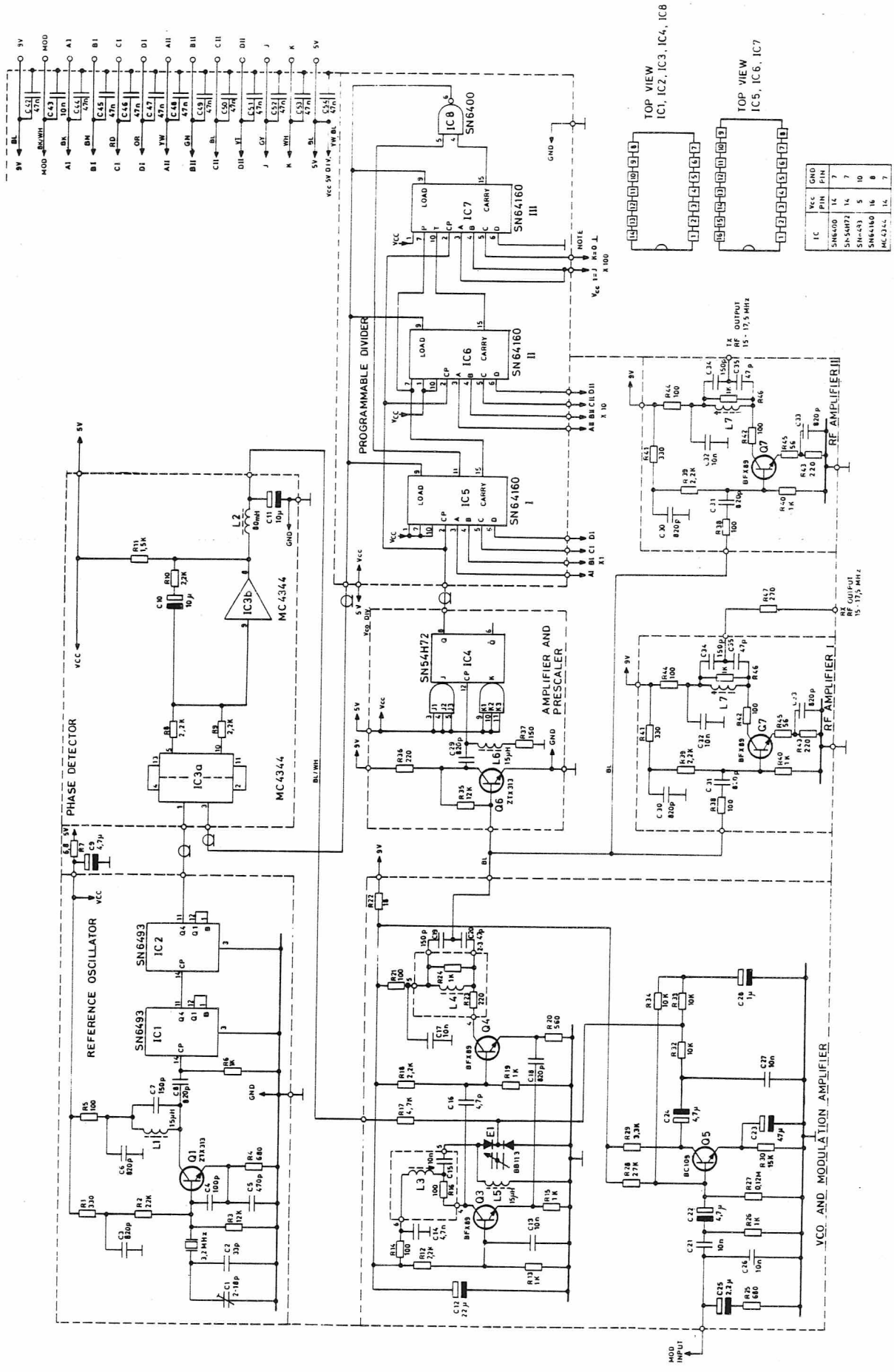
TYPE	NO.	CODE	DATA
	R26	80.5049	1 K Ω 5% carbon film
	R27	80.5074	120 K Ω 5%
	R28	80.5066	27 K Ω 5%
	R29	80.5049	1 K Ω 5%
	R30	80.5053	2.2 K Ω 5%
	R31	80.5043	330 Ω 5%
	R32	80.5061	10 K Ω 5%
	R33	80.5061	10 K Ω 5%
	R34	80.5061	10 K Ω 5%
	L3	61.1220	RF coil
	L4	61.1221	RF coil
	L5	63.5007	15 μ H 20% choke
	E1	99.5292	Triple cap. diode BB113
	Q3	99.5240	Transistor BFX89
	Q4	99.5240	Transistor BFX89
	Q5	99.5201	Transistor BC109
			AMPLIFIER AND PRESCALER
	C29	74.5314	820 pF -20+80% ceram PL
	R35	80.5062	12 K Ω 5% carbon film
	R36	80.5241	220 Ω 5%
	R37	80.5039	150 Ω 5%
	L6	63.5007	15 μ H 20% choke
	Q6	99.5293	Transistor ZTX313
	IC4	14.5062	SN54H172 Gated J-K flip-flop
			PROGRAMMABLE DIVIDER
	IC5	14.5061	SN64160 Synchronus decade counter
	IC6	14.5061	SN64160
	IC7	14.5061	SN64160
	IC8	14.5024	SN6400 Quadr. 2-input NAND-gate
			RF AMPLIFIERS (2 identical modules)
	C30	74.5314	820 pF -20+80% ceram PL
	C31	74.5314	820 pF -20+80% ceram PL
	C32	76.5070	10 nF 10% polyester FL

TYPE	NO.	CODE	DATA
	C33	74.5314	820 pF -20+80% ceram PL
	C34	76.5103	150 pF 2.5% polystyren T1B
	C35	74.5319	47 pF 2% ceram PL
	R38	80.5037	100 Ω 5% carbon film
	R39	80.5053	2.2 K Ω
	R40	80.5049	1 K Ω 5%
	R41	80.5043	330 Ω 5%
	R42	80.5037	100 Ω 5%
	R43	80.5041	220 Ω 5%
	R44	80.5037	100 Ω 5%
	R45	80.5034	56 Ω 5%
	R46	80.5049	1 K Ω 5%
	L7	61.1233	RF coil
	Q7	99.5240	Transistor BFX89

FREQUENCY SYNTHESIZER
FREKVENSSYNTESSENERHED

FS701

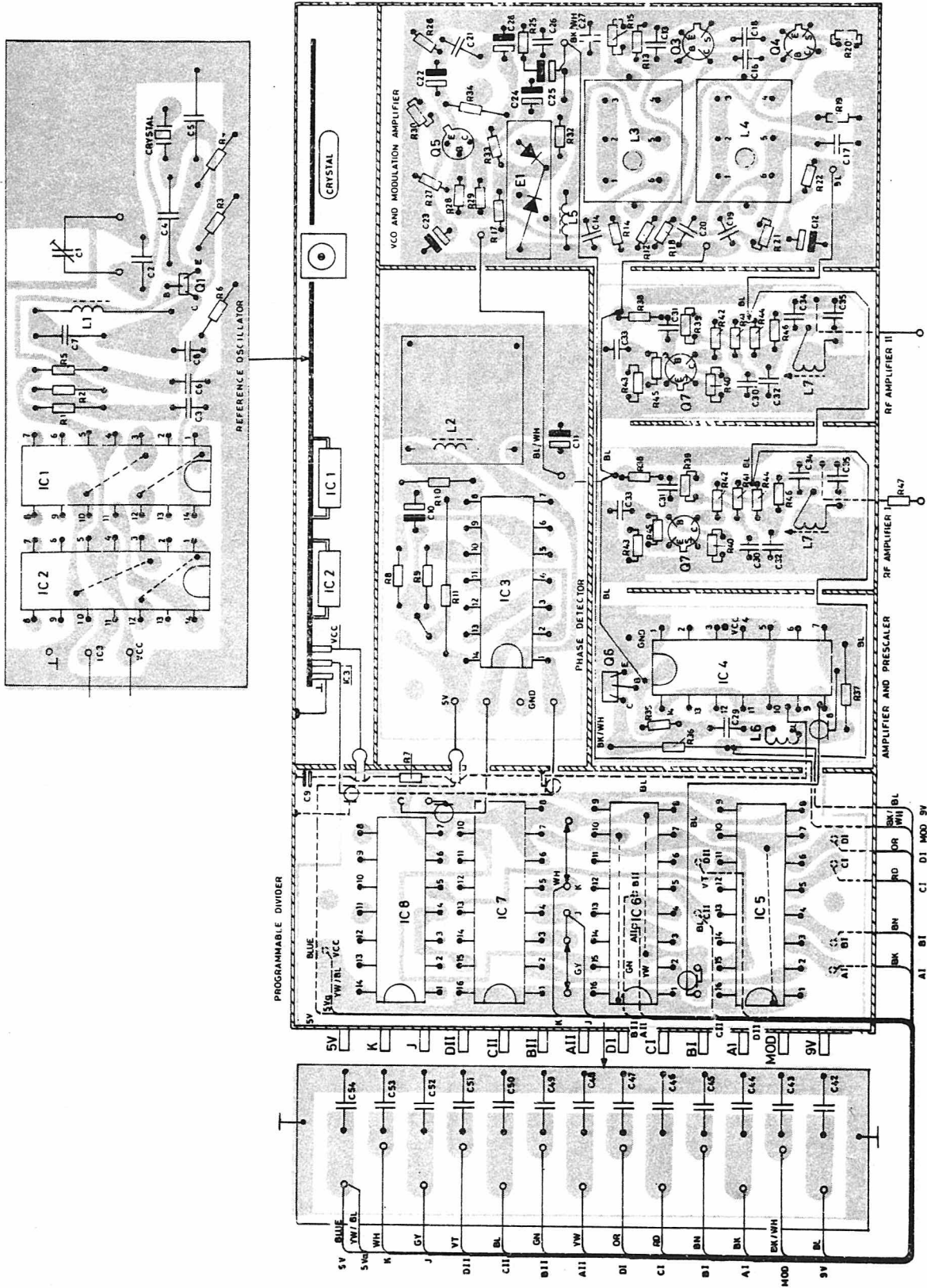
X401.863



FREQUENCY SYNTHESIZER
FREKVENS SYNTESEENHED

FS702

D 402 406



TX
RF OUTPUT
15-17.5 MHz

RX
RF OUTPUT
15-17.5 MHz

VIEWS FROM SOLDERING SIDE

FREQUENCY SYNTHESIZER
FREKVENSSYNTSEENHED

FS702

D402.550

TYPE	N ^o	CODE	DATA
FS702		10. 3503-00	Frequency Synthesizer
	C1	78. 5044	2/18 pF
	C2	74. 5116	33 pF
	C3	74. 5314	820 pF -20/+80%
	C4	76. 5102	100 pF 2.5%
	C5	76. 5065	470 pF 5%
	C6	74. 5314	820 pF -20/+80%
	C7	76. 5103	150 pF 2.5%
	C8	74. 5314	820 pF -20/+80%
	C9	73. 5126	4.7 μF 20%
	C10	73. 5109	10 μF 20%
	C11	73. 5109	10 μF 20%
	C12	73. 5127	22 μF 20%
	C13	76. 5070	10 nF 10%
	C14	76. 5061	4.7 nF 10%
	C15	76. 5070	10 nF 10%
	C16	74. 5318	4.7 pF 0.25 pF
	C17	76. 5070	10 nF 10%
	C18	74. 5314	820 pF -20/+80%
	C19	76. 5103	150 pF 2.5%
	C20	74. 5319	47 pF 2%
	C21	76. 5070	10 nF 10%
	C22	73. 5126	4.7 μF 20%
	C23	73. 5124	47 μF 20%
	C24	73. 5126	4.7 μF 20%
	C25	73. 5102	2.2 μF 20%
	C26	76. 5070	10 nF 10%
	C27	76. 5070	10 nF 10%
	C28	73. 5135	1 μF -20/+50%
	C29	74. 5314	820 pF -20/+80%
	C30	74. 5314	820 pF -20/+80%
	C31	74. 5314	820 pF -20/+80%
	C32	76. 5070	10 nF 10%
	C33	74. 5314	820 pF -20/+80%
	C34	76. 5103	150 pF 2.5%
	C35	74. 5319	47 pF 2%
	C42	74. 5283	47 nF 20%
	C43	74. 5281	10 nF 20%
	C44-C54	74. 5283	47 nF 20%
	C55	74. 5320	1 nF -20/+80%
	C56	74. 5320	1 nF -20/+80%
	R1	80. 5043	330 Ω 5%
	R2	80. 5065	22 kΩ 5%
	R3	80. 5062	12 kΩ 5%
	R4	80. 5047	680 Ω 5%
	R5	80. 5037	100 Ω 5%

TYPE	N ^o	CODE	DATA
	R6	80. 5049	1 kΩ 5%
	R7	80. 5223	6.8 Ω 5%
	R8-R10	80. 5053	2.2 kΩ 5%
	R11	80. 5051	1.5 kΩ 5%
	R12	80. 5053	2.2 kΩ 5%
	R13	80. 5049	1 kΩ 5%
	R14	80. 5037	100 Ω 5%
	R15	80. 5049	1 kΩ 5%
	R16	80. 5037	100 Ω 5%
	R17	80. 5057	4.7 kΩ 5%
	R18	80. 5053	2.2 kΩ 5%
	R19	80. 5049	1 kΩ 5%
	R20	80. 5046	560 Ω 5%
	R21	80. 5037	100 Ω 5%
	R22	80. 5028	18 Ω 5%
	R23	80. 5041	220 Ω 5%
	R24	80. 5049	1 kΩ 5%
	R25	80. 5047	680 Ω 5%
	R26	80. 5049	1 kΩ 5%
	R27	80. 5074	120 kΩ 5%
	R28	80. 5066	27 kΩ 5%
	R29	80. 5055	3.3 kΩ 5%
	R30	80. 5063	15 kΩ 5%
	R32-R34	80. 5061	10 kΩ 5%
	R35	80. 5062	12 kΩ 5%
	R36	80. 5241	220 Ω 5%
	R37	80. 5039	150 Ω 5%
	R38	80. 5037	100 Ω 5%
	R39	80. 5053	2.2 kΩ 5%
	R40	80. 5049	1 kΩ 5%
	R41	80. 5043	330 Ω 5%
	R42	80. 5037	100 Ω 5%
	R43	80. 5041	220 Ω 5%
	R44	80. 5037	100 Ω 5%
	R45	80. 5034	56 Ω 5%
	R46	80. 5049	1 kΩ 5%
	R47	80. 5042	270 Ω 5%
	L1	63. 5007	15 μH 20%
	L2	61. 1222	80 mH
	L3	61. 1220	RF coil
	L4	61. 1221	RF coil
	L5	63. 5007	15 μH 20%
			choke
			choke
			200mA
			200mA

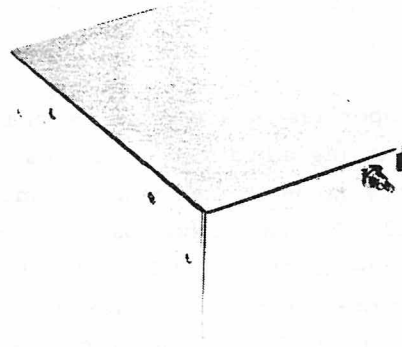
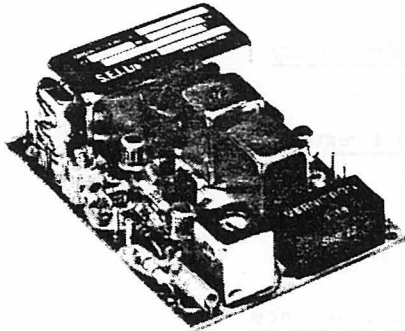
FREQUENCY SYNTHESIZER FS702

X402.467

STORNOPHONE 700
MAINTENANCE MANUAL
VOLUME II
Section 4

TITLE		Code
IC700	Description	60.185-E1
IC701	Schematic	D401.326/3
	Part List	X401.315/3
IC703	Schematic	D401.327/2
	Part List	X401.314/3
IC704	Schematic	D401.365/3
	Part List	X401.795/2
IC705	Schematic	D402.373
	Part List	X402.611
ID701	Schematic	D401.885/2
	Part List	X402.105
MT701	Schematic	D401.844
	Part List	X401.965
MT704	Installation	D402.507/2

IF CONVERTER IC701/IC703/IC704



Description

General

The IF converter converts the receiver section's 1st intermediate frequency of 10.7 MHz to 455 kHz which is the 2nd intermediate frequency

IC701 is employed in equipment for 50 kHz channel separation.

IC703 is employed in equipment for 25 kHz and for 20 kHz separation.

IC704 is employed in equipment for 12.5 kHz channel separation.

All IC700 units contain the following stages:

- a 10.7 MHz crystal filter
- a high intermediate frequency amplifier
- a local oscillator
- a mixer
- a 455 kHz ceramic filter

Crystal Filters

The requirements for selectivity are partly met through use of the crystal filter and partly through the 455 kHz ceramic filter in the output of the unit.

There are 3 different crystal filters employed, according to channel separation. One is for IC701, one is for IC703 and the last is for IC704. In IC701 and IC703 there are 4 crystals in the filter and in IC704 there are 6. The matching impedances for all three types are identical.

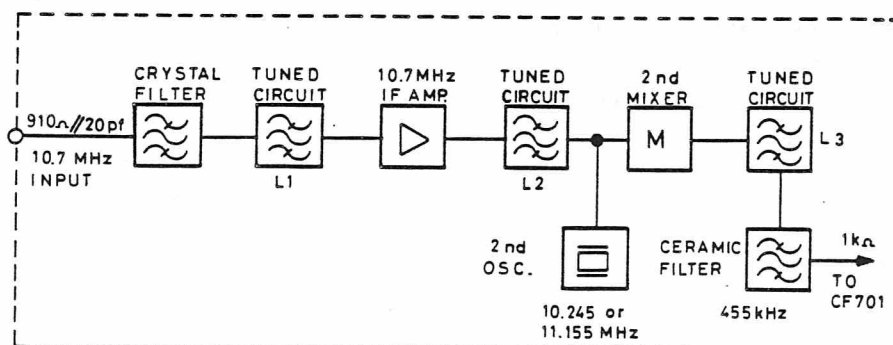
The crystal filter is coupled to the high intermediate frequency stage, Q1, through a parallel resonant circuit.

High IF Amplifier

A transistor having a low noise figure and minimum internal feedback is chosen for this circuit so that variations in the collector impedance will have negligible influence on the crystal matching impedance.

Oscillator

The oscillator is a crystal driven Colpitts oscillator in a grounded collector configuration. The crystal frequency is normally 10.245 MHz but in cases where



a harmonic of the local oscillator coincides with the receiver antenna frequency, interference can occur. Therefore, a crystal frequency of 11.155 MHz would be employed instead.

The crystal operates in a parallel resonant circuit; fine-tuning adjustment of the oscillator frequency is performed with trimmer capacitor C12. The capacitive load for the crystal is made up of C14, C15 and C16, which also forms the necessary feedback loop. Variations in the IF amplifier have negligible influence on the oscillator frequency.

Mixer

The local oscillator signal and the 10.7 MHz IF signal are applied to the base of Q2. To achieve greater amplification, a bipolar transistor is employed here. In order that the bipolar mixer, however, does not deteriorate the excellent blocking and intermodulation characteristics achieved with the FET mixer in the receiver converter module, the crystal filter has been inserted.

Ceramic Filter

From the collector of the 2nd mixer the signal is passed via matching network L3 to a ceramic 455 kHz filter.

There are 3 different types of ceramic filters, one for each IC700 unit.

Strong signals can alter the output impedance of the 2nd mixer as well as the input impedance in the CF701 unit. Attenuating resistors are therefore inserted before and after the ceramic filter in order to ensure the least possible variation in filter matching impedance.

From the output of the ceramic filter the 455 kHz IF signal is coupled to the IF circuitry in CF701.

Technical Specifications

Converter IC701

Input Frequency

10.7 MHz

Output Frequency

455 kHz

Input Impedance

$910 \Omega // 20 \text{ pF}$

Output Impedance

1 k Ω

Maximum Frequency Deviation

$\pm 15 \text{ kHz}$

Bandwidth

At 3 dB attenuation relative to 10.7 MHz:

$> \pm 12 \text{ kHz}$

$< \pm 20 \text{ kHz}$

At 70 dB attenuation relative to 10.7 MHz:

$< \pm 35 \text{ kHz}$

Bandpass Ripple (typ. 1 dB)

gar. $< 3 \text{ dB}$

Oscillator Frequency

Crystal spec. S-98-12 in temp. range

-25° to $+65^{\circ}\text{C}$: 10.245 MHz or 11.155 MHz

Oscillator Frequency adjustable by

$> \pm 30 \times 10^{-6}$

Voltage Gain (typ. 23 dB)

gar. $> 20 \text{ dB}$

Current Consumption typ. 8 mA

Temperature Range

operating range: -25° to $+65^{\circ}\text{C}$

functioning range: -30° to $+75^{\circ}\text{C}$

Converter IC703Input Frequency

10.7 MHz

Output Frequency

455 kHz

Input Impedance910 Ω // 20 pFOutput Impedance1 k Ω Maximum Frequency DeviationAt 20 kHz bandwidth: \pm 4 kHzAt 25 kHz bandwidth: \pm 5 kHzBandwidth

At 3 dB attenuation relative to 10.7 MHz:

 $> \pm$ 5 kHz $< \pm$ 8.5 kHz

At 75 dB attenuation relative to 10.7 MHz:

 \pm 17 kHzBand-pass Ripple(typ. 1 dB)gar. $<$ 3 dBOscillator FrequencyCrystal specification S-98-12 in temp. range
 -25° to $+65^{\circ}$ C: 10.245 MHz or 11.155 MHzOscillator Frequency Adjustable by $> \pm$ 30×10^{-6} Voltage Gain (typ. 26 dB)gar. $>$ 23 dBCurrent Consumption typ. 8 mATemperature Rangeoperating range: -25 to $+65^{\circ}$ Cfunctioning range: -30 to $+75^{\circ}$ CConverter IC704Input Frequency

10.7 MHz

Output Frequency

455 kHz

Input Impedance910 Ω // 20 pFOutput Impedance1 k Ω Maximum Frequency Deviation \pm 2.5 kHzBandwidth

at 3 dB attenuation relative to 10.7 MHz:

 $> \pm$ 2.7 kHz

at 6 dB attenuation relative to 10.7 MHz:

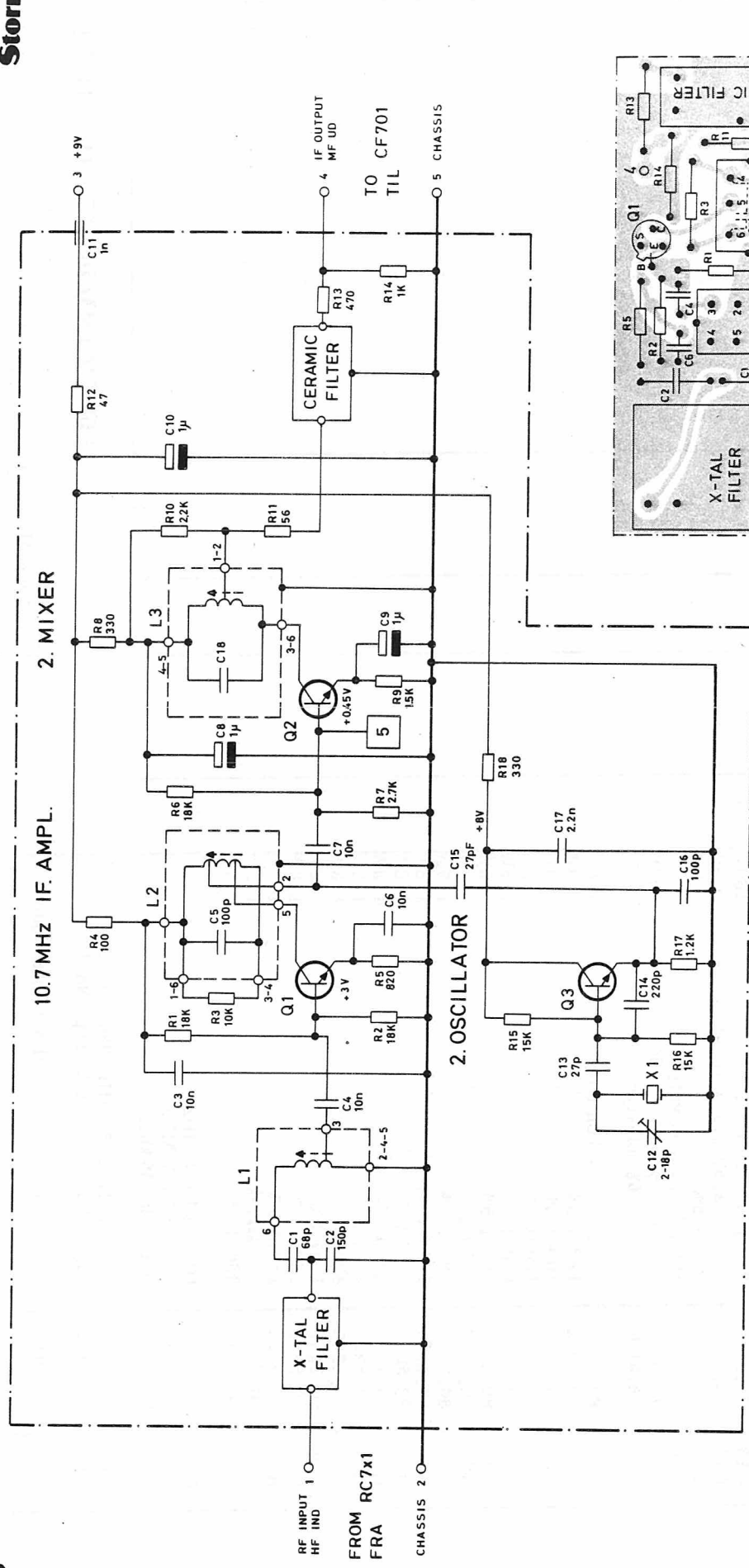
 $< \pm$ 3.8 kHz

at 80 dB attenuation relative to 10.7 MHz:

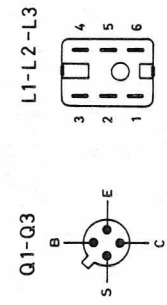
 $< \pm$ 10 kHzEand-Pass Ripple, typ. 1 dB: gar. $<$ 3 dBOscillator FrequencyCrystal spec. S-98-12 in temperature range
 -25° to $+65^{\circ}$ C: 10.245 or 11.155 MHzOscillator Frequency Adjustable by $> \pm$ 30×10^{-6} Voltage Gain (typ. 23 dB)gar. $>$ 20 dBCurrent Consumption

8 mA

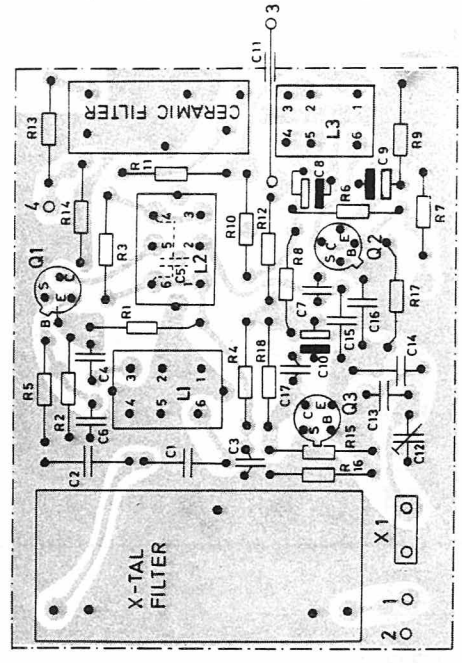
Temperature Rangeoperating range: -25° to $+65^{\circ}$ Cfunctioning range: -30° to $+75^{\circ}$ C



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
 TRYKT KREDSLØB SET FRA KOMPONENTSIDEN



BOTTOM VIEW
 SET FRA BUNDEN

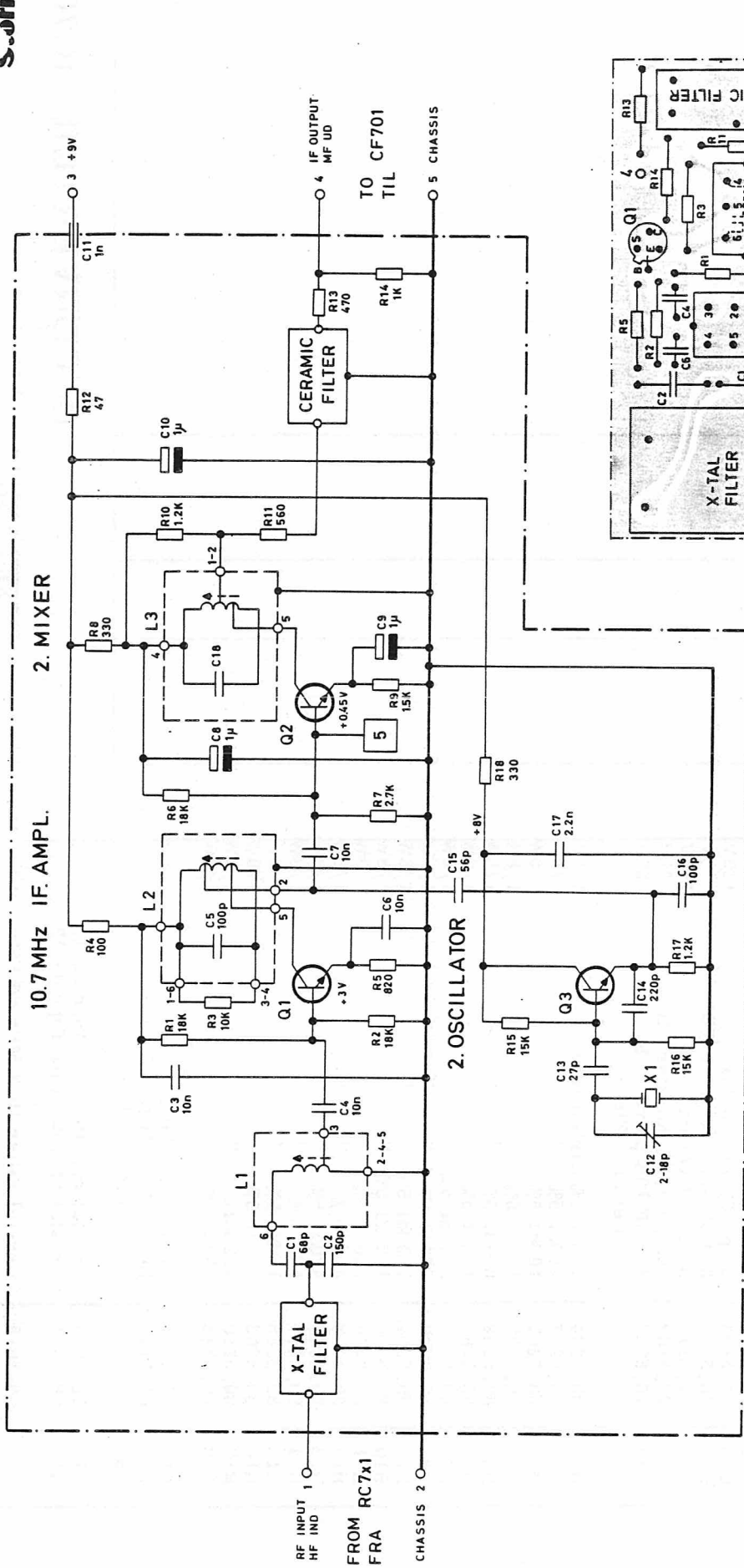


IF CONVERTER IC701

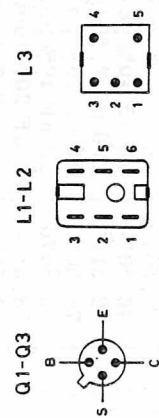
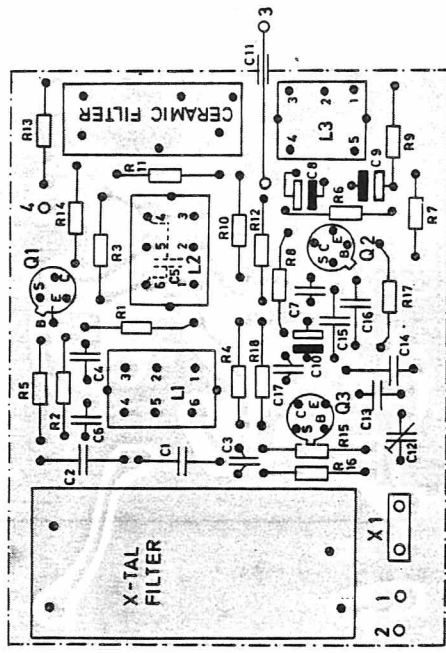
TYPE	NO.	CODE	DATA
IC701		10. 2435	IF Converter
	C1	76. 5101	68 pF 2. 5% polystyr TB 25V
	C2	76. 5103	150 pF 2. 5% polystyr TB 25V
	C3	76. 5070	10 nF 10% polyest. FL 50V
	C4	76. 5070	10 nF 10% polyest. FL 50V
	C5	76. 5102	100 pF 2. 5% polystyr TB 25V
	C6	76. 5070	10 nF 10% polyest. FL 50V
	C7	76. 5070	10 nF 10% polyest. FL 50V
	C8	73. 5114	1 μF 20% tantal 35V
	C9	73. 5114	1 μF 20% tantal 35V
	C10	73. 5114	1 μF 20% tantal 35V
	C11	74. 5167	1 nF -20 +80% ceram FT 300V
	C12	78. 5044	2-18 pF trimmer 300V
	C13	74. 5192	27 pF 5% ceram TB 160V
	C14	76. 5104	220 pF 2. 5% polystyr TB 25V
	C15	74. 5107	27 pF 5% ceram 160V
	C16	76. 5102	100 pF 2. 5% polystyr TB 25V
	C17	76. 5059	2. 2 nF 10% polyest. FL 50V
	C18	76. 5106	470 pF 2. 5% polystyr 25V
	R1	80. 5264	18 kΩ 5% carbon film 1/8W
	R2	80. 5264	18 kΩ 5% " " 1/8W
	R3	80. 5261	10 kΩ 5% " " 1/8W
	R4	80. 5237	100 Ω 5% " " 1/8W
	R5	80. 5248	820 Ω 5% " " 1/8W
	R6	80. 5264	18 kΩ 5% " " 1/8W
	R7	80. 5254	2. 7 kΩ 5% " " 1/8W
	R8	80. 5243	330 Ω 5% " " 1/8W
	R9	80. 5251	1. 5 kΩ 5% " " 1/8W
	R10	80. 5253	2. 2KΩ 5% " " 1/8W
	R11	80. 5234	56 Ω 5% " " 1/8W
	R12	80. 5233	47 Ω 5% " " 1/8W
	R13	80. 5245	470 Ω 5% " " 1/8W
	R14	80. 5249	1 kΩ 5% " " 1/8W
	R15	80. 5263	15 kΩ 5% " " 1/8W
	R16	80. 5263	15 kΩ 5% " " 1/8W
	R17	80. 5250	1. 2 kΩ 5% " " 1/8W
	R18	80. 5243	330 Ω 5% " " 1/8W
	L1	61. 1122	IF coil 10. 7 MHz
	L2	61. 1123	IF coil 10. 7 MHz
	L3	61. 1302	IF Coil 0. 455 MHz
	X1	98. 5010	Crystal 10. 2450 MHz Type 98-12
	X1	98. 5011	Crystal 11. 1550 MHz Type 98-12
		69. 5015	Crystal Filter 10. 7 MHz 50 KHz 50dB

IF CONVERTER IC701

X401. 315/3



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN



BOTTOM VIEW
SET FRA BUNDEN

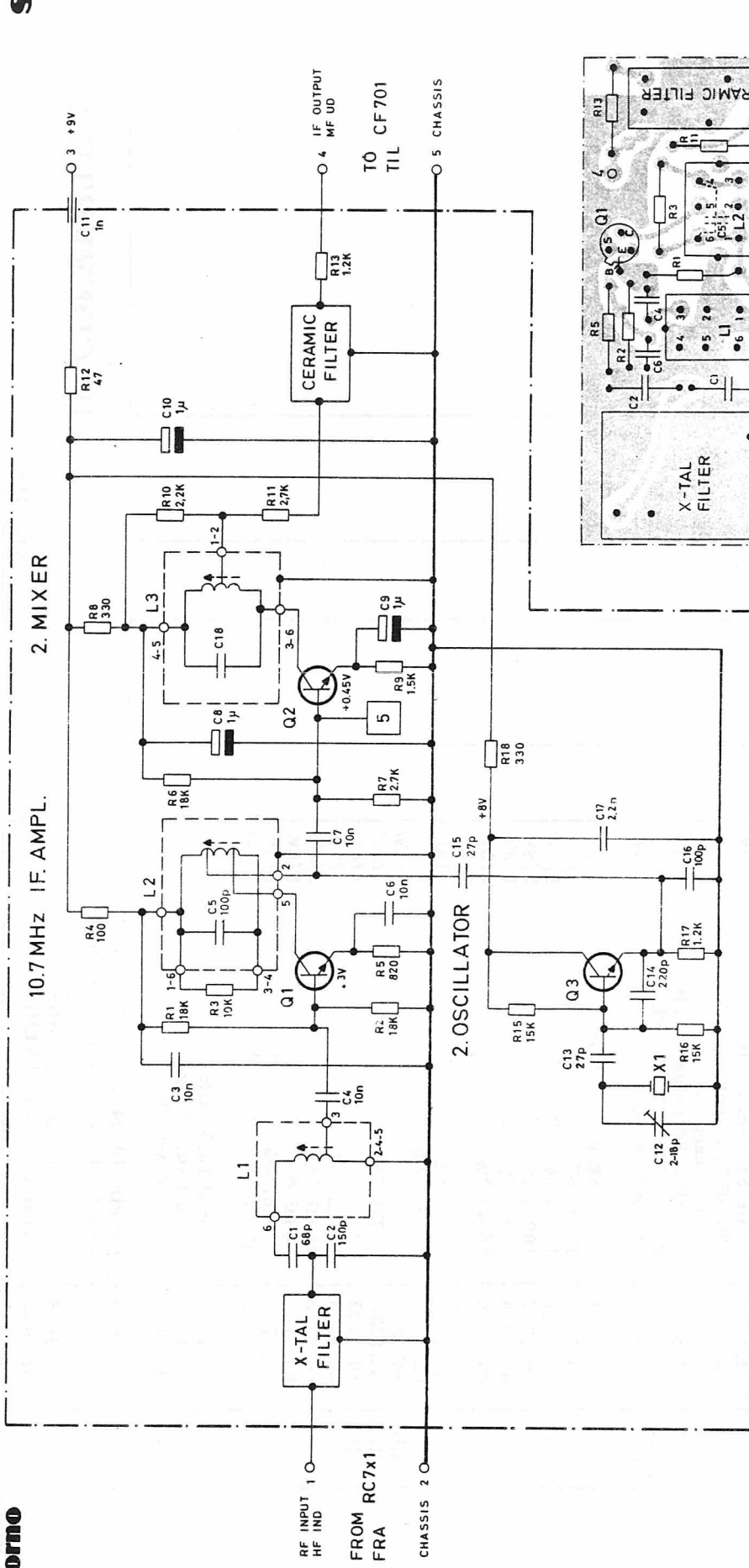
IF CONVERTER IC701

TYPE	NO.	CODE	DATA
IC701		10. 2435	IF Converter
	C1	76. 5101	68 pF 2.5% polystyr TB
	C2	76. 5103	150 pF 2.5% polystyr TB
	C3	76. 5070	10 nF 10% polyest. FL
	C4	76. 5070	10 nF 10% polyest. FL
	C5	76. 5102	100 pF 2.5% polystyr TB
	C6	76. 5070	10 nF 10% polyest. FL
	C7	76. 5070	10 nF 10% polyest. FL
	C8	73. 5114	1 μF 20% tantal
	C9	73. 5114	1 μF 20% tantal
	C10	73. 5114	1 μF 20% tantal
	C11	74. 5167	1 nF -20 +80% ceram FT
	C12	78. 5044	2-18 pF trimmer
	C13	74. 5192	27 pF 5% ceram TB
	C14	76. 5104	220 pF 2.5% polystyr TB
	C15	74. 5111	56 pF 5% ceram
	C16	76. 5102	100 pF 2.5% polystyr TB
	C17	76. 5059	2.2 nF 10% polyest. FL
	C18		See Ceramic Filter
	R1	80. 5264	18 kΩ 5% carbon film
	R2	80. 5264	18 kΩ 5% "
	R3	80. 5261	10 kΩ 5% "
	R4	80. 5237	100 Ω 5% "
	R5	80. 5248	820 Ω 5% "
	R6	80. 5264	18 kΩ 5% "
	R7	80. 5254	2.7 kΩ 5% "
	R8	80. 5243	330 Ω 5% "
	R9	80. 5251	1.5 kΩ 5% "
	R10	80. 5250	1.2 kΩ 5% "
	R11	80. 5246	560 Ω 5% "
	R12	80. 5233	47 Ω 5% "
	R13	80. 5245	470 Ω 5% "
	R14	80. 5249	1 kΩ 5% "
	R15	80. 5263	15 kΩ 5% "
	R16	80. 5263	15 kΩ 5% "
	R17	80. 5250	1.2 kΩ 5% "
	R18	80. 5243	330 Ω 5% "
	L1	61. 1122	IF coil 10.7 MHz
	L2	61. 1123	IF coil 10.7 MHz
	L3		See Ceramic Filter
	X1	98. 5010	Crystal 10.2450 MHz Type 98-12
	X1	98. 5011	Crystal 11.1550 MHz Type 98-12
		69. 5015	Crystal Filter 10.7 MHz 50 KHz 50dB

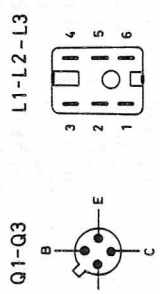
TYPE	NO.	CODE	DATA
		69. 5013-01	Ceramic Filter 455 kHz L3 and C18 included
	Q1	99. 5168	BF173 Transistor
	Q2	99. 5166	BF167 Transistor
	Q3	99. 5168	BF173 Transistor

IF CONVERTER IC701

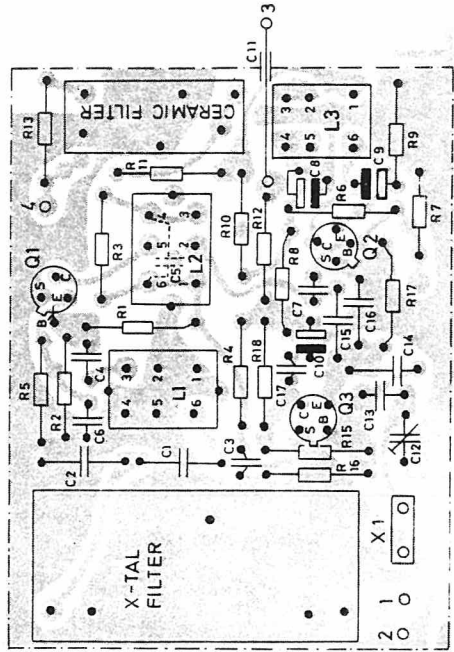
X401.315/2



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN.



BOTTOM VIEW
SET FRA BUNDEN



IF CONVERTER
MF KONVERTER

IC703

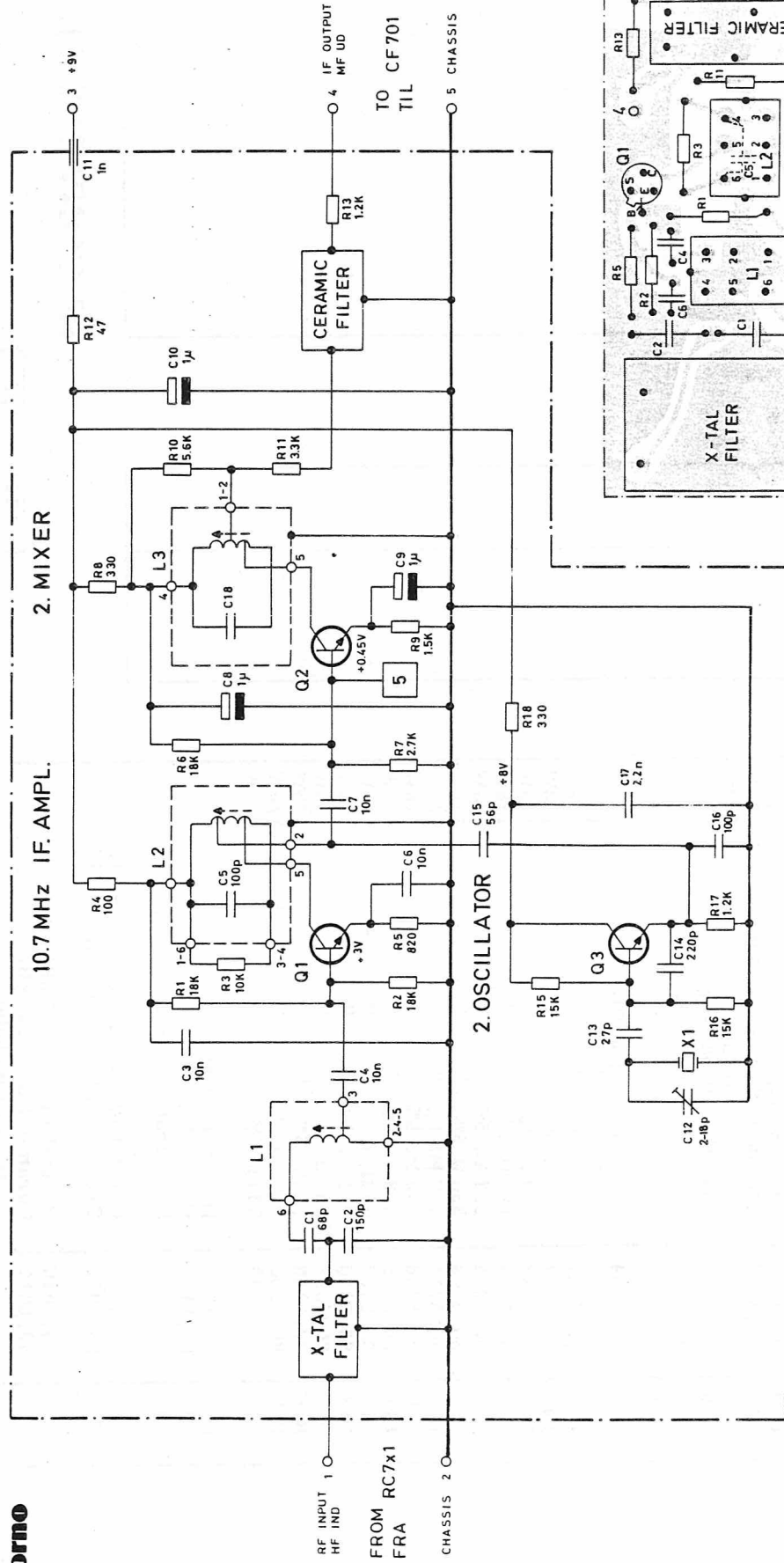
D401327/2

TYPE	NO.	CODE	DATA
IC703		10.2432	IF Converter
	C1	76.5101	68 pF 2.5% polystyr TB 25V
	C2	76.5103	150 pF 2.5% polystyr TB 25V
	C3	76.5070	10 nF 10% polyest. FL 50V
	C4	76.5070	10 nF 10% polyest. FL 50V
	C5	76.5102	100 pF 2.5% polystyr TB 25V
	C6	76.5070	10 nF 10% polyest. FL 50V
	C7	76.5070	10 nF 10% polyest. FL 50V
	C8	73.5114	1 μF 20% tantal 35V
	C9	73.5114	1 μF 20% tantal 35V
	C10	73.5114	1 μF 20% tantal 35V
	C11	74.5167	1 nF -20 +80% ceram FT 300V
	C12	78.5044	2-18 pF trimmer 300V
	C13	74.5192	27 pF 5% ceram TB 160V
	C14	76.5104	220 pF 2.5% polystyr TB 25V
	C15	74.5107	27 pF 5% ceram TB 160V
	C16	76.5102	100 pF 2.5% polystyr TB 25V
	C17	76.5059	2.2 nF 10% polyest. FL 50V
	C18	76.5106	470 pF 2.5% polystyr 25V
	R1	80.5264	18 kΩ 5% carbon film 1/8W
	R2	80.5264	18 kΩ 5% " " 1/8W
	R3	80.5261	10 kΩ 5% " " 1/8W
	R4	80.5237	100 Ω 5% " " 1/8W
	R5	80.5248	820 Ω 5% " " 1/8W
	R6	80.5264	18 kΩ 5% " " 1/8W
	R7	80.5254	2.7 kΩ 5% " " 1/8W
	R8	80.5243	330 Ω 5% " " 1/8W
	R9	80.5254	2.7 kΩ 5% " " 1/8W
	R10	80.5234	56 Ω 5% " " 1/8W
	R11	80.5254	2.7 kΩ 5% " " 1/8W
	R12	80.5233	47 Ω 5% " " 1/8W
	R13	80.5250	1.2 kΩ 5% " " 1/8W
	R15	80.5263	15 kΩ 5% " " 1/8W
	R16	80.5263	15 kΩ 5% " " 1/8W
	R17	80.5250	1.2 kΩ 5% " " 1/8W
	R18	80.5243	330 Ω 5% " " 1/8W
	L1	61.1122	IF coil 10.7 MHz
	L2	61.1123	IF coil 10.7 MHz
	L3	61.1302	IF coil 0.455 MHz
	X1	98.5010	Crystal 10.2450 MHz Type 98-12
	X1	98.5011	Crystal 11.1550 MHz Type 98-12
		69.5016	Crystal Filter 10.7 MHz
		69.5031	Ceramic Filter 455 kHz

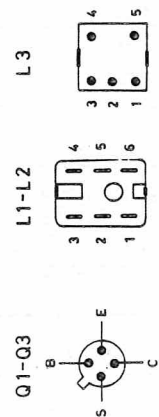
TYPE	NO.	CODE	DATA
	Q1	99.5168	BF173 Transistor
	Q2	99.5166	BF167 Transistor
	Q3	99.5168	BF173 Transistor

IF CONVERTER IC703

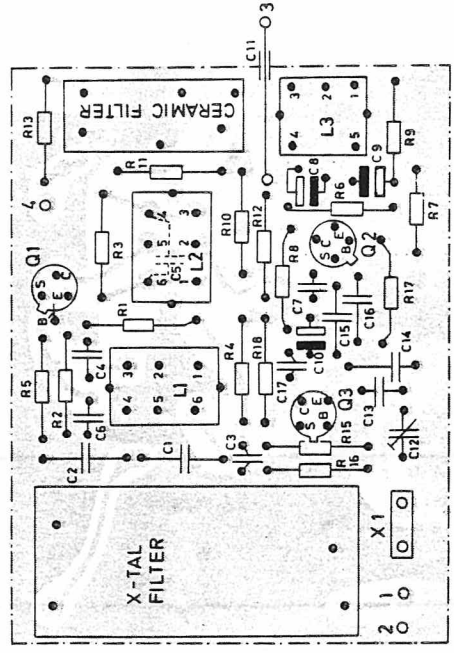
X401.314/4



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
 TRYKT KREDSLØB SET FRA KOMPONENTSIDEN.



BOTTOM VIEW
 SET FRA BUNDEN



IF CONVERTER
 MF KONVERTER

IC703

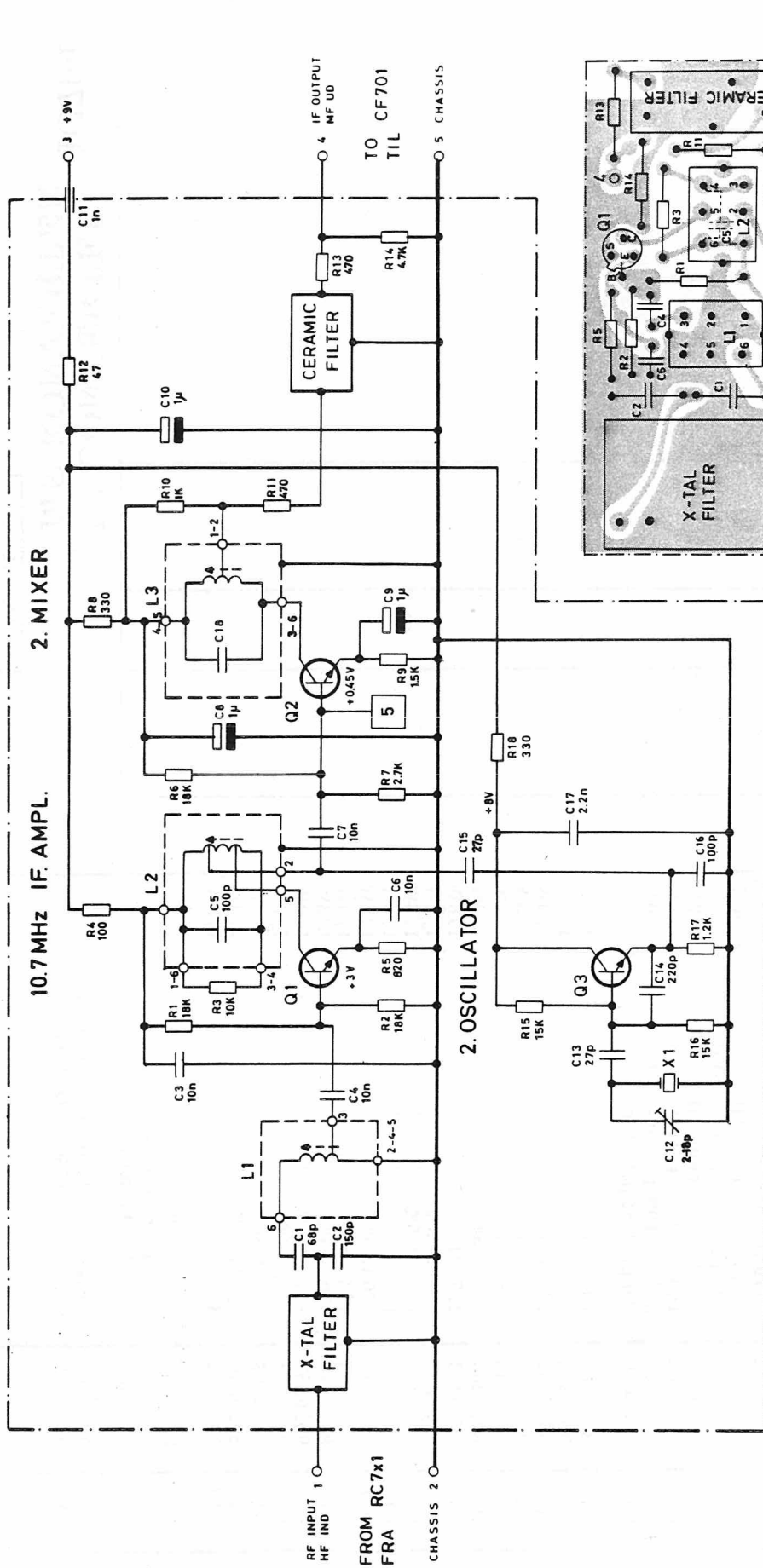
D401.327

TYPE	NO.	CODE	DATA
1C703		10.2432	IF Converter
	C1	76.5101	68 pF 2.5% polystyr TB
	C2	76.5103	150 pF 2.5% polystyr TB
	C3	76.5070	10 nF 10% polyest. FL
	C4	76.5070	10 nF 10% polyest. FL
	C5	76.5102	100 pF 2.5% polystyr TB
	C6	76.5070	10 nF 10% polyest. FL
	C7	76.5070	10 nF 10% polyest. FL
	C8	73.5114	1 μF 20% tantal
	C9	73.5114	1 μF 20% tantal
	C10	73.5114	1 μF 20% tantal
	C11	74.5167	1 nF -20 +80% ceram FT
	C12	78.5044	2-18 pF trimmer
	C13	74.5192	27 pF 5% ceram TB
	C14	76.5104	220 pF 2.5% polystyr TB
	C15	74.5111	56 pF 5% ceram TB
	C16	76.5102	100 pF 2.5% polystyr TB
	C17	76.5059	2.2 nF 10% polyest. FL
	C18		See Ceramic Filter
	R1	80.5264	18 kΩ 5% carbon film
	R2	80.5264	18 kΩ 5% "
	R3	80.5261	10 kΩ 5% "
	R4	80.5237	100 Ω 5% "
	R5	80.5248	820 Ω 5% "
	R6	80.5264	18 kΩ 5% "
	R7	80.5254	2.7 kΩ 5% "
	R8	80.5243	330 Ω 5% "
	R9	80.5254	2.7 kΩ 5% "
	R10	80.5258	5.6 kΩ 5% "
	R11	80.5255	3.3 kΩ 5% "
	R12	80.5233	47 Ω 5% "
	R13	80.5250	1.2 kΩ 5% "
	R15	80.5263	15 kΩ 5% "
	R16	80.5263	15 kΩ 5% "
	R17	80.5250	1.2 kΩ 5% "
	R18	80.5243	330 Ω 5% "
	L1	61.1122	IF coil 10.7 MHz
	L2	61.1123	IF coil 10.7 MHz
	L3		See Ceramic Filter
	X1	98.5010	Crystal 10.2450 MHz Type 98-12
	X1	98.5011	Crystal 11.1550 MHz Type 98-12
		69.5016	Crystal Filter 10.7 MHz
		69.5014	Ceramic Filter 455 kHz
			L3 and C18 included

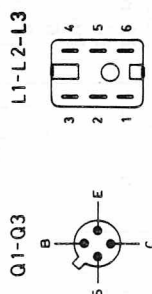
TYPE	NO.	CODE	DATA
	Q1	99.5168	BF173 Transistor
	Q2	99.5166	BF167 Transistor
	Q3	99.5168	BF173 Transistor

IF CONVERTER IC703

X401.314/2



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
 TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

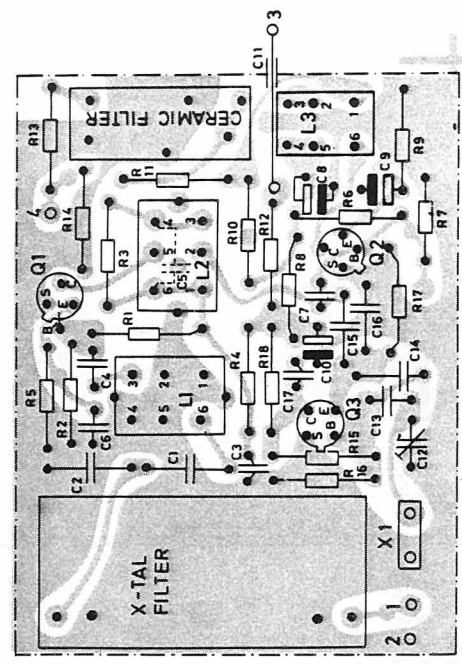


BOTTOM VIEW
 SET FRA BUNDEN

IF CONVERTER
 MF KONVERTER

IC704

D401.365/3

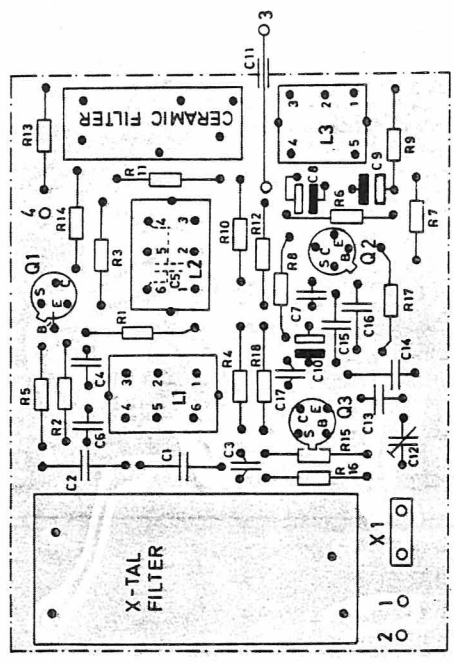
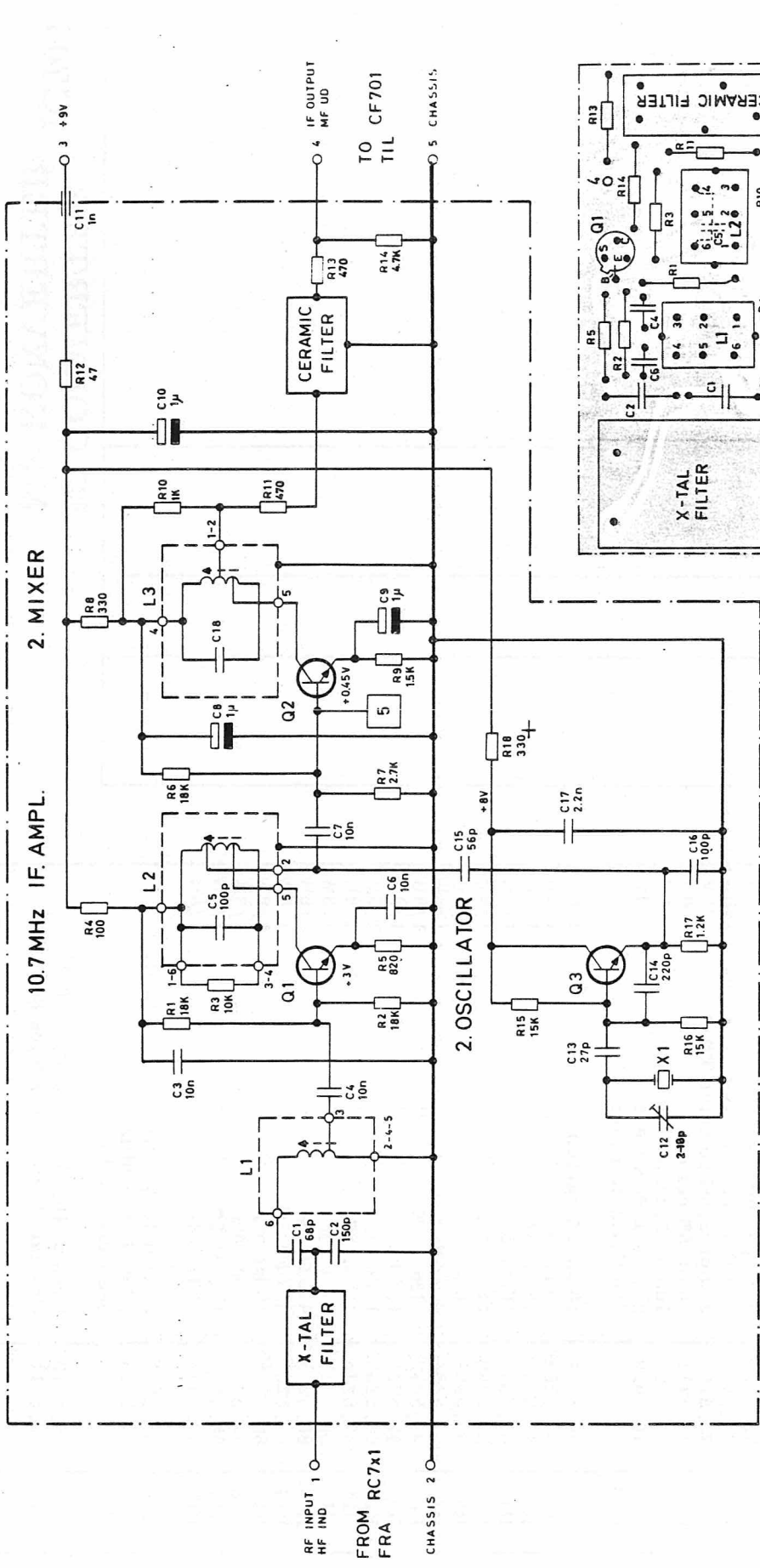


TYPE	NO.	CODE	DATA
IC704		10.2517	IF Converter
	C1	76.5101	68 pF 2.5% polystyr TB
	C2	76.5103	150 pF 2.5% polystyr TB
	C3	76.5070	10 nF 10% polyest. FL
	C4	76.5070	10 nF 10% polyest. FL
	C5	76.5102	100 pF 2.5% polystyr TB
	C6	76.5070	10 nF 10% polyest. FL
	C7	76.5070	10 nF 10% polyest. FL
	C8	73.5114	1 μF 20% tantal
	C9	73.5114	1 μF 20% tantal
	C10	73.5114	1 μF 20% tantal
	C11	74.5167	1 nF -20 +80% ceram FT
	C12	78.5044	2-18 pF trimmer
	C13	74.5192	27 pF 5% ceram TB
	C14	76.5104	220 pF 2.5% polystyr TB
	C15	74.5107	27 pF 5% ceram TB
	C16	76.5102	100 pF 2.5% polystyr TB
	C17	76.5059	2.2 nF 10% polyest. FL
	C18	76.5106	470 pF 2.5% polystyr
	R1	80.5264	18 kΩ 5% carbon film
	R2	80.5264	18 kΩ 5% "
	R3	80.5261	10 kΩ 5% "
	R4	80.5237	100 Ω 5% "
	R5	80.5248	820 Ω 5% "
	R6	80.5264	18 kΩ 5% "
	R7	80.5254	2.7 kΩ 5% "
	R8	80.5243	330 Ω 5% "
	R9	80.5251	1.5 kΩ 5% "
	R10	80.5249	1 kΩ 5% "
	R11	80.5245	470 Ω 5% "
	R12	80.5233	47 Ω 5% "
	R13	80.5245	470 Ω 5% "
	R14	80.5257	4.7 kΩ 5% "
	R15	80.5263	15 kΩ 5% "
	R16	80.5263	15 kΩ 5% "
	R17	80.5250	1.2 kΩ 5% "
	R18	80.5243	330 Ω 5% "
	L1	61.1122	IF coil 10.7 MHz
	L2	61.1123	IF coil 10.7 MHz
	L3	61.1302	IF coil 0.455 MHz
	X1	98.5010	Crystal 10.2450 MHz Type 98-12
	X1	98.5011	Crystal 11.1550 MHz Type 98-12

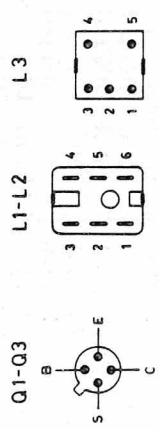
TYPE	NO.	CODE	DATA
		69.5018 69.5014-00	Crystal Filter 10.7 MHz Ceramic Filter 455 kHz
	Q1 Q2 Q3	99.5168 99.5166 99.5168	BF173 Transistor BF167 Transistor BF173 Transistor

IF CONVERTER IC704
MF KONVERTER

X401.795/2



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN



BOTTOM VIEW
SET FRA BUNDEN

IF CONVERTER
MF KONVERTER

IC704

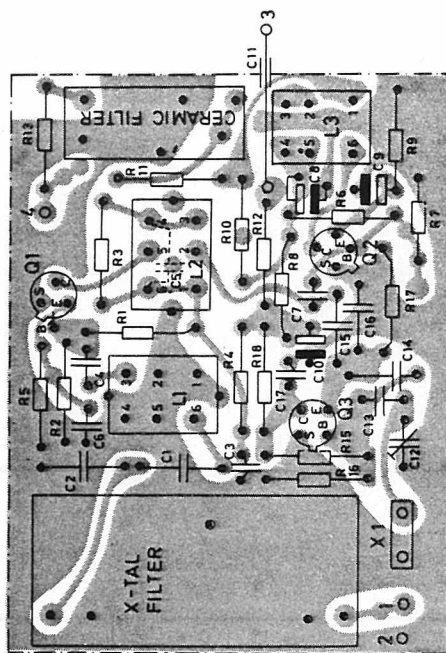
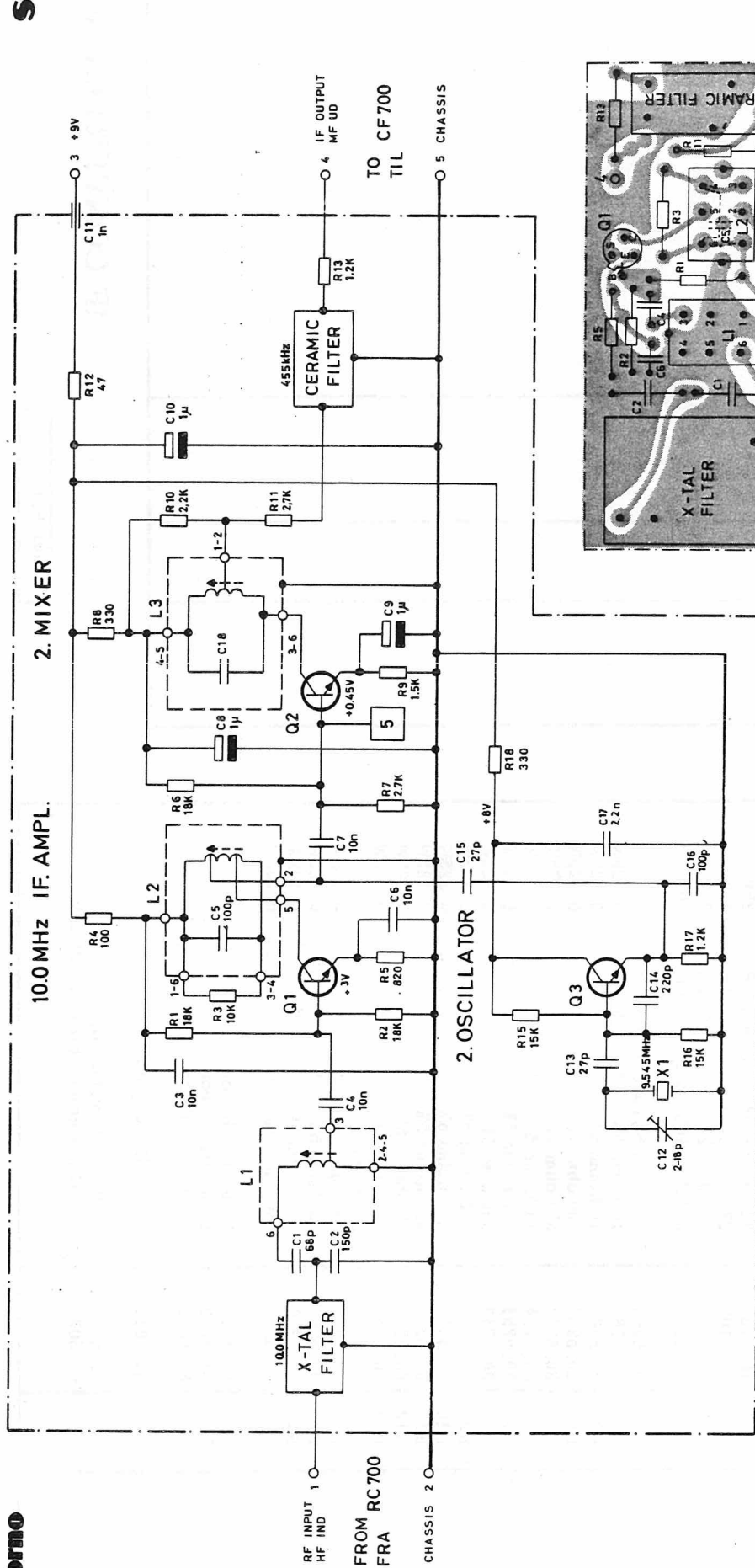
D401.365/2

TYPE	NO.	CODE	DATA
IC704		10.2517	IF Converter
	C1	76.5101	68 pF 2.5% polystyr TB
	C2	76.5103	150 pF 2.5% polystyr TB
	C3	76.5070	10 nF 10% polyester, FL
	C4	76.5070	10 nF 10% polyester, FL
	C5	76.5102	100 pF 2.5% polystyr TB
	C6	76.5070	10 nF 10% polyester, FL
	C7	76.5070	10 nF 10% polyester, FL
	C8	73.5114	1 μ F 20% tantal
	C9	73.5114	1 μ F 20% tantal
	C10	73.5114	1 μ F 20% tantal
	C11	74.5167	1 nF -20 +80% ceram FT
	C12	78.5044	2-18 pF trimmer
	C13	74.5192	27 pF 5% ceram TB
	C14	76.5104	220 pF 2.5% polystyr TB
	C15	74.5111	56 pF 5% ceram TB
	C16	76.5102	100 pF 2.5% polystyr TB
	C17	76.5059	2.2 nF 10% polyester, FL
	C18		See Ceramic Filter
	R1	80.5264	18 k Ω 5% carbon film
	R2	80.5264	18 k Ω 5% " "
	R3	80.5261	" " " "
	R4	80.5237	100 k Ω 5% " "
	R5	80.5248	820 Ω 5% " "
	R6	80.5264	18 k Ω 5% " "
	R7	80.5254	2.7 k Ω 5% " "
	R8	80.5243	330 Ω 5% " "
	R9	80.5251	1.5 k Ω 5% " "
	R10	80.5249	1 k Ω 5% " "
	R11	80.5245	470 Ω 5% " "
	R12	80.5233	47 Ω 5% " "
	R13	80.5245	470 Ω 5% " "
	R14	80.5257	4.7 k Ω 5% " "
	R15	80.5263	15 k Ω 5% " "
	R16	80.5263	15 k Ω 5% " "
	R17	80.5250	1.2 k Ω 5% " "
	R18	80.5243	330 Ω 5% " "
	L1	61.1122	IF coil 10.7 MHz
	L2	61.1123	IF coil 10.7 MHz
	L3		See Ceramic Filter
	X1	98.5010	Crystal 10.2450 MHz Type 98-12
	X1	98.5011	Crystal 11.1550 MHz Type 98-12

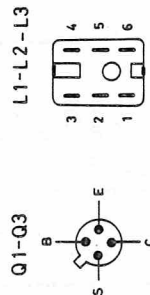
TYPE	NO.	CODE	DATA
		69.5018	Crystal Filter 10.7 MHz
		69.5019	Ceramic Filter 455 kHz L3 and C18 included
	Q1	99.5168	BF173 Transistor
	Q2	99.5166	BF167 Transistor
	Q3	99.5168	BF173 Transistor

IF CONVERTER IC704
MF KONVERTER

X401.795



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
 TRYKT KREDSLØB SET FRA KOMPONENTSIDEN.



BOTTOM VIEW
 SET FRA BUNDEN

IF CONVERTER
 MF KONVERTER

IC705

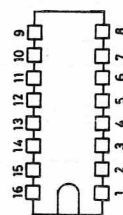
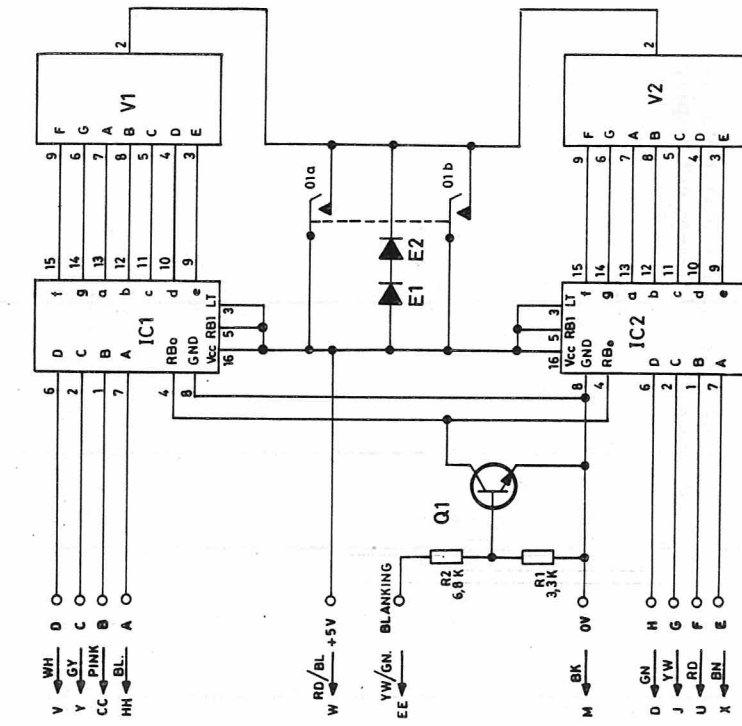
D402.373

TYPE	Nº	CODE	DATA
		10. 3498	IC 705 IF Converter
	C1	76. 5101	68pF 2. 5% polystyr. TB 25V
	C2	76. 5103	150pF 2. 5% polystyr. TB 25V
	C3	76. 5070	10nF 10% polyest. FL 50V
	C4	76. 5070	10nF 10% polyest. FL 50V
	C5	76. 5102	100pF 2. 5% polyest. FL 50V
	C6	76. 5070	10nF 10% polyest. FL 50V
	C7	76. 5070	10nF 10% polyest. FL 50V
	C8	73. 5114	1uF 20% tantal. 35V
	C9	73. 5114	1uF 20% tantal. 35V
	C10	73. 5114	1uF 20% tantal. 35V
	C11	74. 5167	1nF- 20/+80% ceram FT 300V
	C12	78. 5044	2-18pF teflon 300V
	C13	74. 5192	27pF 5% ceram TB 160V
	C14	76. 5104	220pF 2. 5% polystyr. TB 25V
	C15	74. 5107	27pF 5% ceram. TB 160V
	C16	76. 5102	100pF 2. 5% polystyr. TB 25V
	C17	76. 5059	2. 2nF 10% polyest. FL 50V
	R1	80. 5264	18 Kohm 5% carbon film 0. 125W
	R2	80. 5264	18 Kohm 5% " " 0. 125W
	R3	80. 5261	10 Kohm 5% " " 0. 125W
	R4	80. 5237	100 ohm 5% " " 0. 125W
	R5	80. 5248	820 ohm 5% " " 0. 125W
	R6	80. 5264	18 Kohm 5% " " 0. 125W
	R7	80. 5254	2. 7 Kohm 5% " " 0. 125W
	R8	80. 5243	330 ohm 5% " " 0. 125W
	R9	80. 5251	1. 5 Kohm 5% " " 0. 125W
	R10	80. 5253	2. 2 Kohm 5% " " 0. 125W
	R11	80. 5254	2. 7 Kohm 5% " " 0. 125W
	R12	80. 5233	47 ohm 5% " " 0. 125W
	R13	80. 5250	1. 2 Kohm 5% " " 0. 125W
	R14		Not used
	R15	80. 5263	15 Kohm 5% " " 0. 125W
	R16	80. 5263	15 Kohm 5% " " 0. 125W
	R17	80. 5250	1. 2 Kohm 5% " " 0. 125W
	R18	80. 5243	330 ohm 5% " " 0. 125W
	L1	61. 1122	10. 0 MHz IF coil
	L2	61. 5023	10. 0 MHz IF coil
	L3	61. 5021	455 kHz IF coil
	X1	98. 5014	9. 545 MHz Crystal
		69. 5032	10. 0 MHz Crystal Filter
		69. 5031	455 kHz Ceramic Filter 20/25 kHz

TYPE	Nº	CODE	DATA
	Q1	99. 5168	BF 173 Transistor
	Q2	99. 5166	BF 167 Transistor
	Q3	99. 5168	BF 173 Transistor

IF CONVERTER IC705

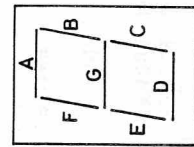
X402.611



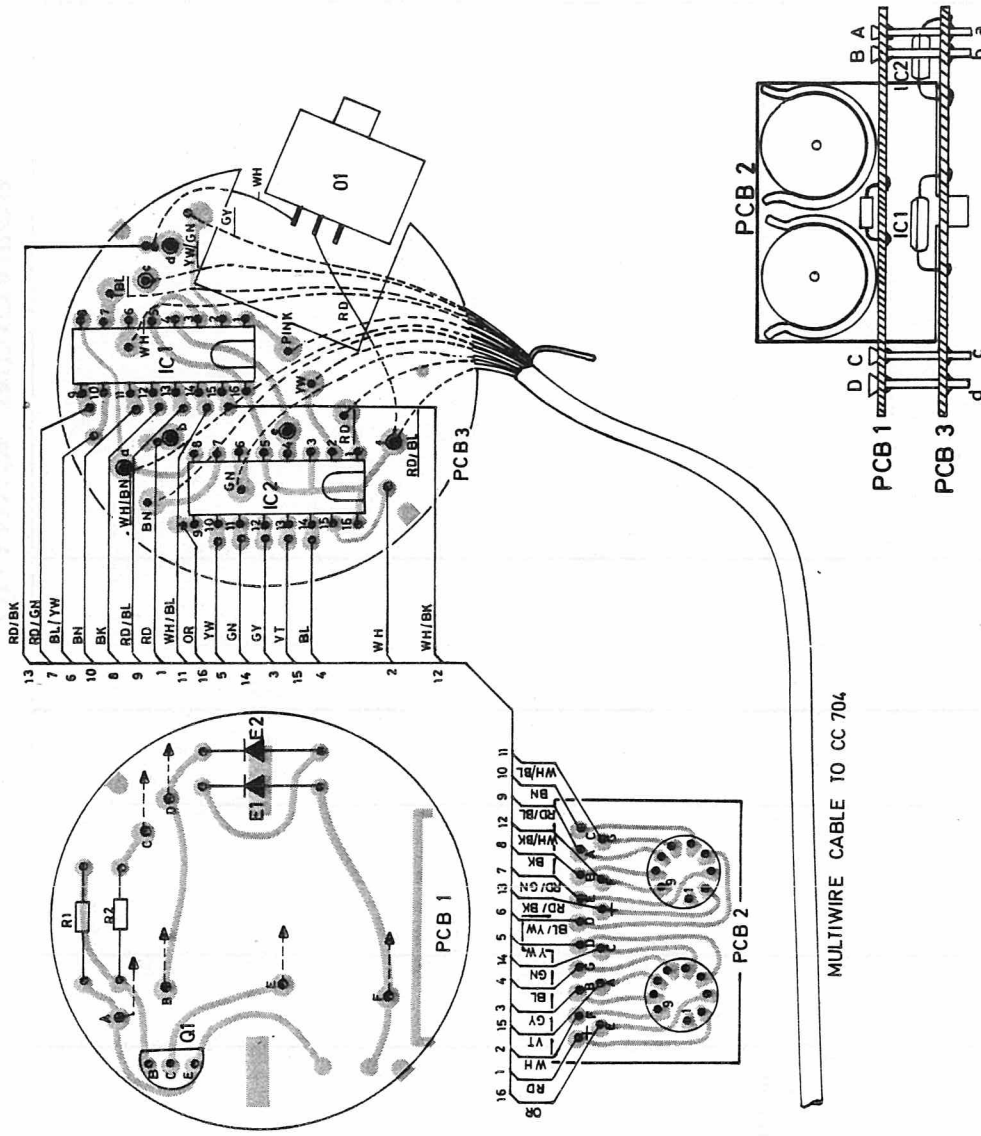
IC1-IC2

V1-V2

BOTTOM VIEW



7-SEGMENT INDICATOR



MULTIWIRED CABLE TO CC 704

CHANNEL INDICATOR ID701
KANALINDIKATOR

D401.885/2

Storno

TYPE	NO.	CODE	DATA
ID701		10. 2930-00	Channel Indicator 00-99
	R1	80. 5255	3. 3K Ω 5%
	R2	80. 5259	6. 8K Ω 5% carbon film 1/8W
	E1	99. 5020	1N4004 Diode
	E2	99. 5020	1N4004 Diode
	01	47. 5103	Switch
	Q1	99. 5117	BC167 Transistor
	IC1	14. 5058	SN6447A 7-segment decoder-driver
	IC2	14. 5058	SN6447A 7-segment decoder-driver
	V1	92. 5106	7-segment display
	V2	92. 5106	7-segment display

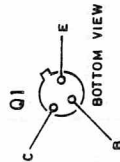
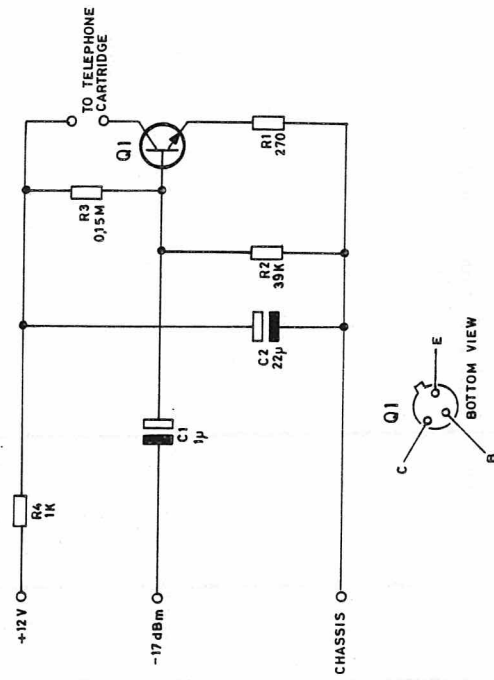
Storno

TYPE	NO.	CODE	DATA

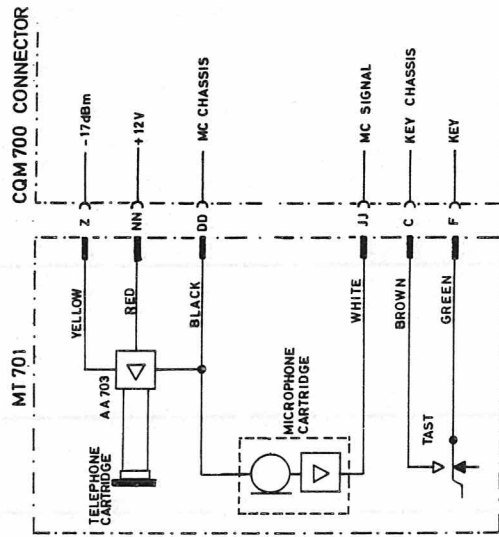
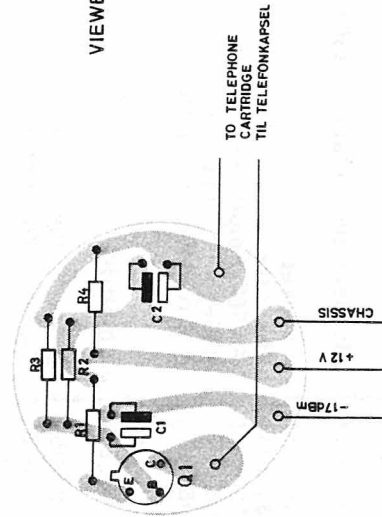
CHANNEL INDICATOR
KANALINDIKATOR

ID701

X402. 105/3



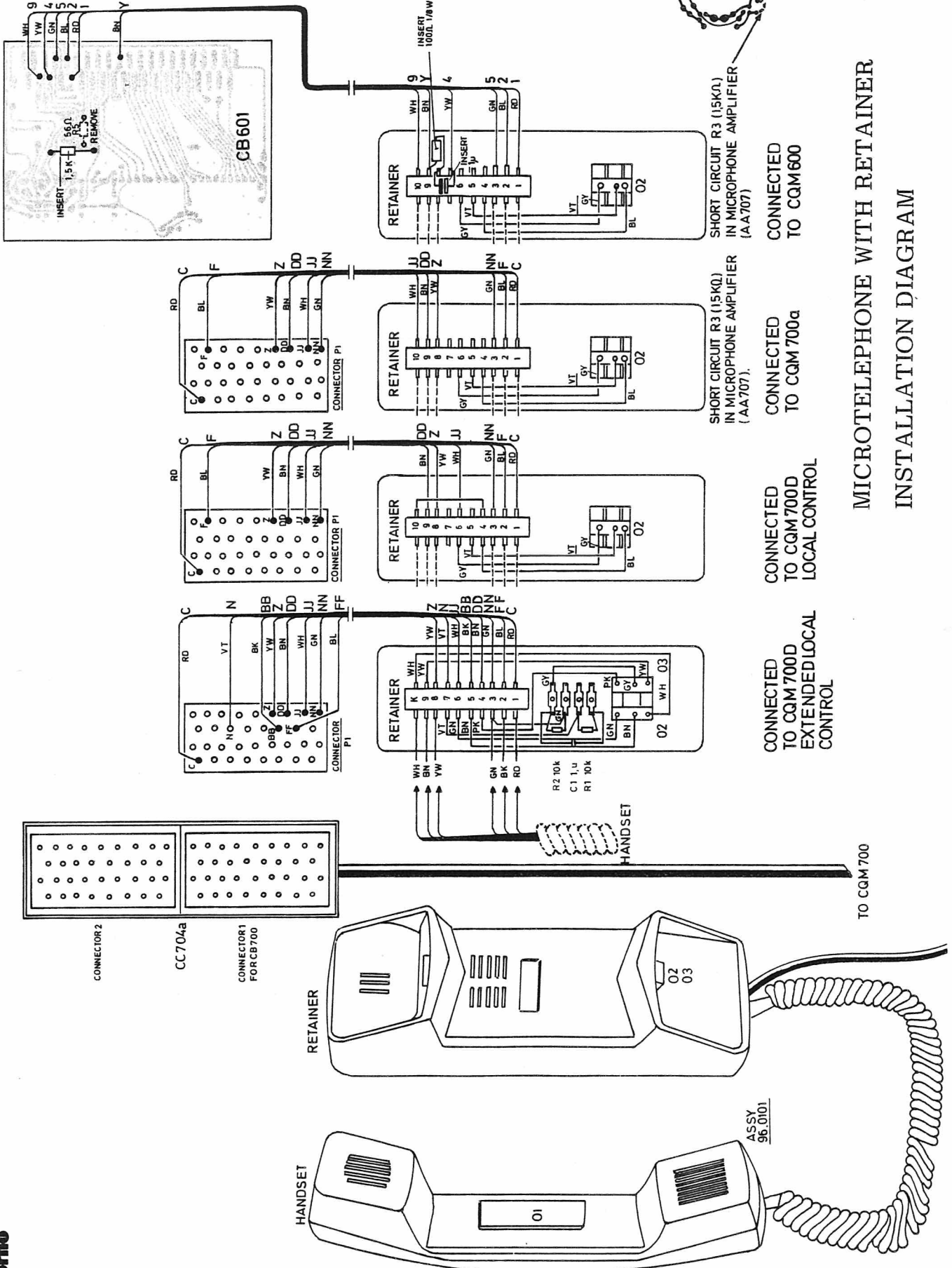
VIEWED FROM COMPONENT SIDE



HANDSET
MIKROTELEFON

MT701

D401.844



TO CQM 700

ASSY 96.0101

MICROTELEPHONE WITH RETAINER
INSTALLATION DIAGRAM

MT704

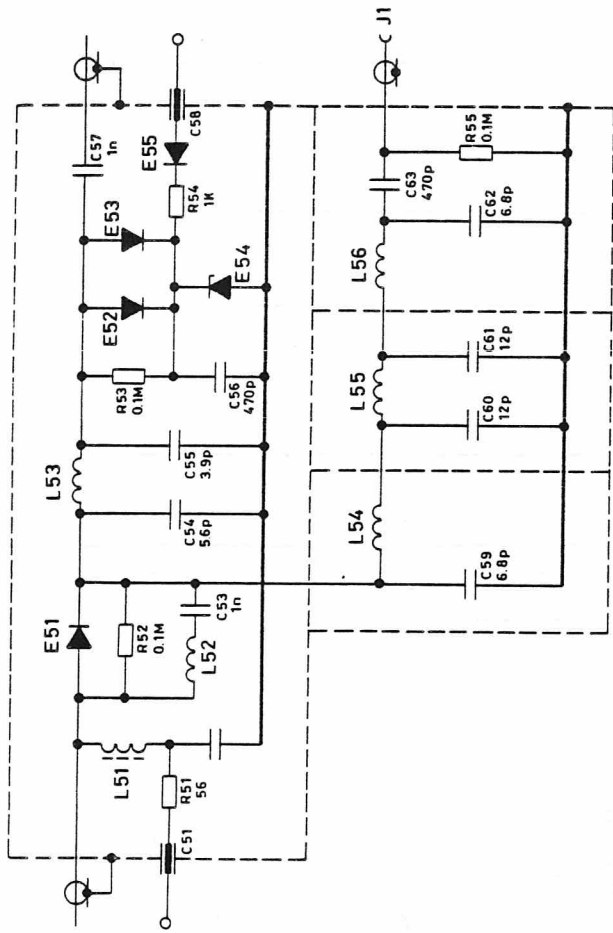
D402.50713

STORNOPHONE 700
 MAINTENANCE MANUAL
 VOLUME II
 Section 5

TITLE		Code
PA711	Description 1 - 2	60.194-E1
AS711	Description	60.197-E1
PA711	Schematic	D401.710
	Part List 1 - 2	X401.782
PA712	Description 1 - 3	60.200-E1
AS712	Description	60.202-E1
	Schematic	D401.654/4
	Component Lay-out	D401.835
	Part List 1 - 2	X401.800
PA713	Schematic	D401.952
	Part List	X401.948
PA714	Schematic	D402.250
	Part List	X402.374/3
PA715	Schematic	D402.335
	Part List	X402.368
PA731	Description 1 - 2	60.195-E1
AS731	Description	60.198-E1
PA731	Schematic	D401.888
	Part List 1 - 2	X401.787
PA732	Description 1 - 3	60.231-E1
	Schematic	D401.956/2
	Component Lay-out	D402.395
	Part List 1 - 2	X401.957
PA761	Description 1 - 2	60.196-E1
AS761	Description 1 - 2	60.199-E1
PA761	Schematic	D401.324/4
	Part List 1 - 2	X401.619

STORNOPHONE 700
MAINTENANCE MANUAL
VOLUME II
Section 5

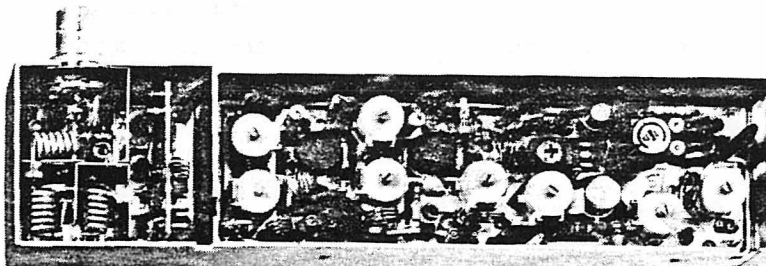
PA762	Description 1 - 3	60. 201-E1
AS762	Description	60. 203-E1
PA762	Schematic	D401. 790
	Component Lay-out	D401. 979
	Part List	X401. 862
PA763	Schematic	D401. 872
	Part List	X401. 861
PA764	Schematic	D402. 080
	Part List	X402. 163
PA765	Scematic	D402. 139/2
	Part List	X402. 164



ANTENNA SWITCH AS761

D401.334

RF POWER AMPLIFIER PA711

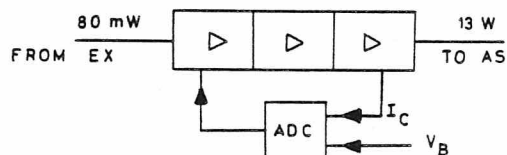


Description

General

PA711 contains 3 power amplifier stages and a current regulating circuit. The unit is completely shielded, being built into a combination heat sink and shield which also contains the antenna switching unit.

The current regulating circuit monitors both the supply voltage and the output transistor collector current, preventing overloading of the transistors due to either too high a voltage or too great a standing wave ratio in the output load. This circuit also allows the output power to be more independent of the power supply or of variations in power output from the exciter.



RF Power Amplifier

The first driver, Q3, gets its collector voltage via the ADC circuit regulating transistor, Q2. Increasing or decreasing the collector voltage to Q3 regulates the drive power applied to the following stages.

π -network C6, L2, C7 and C8 matches the exciter output impedance to the input impedance of Q3. Due to this impedance matching it is also possible to drive the PA stage from a 50 Ω generator. Q3 amplifies the exciter signal of about 80 mW to approx. 400 mW, which is necessary to drive Q4 properly.

Transistor Q4 further amplifies the power to approx. 3 W in order to be able to drive the final power amplifier, Q5.

Output transistor Q5 amplifies the RF power signal to approximately 13 W and the following matching network of L12, C22, C23 and L13 suppresses harmonics of the fundamental VHF frequency while transforming the collector impedance of Q5 to the antenna impedance of 50 Ω . Resistor R13 in the output transistor collector path is the current monitoring resistor for the ADC circuit.

Current Regulating Circuit (ADC)

The purpose of the regulating circuit is to protect the transistors against overloads caused by too high a supply voltage and to limit current through the output transistor in case of mismatching. To accomplish this, the regulating circuit must monitor the supply voltage as well as the collector current through the transistor and from such results regulate the collector voltage to the first RF driver transistor, Q3, and thus the driver power to the following stages.

The circuit consists of two DC coupled transistor stages, Q1 and Q2. Base to Q1 is tied to a reference voltage that can be determined by setting the trimming potentiometer, R2. Reference voltage is developed across diodes E1 and E2, which are biased into forward conduction. This introduces a temperature dependency in the reference voltage that compensates for the temperature dependen-

cy in the reference voltage that compensates for the temperature characteristics of the transistors.

For easier understanding of the circuit principle, first ignore its voltage dependent features; therefore, imagine that resistor R5 is removed from the circuit.

The DC return path for the emitter of Q1 is through R13 to the positive voltage terminal. R13 carries the collector current from the output amplifier Q5. A rise in this collector current will mean an increase in the voltage drop across R13, causing the emitter of Q1 to become less positive and the collector voltage will likewise become less positive. This decreases bias to Q2, decreasing the current through this transistor. Since Q2 is in series with the DC collector path of Q3, the effect will be that of placing a larger resistor in series with the collector supply, thus reducing collector voltage to Q3. The RF drive to the output stage will fall, thereby counteracting the original increase in collector current.

If the supply voltage increases, the current through the output transistors will be kept constant as already explained, but the power dissipation in the transistor will increase along with the voltage. To counteract this effect, a voltage regulating loop is included.

Imagine R5 connected back into the circuit again so that a voltage divider consisting of R4 and R5 will develop a voltage across R4 in proportion to the supply voltage.

When the supply voltage increases so will the voltage drop across R4 and the base-emitter bias for Q1 will fall, again resulting in a reduction of collector voltage to Q3 and a reduction in the drive to the output stage.

The reduction of drive power decreases the current through Q5 and R13 just enough to counteract the original increase of voltage across R4. By selecting a suitable ratio be-

tween resistors R4, R5 and R13, the desired amount of regulation can be achieved.

The transmitter output power can be set to the desired level by means of potentiometer R2 in the ADC circuit.

Technical Specifications

Frequency Range

146 - 174 MHz

Supply Voltage

Nominal 13.6 V (12.5 V)

Operating range 10 - 16 V

Output Power at 13.6 V : 12 W

With output power set for
12 W at 13.6 V,
as measured through AS711 :

Output power at 16 V 11 W

Output power at 12.5 V 11 W

Output power at 10 V 6 W

Current Consumption

at nominal voltage 13.6 V : 2.0 A

at 16 V : 1.8 A

at 10 V : 1.5 A

Input Power

80 mW

Input Impedance

50 Ω

Output Impedance

50 Ω

Gain

24 dB

Temperature Range

Operating range : -25° to $+70^{\circ}$ C

Functioning range : -30° to $+80^{\circ}$ C

Mechanical Dimensions

25 x 42 x 168 mm

(PC board : 35.6 x 119.4 mm)

ANTENNA SWITCH AS711

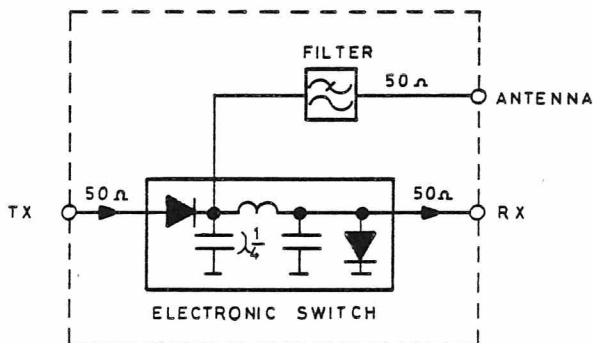
Description

General

The antenna switch AS711 contains a circuit for electronically switching the antenna between the transmitter and the receiver sections, and a low-pass filter that attenuates undesired frequencies, such as harmonics of the signal frequency, thus preventing their being radiated from the antenna.

AS711 mounts directly into the combination heat sink and shield for PA711.

The following simplified diagram shows the operating principle for the AS sub-unit.



The Electronic Switch

Refer to the complete schematic diagram D 401.710.

By switching a +9 V potential between terminals 1 and 2, the antenna is electronically switched between transmit and receive.

When transmitting, diodes E51 + E52 and E53 + E54 conduct. The receiver terminal will see a short circuit.

The 1/4 wave impedance circuit consisting of C54, L53 and C55 transforms the short to an open circuit at the antenna, thus the transmit signal reaches the antenna with minimum loss.

When receiving, the diodes are effectively blocked due to the bias across zener diode E55. Now the diodes only represent a small capacity that includes itself in the 1/4 wave impedance circuit, as far as the receiver terminal is concerned.

The transmitter terminal, however, looks into a parallel resonant circuit made up of L52 and the capacities of E51 and E52, and is thereby isolated from the antenna.

The received signal is now free to pass from the antenna to the receiver input with minimum loss.

The Low-pass Filter

The low-pass filter is a 7-pole Chebishev filter exhibiting negligible band-pass ripple and minimum insertion loss.

The filter is built on a metal plate chassis having three closed compartments. It requires no alignment.

Technical Specification

Frequency Range

146 - 174 MHz

Input and Output Impedance

50 Ω

Insertion Loss (transmitter to antenna)

0.4 dB

Insertion Loss (antenna to receiver)

0.6 dB

Separation between Transmitter and Receiver

28 dB

Second Harmonic (292 MHz) Attenuation

55 dB

Current Drain, transmit

38 mA

Current Drain, receive

4 mA

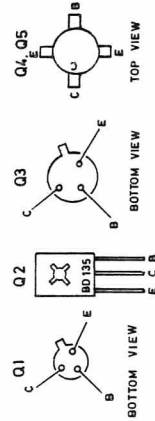
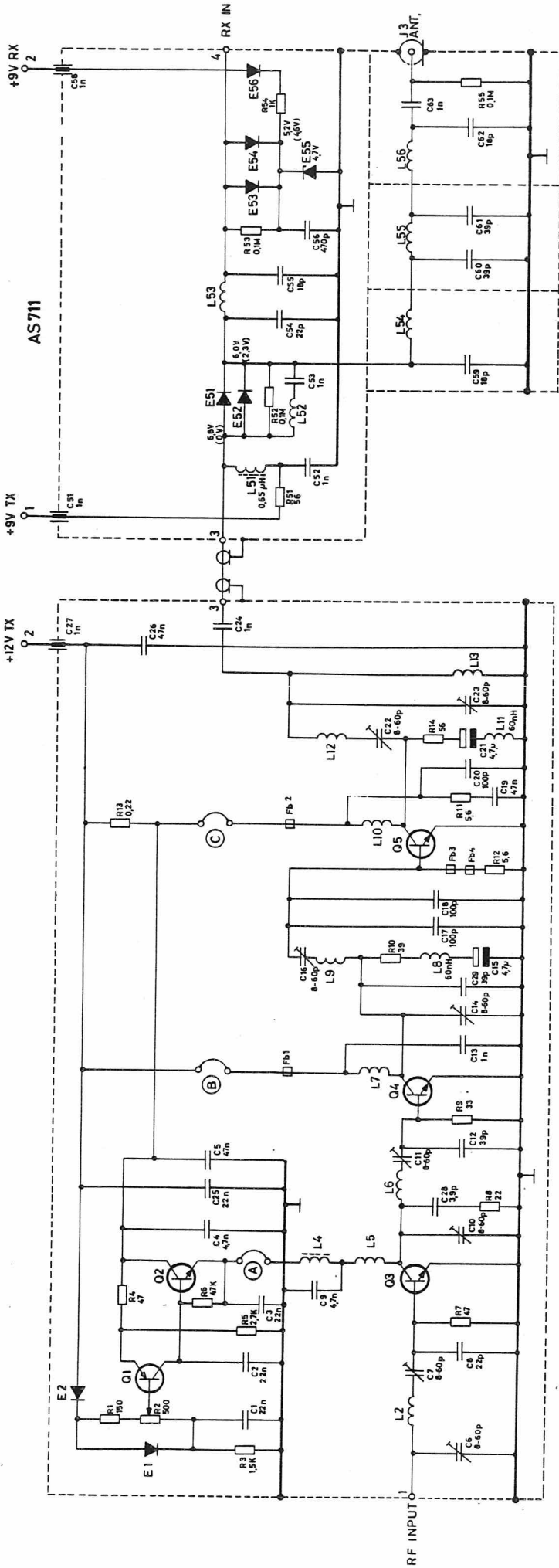
Temperature Range

operating range -25° to $+70^{\circ}$ C

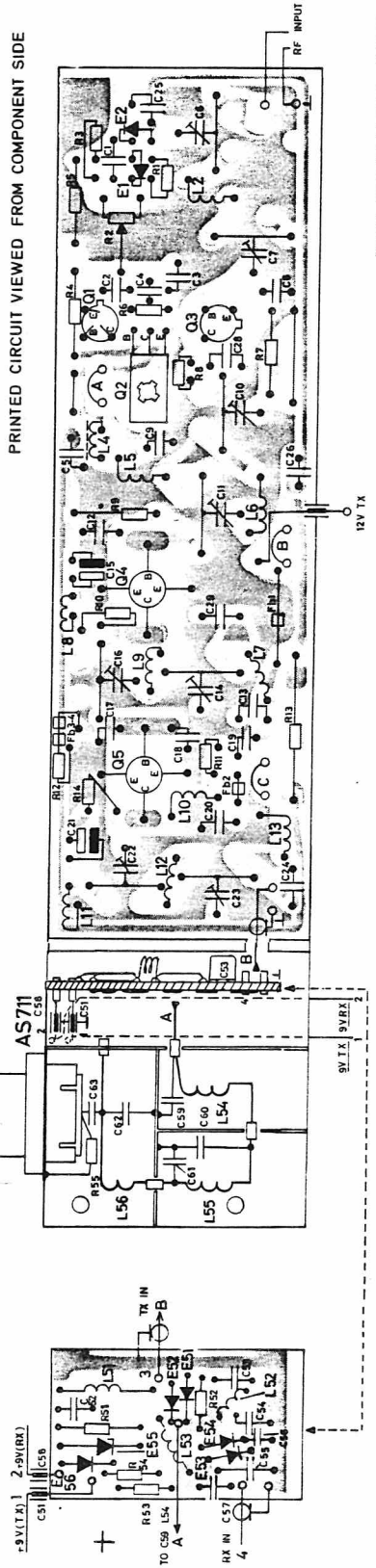
functioning range -30° to $+80^{\circ}$ C

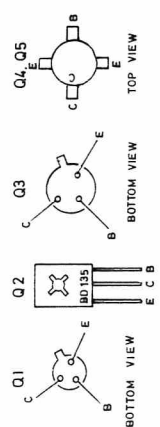
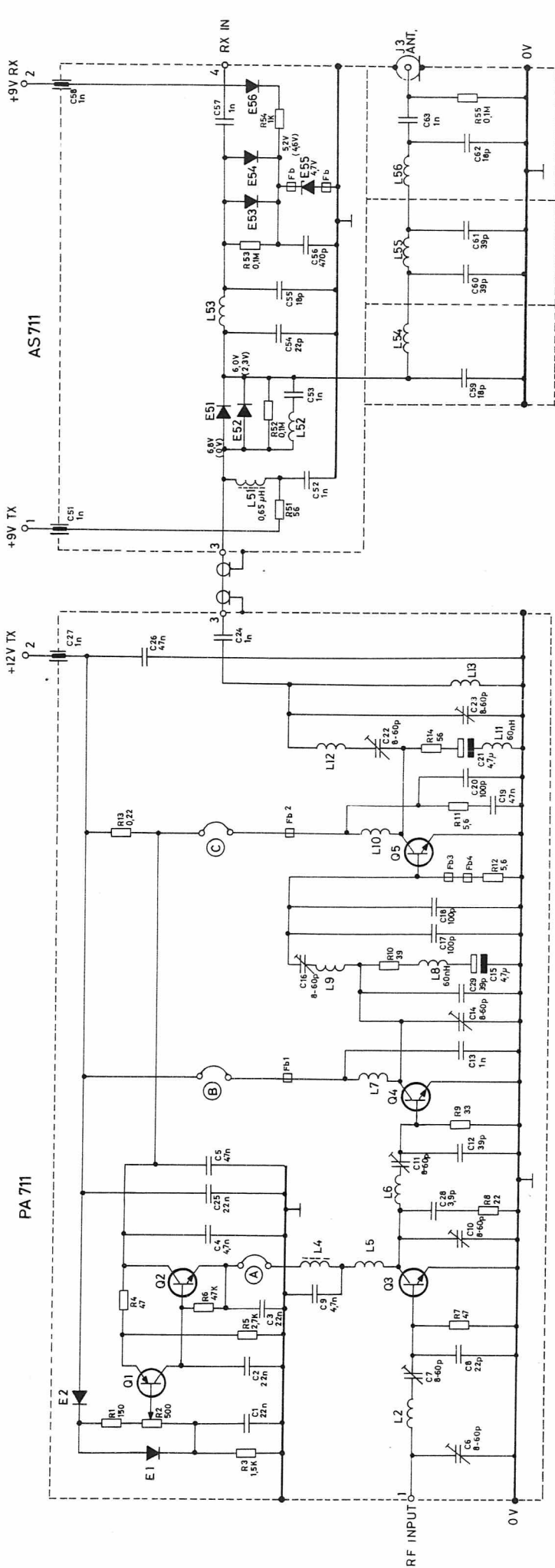
Dimensions

40 x 38 x 22



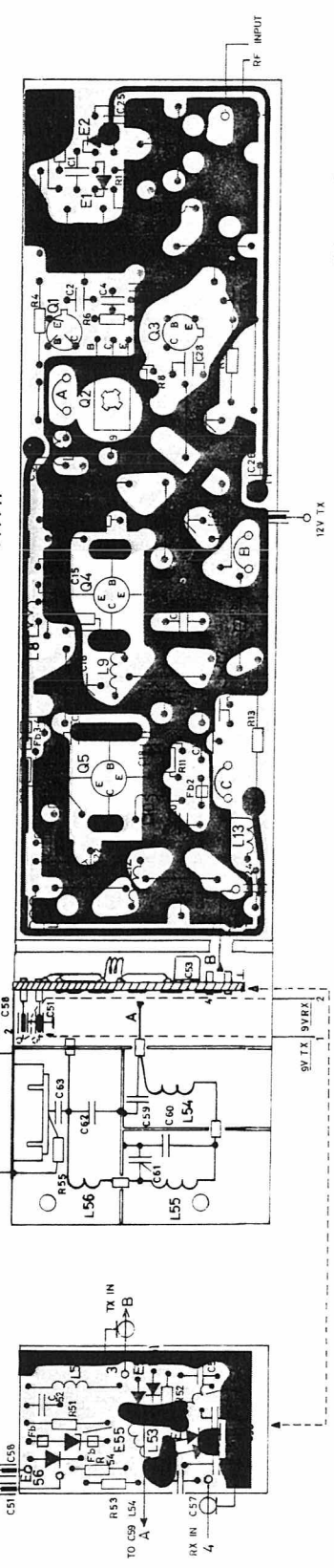
PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE





DC VOLTAGES WITH BRACKET ARE MEASURED IN TRANSMIT MODE.
 DC VOLTAGES WITHOUT BRACKETS ARE MEASURED IN RECEIVE MODE.

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
 PA 711



TYPE	NO.	CODE	DATA
PA711		10.2558	Power Amplifier (incl. AS711)
AS711		10.2553	Antenna Switch
	C1	76.5061	4.7 nF 10% polyester FL
	C2	76.5061	4.7 nF 10% polyester FL
	C3	76.5061	4.7 nF 10% polyester FL
	C4	76.5061	4.7 nF 10% polyester FL
	C5	76.5072	47 nF 10% polyester FL
	C6	78.5052	8-60 pF trimmer
	C7	78.5052	8-60 pF trimmer
	C8	74.5106	22 pF 5% ceram TB
	C9	76.5061	4.7 nF 10% polyester FL
	C10	78.5052	8-60 pF trimmer
	C11	78.5052	8-60 pF trimmer
	C12	74.5117	39 pF 5% ceram TB
	C13	74.5155	1 nF -20+50% ceram PL
	C14	78.5052	8-60 pF trimmer
	C15	73.5126	4.7 μ F 20% tantal
	C16	78.5052	8-60 pF trimmer
	C17	74.5199	100 pF 20% ceram PL
	C18	74.5199	100 pF 20% ceram PL
	C19	76.5052	47 nF 10% polyester FL
	C20	74.5013	100 pF 20% ceram DI
	C21	73.5126	4.7 μ F 20% tantal
	C22	78.5052	8-60 pF trimmer
	C23	78.5052	8-60 pF trimmer
	C24	74.5015	1 nF-20+50% ceram DI
	C25	76.5061	4.7 nF polyester FL
	C26	76.5072	47 nF 10% polyester FL
	C28	74.5130	3.9 pF \pm 25 pF 5% ceram DI
	C29	74.5117	39 pF 5% ceram TB
	R1	80.5239	150 Ω 5% carbon film
	R2	86.5042	500 Ω 20% potentiometer
	R3	80.5251	1.5 K Ω 5% carbon film
	R4	80.5233	47 Ω 5% carbon film
	R5	80.5254	2.7 K Ω 5% carbon film
	R6	80.5269	47 K Ω 5% carbon film
	R7	80.5233	47 Ω 5% carbon film
	R8	80.5229	22 Ω 5% carbon film
	R9	80.5231	33 Ω 5% carbon film
	R10	80.5432	39 Ω 5% carbon film
	R11	80.5222	5.6 Ω 5% carbon film
	R12	80.5222	5.6 Ω 5% carbon film
	R13	82.5205	0.22 Ω 10% wire wound
	R14	80.5434	56 Ω 5% carbon film
	L2	62.0822	RF coil 146-174 MHz

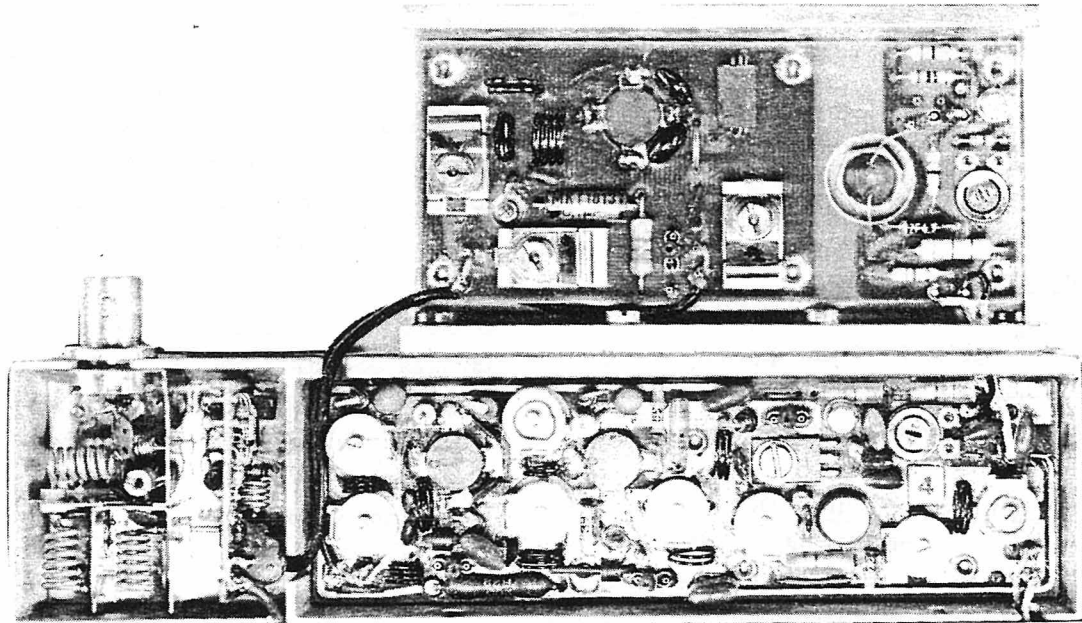
TYPE	NO.	CODE	DATA
	L4	63.5008	0.47 μ H 20% RF choke
	L5	62.0822	RF coil 146-174 MHz
	L6	62.0823	RF coil 146-174 MHz
	L7	62.0824	RF coil 146-174 MHz
	L8	61.5011	0.06 μ H 20% RF choke
	L9	62.0825	RF-coil 146-174 MHz
	L10	62.0824	RF coil 146-174 MHz
	L11	61.5011	0.06 μ H 20% RF choke
	L12	62.0827	RF coil 146-174 MHz
	L13	62.0826	RF coil 146-174 MHz
	E1	99.5028	1N914 Diode
	E2	99.5028	1N914 Diode
	Q1	99.5230	BC178 Transistor
	Q2	99.5235	BD135 Transistor
	Q3	99.5229	2N427 Transistor
	Q4	99.5252	BLY87A Transistor
	Q5	99.5253	BLY88A Transistor
AS711		10.2553	Antenna Switch
	C51	69.5007	VHF feed-through filter
	C52	74.5155	1 nF -20+80% ceram PL
	C53	74.5155	1 nF -20+80% ceram PL
	C54	74.5008	22 pF \pm 5% ceram DI
	C55	74.5138	18 pF 5% ceram DI
	C56	74.5162	470 pF -20+50% ceram DI
	C57	74.5155	1 nF -20+80% ceram PL
	C58	69.5007	VHF feed-through filter
	C59	74.5796	18 pF 5% ceram DI
	C60	74.5197	39 pF 5% ceram DI
	C61	74.5197	39 pF 5% ceram DI
	C62	74.5196	10 pF 5% ceram DI
	C63	74.5015	1 nF 20% ceram DI
	R51	80.5234	56 Ω 5% carbon film
	R52	80.5073	0.1 M Ω 5% carbon film
	R53	80.5073	0.1 M Ω 5% carbon film
	R54	80.5049	1 K Ω 5% carbon film
	R55	80.5273	0.1 M Ω 5% carbon film
	L51	62.0662-01	0.65 μ H RF choke
	L52	62.0818	RF coil

POWER AMPLIFIER EFFEKTFORSTÆRKER

X401.782

PA711

RF POWER AMPLIFIER PA712



Description

PA712 comprises 4 RF power amplifier stages, three in the driver and one in the booster as well as a regulating and temperature protection circuit and, finally, an electronic antenna switching unit with filter, AS712.

PA712 is completely shielded, as it is built into a combination heat sink and shield. However, heat dissipation will be insufficient without the external heat sink/cabinet CA703.

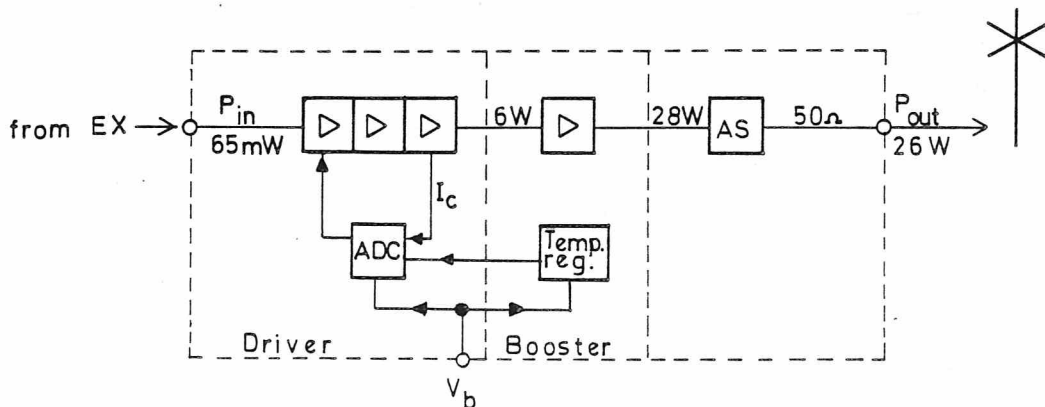
The regulating and temperature protection circuit protects the transistors and other components in the unit against incurring damages when operated within the permissible values of supply voltages and temperatures,

or as a result of prolonged short circuits or too great a standing wave ratio in the output load.

RF Power Amplifier

The first driver, Q3, gets its collector voltage via the ADC circuit regulating transistor, Q2. Increasing or decreasing the collector voltage to Q3 regulates the drive power applied to the following stages.

π -network C6, L2, C7 and C8 matches the exciter output impedance to the input impedance of Q3. Due to this impedance matching it is also possible to drive the PA stage from a 50 Ω generator.



Q3, Q4 and Q5 amplify the exciter output signal of 80 mW to 6 W in order to drive the booster stage. Matching network L12, C22, C23 and L13 suppresses harmonics of the fundamental VHF frequency while transforming the collector impedance of Q5 to 50Ω . Resistor R13 in the collector return of Q5 is the current monitoring resistor for the ADC circuit.

Booster Stage

Q101 amplifies the 6 W output power from the driver stage to 28 W and applies the signal to AS712. Due to the inherent losses in the AS unit the PA output power is then 26 W.

Current Regulating Circuit (ADC)

The purpose of the regulating circuit is to protect the transistors against overloads caused by excessive supply voltage and to limit current through the output transistor in case of mismatching. To accomplish this, the regulating circuit must monitor the supply voltage as well as the collector current through Q5 in the driver stage and from such results regulate the collector voltage to the first driver transistor Q3, and thus the drive power to the following stages.

The circuit consists of two DC coupled transistor stages, Q1 and Q2. Base to Q1 is tied to a reference voltage that can be determined by setting potentiometer R2. Reference voltage is developed across diodes E1 and E2, which are biased into forward conduction. This introduces a temperature dependency in the reference voltage that compensates for the temperature characteristics of the transistors.

For easier understanding of the circuit principle, first ignore its voltage dependent features; therefore, imagine that resistor R5 is removed from the circuit.

The DC return path for the emitter of Q1 is through R13 to the positive voltage terminal. R13 also carries the collector current from transistor Q5. A rise in this collector current will mean an increase in the voltage drop across R13, causing the emitter of Q1 to be-

come less positive and the collector voltage will likewise become less positive. This decreases forward bias to Q2, decreasing the current through this transistor. Since Q2 is in series with the DC collector path of Q3, the effect will be that of placing a larger resistor in series with the collector supply, thus reducing collector voltage to Q3. The RF drive to the output stage will fall, thereby counteracting the original increase in collector current.

If the supply voltage increases, the current through Q5 will be kept constant as already explained, but the power dissipation in the transistor will increase along with the voltage. To counteract this effect, a voltage regulating loop is included.

Imagine R5 connected back into the circuit again so that a voltage divider consisting of R4 and R5 will develop a voltage across R4 in proportion to the supply voltage.

When the supply voltage increases so will the voltage drop across R4 and the base-emitter bias for Q1 will fall, again resulting in a reduction of collector voltage to Q3 and a reduction in the drive to the output stage.

The reduction of drive power decreases the current through Q5 and R13 just enough to counteract the original increase of voltage across R4. By selecting a suitable ratio between resistors R4, R5 and R13 the desired amount of regulation can be achieved.

The transmitter power can be set to the desired level by means of potentiometer R2 in the ADC circuit.

Temperature Protection Circuit

Since transistor Q101 in the booster stage is not directly included in the ADC loop, it requires extra thermal protection which is accomplished by means of a PTC resistor, R102, which is mounted close to Q101. When Q101, and R102 along with it, reach a certain temperature the increasing resistance of R102, which is also a part of the ADC loop of the driver stage, regulates (reduces) the drive to Q101.

Thus the output power of the PA unit is regulated to a preset level that ensures thermal protection of Q101 and other components.

The temperature protection circuit operates in the following manner: Under normal operating conditions (prior to regulation) Q102 is biased to cut-off by the voltage divider network of R104 and the PTC resistor (60 Ω) connected across zener diode E101 for a stable source. As the temperature in the PA stage rises the resistance of R102 increases and Q101 begins to pass current. When R102 reaches 1.2 kΩ Q102 will be completely open. When Q102 opens up, the circuit shunts diodes E1 and E2 and the voltage across these diodes falls, causing the base-emitter voltage for Q1 to fall, as well.

As a result, Q3's collector voltage falls, too, thereby also reducing the drive to the following stages.

The amount of regulation (reduction in output power) is preset by potentiometer R107. Q102's emitter resistor is included to flatten out the regulation characteristic. Diode E102 in the collector lead of Q102 ensures temperature compensation of the reference voltage at the base of Q1 even at maximum regulation.

Technical Specifications

Frequency Range

146 to 174 MHz

Nominal Supply Voltage

13 V

Output Power

With output power set for 26 W at 13 V

output power at 15.5 V 26 W

output power at 10 V 16 W

Current Consumption

At nominal 13 V: 4.3 A

at 15.5 V: 4 A

at 10 V: 3.5 A

Input Power

nominal 80 mW

minimum 65 mW

Input Impedance

50 Ω

Output Impedance

50 Ω

Gain with $P_{in} = 65 \text{ mW}$

26 dB

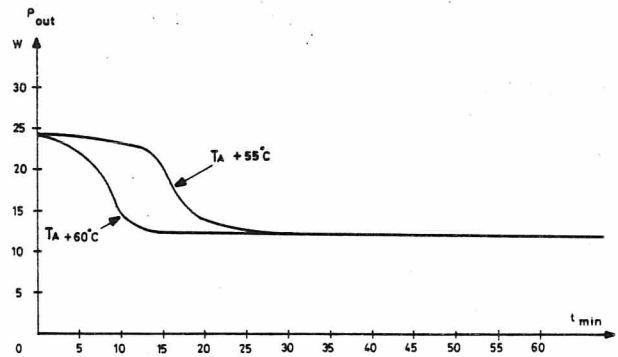
Reduction of Output Power vs. Ambient Temperature

Continuous, $T_A -25^\circ \text{ to } +25^\circ \text{ C}$ 0.8 dB

Intermittent, $T_A -25^\circ \text{ to } +55^\circ \text{ C}$ 0.8 dB

Continuous, $T_A +55^\circ \text{ C}$ 3 dB

(refer to response curve below)



Typical output power regulating characteristic of PA712 with CA703 mounted. Plotted for ambient temperatures of $+55^\circ \text{C}$ and $+60^\circ \text{C}$, at nominal voltage, continuous keying of transmitter.

Temperature Range

operating -25°C to $+55^\circ \text{C}$

functioning -30°C to $+60^\circ \text{C}$.

Mechanical Dimensions

168 x 97 x 32 mm

ANTENNA SWITCH AS712

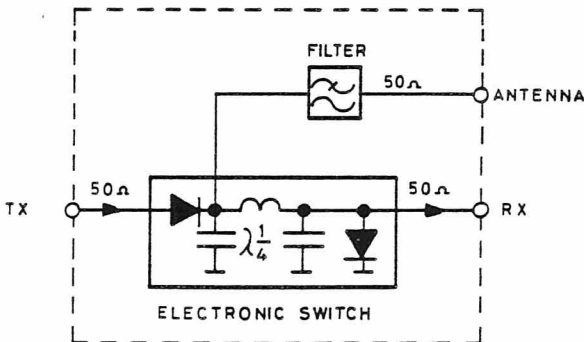
Description

General

The antenna switch AS712 contains a circuit for electronically switching the antenna between the transmitter and the receiver sections, and a low-pass filter that attenuates undesired frequencies, such as harmonics of the signal frequency, thus preventing their being radiated from the antenna.

AS712 mounts directly into the combination heat sink and shield for PA712 and is used in 2 metre simplex equipment for 25 W output power.

The following simplified diagram shows the operating principle for the AS sub-unit.



The Electronic Switch

Refer to the complete schematic diagram D401.654.

By switching a +9 V potential between terminals 1 and 2, the antenna is electronically switched between transmit and receive.

When transmitting, diodes E51, E52, E53 and E54, E55 and E56 conduct. The receiver terminal will see a short circuit.

The $1/4$ wave impedance circuit consisting of C54, L53 and C55 transforms the short to an open circuit at the antenna, thus the transmit signal reaches the antenna with minimum loss.

When receiving, the diodes are effectively blocked due to the bias across zener diode E57. Now the diodes only represent a small

capacity that includes itself in the $1/4$ wave impedance circuit, as far as the receiver terminal is concerned.

The transmitter terminal, however, looks into a parallel resonant circuit made up of L52 and the capacities of E51, E52 and E53, and is thereby isolated from the antenna.

The received signal is now free to pass from the antenna to the receiver input with minimum loss.

The Low-pass Filter

The low-pass filter is a 7-pole Chebishev filter exhibiting negligible band-pass ripple and minimum insertion loss.

The filter is built on a metal plate chassis having three closed compartments. It requires no alignment.

Technical Specifications

Frequency Range

146 to 174 MHz

Input and output Impedance

50 Ω

Insertion Loss (transmitter to antenna)

0.4 dB

Insertion Loss (antenna to receiver)

0.6 dB

Separation between Transmitter and Receiver

28 dB

Second Harmonic (292 MHz) Attenuation

55 dB

Current Consumption, Transmit

46 mA

Current Consumption, Receive

8 mA

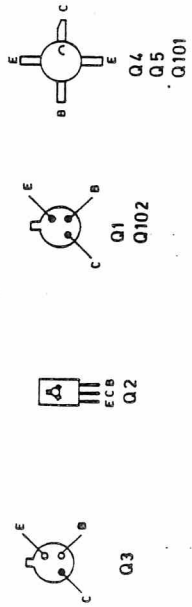
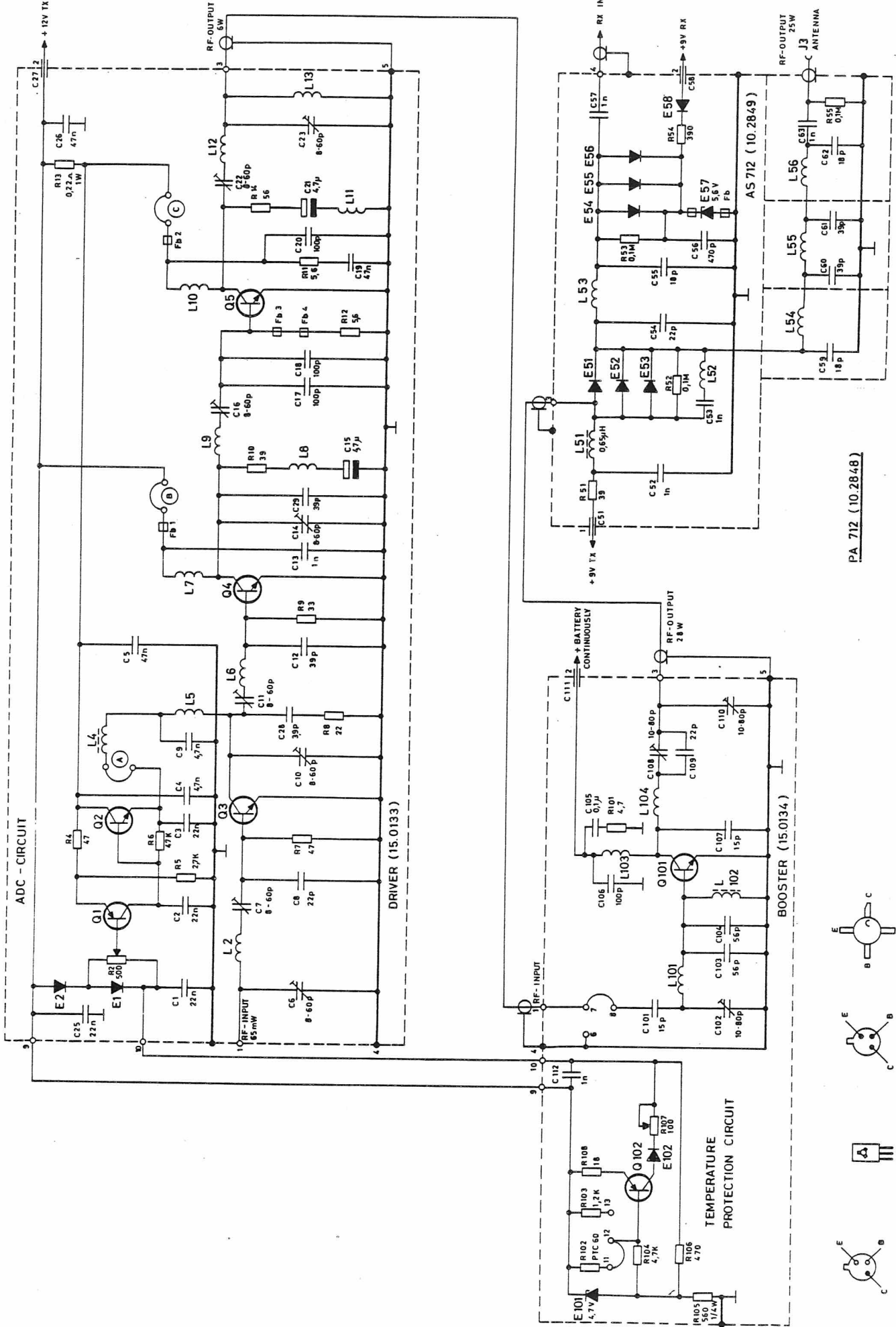
Temperature Range

working range: -25° to $+70^{\circ}$ C

functioning range: -30° to $+80^{\circ}$ C

Dimensions

40 x 38 x 22 mm

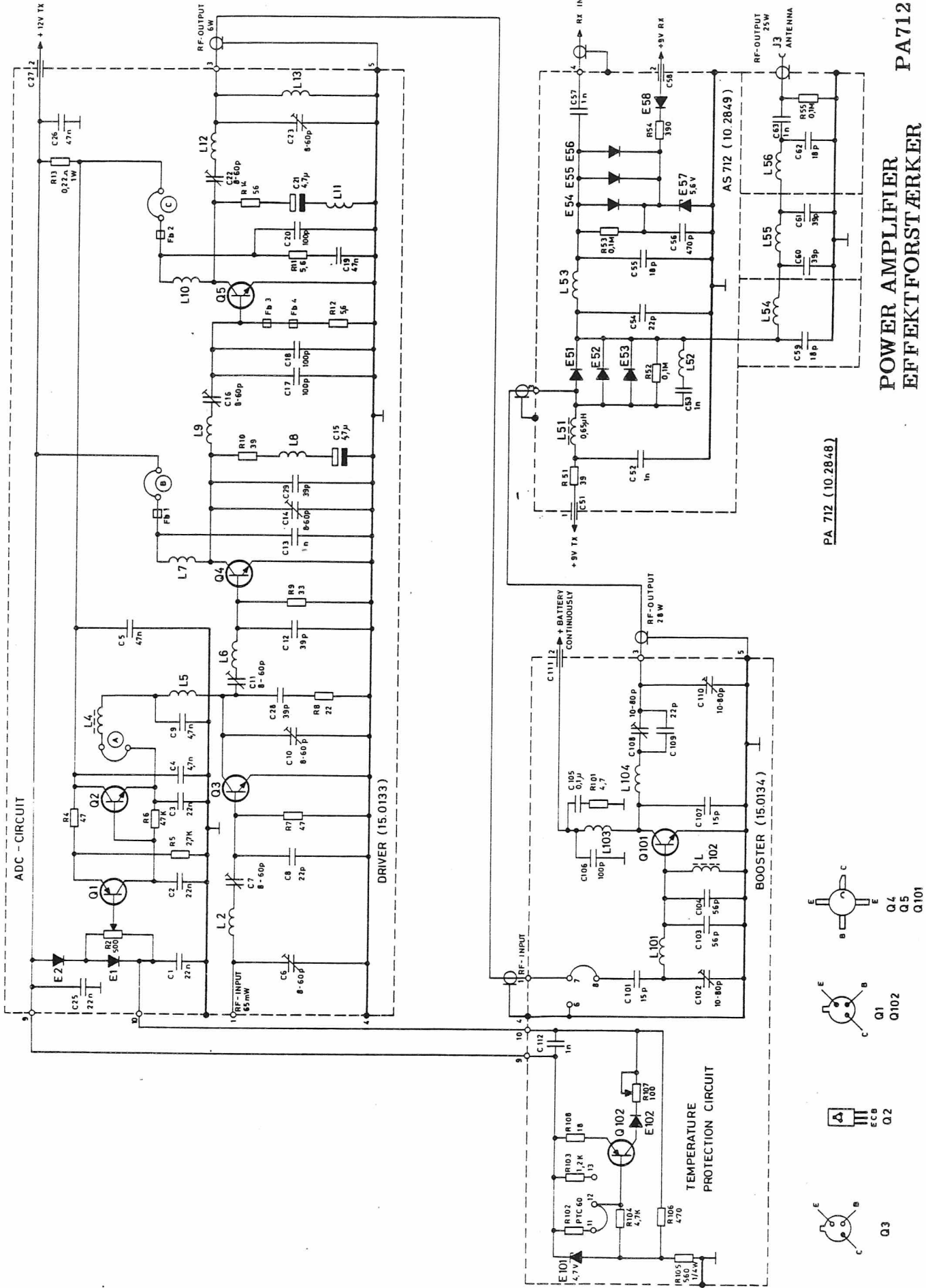


PA 712 (10.2848)

POWER AMPLIFIER EFFEKTFORSTÆRKER

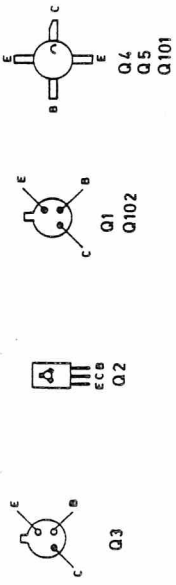
PA712

D 401.654/4

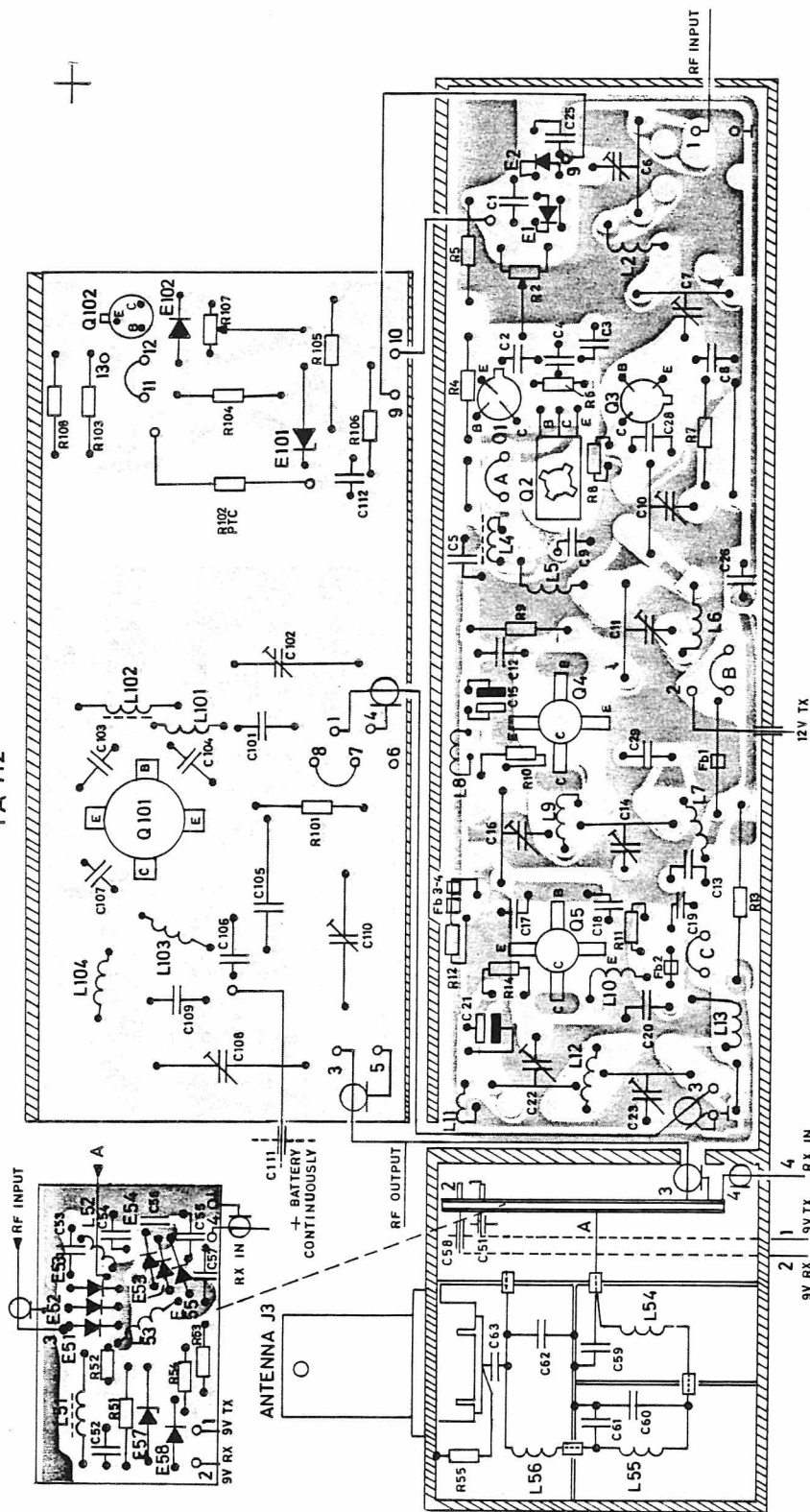


POWER AMPLIFIER
EFFEKTFORSTÆRKER
PA712

D 401.654/2



PA 712 (10.2848)



POWER AMPLIFIER
EFFEKTFORSTÆRKER

PA712

D 401.835

TYPE	NO.	CODE	DATA
PA712	10.2848-00		Power Amplifier
	C1	76.5071	22nF 10% polyester FL
	C2	76.5071	22nF 10% polyester FL
	C3	76.5071	22nF 10% polyester FL
	C4	76.5061	4.7nF polyester FL
	C5	76.5072	47nF 10% polyester FL
	C6	76.5052	8-60pF Trimmer
	C7	78.5052	8-60pF Trimmer
	C8	74.5106	22pF 5% ceram TB
	C9	76.5061	4,7nF 10% polyester FL
	C10	78.5052	8-60pF Trimmer
	C11	78.5052	8-60pF Trimmer
	C12	74.5117	39pF 5% ceram TB
	C13	74.5155	1nF-20+50% ceram PL
	C14	78.5052	8-60pF Trimmer
	C15	73.5126	4,7μF 20% tantal
	C16	78.5052	8-60pF Trimmer
	C17	74.5199	100pF 20% ceram
	C18	74.5199	100pF 20% ceram
	C19	76.5072	47nF 10% polyester FL
	C20	74.5013	100pF 20% ceram DI
	C21	73.5126	4,7nF 20% tantal
	C22	78.5052	8-60pF Trimmer
	C23	78.5052	8-60pF Trimmer
	C25	76.5071	22nF 10% polyester FL
	C26	76.5072	47nF 10% polyester FL
	C27	69.5023	VHF feed-through filter
	C28	74.5130	3,9pF ±0,25pF ceram DI
	C29	74.5117	39pF 5% ceram TB
	C51	69.5007	VHF Feed-through filter
	C52	74.5155	1nF -20+80% ceram PL
	C53	74.5155	1nF-20+80% ceram PL
	C54	74.5008	22pF 5% ceram
	C55	74.5196	18pF 5% ceram DI
	C56	74.5162	470pF-20+50% DI
	C57	74.5155	1nF-20+80% ceram PL
	C58	69.5007	VHF Feed-through filter
	C59	74.5196	18pF 5% ceram DI
	C60	74.5197	39pF 5% ceram DI
	C61	74.5197	39pF 5% ceram DI
	C62	74.5196	18pF 5% ceram DI
	C63	74.5015	1nF 20% ceram DI
	C101	74.5046	15pF 5% ceram DI
	C102	78.5053	10-80pF Trimmer, mica

TYPE	NO.	CODE	DATA
	C103	75.5015	56pF 5% mica
	C104	75.5015	56pF 5% mica
	C105	76.5073	0,1μF 10% polyester TB
	C106	74.5013	100pF 20% ceram DI
	C107	74.5046	15pF 5% ceram DI
	C108	78.5053	10-80pF Trimmer, mica
	C109	75.5017	22pF 5% mica
	C110	78.5053	10-80pF Trimmer, mica
	C111	69.5023	VHF Feed-through filter
	C112	74.5155	1nF-20+80% ceram PL
	R2	86.5042	500Ω 20% potentiometer
	R4	80.5233	47Ω 5% carbon film
	R5	80.5254	2,7kΩ 5% carbon film
	R6	80.5269	47kΩ 5% carbon film
	R7	80.5233	47Ω 5% carbon film
	R8	80.5229	22Ω 5% carbon film
	R9	80.5231	33Ω 5% carbon film
	R10	80.5432	39Ω 5% carbon film
	R11	80.5222	5,6Ω 5% carbon film
	R12	80.5222	5,6Ω 5% carbon film
	R13	82.5205	0,22 Ω 10% wirewound
	R14	80.5434	56 Ω 5% carbon film
	R51	80.5232	39 Ω 5% carbon film
	R52	80.5073	0,1 MΩ 5% carbon film
	R53	80.5073	0,1 MΩ 5% carbon film
	R54	80.5044	390 Ω 5% carbon film
	R55	80.5273	0,1 MΩ 5% carbon film
	R101	80.5421	4,7 Ω 5% carbon film
	R102	89.5066	60 Ω -50 +100% PTC Thermistor
	R103	80.5250	1,2 kΩ 5% carbon film
	R104	80.5257	4,7 kΩ 5% carbon film
	R105	80.5446	560 Ω 5% carbon film
	R106	80.5245	470 Ω 5% carbon film
	R107	86.5051	100 Ω 20% potentiometer
	R108	80.5228	18 Ω carbon film
	L2	62.0822	RF coil 146-174 MHz
	L4	63.5008	0,47 μH 20% RF choke

POWER AMPLIFIER
EFFEKTFORSTÆRKER

X 401.800

1 af 2

PA712

2,2 A

Storno

TYPE	NO.	CODE	DATA
	L5	62.0822	RF coil 146-174 MHz
	L6	62.0823	RF coil 146-174 MHz
	L7	62.0824	RF coil 146-174 MHz
	L8	61.5011	0.06 μ H 20% RF choke
	L9	62.0825	RF coil 146-174 MHz
	L10	62.0824	RF coil 146-174 MHz
	L11	61.5011	0.06 μ H 20% RF choke
	L12	62.0826	RF coil 146-174 MHz
	L13	62.0827	RF coil 146-174 MHz
	L51	62.0662	0.65 μ H RF choke
	L52	62.0818	RF coil
	L53	62.0817	RF coil
	L54		
	L55	62.0816	RF coil
	L56		
	L101	62.0840	RF coil 146-174 MHz
	L102	61.5013	RF-choke
	L103	62.0841	RF coil 146-174 MHz
	L104	62.0842	RF coil 146-174 MHz
	E1	99.5028	1N914 Diode
	E2	99.5028	1N914 Diode
	E51	99.5187-01	BA244 Diode
	E52	99.5187-01	BA244 Diode
	E53	99.5187-01	BA244 Diode
	E54	99.5187-01	BA244 Diode
	E55	99.5187-01	BA244 Diode
	E56	99.5187-01	BA244 Diode
	E57	99.5282	Zenerdiode 5,6 V 5%
	E58	99.5237	1N4148 Diode
	E101	99.5224	Zenerdiode 4,7 V 5%
	E102	99.5237	1N4148 Diode
	Q1	99.5230	BC178 Transistor
	Q2	99.5235	BD135 Transistor
	Q3	99.5229	2N4427 Transistor
	Q4	99.5252	BLY87A Transistor
	Q5	99.5253	BLY88A Transistor
	Q101	99.5230	BC178 Transistor
	Q102	99.5280	BLY89A Transistor

1 W
1/4 W

Storno

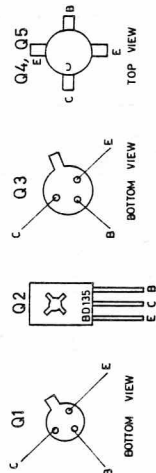
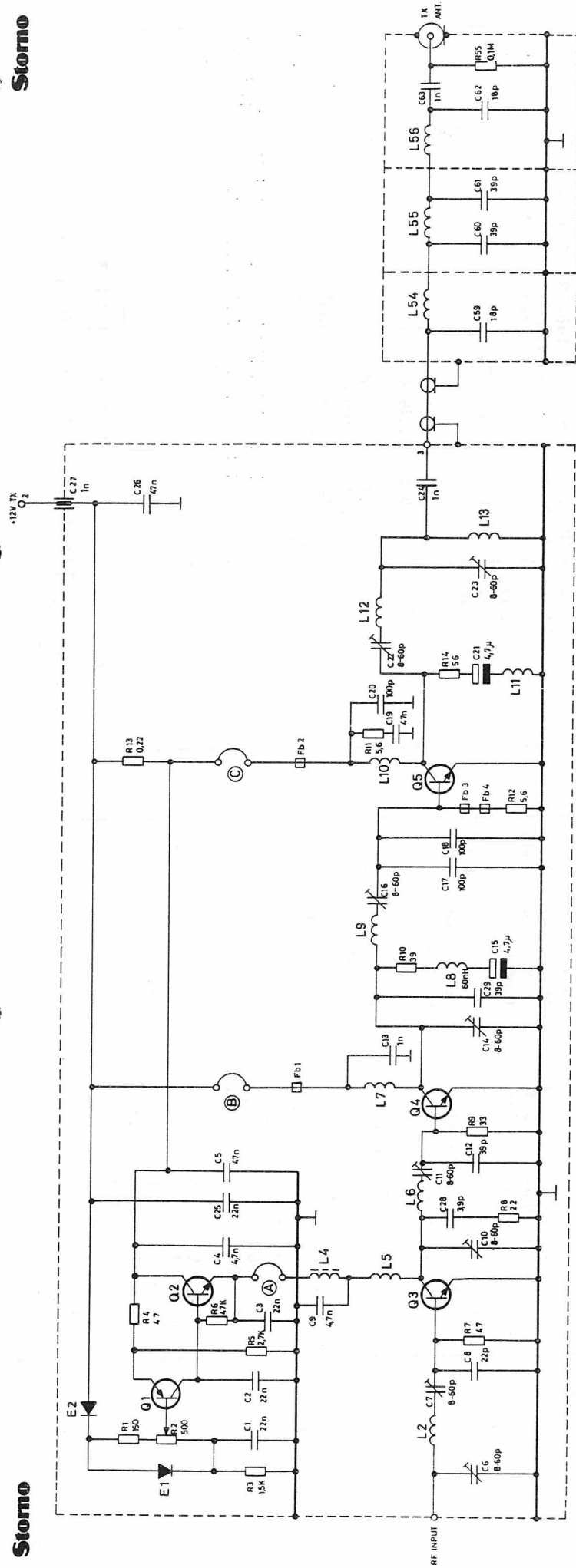
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**POWER AMPLIFIER
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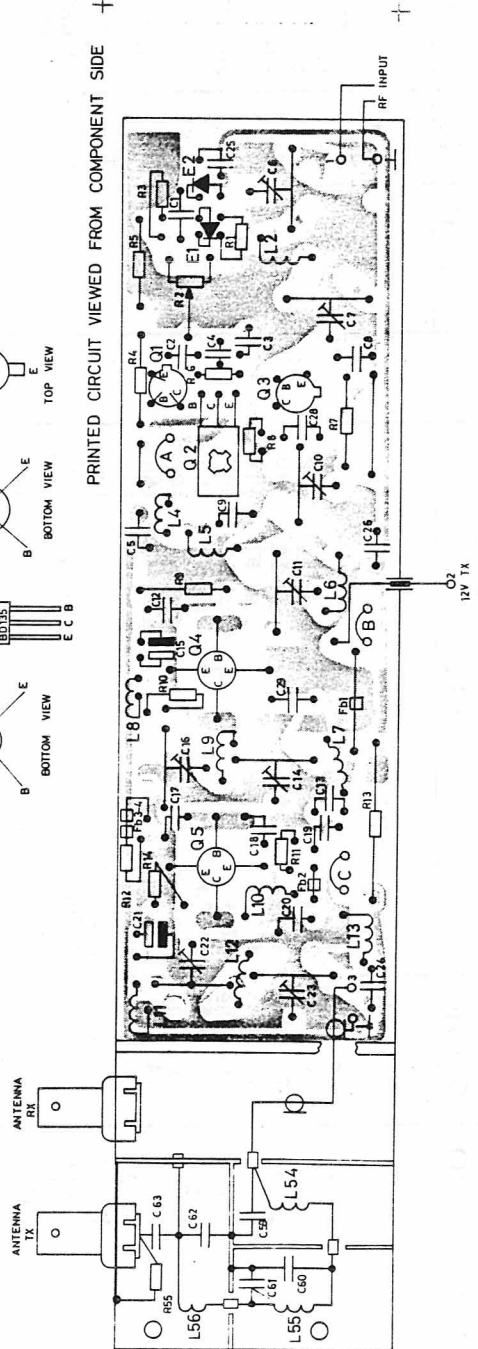
PA712

X401.800

2 af 2



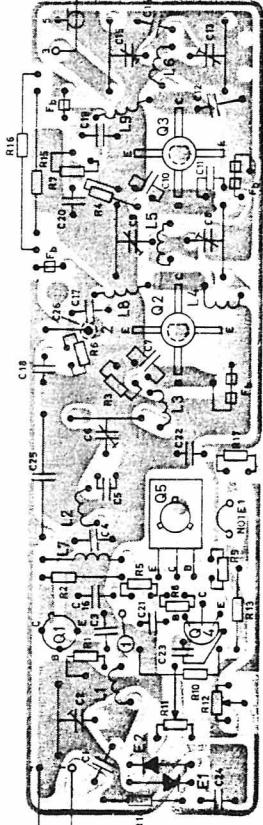
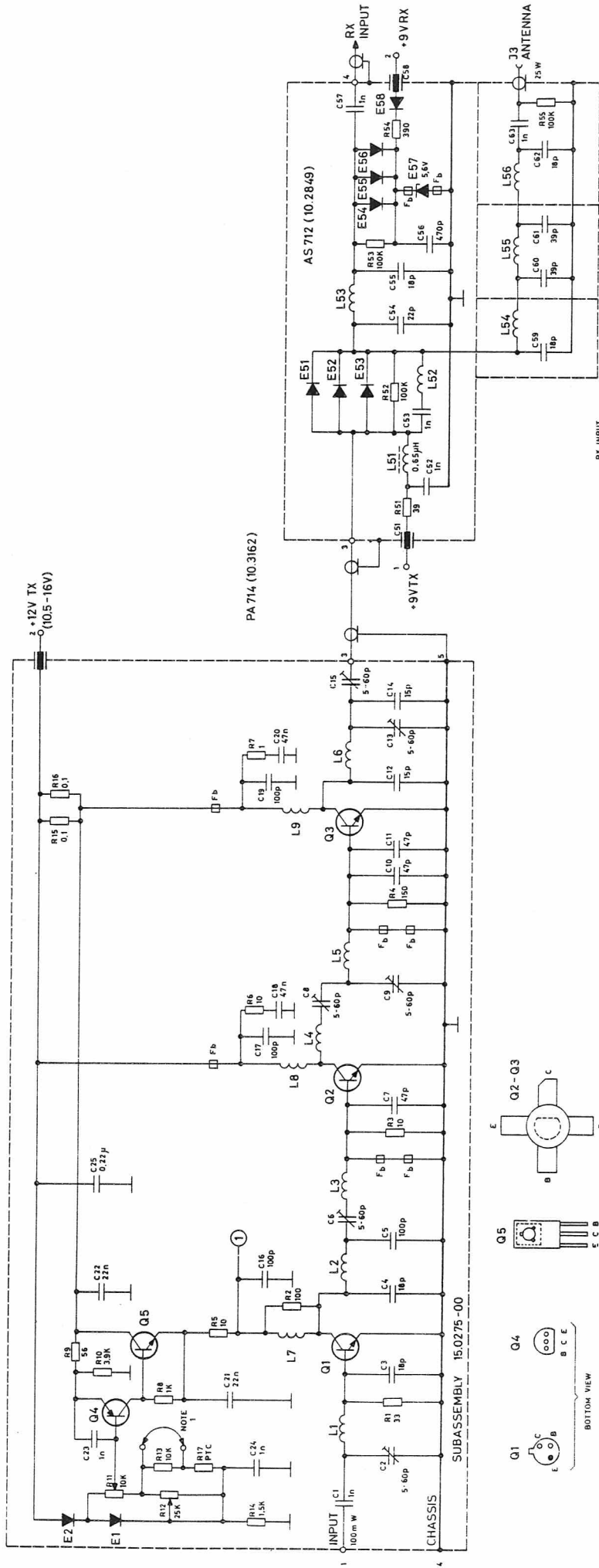
PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE



RF POWER AMPLIFIER
HF EFFEKTFORSTÆRKER

PA713

D401952



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE

NOTE 1 FIERNES VED INSTILLING AF MAX. EFFERT NEDREGULERING. TO BE REMOVED WHEN SETTING THE MAXIMUM POWER DECLINE.

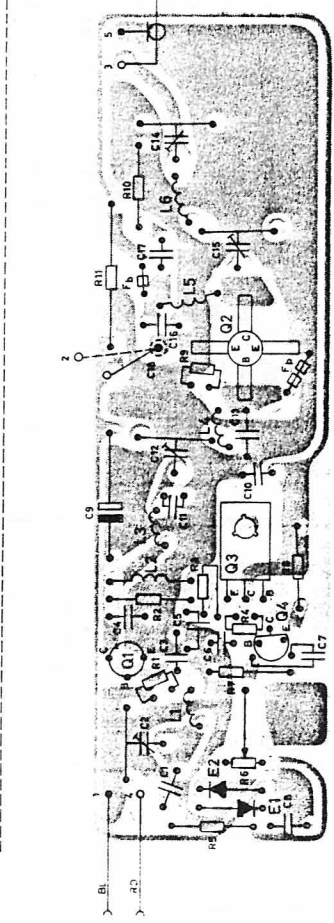
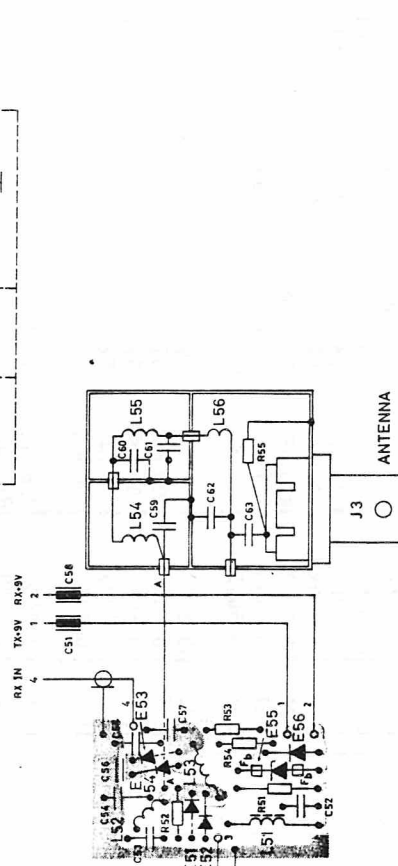
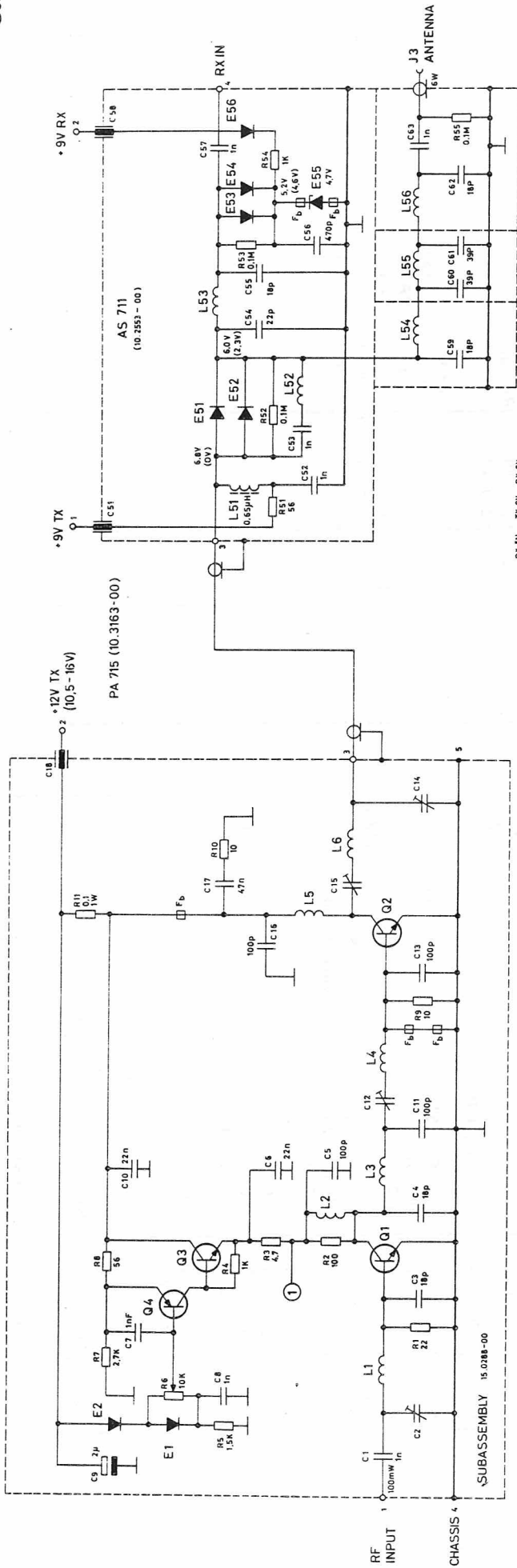
RF POWER AMPLIFIER PA 714

D.402.250

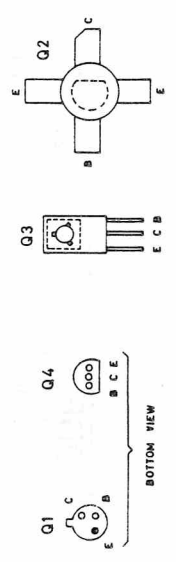
TYPE	Nº	CODE	DATA
PA714		10. 3162-00	Power Amplifier (AS712 incl.)
	C1	74. 5155	1 nF
	C2	78. 5061	5/60 pF
	C3	74. 5138	18 pF
	C4	74. 5138	18 pF
	C5	74. 5342	100 pF
	C6	78. 5061	5/60 pF
	C7	74. 5343	47 pF
	C8	78. 5062	5/60 pF
	C9	78. 5062	5/60 pF
	C10	74. 5343	47 pF
	C11	74. 5343	47 pF
	C12	74. 5046	15 pF
	C13	78. 5062	5/60 pF
	C14	74. 5046	15 pF
	C15	78. 5062	5/60 pF
	C16	74. 5013	100 pF
	C17	74. 5013	100 pF
	C18	76. 5072	47 nF
	C19	74. 5013	100 pF
	C20	76. 5072	47 nF
	C21	76. 5071	22 nF
	C22	76. 5071	22 nF
	C23	74. 5155	1 nF
	C24	74. 5155	1 nF
	C25	76. 5074	0. 22 µF
C26	69. 5023	Filter feed-through	
R1	80. 5231	33 Ω	carbon film
R2	80. 5237	100 Ω	"
R3	80. 5225	10 Ω	"
R4	80. 5239	150 Ω	"
R5	80. 5225	10 Ω	"
R6	80. 5225	10 Ω	"
R7	80. 5213	1 Ω	"
R8	80. 5249	1 KΩ	"
R9	80. 5234	56 Ω	"
R10	80. 5256	3. 9 KΩ	"
R11	86. 5039	10 KΩ	20% trim. carbon film
R12	86. 5060	25 KΩ	"
R13	80. 5261	10 KΩ	carbon film
R14	80. 5251	1. 5 KΩ	"
R15	82. 5208	0. 1 Ω	wire wound
R16	82. 5208	0. 1 Ω	"
R17	89. 5071	60 Ω - 50 KΩ	PTC

TYPE	Nº	CODE	DATA
AS712	L1	62. 0930	RF coil
	L2	62. 0930	RF coil
	L3	62. 0930	RF coil
	L4	62. 0932	RF coil
	L5	62. 0932	RF coil
	L6	62. 0931	RF coil
	L7	62. 0651	RF coil
	L8	62. 0933	RF coil
	L9	62. 0934	RF coil
	E1	99. 5028	1 N 914 Diode
	E2	99. 5028	1 N 914 Diode
	Q1	99. 5321	Transistor
	Q2	99. 5322	Transistor
	Q3	99. 5323	Transistor
	Q4	99. 5144-01	Transistor
	Q5	99. 5323	Transistor
	Fc1-6	65. 5060	Ferrite bead 60 MHz
		10. 2849-00	Antenna Switching Unit
	C51	69. 5007	VHF feed-through filter
	C52	74. 5155	1 nF -20 +80% ceram
	C53	74. 5155	1 nF -20 +80% "
	C54	74. 5008	22 pF 5% "
	C55	74. 5196	18 pF 5% "
	C56	74. 5162	470 pF -20 +50% no lead
	C57	74. 5155	1 nF -20 +80% ceram
	C58	69. 5007	VHF feed-through filter
C59	74. 5196	18 pF 5% ceram	
C60	74. 5197	39 pF 5% "	
C61	74. 5197	39 pF 5% "	
C62	74. 5196	18 pF 5% "	
C63	74. 5015	1 nF 20% "	
R51	80. 5232	39 Ω	carbon film
R52	80. 5073	100 KΩ	"
R53	80. 5073	100 KΩ	"
R54	80. 5044	390 Ω	"
R55	80. 5273	100 KΩ	"

POWER AMPLIFIER PA714



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE



RF POWER AMPLIFIER PA715

D.402.335

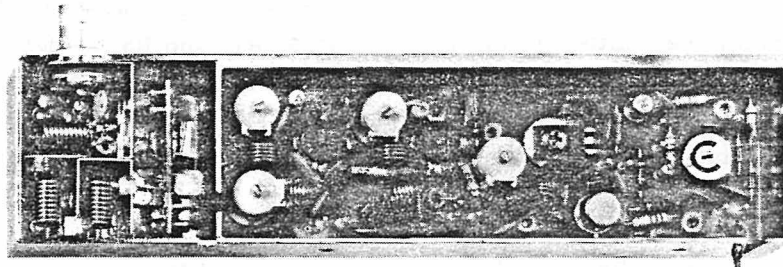
TYPE	Nº	CODE	DATA
PA715		10. 3163-00	Power Amplifier (AS711 incl.)
C1		74. 5115	ceram 63 V
C2		78. 5061	teflon trimmer 300 V
C3		74. 5138	ceram 125 V
C4		74. 5138	" 125 V
C5		74. 5013	" 400 V
C6		76. 5071	polyester 50 V
C7		74. 5155	ceram 63 V
C8		74. 5155	" 63 V
C9		73. 5064	2 µF -10 + 100%
C10		76. 5071	polyester 70 V
C11		74. 5342	ceram 50 V
C12		78. 5061	teflon trimmer 63 V
C13		74. 5013	ceram 300 V
C14		78. 5061	teflon trimmer 400 V
C15		78. 5061	teflon trimmer 300 V
C16		74. 5013	teflon trimmer 300 V
C17		76. 5072	ceram 400 V
C18		69. 5023	polyester 50 V
			Filter feed-through
R1		80. 5229	22 Ω 5%
R2		80. 5237	100 Ω 5%
R3		80. 5221	4.7 Ω 5%
R4		80. 5249	1 KΩ 5%
R5		80. 5251	1.5 KΩ 5%
R6		86. 5039	10 KΩ 20% trim
R7		80. 5254	2.7 KΩ 5%
R8		80. 5234	56 Ω 5%
R9		80. 5225	10 Ω 5%
R10		80. 5225	10 Ω 5%
R11		82. 5208	0.1 Ω 10%
E1		99. 5028	1 N 914 Diode
E2		99. 5028	1 N 914 Diode
L1		62. 0941	RF coil 146 - 174 MHz
L2		62. 0651	0.08 µH RF choke
L3		62. 0930	RF coil 146 - 174 MHz
L4		62. 0930	RF coil 146 - 174 MHz
Q1		99. 5321	Transistor MRF237
Q2		99. 5322	Transistor MRF212
Q3		99. 5235	Transistor BD135
Q4		99. 5144-01	Transistor BC214L
		15. 0288	Subassembly

TYPE	Nº	CODE	DATA
AS711		10. 2553-00	Antenna Switching Unit
C52		74. 5155	1 nF -20 + 80% ceram 63 V
C53		74. 5155	1 nF -20 + 80% " 63 V
C54		74. 5008	22 pF 5% " 400 V
C55		74. 5138	18 pF 5% " 125 V
C56		74. 5162	470 pF -20 + 50% " 400 V
C57		74. 5155	1 nF -20 + 80% ceram 63 V
C63		74. 5015	1 nF 20% " 400 V
R51		80. 5234	56 Ω 5% carbon film 1/10 W
R52		80. 5073	100 KΩ 5% " 1/10 W
R53		80. 5073	100 KΩ 5% " 1/10 W
R54		80. 5049	1 KΩ 5% " 1/10 W
R55		80. 5273	100 KΩ 5% " 1/8 W
L51		62. 0662-01	0.65 µH RF choke
L52		62. 0818	RF coil
L53		62. 0817	RF coil
E51		99. 5244	Diode BA182
E52		99. 5244	Diode BA182
E53		99. 5244	Diode BA182
E54		99. 5244	Diode BA182
E55		99. 5224	Zenerdiode 4.7 V 5%
E56		99. 5237	Diode 1N4148 0.25 W

POWER AMPLIFIER PA715

X402.368

RF POWER AMPLIFIER PA731



Description

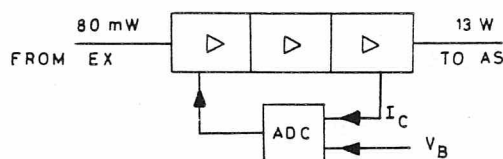
General

PA731 contains 3 power amplifier stages and a current regulating circuit.

The unit is completely shielded, being built into a combination heat sink and shield which also contains the antenna switching unit.

The current regulating circuit monitors both the supply voltage and the output transistor collector current, preventing overloading of the transistors due to either too high a voltage or too great a standing wave ratio in the output load. This circuit also allows the output power to be more independent of the power supply or of variations in power output from the exciter.

RF Power Amplifier



The first driver, Q1, gets its collector voltage via the ADC circuit regulating transistor, Q5. Increasing or decreasing the collector voltage to Q1 regulates the drive power applied to the following stages.

Q1 amplifies the exciter signal of about 80 mW to approx. 400 mW, which is necessary to drive Q2 properly.

Transistor Q2 further amplifies the power to approx. 3 W in order to be able to drive the final power amplifier, Q3.

Output transistor Q3 amplifies the RF power signal to approximately 14 W and the following matching network of L7, C18/C19 and C20/C21 suppresses harmonics of the fundamental VHF frequency while transforming the collector impedance of Q3 to the antenna impedance of 50 Ω . Resistor R8 in the output transistor collector path is the current monitoring resistor for the ADC circuit.

Current Regulating Circuit (ADC)

The purpose of the regulating circuit is to protect the transistors against overloads caused by too high a supply voltage and to limit current through the output transistor in case of mismatching. To accomplish this, the regulating circuit must monitor the supply voltage as well as the collector current through the transistor and from such results regulate the collector voltage to the first RF driver transistor, Q1, and thus the drive power to the following stages.

The circuit consists of two DC coupled transistor stages, Q4 and Q5. Base to Q4 is tied to a reference voltage that can be determined by setting the trimming potentiometer, R10. Reference voltage is developed across diodes E1 and E2, which are biased into forward conduction. This introduces a temperature dependency in the reference voltage that compensates for the temperature characteristics of the transistors.

For easier understanding of the circuit principle, first ignore its voltage dependent features; therefore, imagine that resistor R13 is removed from the circuit.

The DC return path for the emitter of Q4 is through R8 to the positive voltage terminal. R8 carries the collector current from the output amplifier Q3. A rise in this collector current will mean an increase in the voltage drop across R8, causing the emitter of Q4 to become less positive and the collector voltage will likewise become less positive. This decreases bias to Q5, decreasing the current through this transistor. Since Q5 is in series with the DC collector path of Q1, the effect will be that of placing a larger resistor in series with the collector supply, thus reducing collector voltage to Q1. The RF drive to the output stage will fall, thereby counteracting the original increase in collector current.

If the supply voltage increases, the current through the output transistors will be kept constant as already explained, but the power dissipation in the transistor will increase along with the voltage. To counteract this effect, a voltage regulating loop is included.

Imagine R13 connected back into the circuit again so that a voltage divider consisting of R15 and R13 will develop a voltage across R15 in proportion to the supply voltage.

When the supply voltage increases so will the voltage drop across R15 and the base-emitter bias for Q4 will fall, again resulting in a reduction of collector voltage to Q1 and a reduction in the drive to the output stage.

The reduction of drive power decreases the current through Q3 and R8 just enough to counteract the original increase of voltage across R15.

The transmitter output power can be set to the desired level by means of potentiometer R10 in the ADC circuit.

By selecting a suitable ratio between resistors R15, R13 and R8 the desired amount of regulation can be achieved.

Technical Specification

Frequency Range

68 - 88 MHz

Supply Voltage

Nominal 13.6 V (12.5 V)

Operating range 10 - 16 V

Output Power at 13.6 V : 13.5 W

With output power set for
12 W at 13.6 V,
as measured through AS731 :

Output power at 16 V 13 W

Output power at 10 V 8 W

Current Consumption

at nominal voltage 13.6 V : 2.0 A

at 16 V : 1.85 A

at 10 V : 1.7 A

Input Power

(min. 50 mW, max. 150 mW) 80 mW

Input Impedance

50 Ω

Output Impedance

50 Ω

Gain at $P_{in} = 50 \text{ mW}$

24 dB

Temperature Range

Operating range : -25° to $+70^{\circ}$ C

Functioning range : -30° to $+80^{\circ}$ C

Mechanical Dimensions

25 x 42 x 168 mm

(PC board : 35.6 x 119.4 mm)

ANTENNA SWITCH AS731

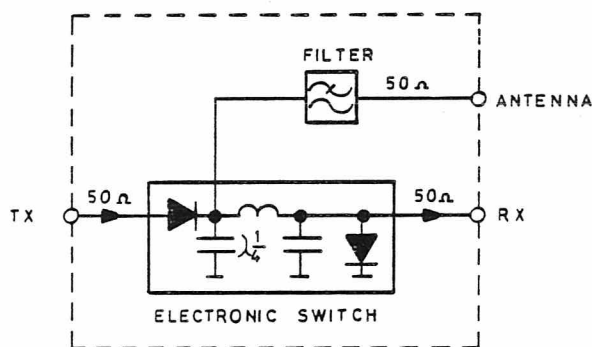
Description

General

The antenna switch AS731 contains a circuit for electronically switching the antenna between the transmitter and the receiver sections, and a low-pass filter that attenuates undesired frequencies, such as harmonics of the signal frequency, thus preventing their being radiated from the antenna.

AS731 mounts directly into the combination heat sink and shield for PA731.

The following simplified diagram shows the operating principle for the AS sub-unit.



The Electronic Switch

Refer to the complete schematic diagram D401.364.

By switching a +9 V potential between terminals 1 and 2, the antenna is electronically switched between transmit and receive.

When transmitting, diodes E51, E52, E53, and E54 conduct. The receiver terminal will see a short circuit.

The $1/4$ wave impedance circuit consisting of C53, L52 and C54 transforms the short to an open circuit at the antenna, thus the transmit signal reaches the antenna with minimum loss.

When receiving, the diodes are effectively blocked due to the bias across zener diode E55. Now the diodes only represent a small capacity which, at the frequencies involved, has negligible influence upon the signal path from antenna to receiver.

The transmitter terminal, however, is isolated from the antenna.

The received signal is now free to pass from the antenna to the receiver input with minimum loss.

The Low-pass Filter

The low-pass filter is a 7-pole Chebishev filter exhibiting negligible band-pass ripple and minimum insertion loss.

The filter is built on a metal plate chassis having three closed compartments. It requires no alignment.

Technical Specification

Frequency Range

68 - 88 MHz

Input and Output Impedance

50 Ω

Insertion Loss (transmitter to antenna)

0.5 dB

Insertion Loss (antenna to receiver)

0.6 dB

Separation between Transmitter and Receiver

27 dB

Second Harmonic (136 MHz) Attenuation

46 dB

Current Drain, transmit

38 mA

Current Drain, receive

4 mA

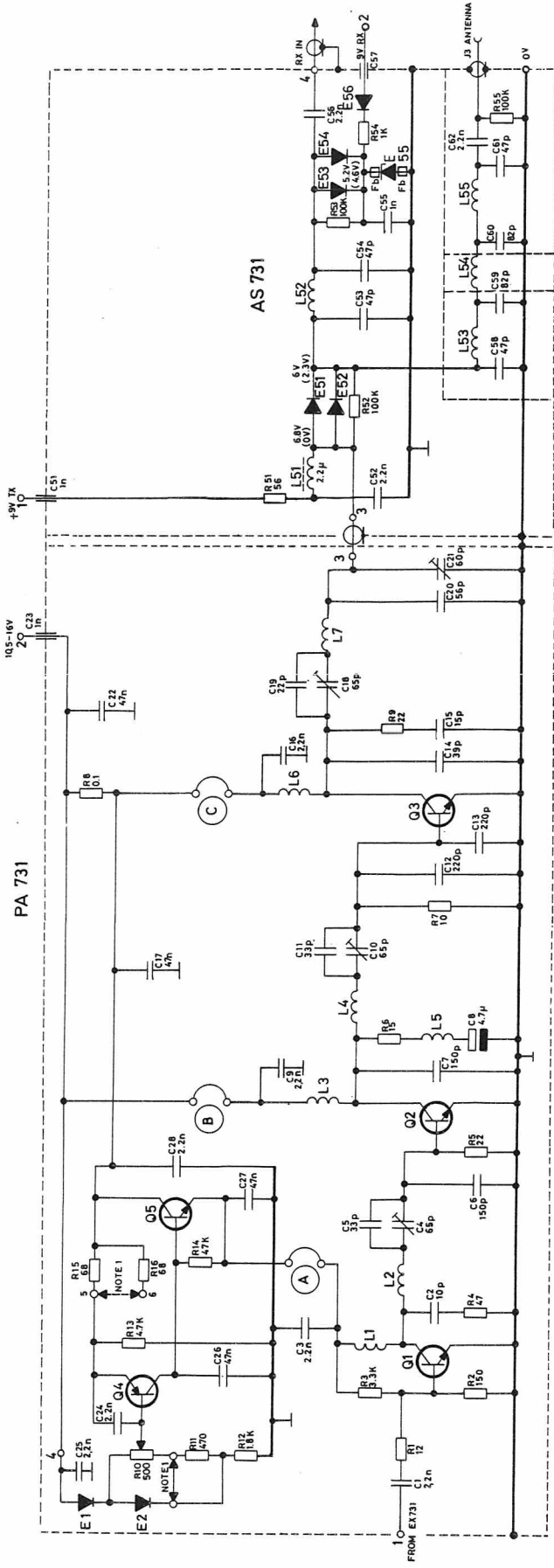
Temperature Range

operating range -25° to $+70^{\circ}$ C

functioning range -30° to $+70^{\circ}$ C

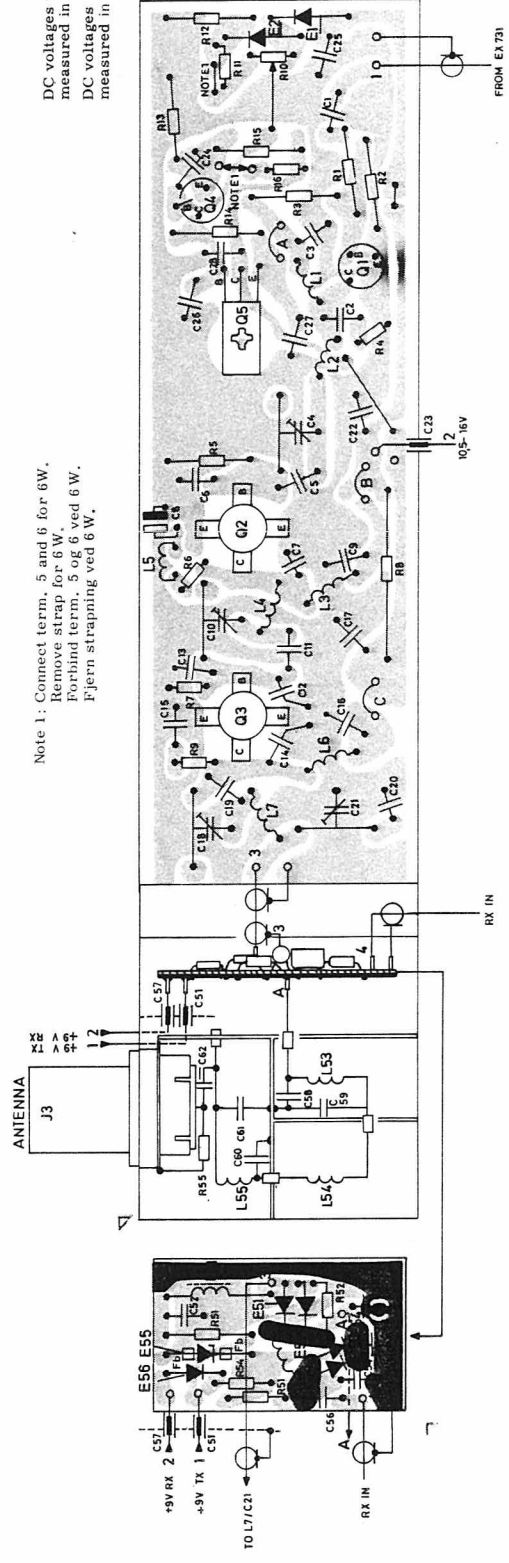
Dimensions

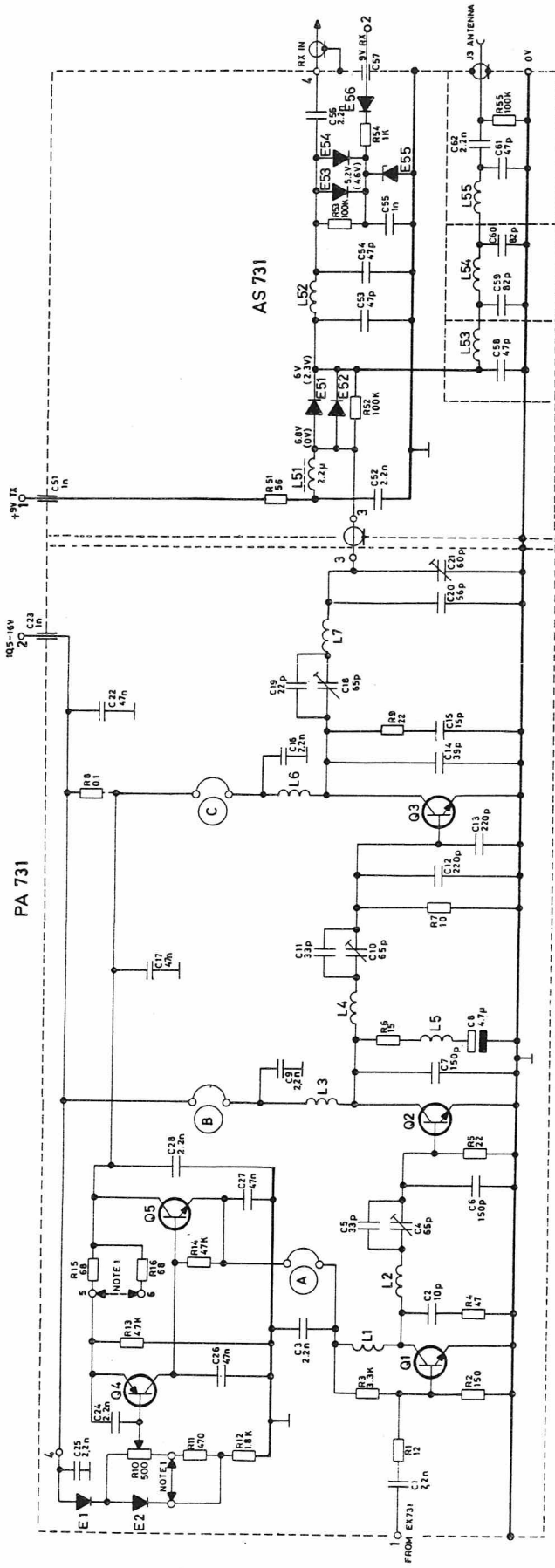
40 x 38 x 22 mm



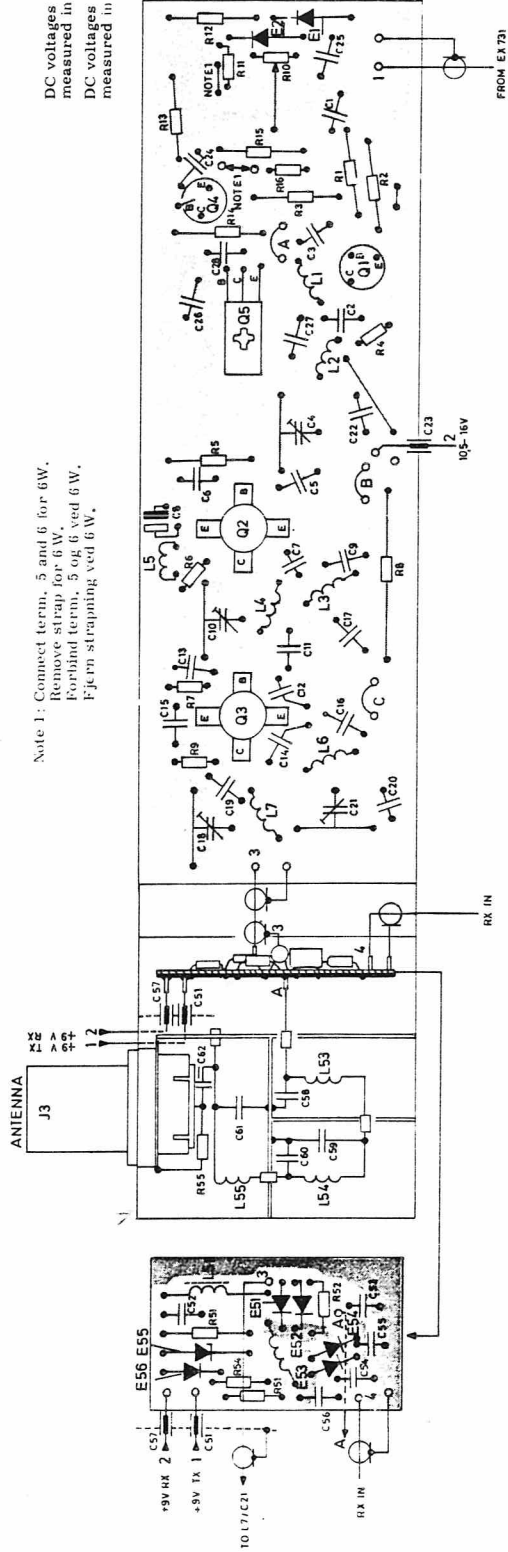
DC voltages without paranthesis
measured in transmit mode
DC voltages with paranthesis
measured in receive mode

Note 1: Connect term. 5 and 6 for 6W.
Remove strap for 6W.
Forbind term. 5 og 6 ved 6 W.
Fjern strapping ved 6W.





Note 1: Connect term. 5 and 6 for 6W.
 Remove strap for 6W.
 Forbind term. 5 og 6 ved 6W.
 Fjern strapping ved 6W.



DC voltages without paranthesis
 measured in transmit mode
 DC voltages with paranthesis
 measured in receive mode

POWER AMPLIFIER
 EFFEKTFORSTÆRKER

PA731

D401888

TYPE	NO.	CODE	DATA
PA 731		10.2629-00	Power amplifier (AS 731 incl.)
	C1	74.5163	2.2nF - 20+80% ceram PL 63V
	C2	74.5135	10pF 5% ceram DI 125V
	C3	74.5163	22nF - 20+80% ceram PL 63V
	C4	78.5052	8 - 60pF trimmer 100V
	C5	74.5116	33pF 5% ceram TB 160V
	C6	74.5202	150pF 10% ceram PL 25V
	C7	74.5202	150pF 10% ceram PL 25V
	C8	73.5126	4.7μF 20% tantal 35V
	C9	74.5163	2.2nF - 20+80% ceram PL 63V
	C10	78.5052	8 - 60pF trimmer 100V
	C11	74.5116	33pF 5% ceram TB 160V
	C12	74.5203	220pF 10% ceram 25V
	C13	74.5203	220pF 10% ceram PL 25V
	C14	74.5197	39pF 5% ceram DI 400V
	C15	74.5137	15pF 5% ceram DI 125V
	C16	74.5163	2.2nF - 20+80% ceram PL 63V
	C17	76.5072	47nF 10% polyest FL 50V
	C18	78.5052	8 - 60pF trimmer 100V
	C19	74.5008	22pF 5% ceram DI 400V
	C20	75.5015	56pF 5% mica 500V
	C21	78.5052	8 - 60pF trimmer 100V
	C22	76.5072	47nF 10% polyest. FL 50V
	C23	69.5023	VHF feed - through filter
	C24	74.5163	2.2nF - 20+80% ceram PL 63V
	C25	74.5163	2.2nF - 20+80% ceram PL 63V
	C26	76.5072	47nF 10% polyest FL 50V
	C27	76.5072	47nF 10% polyest FL 50V

TYPE	NO.	CODE	DATA
	C28	74.5163	2.2nF - 20x80% ceram PL 63V
	R1	80.5226	12Ω 5% carbonfilm 1/8W
	R2	80.5239	150Ω 5% carbon film 1/8W
	R3	80.5255	3.3kΩ 5% carbon film 1/8W
	R4	80.5233	47Ω 5% carbon film 1/8W
	R5	80.5229	22Ω 5% carbon film 1/8W
	R6	80.5427	15Ω 5% carbon film 1/4W
	R7	80.5225	10Ω 5% carbon film 1/8W
	R8	82.5208	0.1Ω 10% wire wound 1W
	R9	80.5429	22Ω 5% carbon film 1/4W
	R10	86.5042	500Ω 20% potentiometer 0.1W
	R11	80.5245	470Ω 5% carbon film 1/8W
	R12	80.5252	1.8kΩ 5% carbon film 1/8W
	R13	80.5257	4.7kΩ 5% carbon film 1/8W
	R14	80.5269	47kΩ 5% carbob film 1/8W
	R15	80.5235	68Ω 5% carbon film 1/8W
	R16	80.5235	68Ω 5% carbon film 1/8W
	L1	62.0828	RF coil 68 - 88 MHz
	L2	62.0832	RF coil 68 - 88 MHz
	L3	62.0829	RF coil 68 - 88 MHz
	L4	62.0830	RF coil 68 - 88 MHz
	L5	62.0651	0.08μH RF choke
	L6	62.0831	RF coil 68 - 88 MHz
	L7	62.0829	RF coil 68 - 88 MHz

RF POWER AMPLIFIER
HF EFFEKTFORSTÆRKER

PA731

X 401.787

TYPE	NO.	CODE	DATA
	E1	99.5028	1N 914 diode
	E2	99.5028	1N 914 diode
	Q1	99.5229	2N 4427 transistor
	Q2	99.5252	BLY 87 A transistor
	Q3	99.5253	BLY 88 A transistor
	Q4	99.5230	BC 178 transistor
	Q5	99.5235	BD 135 transistor
AS 731		10.2668-00	Antenna switch
	C51	69.5007	VHF feed - through filter
	C52	74.5163	2.2nF -20 +80% ceram PL 63V
	C53	74.5014	47pF 5% mica 500V
	C54	74.5118	47pF 5% ceram TB 160V
	C55	74.5204	1nF - 20+80% ceram DI 400V
	C56	74.5163	2.2 nF -20+80% ceram PL 63V
	C57	69.5007	VHF.feed - through filter
	C58	75.5014	47pF 5% mica 500V
	C59	75.5016	82pF 5% mica 500V
	C60	75.5016	82pF 5% mica 500V
	C61	75.5014	47pF 5% mica 500V
	C62	74.5093	2.2nF - 20+80% ceram DI 400V
	R51	80.5234	56Ω 5% carbon film 1/8W
	R52	80.5073	0.1MΩ 5% carbon film 0.1W
	R53	80.5073	0.1MΩ 5% carbon film 0.1W
	R54	80.5049	1kΩ 5% carbon film 0.1W
	R55	80.5273	0.1MΩ 5% carbon film 1/8W

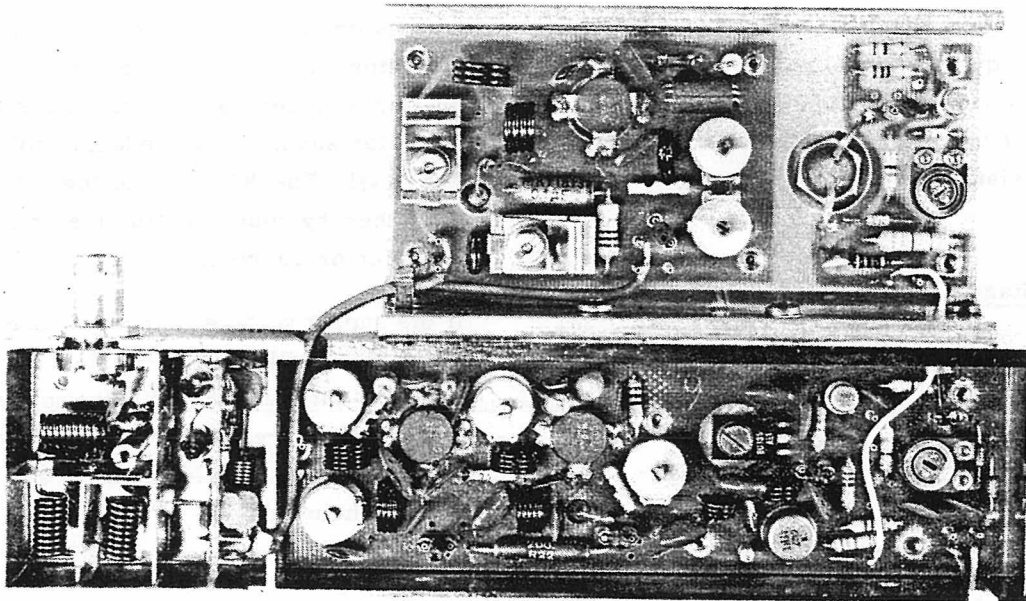
TYPE	NO.	CODE	DATA
	L51	63.5006	2.2μH 20% RF choke 0.6A
	L52	62.0836	RF coil 68 - 88 MHz
	L53	62.0837	RF coil 68 - 88 MHz
	L54	62.0837	RF coil 68 - 88 MHz
	L55	62.0837	RF coil 68 - 88 MHz
	E51	99.5214	BA 182 diode
	E52	99.5214	BA 182 diode
	E53	99.5214	BA 182 diode
	E54	99.5214	BA 182 diode
	E55	99.5224	4.7V 5% zenerdiode 0.25W
	E56	99.5237	1N 4148 diode

POWER AMPLIFIER
EFFEKTFORSTÆRKER

PA731

X401.787

RF POWER AMPLIFIER PA732



Description

PA732 comprises 4 RF power amplifier stages, three in the driver and one in the booster as well as a regulating and temperature protection circuit and, finally, an electronic antenna switching unit with filter, AS732.

PA732 is completely shielded, as it is built into a combination heat sink and shield. However, heat dissipation will be insufficient without the external heat sink/cabinet CA703.

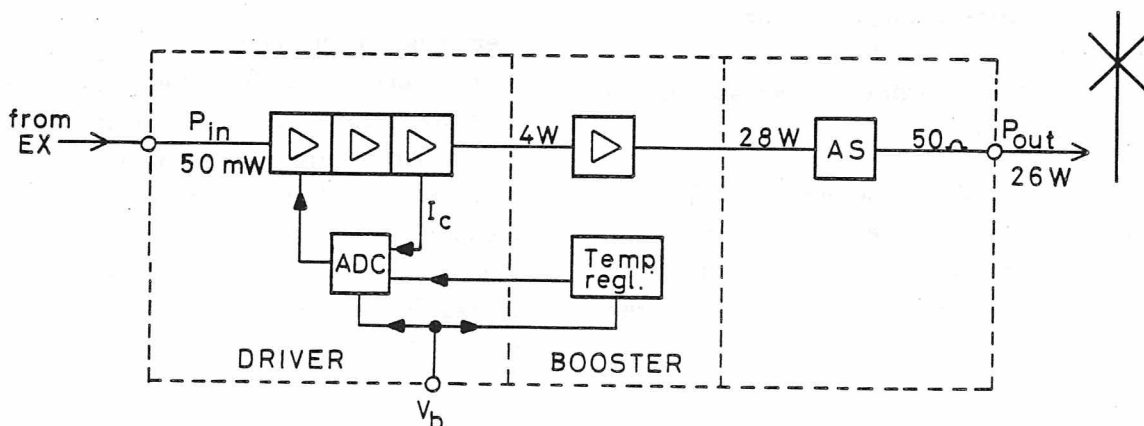
The regulating and temperature protection circuit protects the transistors and other components in the unit against incurring damages when operated within the permissible values of supply voltages and temperatures, or as a re-

sult of prolonged short circuits or too great a standing wave ratio in the output load.

RF Power Amplifier

The first driver, Q1, gets its collector voltage via the ADC circuit regulating transistor, Q5. Increasing or decreasing the collector voltage to Q1 regulates the drive power applied to the following stages.

RC-network C1, R1, R2 and R3 matches the exciter output impedance to the input impedance of Q1. Due to this impedance matching it is also possible to drive the PA stage from a 50 Ω generator.



Q1, Q2 and Q3 amplify the exciter output signal of 50 mW to 4 W in order to drive the booster stage. Matching network L7, C18, C19, C20 and C21 suppresses harmonics of the fundamental VHF frequency while transforming the collector impedance of Q3 to 50 Ω . Resistor R8 in the collector return of Q3 is the current monitoring resistor for the ADC circuit.

Booster Stage

Q101 amplifies the 4 W output power from the driver stage to 28 W and applies the signal to AS732. Due to the inherent losses in the AS unit the PA output power is then 26 W.

Current Regulating Circuit (ADC)

The purpose of the regulating circuit is to protect the transistors against overloads caused by excessive supply voltage and to limit current through the output transistor in case of mismatching. To accomplish this, the regulating circuit must monitor the supply voltage as well as the collector current through Q3 in the driver stage and from such results regulate the collector voltage to the first driver transistor Q1, and thus the drive power to the following stages.

The circuit consists of two DC coupled transistor stages, Q4 and Q5. Base to Q4 is tied to a reference voltage that can be determined by setting potentiometer R10. Reference voltage is developed across diodes E1 and E2, which are biased into forward conduction. This introduces a temperature dependency in the reference voltage that compensates for the temperature characteristics of the transistors.

For easier understanding of the circuit principle, first ignore its voltage dependent features; therefore, imagine that resistor R13 is removed from the circuit.

The DC return path for the emitter of Q4 is through R8 to the positive voltage terminal. R8 also carries the collector current from transistor Q3. A rise in this collector current will mean an increase in the voltage drop across R8, causing the emitter of Q4 to become less

positive and the collector voltage will likewise become less positive. This decreases forward bias to Q5, decreasing the current through this transistor. Since Q5 is in series with the DC collector path of Q1, the effect will be that of placing a larger resistor in series with the collector supply, thus reducing collector voltage to Q1. The RF drive to the output stage will fall, thereby counteracting the original increase in collector current.

If the supply voltage increases, the current through Q3 will be kept constant as already explained, but the power dissipation in the transistor will increase along with the voltage. To counteract this effect, a voltage regulating loop is included.

Imagine R13 connected back into the circuit again so that a voltage divider consisting of R15 and R13 will develop a voltage across R15 in proportion to the supply voltage.

When the supply voltage increases so will the voltage drop across R15 and the base-emitter bias for Q4 will fall, again resulting in a reduction of collector voltage to Q1 and a reduction in the drive to the output stage.

The reduction of drive power decreases the current through Q3 and R8 just enough to counteract the original increase of voltage across R15. By selecting a suitable ratio between resistors R15, R13 and R8 the desired amount of regulation can be achieved.

The transmitter power can be set to the desired level by means of potentiometer R10 in the ADC circuit.

Temperature Protection Circuit

Since transistor Q101 in the booster stage is not directly included in the ADC loop, it requires extra thermal protection which is accomplished by means of a PTC resistor, R109, which is mounted close to Q101. When Q101, and R109 along with it, reach a certain temperature the increasing resistance of R109, which is also a part of the ADC loop of the driver stage, regulates (reduces) the drive to Q101.

Thus the output power of the PA unit is regulated to a preset level that ensures thermal protection of Q101 and other components.

The temperature protection circuit operates in the following manner: Under normal operating conditions (prior to regulation) Q102 is biased to cut-off by the voltage divider network of R104 and the PTC resistor (60 Ω) connected across zener diode E101 for a stable source. As the temperature in the PA stage rises the resistance of R109 increases and Q102 begins to pass current. When R109 reaches 1.2 kΩ Q102 will be completely open. When Q102 opens up, the circuit shunts diodes E1 and E2 and the voltage across these diodes falls, causing the base-emitter voltage for Q4 to fall, as well.

As a result, Q1's collector voltage falls, too, thereby also reducing the drive to the following stages.

The amount of regulation (reduction in output power) is preset by potentiometer R107. Q102's emitter resistor is included to flatten out the regulation characteristic. Diode E102 in the collector lead of Q102 ensures temperature compensation of the reference voltage at the base of Q4 even at maximum regulation.

Technical Specifications

Frequency Range

68 to 88 MHz

Nominal Supply Voltage

13 V

Output Power

With output power set for 26 W at 13 V

output power at 15.5 V 26 W

output power at 10 V 16 W

Current Consumption

At nominal 13 V: 4.3 A

at 15.5 V: 4 A

at 10 V: 3.5 A

Input Power

nominal 80 mW

minimum 50 mW

Input Impedance

50 Ω

Output Impedance

50 Ω

Gain with $P_{in} = 50 \text{ mW}$

27 dB

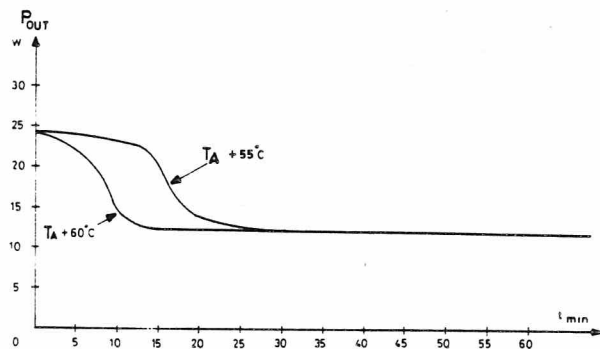
Reduction of Output Power vs. Ambient Temperature

Continuous, $T_A -25^\circ \text{ to } +25^\circ \text{C}$ 0.6 dB

Intermittent, $T_A -25^\circ \text{ to } +55^\circ \text{C}$ 0.6 dB

Continuous, $T_A +55^\circ \text{C}$ 3 dB

(refer to response curve below)



Typical output power regulating characteristic of PA732 with CA703 mounted. Plotted for ambient temperatures of +55°C and +60°C, at nominal voltage, continuous keying of transmitter.

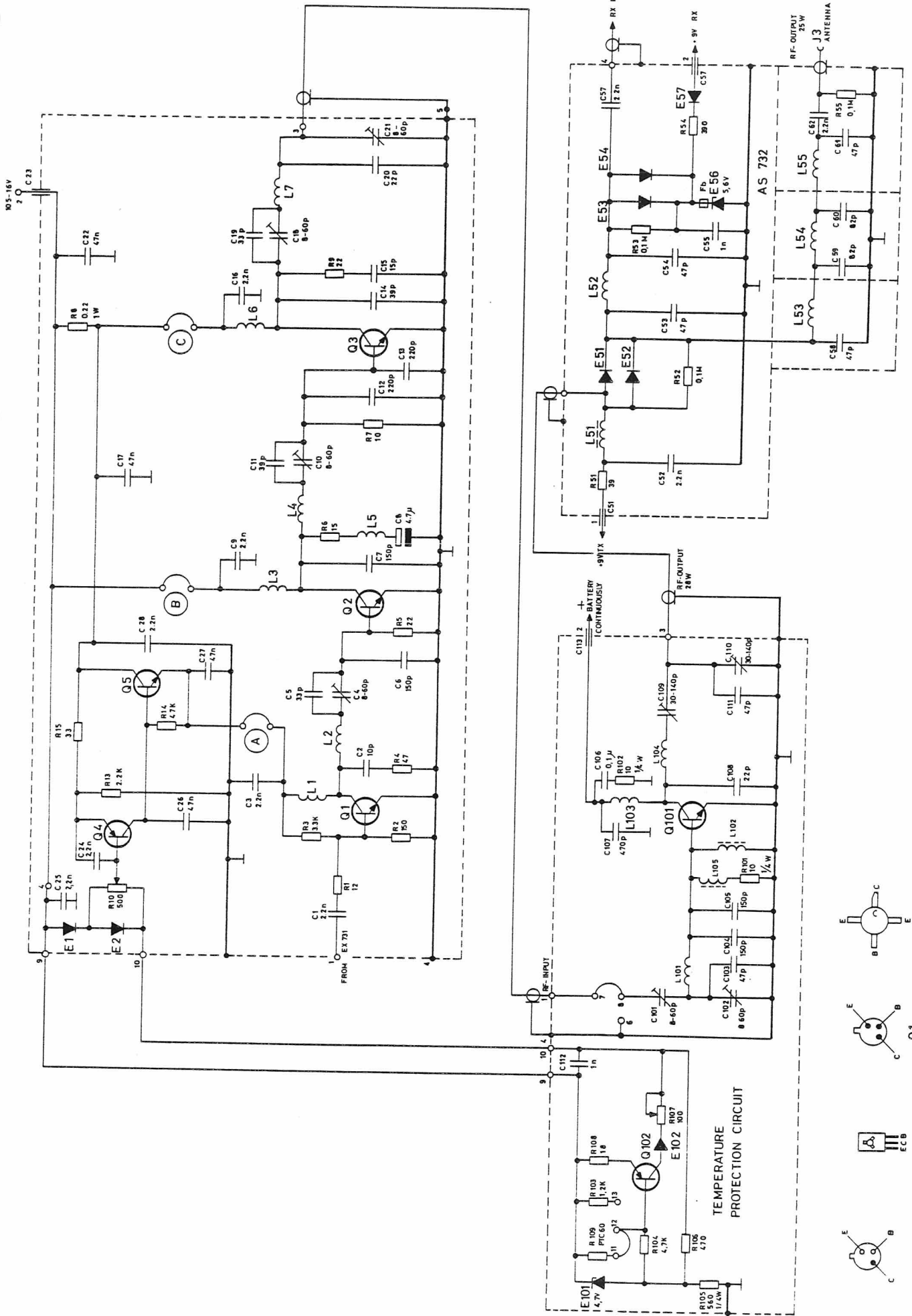
Temperature Range

operating $-25^\circ \text{C to } +55^\circ \text{C}$

functioning $-30^\circ \text{C to } +60^\circ \text{C}$.

Mechanical Dimensions

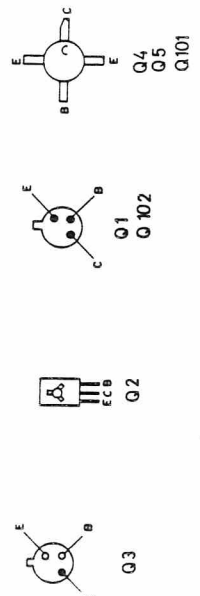
168 x 97 x 32 mm

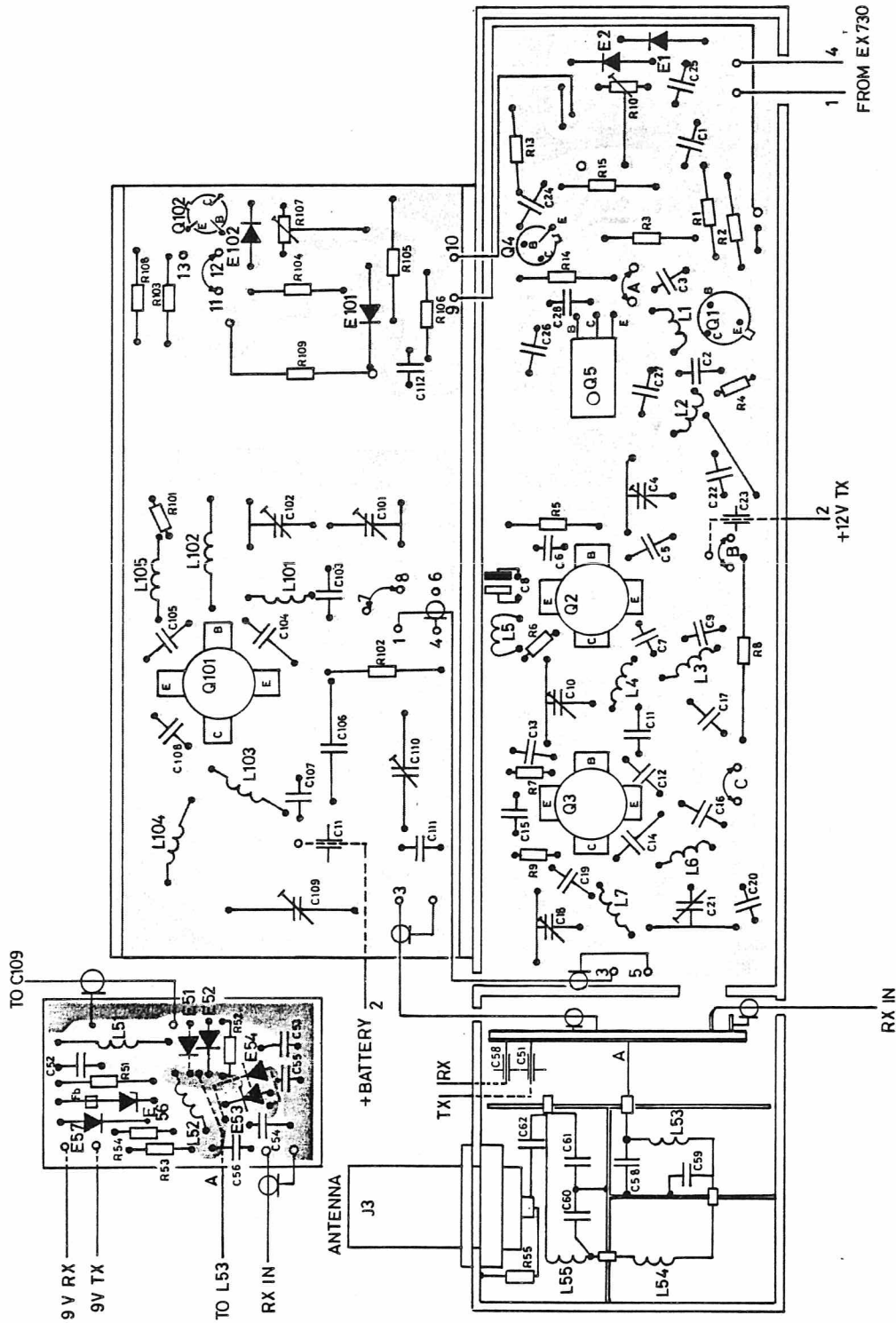


**POWER AMPLIFIER
EFFEKTFORSTÆRKER**

PA732

D 401.956/2





POWER AMPLIFIER
EFFEKTFORSTÆRKER

PA732

D402.168

TYPE	NO.	CODE	DATA
PA732		10. 3044	POWER AMPLIFIER
	C1	74. 5163	2. 2nF -20+80% ceram PL
	C2	74. 5135	10pF ± 5% N150 ceram DI
	C3	74. 5163	2. 2nF -20+80% ceram PL
	C4	78. 5052	8-60pF Trimmer
	C5	74. 5116	33pF ± 5% N075 ceram TB
	C6	74. 5202	150pF ± 10% N750 ceram PL
	C7	74. 5202	150pF ± 10% N750 ceram PL
	C8	73. 5126	4. 7μF 20% tantal
	C9	74. 5163	2. 2nF -20+80% ceram PL
	C10	78. 5052	8-60pF Trimmer
	C11	74. 5117	39pF ± 5% N075 ceram TB
	C12	74. 5203	220pF ± 10% N750 ceram PL
	C13	74. 5203	220pF ± 10% N750 ceram PL
	C14	74. 5197	39pF ± 5% N150 DI
	C15	74. 5137	15pF ± 5% N150 ceram DI
	C16	74. 5163	2. 2nF -20+80% ceram PL
	C17	76. 5072	47nF 10% polyester, FL
	C18	78. 5052	8-60pF Trimmer
	C19	74. 5116	33pF ± 5% N075 ceram TB
	C20	74. 5008	22pF ± 5% N150 ceram DI
	C21	78. 5052	8-60pF Trimmer
	C22	76. 5072	47nF 10% polyester, FL
	C23	69. 5023	VHF feed-through filter
	C24	74. 5163	2. 2nF -20+80% ceram PL
	C25	74. 5163	2. 2nF -20+80% ceram PL
	C26	76. 5072	47nF 10% polyester, FL
	C27	76. 5072	47nF 10% polyester, FL
	C28	74. 5163	2. 2nF -20+80% ceram PL
	C51	69. 5007	VHF feed-through filter
	C52	74. 5163	2. 2nF -20+80% ceram PL
	C53	75. 5014	47pF ± 5% mica
	C54	74. 5118	47pF 5% N075 TB
	C55	74. 5204	1nF -20+80% ceram DI
	C56	74. 5163	2. 2nF -20+80% ceram PL
	C57	69. 5007	VHF feed-through filter
	C58	75. 5014	47pF 5% mica
	C59	75. 5016	82pF 5% mica
	C60	75. 5016	82pF 5% mica
	C61	75. 5014	47pF 5% mica
	C62	74. 5093	2. 2nF -20+50% ceramic DI
	C101	78. 5052	8-60pF Trimmer
	C102	78. 5052	8-60pF Trimmer
	C103	74. 5118	47pF 5% N075 ceram TB
	C104	74. 5166	150pF ± 10% N750 ceram PL
	C105	74. 5166	150pF ± 10% N750 ceram PL

TYPE	NO.	CODE	DATA
	C106	76. 5073	0. 1μF ± 10% polyester, TB
	C107	74. 5094	470pF ± 20% K2000D
	C108	74. 5008	22pF ± 5% N150 ceram DI
	C109	78. 5057	30-140pF mica
	C110	78. 5057	30-140pF mica
	C111	75. 5014	47pF ± 5% mica
	C112	74. 5155	1nF -20+80% ceram PL
	C113	69. 5023	VHF feed-through filter
	R1	80. 5226	12Ω 5% carbon film
	R2	80. 5239	150Ω 5% carbon film
	R3	80. 5255	3. 3k 5% carbon film
	R4	80. 5233	47k 5% carbon film
	R5	80. 5229	22Ω 5% carbon film
	R6	80. 5427	15Ω 5% carbon film
	R7	80. 5225	10Ω 5% carbon film
	R8	82. 5205	0. 22Ω 10% Wire wound
	R9	80. 5429	22Ω 5% carbon film
	R10	86. 5042	500Ω 20% trim carbon
	R13	80. 5253	2. 2kΩ 5% carbon film
	R14	80. 5269	47kΩ 5% carbon film
	R15	80. 5231	33Ω 5% carbon film
	R51	80. 5232	39Ω 5% carbon film
	R52	80. 5073	100kΩ 5% carbon film
	R53	80. 5073	100kΩ 5% carbon film
	R54	80. 5044	390Ω 5% carbon film
	R55	80. 5273	0. 1 MΩ 5% carbon film
	R101	80. 5425	10Ω 5% carbon film
	R102	80. 5425	10Ω 5% carbon film
	R103	80. 5250	1. 2kΩ 5% carbon film
	R104	80. 5257	4. 7kΩ 5% carbon film
	R105	80. 5446	560Ω 5% carbon film
	R106	80. 5245	470Ω 5% carbon film
	R107	86. 5051	100Ω 20% potentiometer
	R108	80. 5228	18Ω 5% carbon film
	R109	89. 5066	60Ω -50+100% PTC thermistor
	L1	62. 0828	RF coil 68-88 MHz
	L2	62. 0832	RF coil 68-88 MHz
	L3	62. 0829	RF coil 68-88 MHz
	L4	62. 0830	RF coil 68-88 MHz

POWER AMPLIFIER EFFEKTFORSTÆRKER

PA732

X 401. 957

Storno

TYPE	NO.	CODE	DATA
L5	62.0651	0.08 μ H RF choke	
L6	62.0831	RF coil 68-88 MHz	
L7	62.0829	RF coil 68-88 MHz	
L51	63.5006	2.2 μ H +20% RF choke 0.6A	
L52	62.0836	RF coil	
L53	62.0837	RF coil	
L54	62.0837	RF coil	
L55	62.0837	RF coil	
L101	62.0893	RF coil 68-88 MHz	
L102	61.5016	Wide band RF choke	
L103	62.0841	RF coil 68-88 MHz	
L104	62.0894	RF coil 68-88 MHz	
L105	62.0651	0.08 μ H RF choke	
E1	99.5028	1N914 diode	
E2	99.5028	1N914 diode	
E51	99.5244	BA182 diode	
E52	99.5244	BA182 diode	
E53	99.5244	BA182 diode	
E54	99.5244	BA182 diode	
E56	99.5282	Zener diode 5.6V 5%	
E57	99.5237	1N4148 diode	
E101	99.5224	Zener diode 4.7V 5%	
E102	99.5237	1N4148 diode	
Q1	99.5229	2N4427 transistor	
Q2	99.5252	BLY87A transistor	
Q3	99.5253	BLY88A transistor	
Q4	99.5230	BC178 transistor	
Q5	99.5235	BD135 transistor	
Q101	99.5280	BLY89A transistor	
Q102	99.5230	BC178 transistor	

Storno

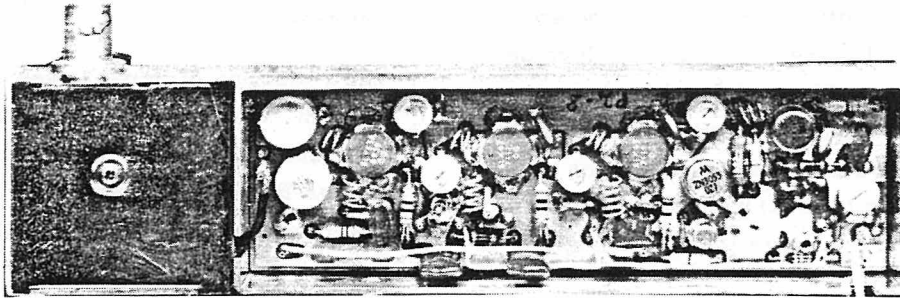
TYPE	NO.	CODE	DATA

POWER AMPLIFIER
EFFEKTFORSTÆRKER

PA732

X 401.957

RF POWER AMPLIFIER PA761

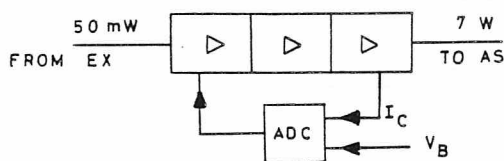


Description

General

PA761 contains 4 power amplifier stages and a current regulating circuit. It is built on a double-sided printed circuit board and includes transistors packaged in capstan-type housings. The unit is completely shielded, being built into a combination heat sink and shield which also contains the antenna switching unit.

The current regulating circuit monitors both the supply voltage and the output transistor collector current, preventing overloading of the transistors due to either too high a voltage or too great a standing wave ratio in the output load. This circuit also allows the output power to be more independent of the power supply or of variations in power output from the exciter.



RF Power Amplifier

The first driver, Q3, gets its collector voltage via the ADC circuit regulating transistor, Q2. Increasing or decreasing the collector voltage to Q3 regulates the drive power applied to the following stages.

π -network C3, L1 and C4 matches the exciter output impedance to the input impedance of Q3. Due to this impedance matching it is also possible to drive the PA stage from a 50 Ω generator. Q3 amplifies the exciter signal of about 50 mW to approx. 100 mW, which is necessary to drive Q4 properly.

Transistors Q4 and Q5 further amplify the power to approx. 2W in order to drive the final power amplifier, Q6.

Output transistor Q6 amplifies the RF power signal to approximately 7 W and the following matching network of L12, C21 and C22 suppresses harmonics of the fundamental VHF frequency while transforming the collector impedance of Q6 to the antenna impedance of 50 Ω . Resistor R12 in the output transistor collector path is the current monitoring resistor for the ADC circuit.

Current Regulating Circuit (ADC)

The purpose of the regulating circuit is to protect the transistors against overloads caused by too high a supply voltage and to limit current through the output transistor in case of mismatching. To accomplish this, the regulating circuit must monitor the supply voltage as well as the collector current through the transistor and from such results regulate the collector voltage to the first RF driver transistor, Q3, and thus the drive power to the following stages.

The circuit consists of two DC coupled transistor stages, Q1 and Q2. Base to Q1 is tied to a reference voltage that can be determined by setting the trimming potentiometer, R2. Reference voltage is developed across diodes E1 and E2, which are biased into forward conduction. This introduces a temperature dependency in the reference voltage that compensates for the temperature characteristics of the transistors.

For easier understanding of the circuit principle, first ignore its voltage dependent features; therefore, imagine that resistor R4 is removed from the circuit.

The DC return path for the emitter of Q1 is through R12 to the positive voltage terminal. R12 carries the collector current from the output amplifier, Q6. A rise in this collector current will mean an increase in the voltage drop across R12, causing the emitter of Q1 to become less positive and the collector voltage will likewise become less positive. This decreases bias to Q2, decreasing the current through this transistor. Since Q2 is in series with the DC collector path of Q3, the effect will be that of placing a larger resistor in series with the collector supply, thus reducing collector voltage to Q3. The RF drive to the output stage will fall, thereby counteracting the original increase in collector current.

If the supply voltage increases, the current through the output transistors will be kept constant as already explained, but the power dissipation in the transistor will increase along with the voltage. To counteract this effect, a voltage regulating loop is included.

Imagine R4 connected back into the circuit again so that a voltage divider consisting of R3 and R4 will develop a voltage across R3 in proportion to the supply voltage.

When the supply voltage increases so will the voltage drop across R3 and the base-

emitter bias for Q1 will fall, again resulting in a reduction of collector voltage to Q3 and a reduction in the drive to the output stage.

The reduction of drive power decreases the current through Q6 and R12 just enough to counteract the original increase of voltage across R3. By selecting a suitable ratio between resistors R3, R4 and R12 the desired amount of regulation can be achieved.

Technical Specification

Frequency Range

400 to 470 MHz

Supply Voltage

Nominal 13.6 V (12.5 V)

Operating range 10 - 16 V

Output Power at 13.6 V : 6.5 W

With output power set for
6 W at 16 V,
as measured through AS761 :

Output power at 16 V 6 W

Output power at 12.5 V 6 W

Output power at 10 V 4 W

Current Consumption

at nominal voltage 13.6 V : 1.2 A

at 16 V : 1.0 A

at 10 V : 1.1 A

Input Power

50 mW

Input Impedance

50 Ω

Output Impedance

50 Ω

Gain

22 dB

Temperature Range

Operating range : -25° to $+70^{\circ}$ C

Functioning range : -30° to $+80^{\circ}$ C

Mechanical Dimensions

25 x 42 x 168 mm

(PC board : 35.6 x 119.4 mm)

ANTENNA SWITCH AS761

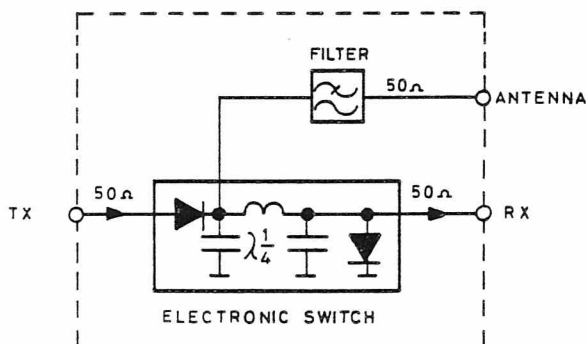
Description

General

The antenna switch AS761 contains a circuit for electronically switching the antenna between the transmitter and the receiver sections, and a low-pass filter that attenuates undesired frequencies, such as harmonics of the signal frequency, thus preventing their being radiated from the antenna.

AS761 mounts directly into the combination heat sink and shield for PA761.

The following simplified diagram shows the operating principle for the AS sub-unit.



The Electronic Switch

Refer to the complete schematic diagram.

By switching a +9 V potential between terminals 1 and 2, the antenna is electronically switched between transmit and receive.

When transmitting, diodes E51 and E52/E53 conduct and the receiver terminal will see a short circuit.

The 1/4 wave impedance circuit consisting of C54, L53 and C55 transforms the short to an open circuit at the antenna, thus the transmit signal reaches the antenna with minimum loss.

When receiving, the diodes are effectively blocked due to the bias across zener diode E54. Now the diodes only represent

a small capacity that includes itself in the 1/4 wave impedance circuit, as far as the receiver terminal is concerned.

The transmitter terminal, however, looks into a parallel resonant circuit made up of L52 and the capacity of E51, and is thereby isolated from the antenna.

The received signal is now free to pass from the antenna to the receiver input with minimum loss.

The Low-pass Filter

The low-pass filter is a 7-pole Chebishev filter exhibiting negligible band-pass ripple and minimum insertion loss.

The filter is built on a metal plate chassis having three closed compartments. It requires no alignment.

Technical Specifications

Frequency Range

420 - 470 MHz

Input and Output Impedance

50 Ω

Insertion Loss (transmitter to antenna)

0.5 dB

Insertion Loss (antenna to receiver)

0.6 dB

Separation between Transmitter and Receiver

25 dB

Second Harmonic (840 MHz) Attenuation

70 dB

Current Drain, transmit

38 mA

Current Drain, receive

4 mA

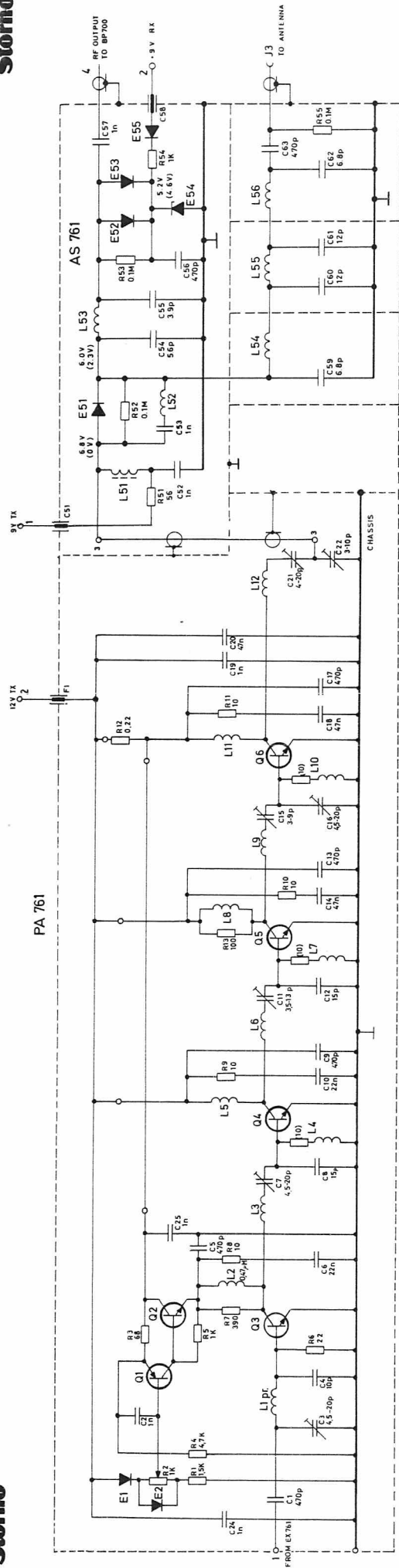
Temperature Range

operating range -25° to $+70^{\circ}$ C

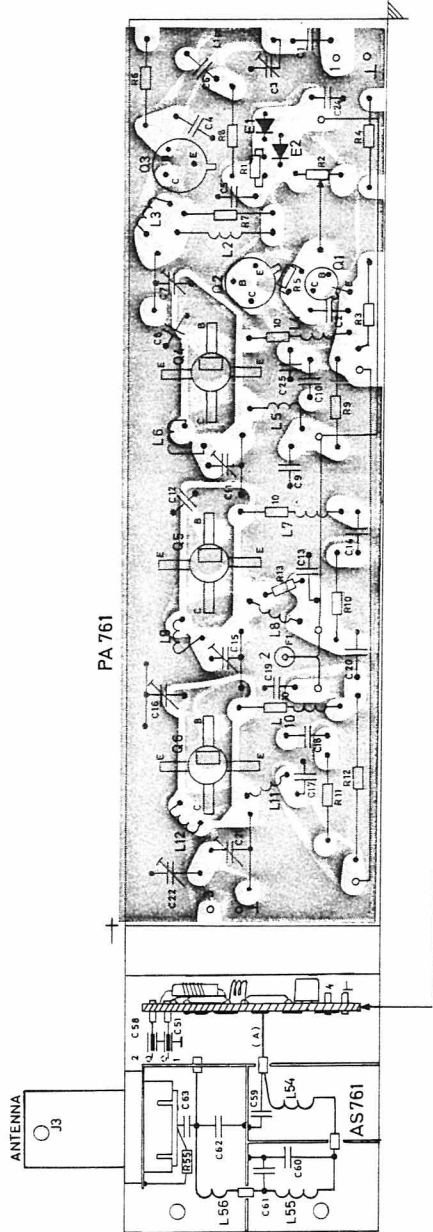
functioning range -30° to $+80^{\circ}$ C

Dimensions

40 x 38 x 22 mm



DC VOLTAGE WITHOUT () DURING TRANSMITTING
 DC VOLTAGE WITH () DURING RECEIVING



POWER AMPLIFIER PA761

D.401.324/5

TYPE	NO.	CODE	DATA
PA761		10. 2428	Power Amplifier (incl. AS761)
	C1	74. 5161	470pF-20/+80% ceram PL
	C2	74. 5155	1nF-20/+80% ceram PL
	C3	78. 5026	4, 5-20pF trimmer
	C4	74. 5006	10pF 5% ceram DI
	C5	74. 5161	470pF-20-80% ceram PL
	C6	76. 5071	22nF 10% polyest. FL
	C7	78. 5026	4, 5-20pF trimmer
	C8	74. 5046	15pF 5% ceram DI
	C9	74. 5161	470pF-20/+80% ceram PL
	C10	76. 5071	22nF 10% polyest. FL
	C11	78. 5025	3, 5-13pF trimmer
	C12	74. 5046	15pF 5% ceram DI
	C13	74. 5161	470pF-20/+80% ceram PL
	C14	76. 5072	47nF 10% polyest. FL
	C15	78. 5050	3-9pF trimmer
	C16	78. 5026	4, 5-20pF trimmer
	C17	74. 5161	470pF-20/+80% ceram PL
	C18	76. 5072	47nF 10% polyest. FL
	C19	74. 5155	1nF-20/+80% ceram PL
	C20	76. 5072	47nF 10% polyest. FL
	C21	78. 5031	4-20pF trimmer
	C22	78. 5051	3-10pF trimmer
	C23		
	C24	74. 5155	1nF-20/+80% ceram PL
	C25	74. 5155	1nF-20/+80% ceram PL
	R1	80. 5251	1, 5k Ω 5% carbon film
	R2	86. 5058	1 k Ω 20% trim. pot.
	R3	80. 5235	68 Ω 5% carbon film
	R4	80. 5257	4, 7k Ω 5% carbon film
	R5	80. 5270	56k Ω 5% carbon film
	R6	80. 5229	22 Ω 5% carbon film
	R7	80. 5244	390 Ω 5% carbon film
	R8	80. 5225	10 Ω 5% carbon film
	R9	80. 5225	10 Ω 5% carbon film
	R10	80. 5225	10 Ω 5% carbon film
	R11	80. 5225	10 Ω 5% carbon film
	R12	82. 5205	0, 22 Ω 10% wire wound
	R13	80. 5237	100 Ω 5% carbon film
	L1		Printed coil
	L2	63. 5008	0, 47 μ H 20% RF choke 2, 2A
	L3	62. 0794	RF coil 420-470 MHz
	L4	62. 0795	RF coil 420-470MHz (10 Ω 1/8W)
	L5	62. 0796	RF coil 420-470MHz
	L6	62. 0797	RF coil 420-470MHz

TYPE	NO.	CODE	DATA
	L7	62. 0795	RF coil 420-470MHz (10 Ω 1/8W)
	L8	62. 0798	RF coil 420-470MHz
	L9	62. 0797	RF coil 420-470MHz
	L10	62. 0795	RF coil 420-470MHz (10 Ω 1/8W)
	L11	62. 0799	RF coil 420-470MHz
	L12	62. 0797	RF coil 420-470 MHz
	F1	69. 5023	Feed-through filter
	E1	99. 5028	1N914 Diode
	E2	99. 5028	1N914 Diode
	Q1	99. 5230	BC178 Transistor
	Q2	99. 5128	2N3053 Transistor
	Q3	99. 5229	2N4427 Transistor
	Q4	99. 5242	BLX67 Transistor
	Q5	99. 5242	BLX67 Transistor
	Q6	99. 5243	BLX68 Transistor
AS761		10. 2427	Antenna Switching Unit
	C51	69. 5007	VHF Filter FT
	C52	74. 5155	1 nF -20 +80% ceram PL
	C53	74. 5155	1 nF -20 +80% ceram PL
	C54	74. 5004	5. 6 pF \pm 0. 25 pF ceram DI
	C55	74. 5130	3. 9 pF \pm 0. 25 pF ceram DI
	C56	74. 5162	470 pF -20 +50% ceram DI
	C57	74. 5155	1 nF -20 +80% ceram PL
	C58	69. 5007	VHF Filter FT
	C59	74. 5021	6. 8 pF \pm 0. 25 pF ceram DI
	C60	74. 5194	12 pF 5% ceram DI
	C61	74. 5194	12 pF 5% ceram DI
	C62	74. 5021	6. 8 pF \pm 0. 25 pF ceram DI
	C63	74. 5094	470 pF 20% ceram DI
	R51	80. 5234	56 Ω 5% carbon film
	R52	80. 5273	0. 1 M Ω 5% " "
	R53	80. 5273	0. 1 M Ω 5% " "
	R54	80. 5049	1 k Ω 5% " "
	R55	80. 5073	0. 1 M Ω 5% " "

POWER AMPLIFIER EFFEKTFORSTÆRKER

PA761

X401. 619

Storno

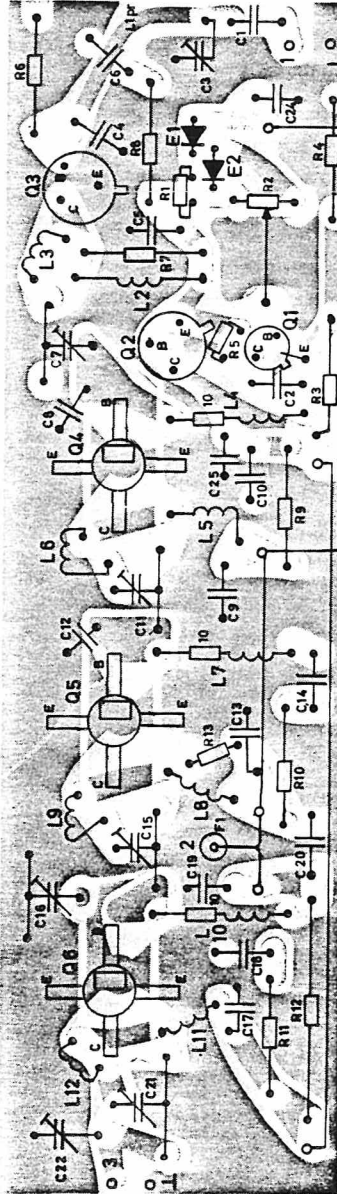
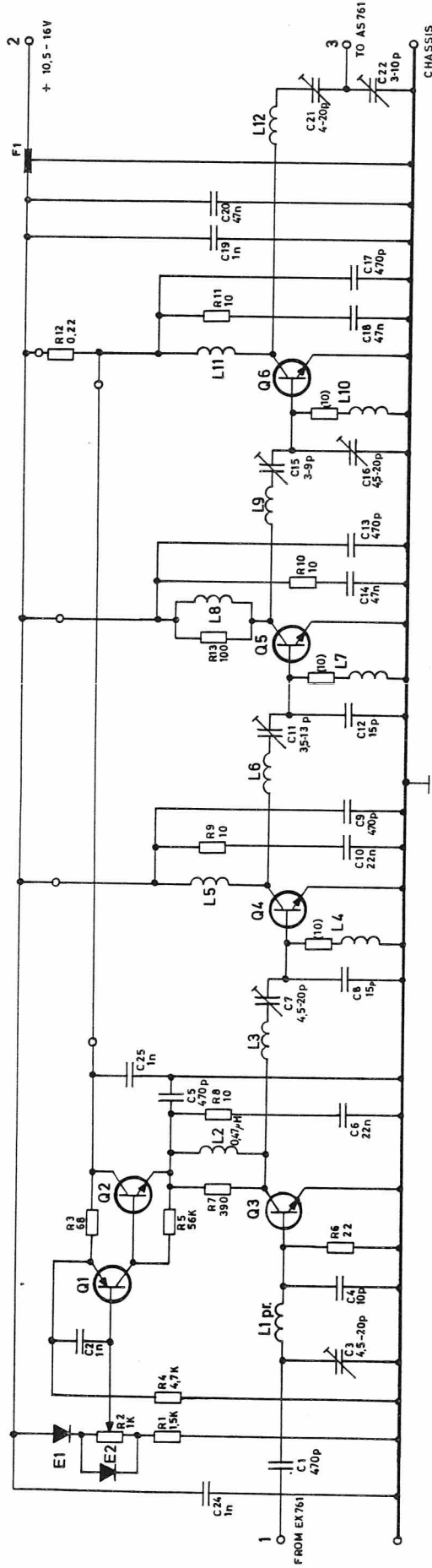
TYPE	NO.	CODE	DATA
	L51	63.5008	0.47 μ H 20% RF choke
	L52	62.0809	RF coil
	L53	62.0810	RF coil
	L54	62.0811	RF coil
	L55	62.0811	RF coil
	L56	62.0811	RF coil
	E51	99.5244	BA182 Diode
	E52	99.5244	BA182 Diode
	E53	99.5244	BA182 Diode
	E54	99.5224	Zenerdiode 4.7V 5%
	E55	99.5237	1N4148 Diode
			2.2A

Storno

TYPE	NO.	CODE	DATA
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POWER AMPLIFIER PA761
EFFEKTFORSTÆRKER

X401.619

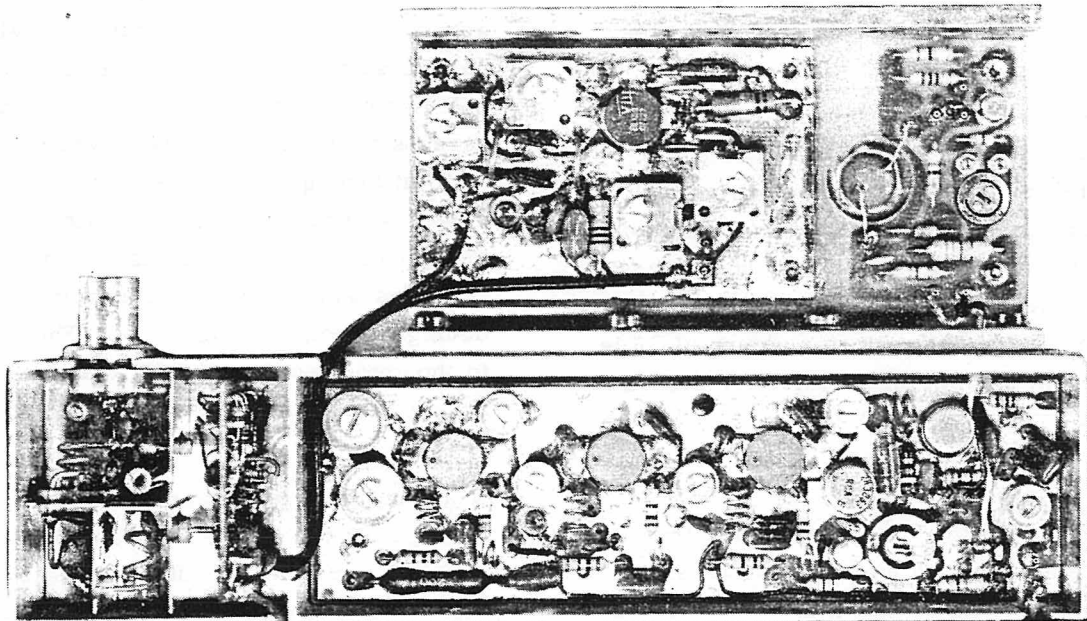


PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
 TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

POWER AMPLIFIER PA761

D401.324/3

RF POWER AMPLIFIER PA762



Description

The PA762 RF power amplifier is designed to operate with supply voltages between 10 and 16 volts. At nominal supply voltages it will amplify the driving power at its input (50 mW) to an output level of 15 W into the antenna load.

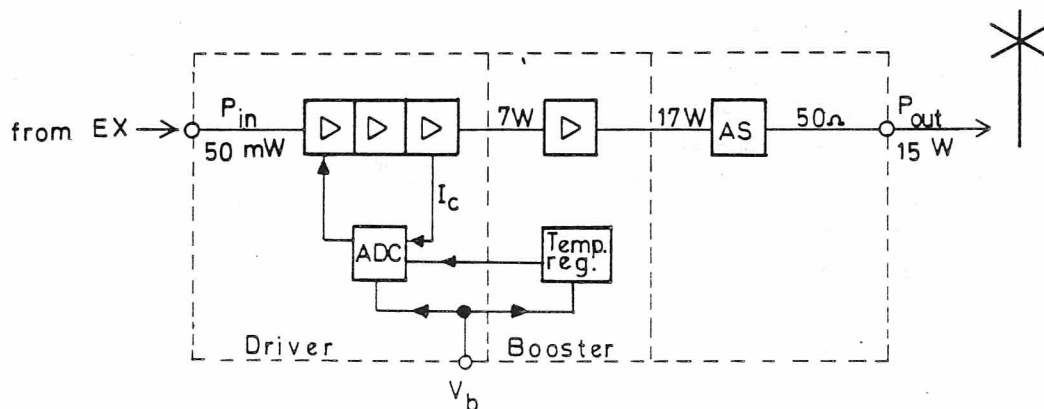
The unit comprises 5 RF power amplifier stages, four in the driver and one in the booster as well as a regulating and temperature protection circuit and, finally, an electronic antenna switching unit with filter, AS762.

PA762 is completely shielded, as it is built into a combination heat sink and shield. However, heat dissipation will be insufficient without the external heat sink / cabinet CA703.

The regulating and temperature protection circuit protects the transistors and other components in the unit against incurring damages when operated within the permissible values of supply voltages and temperatures, or as a result of prolonged short circuits or too great a standing wave ratio in the output load.

RF Power Amplifier

The first driver, Q3, gets its collector voltage via the ADC circuit regulating transistor, Q2. Increasing or decreasing the collector voltage to Q3 regulates in the drive power applied to the following stages.



Π -network C3, L1, and C4 match the exciter output impedance to the input impedance of Q3. Due to this impedance matching it is also possible to drive the PA stage from a 50 Ω generator.

Q3, Q4, Q5 and Q6 amplify the exciter output signal of 80 mW to 7 W in order to drive the booster stage. Matching network L12, C21 and C22 suppresses harmonics of the fundamental VHF frequency while transforming the collector impedance of Q6 to 50 Ω . Resistor R12 in the collector return of Q6 is the current monitoring resistor for the ADC circuit.

Booster Stage

Q101 amplifies the 7 W output power from the driver stage to 17 W and applies the signal to AS762. Due to the inherent losses in the AS unit the PA output power is then 15 W.

Current Regulating Circuit (ADC)

The purpose of the regulating circuit is to protect the transistors against overloads caused by excessive supply voltage and to limit current through the output transistor in case of mismatching. To accomplish this, the regulating circuit must monitor the supply voltage as well as the collector current through Q6 in the driver stage, and from such results regulate the collector voltage to the first driver transistor, Q3, and thus the drive power to the following stages.

The circuit consists of two DC coupled transistor stages Q1 and Q2. Base to Q1 is tied to a reference voltage that can be determined by setting potentiometer R2. Reference voltage is developed across diodes E1 and E2, which are biased into forward conduction. This introduces a temperature dependency in the reference voltage that compensates for the temperature characteristics of the transistors.

For easier understanding of the circuit principle, first ignore its voltage dependent features; therefore, imagine that resistor R4 is removed from the circuit.

The DC return path for the emitter of Q1 is through R12 to the positive voltage terminal.

R12 also carries the collector current from transistor Q6. A rise in this collector current will mean an increase in the voltage drop across R12, causing the emitter of Q1 to become less positive and the collector voltage will likewise become less positive. This decreases forward bias to Q2, decreasing the current through this transistor. Since Q2 is in series with the DC collector path of Q3, the effect will be that of placing a larger resistor in series with the collector supply, thus reducing collector voltage to Q3. The RF drive to the output stage will fall, thereby counteracting the original increase in collector current.

If the supply voltage increases, the current through Q6 will be kept constant as already explained, but the power dissipation in the transistor will increase along with the voltage. To counteract this effect, a voltage regulating loop is included.

Imagine R4 connected back into the circuit again so that a voltage divider consisting of R3 and R4 will develop a voltage across R3 in proportion to the supply voltage.

When the supply voltage increases so will the voltage drop across R3 and the base-emitter bias for Q1 will fall, again resulting in a reduction of collector voltage to Q3 and a reduction in the drive to the output stage.

The reduction of drive power decreases the current through Q6 and E12 just enough to counteract the original increase of voltage across R3. By selecting a suitable ratio between resistors R3, R4 and R12 the desired amount of regulation can be achieved.

The transmitter power can be set to the desired level by means of potentiometer R2 in the ADC circuit.

Temperature Protection Circuit

Since transistor Q101 in the booster stage is not directly included in the ADC loop, it requires extra thermal protection which is accomplished by means of a PTC resistor, R109, which is mounted close to Q101. When Q101, and R109 along with it, reach a certain temper-

ature the increasing resistance of R109, which is also a part of the ADC loop of the driver stage, regulates (reduces) the drive to Q101. Thus the output power of the PA unit is regulated to a preset level that ensures thermal protection of Q101 and other components.

The temperature protection circuit operates in the following manner: Under normal operating conditions (prior to regulation) Q102 is biased to cut-off by the voltage divider network of R104 and the PTC resistor ($60\ \Omega$) connected across zener diode E101 for a stable source. As the temperature in the PA stage rises the resistance of R109 increases and Q101 begins to pass current. When R109 reaches $1.2\ \text{k}\Omega$, Q102 will be completely open. When Q102 opens up, the circuit shunts diodes E1 and E2 and the voltage across these diodes falls causing the base-emitter voltage for Q1 to fall, as well.

As a result, Q3's collector voltage falls, too, thereby also reducing the drive to the following stages.

The amount of regulation (reduction in output power) is preset by potentiometer R107. Q102's emitter resistor is included to flatten out the regulation characteristic. Diode E102 in the collector lead of Q102 ensures temperature compensation of the reference voltage at the base of Q1 even at maximum regulation.

Technical Specifications

Frequency Range

420 to 470 MHz

Nominal Supply Voltage

13 V

Output Power at 13 V

17 W

Output power as measured through AS762:

at 15.5 V: 18 W

at 10 V: 10 W

Current Drain

3.4 A

at 15.5 V: 3.2 A

at 10 V: 2.5 A

Input Power

80 mW

Minimum: 50 mW

Generator Impedance

$50\ \Omega$

Gain with $P_{IN} = 50\ \text{mW}$: 25 dB

Reduction of Output Power vs. Ambient

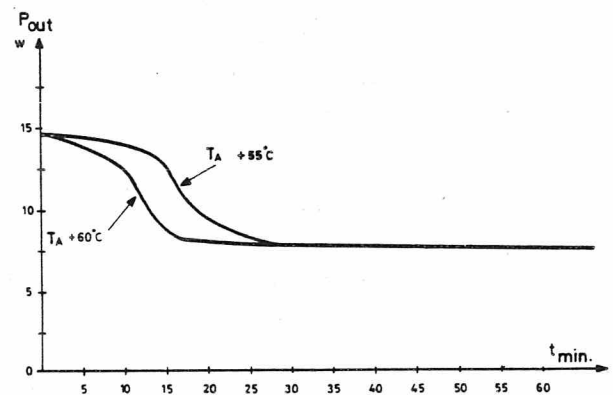
Temperature

Continuous, $T_A -25^\circ$ to $+25^\circ\text{C}$: 0.8 dB

Intermittent, $T_A -25^\circ$ to $+55^\circ\text{C}$: 0.8 dB

Continuous, $T_A +55^\circ\text{C}$: 3 dB

(refer to response curve below)



Typical output power regulating characteristics of PA762 with CA703 mounted. Plotted for ambient temperatures of $+55^\circ\text{C}$ and $+60^\circ\text{C}$, at nominal voltage, continuous keying of transmitter.

Temperature Range

operating range -25° to $+55^\circ\text{C}$

functioning range -30° to $+60^\circ\text{C}$

Mechanical Dimensions

168 x 97 x 32 mm

ANTENNA SWITCH AS762

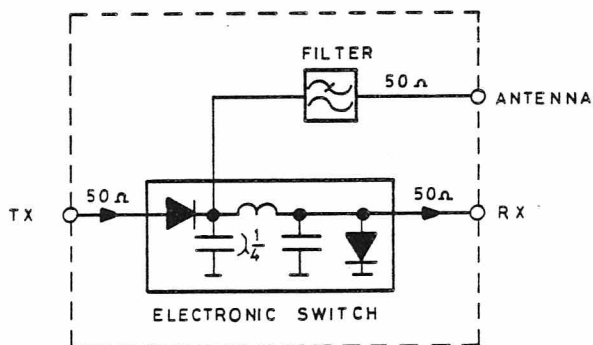
Description

General

The antenna switch AS762 contains a circuit for electronically switching the antenna between the transmitter and the receiver sections, and a low-pass filter that attenuates undesired frequencies, such as harmonics of the signal frequency thus preventing their being radiated from the antenna.

AS762 mounts directly into the combination heat sink and shield for PA761 for use in 450 MHz simplex equipment having 15 W output power.

The following simplified diagram shows the operating principle for the AS sub-unit.



The Electronic Switch

Refer to the complete schematic diagram.

By switching a +9 V potential between terminals 1 and 2, the antenna is electronically switched between transmit and receive.

When transmitting, diodes E51, E52 + E53 and E54, E55 and E56 conduct and the receiver terminal will see a short circuit.

The 1/4 wave impedance circuit consisting of C54, L53 and C55 transforms the short to an open circuit at the antenna, thus the transmit signal reaches the antenna with minimum loss.

When receiving, the diodes are effectively blocked due to the bias across zener diode E57. Now the diodes only represent

a small capacity that includes itself in the 1/4 wave impedance circuit, as far as the receiver terminal is concerned.

The transmitter terminal, however, looks into a parallel resonant circuit made up of L52 and the capacities of E51, E52 and E53, and is thereby isolated from the antenna.

The received signal is now free to pass from the antenna to the receiver input with minimum loss.

The Low-pass Filter

The low-pass filter is a 7-pole Chebisev filter exhibiting negligible band-pass ripple and minimum insertion loss.

The filter is built on a metal plate chassis having three closed compartments. It requires no alignment.

Technical Specifications

Frequency Range

420 - 470 MHz

Input and Output Impedance

50 Ω

Insertion Loss (transmitter to antenna)

0.5 dB

Insertion Loss (antenna to receiver)

0.6 dB

Separation between Transmitter and Receiver

25 dB

Second Harmonic (840 MHz) Attenuation

70 dB

Current Drain, transmit

46 mA

Current Drain, receive

8 mA

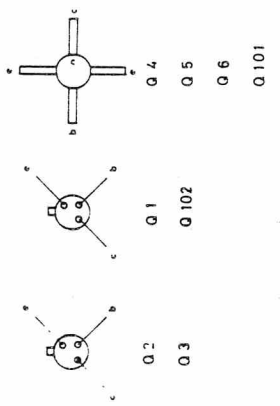
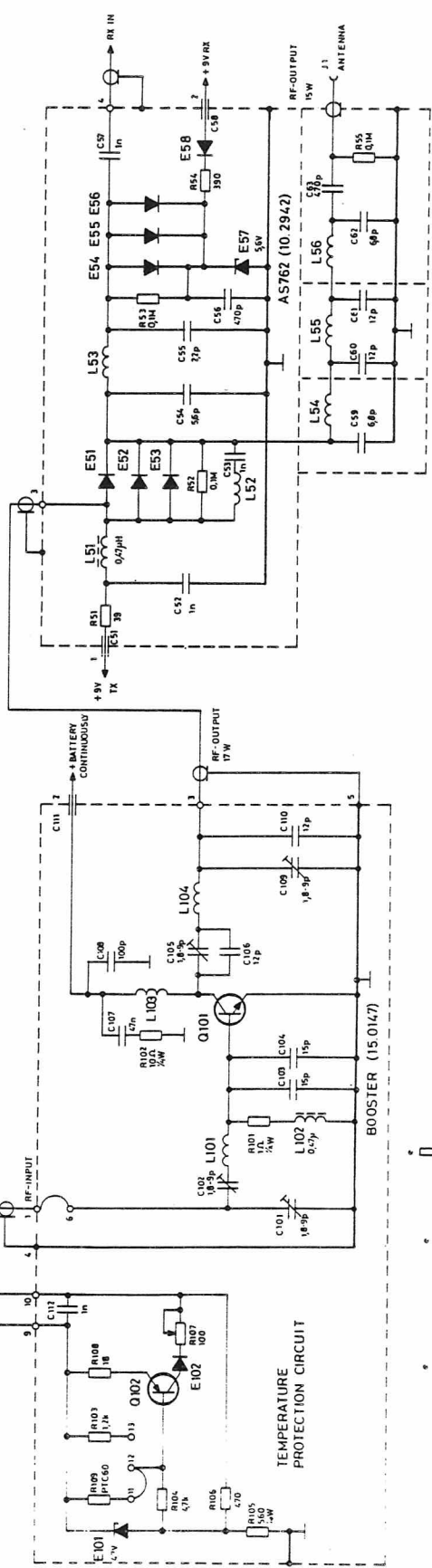
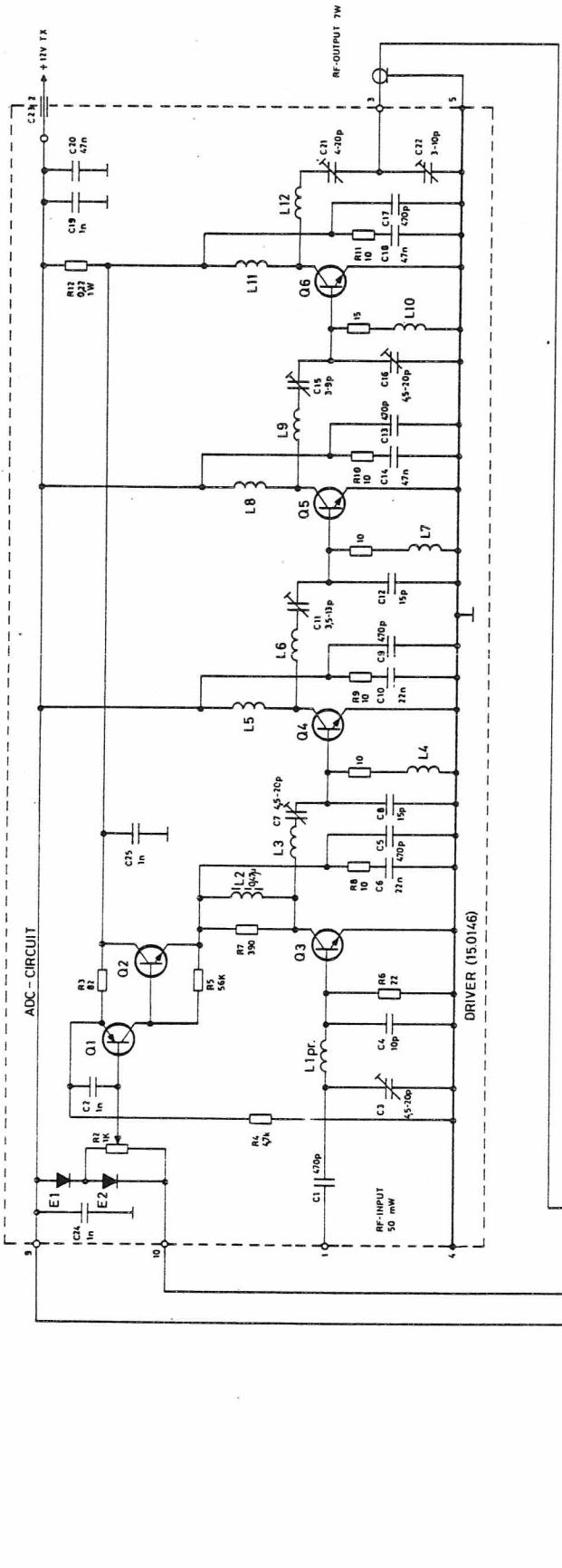
Temperature Range

operating range -25^o to +70^oC

functioning range -30^o to +80^oC

Dimensions

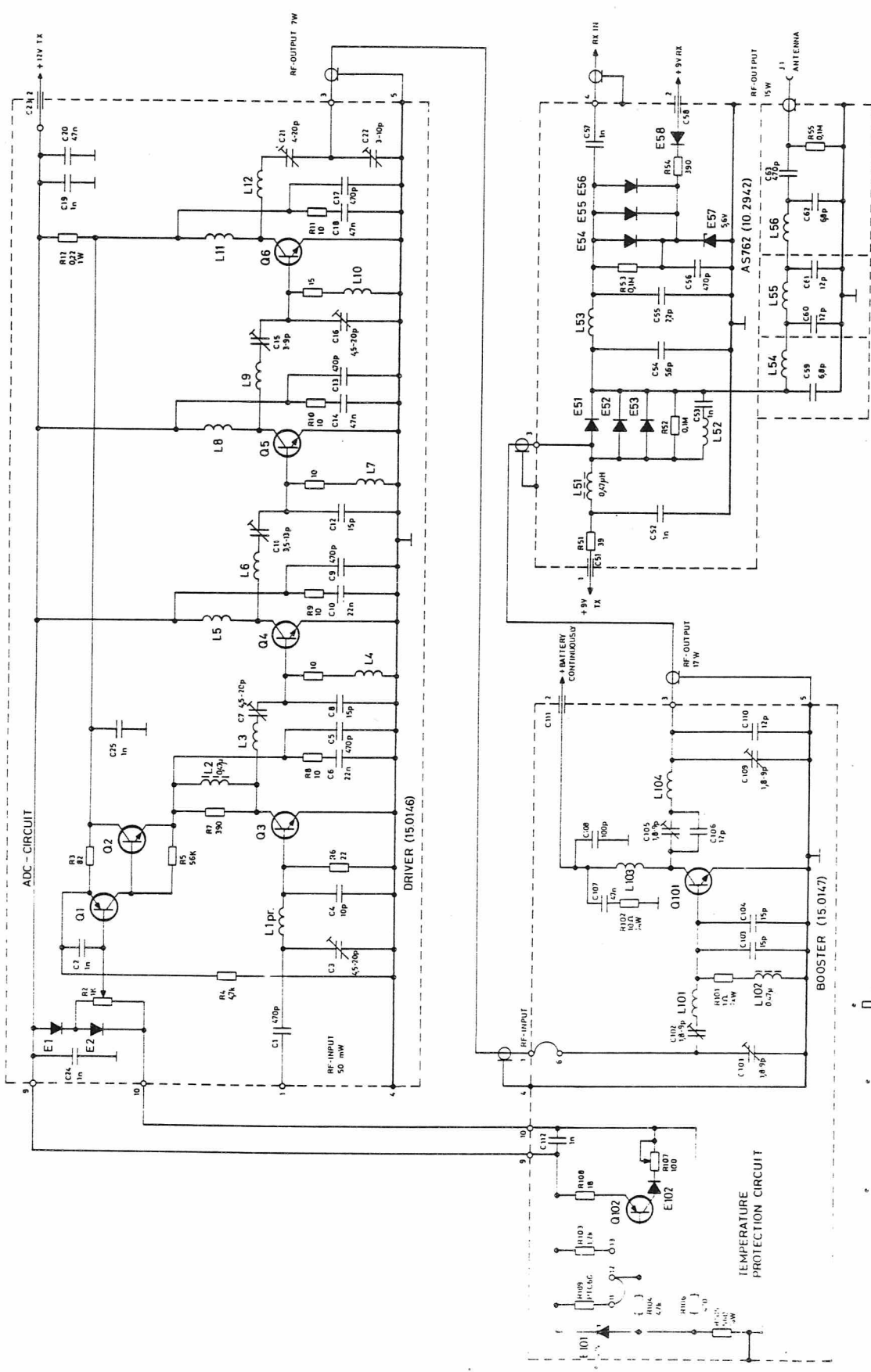
40 x 38 x 22 mm



PA762 (10.2941)

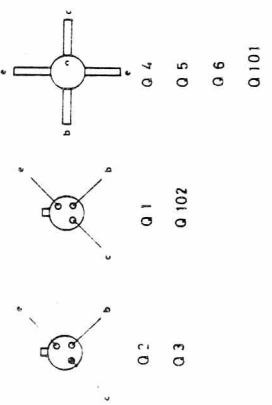
POWER AMPLIFIER
EFFEKTFORSTÆRKER

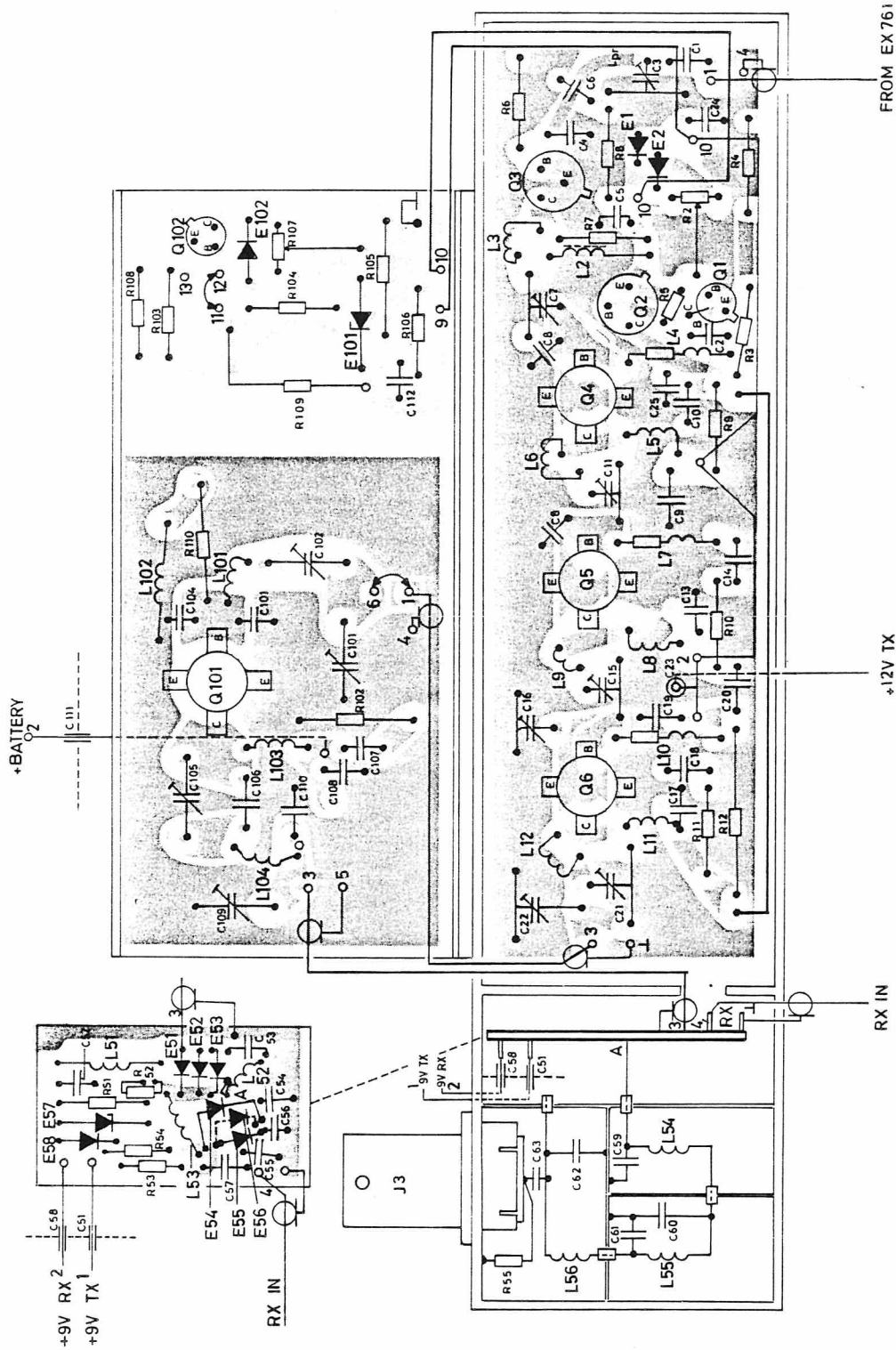
PA762
D401790



PA752 (102941)

POWER AMPLIFIER
EFFEKTFORSTÆRKER





POWER AMPLIFIER
EFFEKT FORSTÆRKER

PA762

D401979

TYPE	NO.	CODE	DATA
PA762		10.2941	Power Amplifier
	C1	74.5161	DRIVER
	C2	74.5155	470 pF -20+80% ceram PL
	C3	78.5026	1 nF -20+80% ceram PL
	C4	74.5006	4.5 - 20 pF trimmer
	C5	74.5161	10 pF 5% ceram DI
	C6	76.5071	470 pF -20+80% ceram PL
	C7	78.5026	22 nF 10% polyest FL
	C8	74.5046	4.5 - 20 pF trimmer
	C9	74.5161	15 pF 5% ceram DI
	C10	76.5071	470 pF -20+80% ceram PL
	C11	78.5025	22 nF 10% polyest. FL
	C12	74.5046	3.5-13 pF trimmer
	C13	74.5161	15 pF 5% ceram DI
	C14	76.5072	470 pF -20+80% ceram PL
	C15	78.5050	47 nF 10% polyest. FL
	C16	78.5026	3-9 pF trimmer
	C17	74.5161	4.5-20 pF trimmer
	C18	76.5072	470 pF -20+80 ceram PL
	C19	74.5155	47 nF 10% polyest. FL
	C20	76.5072	1 nF -20+80% ceram PL
	C21	78.5031	47 nF 10% polyest FL
	C22	78.5051	4-20 pF trimmerø
	C23	69.5023	3-10 pF trimmer
	C24	74.5155	Feed-trhough filter
	C25	74.5155	1 nF -20+80% ceram PL
	R2	86.5058	1 KΩ 20% potentiometer
	R3	80.5236	82 Ω 5% carbon filter
	R4	80.5257	4.7 KΩ 5%
	R5	80.5270	56 KΩ 5%
	R6	80.5229	22 Ω 5%
	R7	80.5244	390Ω 5%
	R8	80.5225	10Ω 5%
	R9	80.5225	10Ω 5%
	R10	80.5225	10Ω 5%
	R11	80.5225	10Ω 5%
	R12	82.5205	0.22Ω 10% wire wound
	L2	63.5008	0.47 μH 20% RF choke
	L3	62.0794	RF coil 420-470 MHz
	L4	62.0795	RF coil 420-470 MHz
	L5	62.0796	(made with 10Ω resistor 80.5225)
	L6	62.0797	RF coil 420-470 MHz
	L7	62.0795	RF coil 420-470 MHz
			(made with 10Ω resistor 80.5225)

TYPE	NO.	CODE	DATA
	L8	62.0798	RF coil 420-470 MHz
	L9	62.0797	RF coil 420-470 MHz
	L10	62.0880	RF coil 420-470 MHz
	L11	62.0799	(made with 15Ω resistor 80.5227)
	L12	62.0797	RF coil 420-470 MHz
	E1	99.5028	Diode 1N914
	E2	99.5028	Diode 1 N914
	Q1	99.5230	Transistor BC178
	Q2	99.5128	Transistor 2N3053
	Q3	99.5229	Transistor 2N4427
	Q4	99.5242	Transistor BLX67
	Q5	99.5242	Transistor BLX67
	Q6	99.5243	Transistor BLX68
			BOOSTER
	C101	78.5056	1.8-9 pF trimmer
	C102	78.5056	1.8-9 pF trimmer
	C103	74.5317	15 pF 10 % ceram
	C104	74.5317	15 pF 10% ceram
	C105	78.5056	1.8-9 pF trimmer
	C106	74.5194	12 pF 5% ceram DI
	C107	76.5072	47 nF 10% polyest. FL
	C108	74.5013	100 pF 20% ceram DI
	C109	78.5056	1.8-9 pF trimmer
	C110	74.5194	12 pF 5% ceram DI
	C111	69.5023	Feed-through filter
	C112	74.5155	1 nF -20+80% ceram PL
	R101	89.5031	1 Ω 10% oxide
	R102	80.5425	10Ω 5% carbon film
	R103	80.5250	1.2 KΩ 5% carbon film
	R104	80.5257	4.7 KΩ 5% carbon film
	R105	80.5446	560 Ω 5%
	R106	80.5245	470 Ω 5%
	R107	86.5051	100Ω 20% potentiometer
	R108	80.5228	18 Ω 5% carbon film
	R109	89.5066	Thermistor PTC, 60Ω -50+100%
	L101	62.0879	RF coil 420-470 MHz
	L102	63.5008	0.47 μH ± 20% RF choke
			400 V
			400 V
			400 V
			50 V
			500 V
			400 V
			63 V
			1/2W
			1/4 W
			1/8 W
			1/8 W
			1/4 W
			1/8 W
			0.1 W
			1/8 W
			2.2 A

**POWER AMPLIFIER
EFFEKTFORSTÆRKER**

PA762

X401.862

TYPE	NO.	CODE	DATA
	L103 L104	62.0840 62.0840	RF coil 420-470 MHz RF coil 420-470 MHz
	E101 E102	99.5224 99.5237	Zener Diode 4,7 V 5% Diode 1N4148
	Q101 Q102	99.5284 99.5230	Transistor BLX69 Transistor BC178

1/4W

TYPE	NO.	CODE	DATA
AS762		10.2942	Antenna Switch
	C51	69.5007	VHF feed-through filter
	C52	74.5155	1nF -20/+80% ceram PL 63V
	C53	74.5155	1nF -20/+80% ceram PL 63V
	C54	74.5004	5.6pF ± 0.25pF ceram DI 400V
	C55	74.5315	2.2pF ± 0.25pF ceram DI 400V
	C56	74.5162	470pF -20/+50% ceram DI 400V
	C57	74.5155	1nF -20/+80% ceram PL 63V
	C58	69.5007	VHF feed-through filter
	C59	74.5021	6.8pF ± 0.25pF ceram DI 400V
	C60	74.5194	12pF 5% ceram DI 400V
	C61	74.5194	12pF 5% ceram DI 400V
	C62	74.5021	6.8pF ± 0.25pF ceram DI 400V
	C63	74.5094	470pF 20% ceram DI 400V
	R51	80.5232	39 Ω 5% carbon film 1/8W
	R52	80.5073	100kΩ 5% carbon film 1/10W
	R53	80.5073	100kΩ 5% carbon film 1/10W
	R54	80.5044	390Ω 5% carbon film 1/10W
	R55	80.5273	100kΩ 5% carbon film 1/8W
	L51	63.5008	RF choke 0.47μH ± 20% 2.2A
	L52	62.0871	RF coil
	L53	62.0810	RF coil
	L54	62.0811	RF coil
	L55	62.0811	RF coil
	L56	62.0811	RF coil
	E51	99.5187	Diode BA244
	E52	99.5187	Diode BA244
	E53	99.5187	Diode BA244
	E54	99.5187	Diode BA244
	E55	99.5187	Diode BA244
	E56	99.5187	Diode BA244
	E57	99.5282	Zener Diode 5.6V 5%
	E58	99.5237	Diode 1N4148 1W

**POWER AMPLIFIER
EFFEKTFORSTÆRKER**

PA762

X401.862

TYPE	NO.	CODE	DATA
PA762		10.2941	Power Amplifier DRIVER
	C1	74.5161	470 pF -20+80% ceram PL
	C2	74.5155	1 nF -20+80% ceram PL
	C3	78.5026	4.5 - 20 pF trimmer
	C4	74.5006	10 pF 5% ceram DI
	C5	74.5161	470 pF -20+80% ceram PL
	C6	76.5071	22 nF 10% polyester FL
	C7	78.5026	4.5 - 20 pF trimmer
	C8	74.5046	15 pF 5% ceram DI
	C9	74.5161	470 pF -20+80% ceram PL
	C10	76.5071	22 nF 10% polyester FL
	C11	78.5025	3.5-13 pF trimmer
	C12	74.5046	15 pF 5% ceram DI
	C13	74.5161	470 pF -20+80% ceram PL
	C14	76.5072	47 nF 10% polyester FL
	C15	78.5050	3-9 pF trimmer
	C16	78.5026	4.5-20 pF trimmer
	C17	74.5161	470 pF -20+80 ceram PL
	C18	76.5072	47 nF 10% polyester FL
	C19	74.5155	1 nF -20+80% ceram PL
	C20	76.5072	47 nF 10% polyester FL
	C21	78.5031	4-20 pF trimmer
	C22	78.5051	3-10 pF trimmer
	C23	69.5023	Feed-trhrough filter
	C24	74.5155	1 nF -20+80% ceram PL
	C25	74.5155	1 nF -20+ 80% ceram PL
	R2	86.5058	1 K Ω 20% potentiometer
	R3	80.5236	82 Ω 5% carbon filter
	R4	80.5257	4.7 K Ω 5%
	R5	80.5270	56 K Ω 5%
	R6	80.5229	22 Ω 5%
	R7	80.5244	390 Ω 5%
	R8	80.5225	10 Ω 5%
	R9	80.5225	10 Ω 5%
	R10	80.5225	10 Ω 5%
	R11	80.5225	10 Ω 5%
	R12	82.5205	0.22 Ω 10% wire wound
	L2	63.5008	0.47 μ H 20% RF choke
	L3	62.0794	RF coil 420-470 MHz
	L4	62.0795	RF coil 420-470 MHz
	L5	62.0796	(made with 10 Ω resistor 80.5225)
	L6	62.0797	RF coil 420-470 MHz
	L7	62.0795	RF coil 420-470 MHz
			(made with 10 Ω resistor 80.5225)

TYPE	NO.	CODE	DATA
	L8	62.0798	RF coil 420-470 MHz
	L9	62.0797	RF coil 420-470 MHz
	L10	62.0880	RF coil 420-470 MHz
	L11	62.0799	(made with 15 Ω resistor 80.5227)
	L12	62.0797	RF coil 420-470 MHz
	E1	99.5028	Diode 1N914
	E2	99.5028	Diode 1 N914
	Q1	99.5230	Transistor BC178
	Q2	99.5128	Transistor 2N3053
	Q3	99.5229	Transistor 2N4427
	Q4	99.5242	Transistor BLX67
	Q5	99.5242	Transistor BLX67
	Q6	99.5243	Transistor BLX68
			BOOSTER
	C101	78.5056	1.8-9 pF trimmer
	C102	78.5050	1.8-9 pF trimmer
	C103	74.5317	15 pF 10% ceram
	C104	74.5317	15 pF 10% ceram
	C105	78.5056	1.8-9 pF trimmer
	C106	74.5194	12 pF 5% ceram DI
	C107	76.5072	47 nF 10% polyester FL
	C108	74.5013	100 pF 20% ceram DI
	C109	78.5056	1.8-9 pF trimmer
	C110	74.5194	12 pF 5% ceram DI
	C111	69.5023	Feed-through filter
	C112	74.5155	1 nF -20+80% ceram PL
	R101	89.5031	1 Ω 10% oxide
	R102	80.5425	10 Ω 5% carbon film
	R103	80.5259	1.2 K Ω 5% carbon film
	R104	80.5257	4.7 K Ω 5% carbon film
	R105	80.5446	560 Ω 5%
	R106	80.5245	470 Ω 5%
	R107	86.5051	100 Ω 20% potentiometer
	R108	80.5228	18 Ω 5% carbon film
	R109	89.5066	Thermistor PTC, 60 Ω -50+100%
	L101	62.0879	RF coil 420-470 MHz
	L102	63.5008	0.47 μ H \pm 20% RF choke

**POWER AMPLIFIER
EFFEKTFORSTÆRKER**

PA762

X401.862

Storno

TYPE	NO.	CODE	DATA
	L103	62.0840	RF coil 420-470 MHz
	L104	62.0840	RF coil 420-470 MHz
	E101	99.5224	Zener Diode 4.7 V 5%
	E102	99.5237	Diode 1N4148
	Q101	99.5284	Transistor BLX69
	Q102	99.5230	Transistor BC178

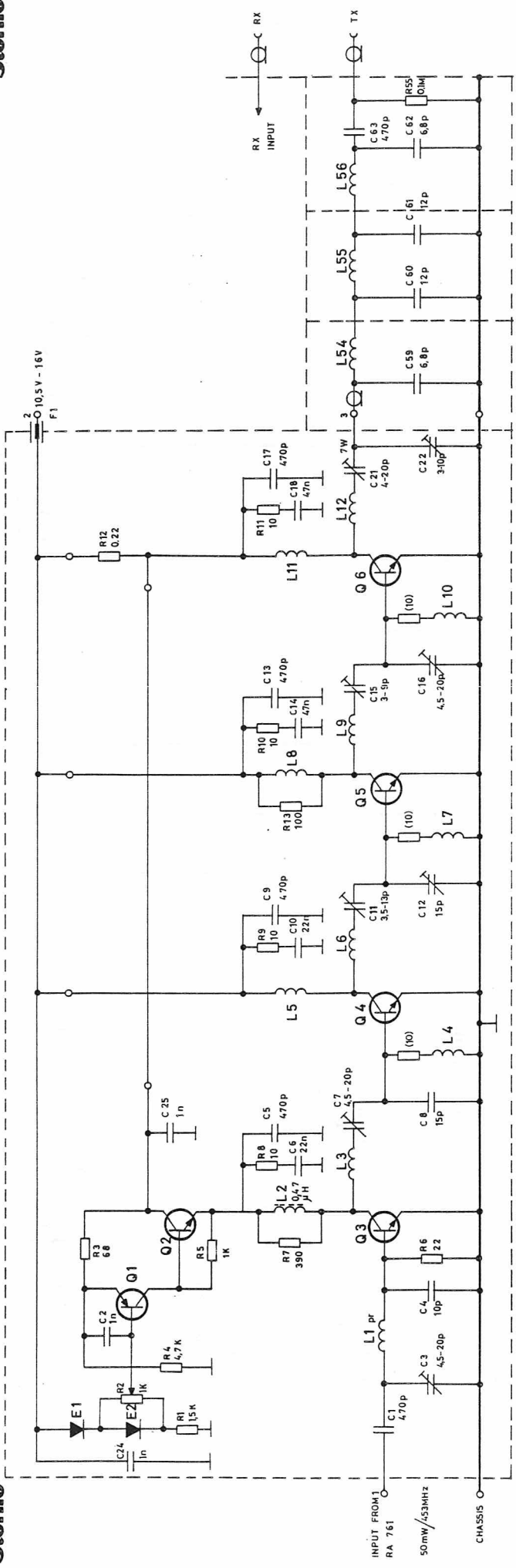
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TYPE	NO.	CODE	DATA
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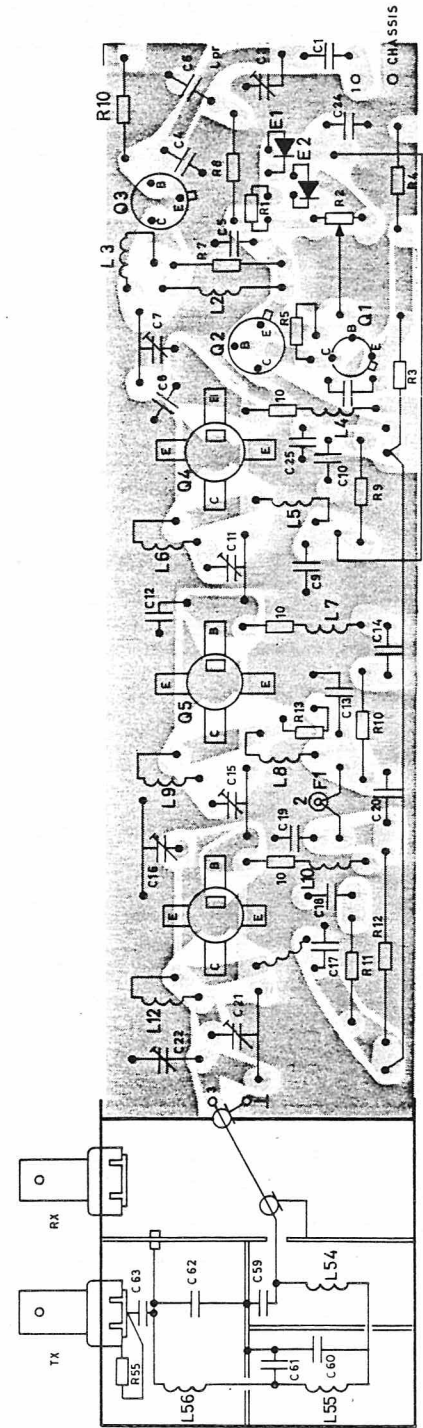
**POWER AMPLIFIER
EFFEKTFORSTÆRKER**

PA762

X401.862



COMPONENT SIDE VIEW
SET FRA KOMPONENTSIDE



POWER AMPLIFIER
EFFEKTFORSTÆRKER

PA763

D401.872

TYPE	NO.	CODE	DATA
PA763		10. 2926	Power Amplifier
	C1	74. 5161	470 pF -20 +80% ceram PL
	C2	74. 5155	1 nF -20+80% ceram PL
	C3	78. 5026	4.5-20 pF trimmer
	C4	74. 5006	10 pF 5% ceram DI
	C5	74. 5161	470 pF -20+80% ceram PL
	C6	76. 5071	22 nF 10% polyest FL
	C7	78. 5026	4.5-20 pF trimmer
	C8	74. 5046	15 pF 5% ceram DI
	C9	74. 5161	470 pF -20+80% ceram PL
	C10	76. 5071	22 nF 10% polyest FL
	C11	78. 5025	3.5-13 pF trimmer
	C12	74. 5046	15 pF 5% ceram DI
	C13	74. 5161	470 pF -20+80% ceram PL
	C14	76. 5072	47 nF 10% polyest FL
	C15	78. 5050	3-9 pF trimmer
	C16	78. 5026	4.5-20 pF trimmer
	C17	74. 5161	470 pF -10+80% ceram PL
	C18	76. 5072	47 nF 10% polyest FL
	C19	74. 5155	1 nF -20+80% ceram PL
	C20	76. 5072	47 nF 10% polyest FL
	C21	78. 5031	4-20pF trimmer
	C22	78. 5051	3-10 pF trimmer
	C24	74. 5155	1 nF -20+80% ceram PL
	C25	74. 5155	1 nF -20+80% ceram PL
	R1	80. 5251	1.5 KΩ 5% carbon film
	R2	86. 5058	1 KΩ 20% potentiometer
	R3	80. 5235	68 Ω 5% carbon film
	R4	80. 5257	4.7 KΩ 5% carbon film
	R5	80. 5270	56 KΩ 5%
	R6	80. 5229	22 Ω 5%
	R7	80. 5244	390 Ω 5%
	R8	80. 5225	10 Ω 5%
	R9	80. 5225	10 Ω 5%
	R10	80. 5225	10 Ω 5%
	R11	80. 5225	10 Ω 5%
	R12	82. 5205	0.22 Ω 10% wire wound
	R13	80. 5237	100 Ω 5% carbon film
	L2	63. 5008	0.47 μH 20% RF choke
	L3	62. 0794	RF Coil 420-470 MHz
	L4	62. 0795	RF Coil 420-470 MHz
	L5	62. 0796	(made with 10 Ω resistor 80. 5225)
	L6	62. 0797	RF Coil 420-470 MHz

TYPE	NO.	CODE	DATA
	L7	62. 0795	RF Coil 420-470 MHz (made with 10 Ω resistor 80. 5225)
	L8	62. 0798	RF Coil 420-470 MHz
	L9	62. 0797	RF Coil 420-470 MHz
	L10	62. 0795	RF Coil 420-470 MHz
	L11	62. 0799	(made with 10 Ω resistor 80. 5225)
	L12	62. 0797	RF Coil 420-470 MHz
	E1	99. 5028	Diode 1N914
	E2	99. 5028	Diode 1N914
	Q1	99. 5230	Transistor BC178
	Q2	99. 5128	Transistor 2N3053
	Q3	99. 5229	Transistor 2N4427
	Q4	99. 5242	Transistor BLX67
	Q5	99. 5242	Transistor BLX67
	Q6	99. 5243	Transistor BLX66

POWER AMPLIFIER
EFFEKTFORSTÆRKER

PA763

X 401. 861

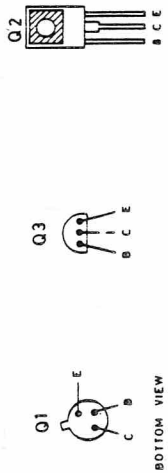
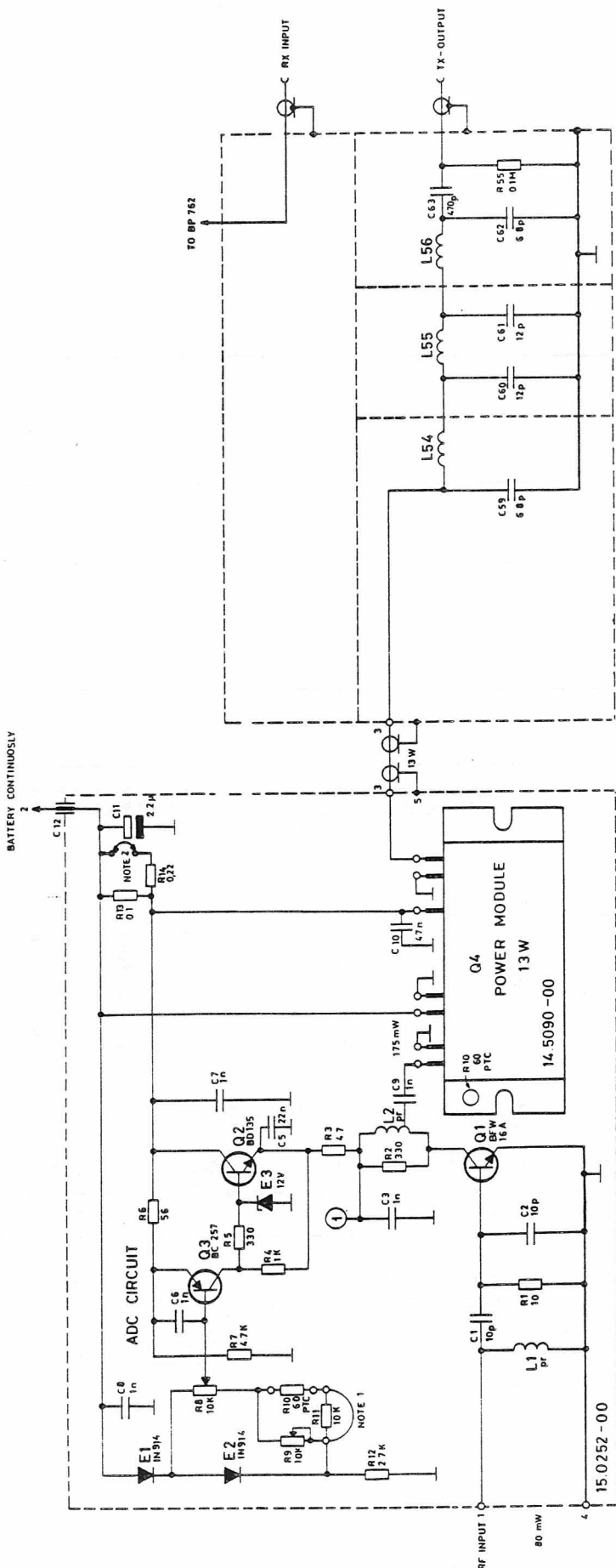
TYPE	NO.	CODE	DATA
PA764		10. 3177-00	UHF Power Amplifier
	C1	74. 5006	10 pF 5% ceram DI 400V
	C2	74. 5006	10 pF 5% ceram DI 400V
	C3	74. 5325	1 nF -20% + 80% ceram no lead 400V
	C4		not used
	C5	76. 5071	22 nF 10% polyester FL 50V
	C6	74. 5155	1 nF -20% +80% ceram PL 63V
	C7	74. 5155	1 nF -20% +80% ceram PL 63V
	C8	74. 5155	1 nF -20% +80% ceram PL 63V
	C9	74. 5155	1 nF -20% +80% ceram PL 63V
	C10	76. 5072	47 nF 10% polyester FL 50V
	C11	73. 5064	2.2 μF -10% +100% elco 63V
	C12	69. 5023	VHF feed through filter
	R1	80. 5225	10 Ω 5% carbon filter 1/8W
	R2	80. 5243	330 Ω 5% " " 1/8W
	R3	80. 5233	47 Ω 5% " " 1/8W
	R4	80. 5249	1KΩ 5% " " 1/8W
	R5	80. 5243	330 Ω 5% " " 1/8W
	R6	80. 5234	56 Ω 5% " " 1/8W
	R7	80. 5257	4.7KΩ 5% " " 1/8W
	R8	86. 5039	10KΩ 20% potentiometer 0.1W
	R9	86. 5037	10KΩ 20% " " 0.05W
	R10	89. 5071	60 Ω - 50KΩ PTC 30V
	R11	80. 5261	10KΩ 5% carbon film 1/8W
	R12	80. 5254	2.7KΩ 5% " " 1/8W
	R13	82. 5208	0.1 Ω 10% wirewound 1W
	R14	82. 5205	0.22 Ω 10% wirewound 1W
	E1	99. 5028	IN914 Diode
	E2	99. 5028	IN914 Diode
	E3	99. 5223	12V 5% Zenerdiode 1/4W
	Q1	99. 5298	BFW16A Transistor
	Q2	99. 5235	BD135 Transistor
	Q3	99. 5144	BC214L Transistor
	Q4	14. 5090	UHF Power Module 13W
		10. 3178	AS763 Antenna Switch
	C51	69. 5007	VHF feed through filter
	C52	74. 5155	1 nF -20% +80% ceram PL 50V
	C53	74. 5155	1 nF -20% +80% ceram PL 50V
	C54	74. 5004	5.6 pF ± 0.25 pF ceram DI 400V
	C55	74. 5130	3.9 pF ± 0.25 pF ceram DI 250V
	C56	74. 5162	470 pF -20% +50% ceram DI 250V
	C57	74. 5155	1 nF -20% +80% ceram PL 50V

TYPE	NO.	CODE	DATA
	C58	69. 5007	VHF feed through filter
	C59	74. 5021	6.8 pF ± 0.25 ceram DI 400V
	C60	74. 5194	12 pF 5% ceram DI 400V
	C61	74. 5194	12 pF 5% ceram DI 400V
	C62	74. 5021	6.8 pF ± 0.25 pF ceram DI 400V
	C63	74. 5094	470 pF 20% ceram DI 400V
	R51	80. 5232	39 Ω 5% carbon film 1/8W
	R52	80. 5073	100KΩ 5% " " 1/8W
	R53	80. 5073	100KΩ 5% " " 1/8W
	R54	80. 5044	390KΩ 5% " " 1/8W
	R55	80. 5273	100KΩ 5% " " 1/8W
	L51	63. 5008	0.47 μH 20% RF choke 2.2A
	L52	62. 0923	RF coil
	L53	62. 0810	RF coil
	L54	62. 0811	RF coil
	L55	62. 0811	RF coil
	L56	62. 0811	RF coil
	E51	99. 5244	BA182 Diode
	E52	99. 5244	BA182 Diode
	E53	99. 5244	BA182 Diode
	E54	99. 5244	BA182 Diode
	E55	99. 5282	5.6V 5% Zenerdiode 1/8W
	E56	99. 5237	IN4148 Diode

POWER AMPLIFIER

PA764

X402. 163



NOTE 1.
REMOVE SHORTING LINK WHEN ADJUSTING ADC RANGE

NOTE 2.
REMOVE STRAP FOR 6W RF OUTPUT

BOTTOM VIEW

POWER AMPLIFIER PA 765 (10.3238-00)

D-402.139/2

STORNOPHONE 700
 MAINTENANCE MANUAL
 VOLUME II
 Section 6

TITLE		Code
PS701	Description 1 - 2	60. 204-E1
	Schematic	D401. 647/2
	Part List	X401. 789
PS702	Description 1 - 6	60. 244-E1
	Schematic	D401. 870/2
	Part List	X401. 937
	Component Lay-out	D402. 096
PS703	Description	60. 245-E1
	Schematic	D402. 009
	Part List	X402. 398
PS704	Description	60. 246-E1
	Schematic	D402. 044
	Part List	X402. 397
RA711	Schematic	D401. 848/2
	Part List	X401. 941
RA712	Schematic	D402. 183
	Part List	X402. 367
RA761	Schematic	D401. 778/2
	Part List	X401. 860
RC711	Description 1 - 2	60. 189-E1
	Schematic	D401. 342/2
	Part List	X401. 382
RC712	Schematic	D401. 846
	Component Lay-out	D401. 976
	Part List 1 - 2	X401. 942
RC731	Description 1 - 2	60. 190-E1
	Schematic	D401. 341/3
	Part List	X401. 537

STORNOPHONE 700
MAINTENANCE MANUAL
VOLUME II
Section 6

RC761	Description 1 - 2	60. 191-E1
	Schematic	D401. 333/2
	Part List	X401. 332/2
RC762	Schematic	D401. 785
	Component Lay-out	D401. 896
	Part List 1 - 2	X401. 865/2
RC763	Schematic	D402. 259
	Part List	X402. 366
	Component Lay-out	D402. 422
RC764	Schematic	D402. 369
	Part List	X402. 547

POWER SUPPLY PS701

Description

General

This power supply is designed for mobile radio sets in the CQM700 series. The unit operates from a DC supply in the neighbourhood of 24 V, supplying a DC voltage in the proximity of 12 V from its output.

The input to the power supply has no DC connection to chassis ground and thus is floating in reference to ground. The negative side of the output, however, is at chassis ground potential.

By means of taps on the secondary of the transformer T1 the output can be wired to accommodate a maximum current drain of either 4.0 A or 8.0 A.

The unit is housed in a cast metal cabinet and contains three stages; an input filter, a DC/DC converter, and a series voltage regulator circuit.

When installing the PS701 the positive output lead must be protected with either a 5.0 A fuse (for the 4.0 A version) or an 8.0 A fuse (for the 8.0 A version). In the input, in the battery lead that is NOT connected to the vehicle chassis, a 6.0 A fuse must be inserted. Moreover, an on/off switch needs also to be incorporated into the input lead since there is no start relay in the power supply.

The DC Converter

The DC/DC converter consists of the converter circuit and transformer T1. The converter transistors, Q1 and Q2, are coupled in a normal, common-emitter push-pull configuration.

The converter operating frequency is determined by the characteristics of T2 and the voltage across its primary winding and is approximately 12 to 15 kHz. T2, the saturation transformer, is dimensioned to saturate before T1 in order to prevent excessive peak currents through the transistors.

The primary winding of the saturation transformer, T2, and a series resistor, R6, are inserted between the collectors of Q1 and Q2. The secondary winding of T2, which is a bifilar winding, is placed between the bases of these same transistors.

When power is initially applied to the input there is 0 V across the series resistor and the primary of T2. Therefore, in order to start the switching action in the converter a starting circuit must be employed. This circuit consists of Q3 and Q4. Q3, a programmed unijunction transistor, is the starting element and Q4 acts as an amplifier for Q3, ensuring that the converter circuit will start even under full load conditions.

When power is applied to the input a current from the battery, through the primary winding of T1 and resistor R4, builds up a voltage across capacitor C6 until it reaches a level where it causes Q3 to open. C6 discharging through Q3 drives the base of Q4 in the forward direction, providing forward bias to Q2. Q2 begins to pass current, and now the converter action can begin.

The time constant of the starting circuit is so long in comparison to the converter frequency that the starter will remain passive during operation.

The primary of T1, which is connected between the two collectors (Q1 and Q2), is made up of two identical bifilar windings. The secondary consists of two identical main windings, a winding for generating an auxiliary voltage for the series regulator circuit (transformer terminals 7 and 8), and a special auxiliary winding (transformer terminals 5 and 6) that can supply approx. 5 V for certain types of special equipment.

The connections to the main secondary windings will depend upon the maximum output

load requirements. The converter comes wired as a 4.0 A version from the factory. To modify it to the 8.0 A version, the lead from transformer terminal 10 must be interchanged with that from terminal 9, and the lead from terminal 13 must be interchanged with that from terminal 12. In addition, the fuse in the output lead must be replaced with an 8.0 A fuse.

The two main secondary windings are connected as a full-wave rectifier incorporating diodes E7 and E8.

The Series Regulator

The purpose of the series voltage regulator circuit is to maintain the output voltage at some preset value within the proximity of 12 V. For maximum efficiency the regulator circuit setting should be 16 V with unloaded output.

The regulator circuit contains 2 transistor stages; a series element and driver, and an amplifier with a reference zener diode. The series element, Q5, operates in the grounded collector (emitter-follower) mode. Q5 and Q6 are a Darlington coupled amplifier which is controlled by the reference amplifier, Q7, whose base monitors any variations in the output voltage and compares it with the constant zener reference voltage at its emitter.

The auxiliary half-wave rectifier circuit incorporating diode E9 ensures that Q5 can be driven into complete saturation. Otherwise, the minimal voltage drop across Q5 would be:

$$V_{BE}(Q5) + V_{CE}(Q6) .$$

Thanks to the auxiliary voltage, the least drop is now : $V_{CE}(Q5) .$

The Input Filter

The filter employed in the input leads ensures compliance to the noise/interference specifications set forth in the German norm VDE 0875. Coil L1, consisting of identical windings both wound on the same core, forms a low-pass filter in conjunction with C1 and C2.

Technical Specifications

Supply Voltage

minimum: 21.0 V
normal: 25.2 V
maximum: 32.0 V

Output Voltage

minimum: 10.5 V
maximum: 16.0 V

Output Load

4.0 A version: 4.0 A
8.0 A version: 8.0 A

Output Voltage Ripple

< 60 mV p.p.

Current Consumption

25.2 V supply, unloaded output: 400 mA
25.2 V supply, 4.0 A output load: 3.0 A
25.2 V supply, 8.0 A output load: 6.1 A

Converter Frequency

12 to 15 kHz

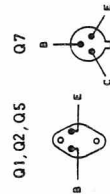
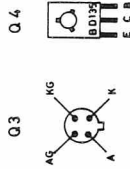
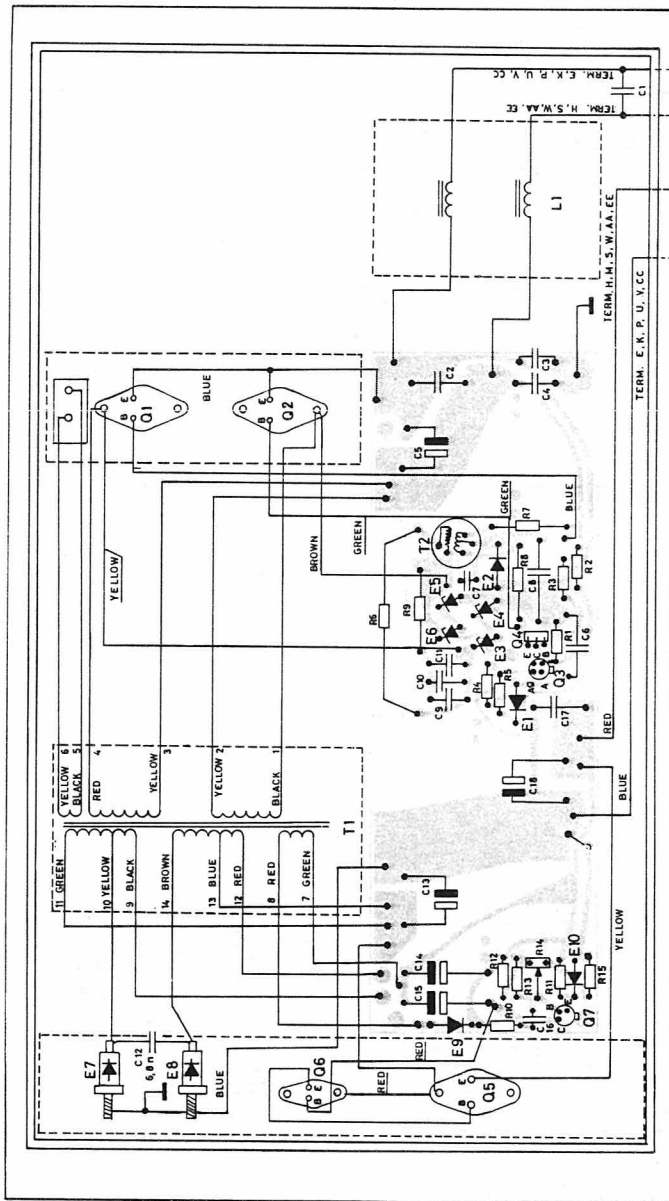
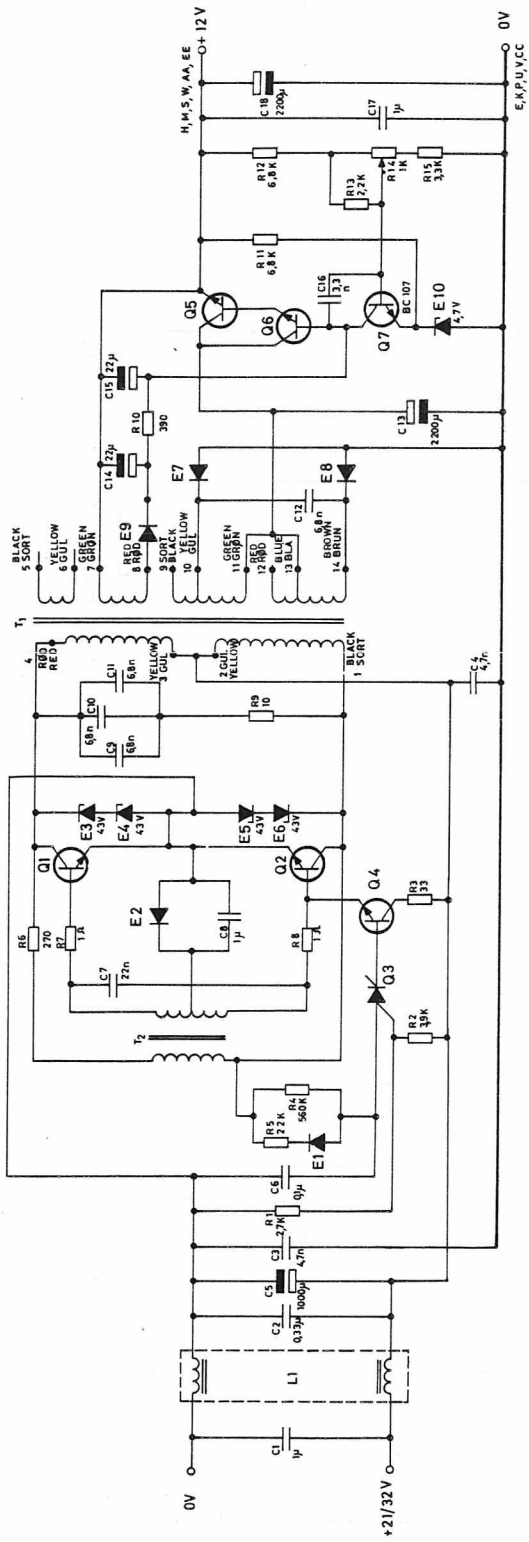
Ambient Temperature Range

4.0 A version

operating range: -25° to $+60^{\circ}$ C
functioning range: -25° to $+80^{\circ}$ C

8.0 A version, 30 minute duty period

operating range: -25° to $+60^{\circ}$ C
functioning range: -25° to $+80^{\circ}$ C



POWER SUPPLY UNIT
STRØMFORSYNING

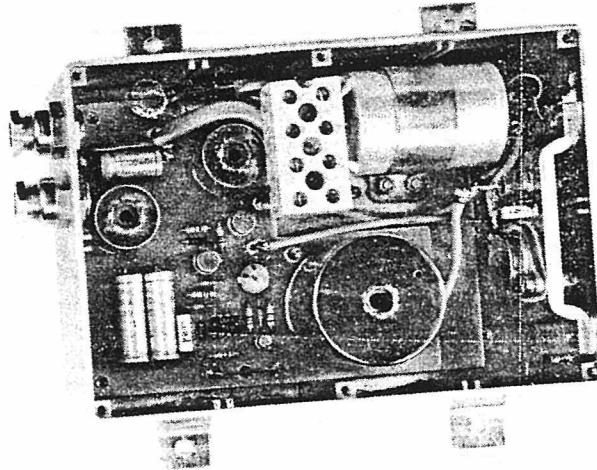
TYPE	NO.	CODE	DATA
PS701		10. 2448-00	Power supply unit
	C1	76. 5078	1µF 10% polyester TB 100V
	C2	76. 5075	0. 33µF10% polyester TB 100V
	C3	74. 5285	4. 7nF - 20+80% ceram DI 2000V
	C4	74. 5285	4. 7nF -20+80% ceram DI 2000V
	C5	73. 5146	1000µF -10+100% elco 100V
	C6	76. 5073	0. 1µF 10% polyester TB 100V
	C7	76. 5071	22nF 10% polyester FL 50V
	C8	76. 5078	1µF 10% polyester TB 100V
	C9	74. 5286	6. 8nF 20% ceram DI 400V
	C10	74. 5286	6. 8nF 20% ceram DI 400V
	C11	74. 5286	6. 8nF 20% ceram DI 400V
	C12	74. 5286	6. 8nF 20% ceram DI 400V
	C13	73. 5139	2200µF - 10+100% elco 40V
	C14	73. 5145	22µF - 10+100% elco 40V
	C15	73. 5145	22µF - 10+100% elco 40V
	C16	76. 5060	3. 3nF 10% polyester 50V
	C17	76. 5096	1µF 20% polyester 100V
	C18	73. 5139	2200µF - 10+100% elco 40V
	R1	80. 5254	2. 7kΩ 5% carbon film 1/8W
	R2	80. 5256	3. 9kΩ 5% carbon film 1/8W
	R3	80. 5231	33Ω 5% carbon film 1/8W
	R4	80. 5282	056MΩ 5% carbon film 1/8W
	R5	80. 5253	2. 2kΩ 5% carbon film 1/8W
	R6	84. 5225	27(Ω) wire wound 9W
	R7	82. 5201	1Ω 10% wire wound 1W
	R8	82. 5201	1Ω 10% wire wound 1W
	R9	84. 5019	10Ω 10% wire wound 5. 5W
	R10	80. 5244	390Ω 5% carbon film 1/8W
	R11	80. 5259	6. 8kΩ 5% carbon film 1/8W
	R12	80. 5259	6. 8kΩ 5% carbon film 1/8W
	R13	80. 5253	2. 2kΩ 5% carbon film 1/8W
	R14	86. 5058	1KΩ 20% potentiometer 0. 1W
	R15	80. 5255	3. 3kΩ 5% carbon film 1/8W
	L1	60. 5161	Line filter
	T1	60. 5160	Converter transformer 24-12V 175W
	T2	61. 1118	Transformer, saturation
	E1	99. 5237	1N4148 diode
	E2	99. 5020	1N4004 diode
	E3	99. 5226	BZX70C43 zenerdiode
	E4	99. 5262	BZX70C43 zenerdiode
	E5	99. 5262	BZX70C43 zenerdiode
	E6	99. 5262	BZX70C43 zenerdiode

TYPE	NO.	CODE	DATA
	E7	99. 5260	BYX30-200R diode
	E8	99. 5260	BY30-200R diode
	E9	99. 5020	1N4004 diode
	E10	99. 5224	4. 7V 5% zenerdiode
	Q1	99. 5261	BDY91 Transistor
	Q2	99. 5261	BDY91 Transistor
	Q3	99. 5238	BRY39 Transistor
	Q4	99. 5235	BD135 Transistor
	Q5	99. 5261	BDY91 Transistor
	Q6	99. 5193	2N3054 Transistor
	Q7	99. 5121	BC107 Transistor

POWER SUPPLY UNIT
STRØMFORSYNING PS701

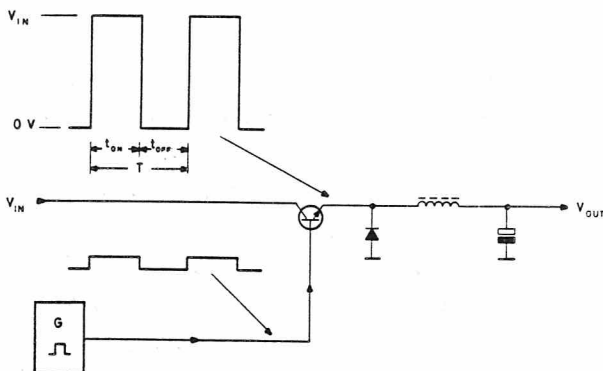
X 401. 789

Power Supply Unit PS702



The PS702 power supply is a switching regulator for converting a 24 V input voltage to 12 V output to supply a CQM700 radiotelephone.

The conversion from a high to a lower voltage is accomplished by alternately applying the input voltage (V_{IN}) and 0 volts (ground potential) to an LC lowpass filter, as shown below.



The output voltage will be the average value of the switched waveform. If the voltage drop across the transistor and diode is neglected, the output voltage will be:

$$V_{OUT} = V_{IN} \times \frac{t_{ON}}{T}$$

which, in the case of a symmetric square wave and a 24 V input will be:

$$24 \text{ V} \times 1/2 = 12 \text{ V}$$

In addition, there will be a small amount of ripple voltage whose fundamental frequency is the switching frequency.

Notice that the output voltage, according to the formula, is independent of the load current.

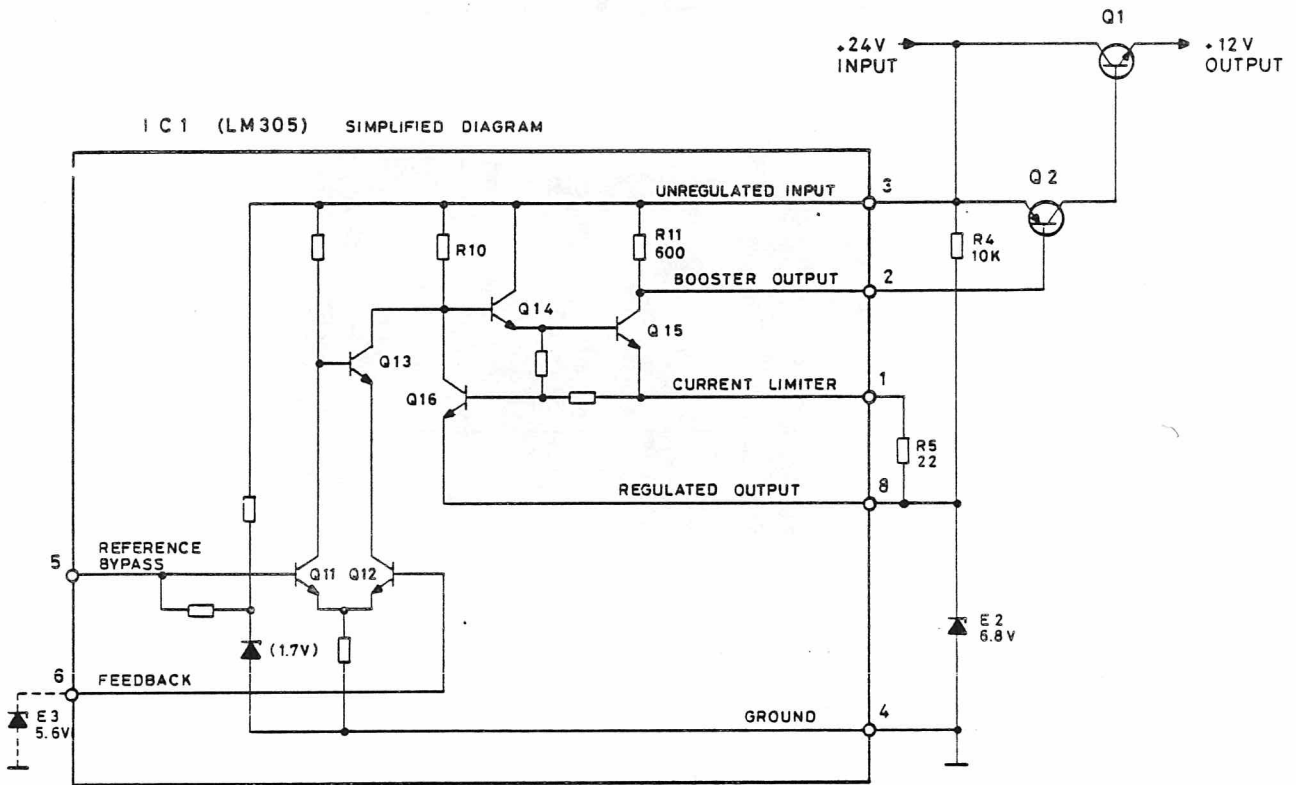
A regulating circuit monitors the output voltage and compares it to a reference voltage. The regulating circuit then accordingly regulates the ratio between ON and OFF time. Thus the output voltage is maintained at the proper level regardless of input voltage or load current.

A current regulating circuit protects the series switch transistors against being destroyed by overloads or short circuits at the power supply output.

LC filters in both the input and output circuits prevent excessive radiation of noise along the input and output leads.

Due to the switching principle the efficiency of this power supply is high, efficiency is on the order of 85%.

SWITCHING CIRCUIT



The LM305 integrated voltage regulator, IC1, drives the PNP switching transistor, Q2. An additional, NPN transistor, Q1, enables the circuit to handle the heavy currents required by the radiotelephone set (up to 8 amperes).

Q11 and Q12 make up a differential amplifier. The input from IC pin 6 is the inverting input, referred to as the feedback input. The non-inverting input, from IC pin 5, is called the reference bypass. This input is held at a potential of 1.7 V (typical value) by the internal IC circuitry. This potential is called the reference voltage.

If the voltage on input pin 6 is less positive than the reference voltage at the base of Q11, the differential amplifier turns Q13 OFF. This is how: Q11 conducts, pulling the base of Q13 LO while at the same time Q12 cuts off via emitter feedback, preventing any emitter current to flow through Q13. When Q13 goes OFF its collector is pulled up by R10, turning Q14

and Q15 ON. Notice that Q15's 600 ohm collector resistor, R11, is also the emitter-base biasing circuit for Q2, the switching transistor. Thus, when Q15 is driven ON, the collector current through R11 turns Q2 ON, as well. Q2 supplies drive to Q1, which also switches ON.

Now, if a voltage more positive than the internally generated reference voltage is applied to IC pin 6, Q12 will go ON, cutting Q11 OFF. The differential amplifier now forward biases Q13, which goes ON, turning Q14 and Q15 OFF. With no collector current through R11, Q2 loses its forward bias and switches OFF, also switching Q1 OFF.

In addition, there is a built-in current limiting feature in this circuit. Base current for Q2 flows via IC pin 2 (booster output), Q15, R5, and E2 to ground. The 22 ohm resistor R5 is called the current limiting resistor and is also the source of emitter-base bias for Q16. Whenever base current for Q2 tends to exceed the limit set by

the value of R5, Q16 will begin to draw current through R10. This reduces the bias to Q14 and Q15, creating a state of equilibrium where the amount of base drive to Q2 is determined by the value of R5.

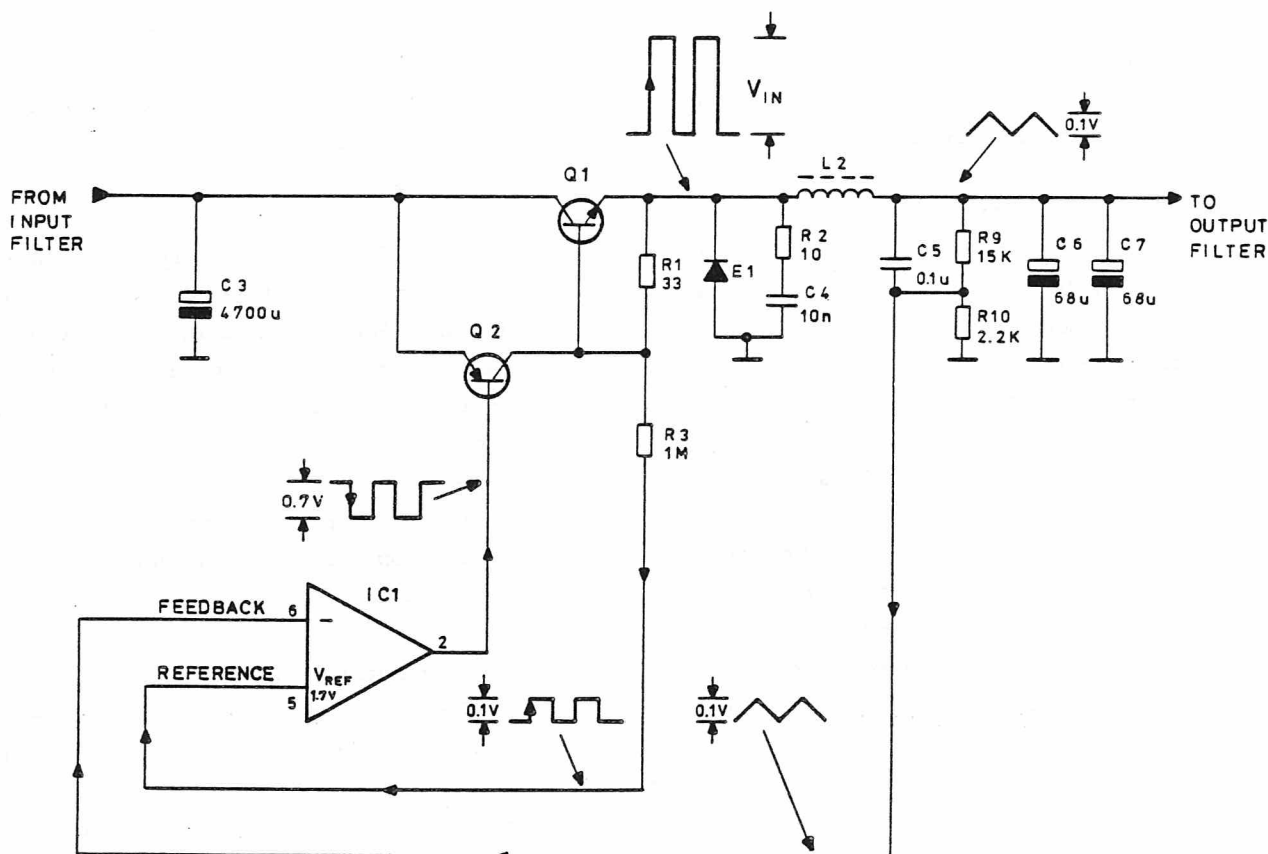
With a value of 22 ohms chosen for R5, the current will be limited to about 15 mA for temperatures within the nominal operating range.

Zener diode E2 keeps the regulated output voltage at IC pin 8 at approximately 6.8 V. E3, a 5.6 V Zener diode, is wired to IC pin 6. This ensures that the voltage to the feedback terminal cannot rise higher than the voltage at IC pin 1. Otherwise the circuit can latch up and burn out.

OSCILLATOR CIRCUIT

The integrated voltage regulator, IC1, monitors the output voltage by measuring the portion of the DC voltage that is dropped across R10. It also measures the full amplitude of the output ripple via bypass capacitor C5. Thus the instantaneous ripple amplitude adds with the sampled DC voltage at input terminal 1, pin 6 of IC1.

When power is initially to the PS702 there is no voltage at the output. Therefore there can be no bias available at pin 6 of IC1, and the internally generated reference voltage present at the noninverting input, pin 5, will then be able to drive the IC ON, which in turn drives Q2, then Q1, into conduction as well.



A positive voltage now begins building up on the collector of Q2 as well as on the emitter of Q1. A small portion of this rising voltage is fed back through resistor R3 to IC1 input terminal, pin 5. The amplitude of the feedback signal is determined by the ratio of R3 to the input impedance of the terminal. The polarity of the feedback signal is such that it causes the voltage at terminal 5 to become even more positive. This regenerative feedback therefore increases the gain of the amplifier, driving Q1 and Q2 even harder. (In fact, the amplitude of the feedback signal is sufficient to sustain oscillation in the circuit). Of course, this all happens very quickly, during the rise time of the square wave.

Meanwhile, filter capacitors C6 and C7 are charging up to the input voltage through L2 and Q1. The DC charge on these parallel capacitors is divided between R9 and R10. Remember, too, that C5 bypasses ripple voltages (including charging waveforms) around R9, directly to pin 6 of the regulator IC.

At some point the combined AC and DC voltages as seen at pin 6 of IC1 will become greater than the bias at pin 5, which bias is equal to the internal reference voltage plus the instantaneous value of the feedback signal. Now when the potential at terminal 6 has become more positive than that at terminal 5, the regulator switches state and cuts Q2 and Q1 OFF.

When this happens the magnetic field induced in coil L2 will attempt to maintain the current flow through the coil and in so doing biases catch diode E1 into forward conduction, in effect grounding the emitter of Q1. As seen at IC pin 5, the regenerative feedback via R3 is now a negative-going pulse. This, of course, is the correct polarity for driving the integrated amplifier and the switching transistors even further into cut-off.

The circuit remains cut off until C6 and C7 discharge enough so that the potential seen at pin 6 falls below that at pin 5 (the reference voltage minus the feedback signal). At this point the IC switches state again and the circuit continues in this way to oscillate at a frequency determined by the reactance of L2, the capacitances of C6 and C7, and the amplitude of the feedback signal. Feedback resistor R3 is what determines the amplitude of the feedback signal.

(It is worth mentioning here that the output voltage does not reach its full 12 V potential immediately, but in several increments governed by the oscillator excursions and the frequency of oscillation. However, once the output voltage reaches its full value, it remains constant with only a slight ripple voltage).

The amplitude of the feedback signal, typically 100 mV, determines how great a voltage excursion the oscillator circuit must self-compensate for, the ripple superimposed on the filter capacitors C6 and C7 will have essentially the same amplitude as the feedback signal voltage. With L2, C6, and C7 as circuit constants, the rate of charging the filter capacitors is also constant. Thus, if the capacitors have to charge (or discharge) to a relatively greater voltage before the oscillator switches state, it will take a longer time to do so. On the other hand, if the feedback and ripple amplitudes are relatively less, the capacitors can reach the threshold levels in less time. This is what determines the frequency of oscillation.

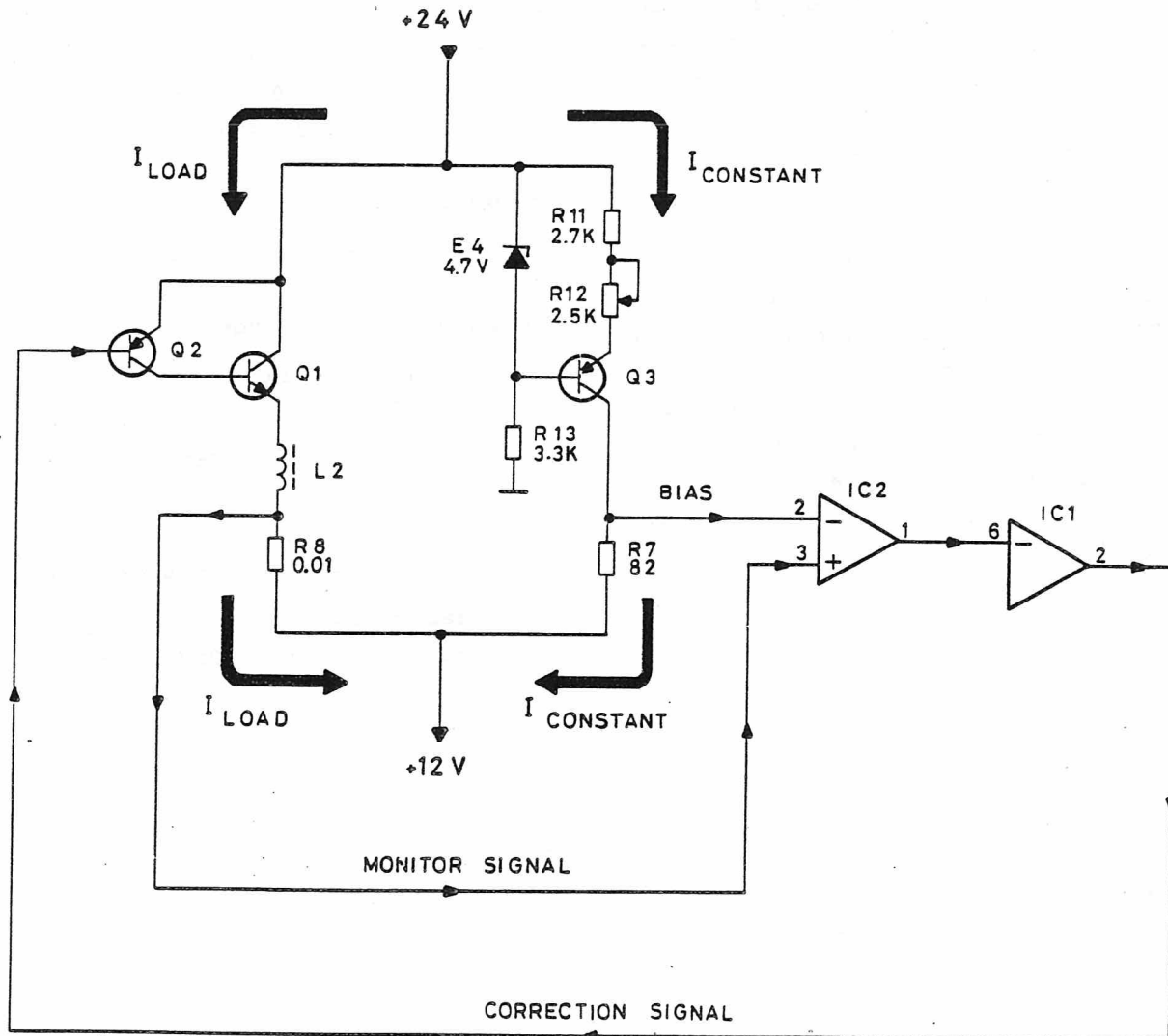
The oscillator frequency is approximately 25 kHz. This frequency was chosen as a compromise between efficiency, which improves with lowering frequency, and the necessity of ensuring against radiating undesired signals that would fall within the audible range.

An RC network consisting of R2 and C10, across catch diode E1, is a damping circuit used to attenuate switching transients that appear across E1. As explained earlier, E1 conducts heavily when Q1 is turned OFF. Right as Q1 goes ON again, E1 will still conduct because of its inherent reverse recovery time. The diode will thus act as a short circuit and a strong surge will pass from C3 through Q1 and E1. When all the charge stored in the catch diode is removed, the diode no longer conducts and pulse transients arise. At this point the damping circuit must handle the surge transients. This current surge, with its attendant transients, is the main cause of RF noise generated in the power supply.

OUTPUT CURRENT LIMITER CIRCUIT

Output current limiting is performed by comparator IC2. It compares the voltage drop across the 0.01 ohm resistor, R8, to the 82 ohm resistor, R7. Resistor R7 is in series with the constant current generator, Q3, and there will therefore be a uniform voltage drop across the resistor. On the other hand, resistor R8 is in series with the output load, so the voltage drop across R8 will depend upon the varying load conditions.

As long as the load current remains below a certain limit the voltage drop across R8 will be less than that across R7, and IC2 is held OFF.



When the load current increases, so does the voltage drop across R8, and if the current surpasses the set limit the voltage across R8 becomes greater than the voltage across R7. Now just the opposite condition exists: IC2 goes ON, driving IC1 OFF, which in turn switches Q2 and Q1 OFF, as well.

The maximum allowable load current before limiting will take place is set by adjusting potentiometer R12. Since R12 is in the emitter circuit of the constant current generator, Q3, its setting determines the voltage drop across R7.

Battery Protection

A double fuse box with two 5A fuses must be inserted in the leads from the battery and the vehicle chassis, one fuse in the battery lead and one in the chassis lead. It is not necessary to fuse the connections between power supply and CQM700 equipment.

SERVICING

A good practice to observe when servicing the PS702 is to load the output with a 50 ohm, 15W resistor or a suitable rheostat. Otherwise, if allowed to operate unloaded, the oscillator runs irregularly. This is a normal phenomenon and has no bad effect on the power supply, but it could be misleading when checking the performance of a unit.

Technical Specifications

Supply Voltage

minimum:	21.0 V
nominal:	27.2 V
maximum:	32.0 V

Output Voltage

minimum:	10.5 V
maximum:	16.0 V

Output Load

for output voltage > 10.5 V: 8 A min.

Output Ripple Voltage

< 50 mV p.p.

Current Consumption

27.2 V supply, unloaded output:	10 mA
21.0 V supply, 8.0 A output load:	5.8 A
27.2 V supply, 8.0 A output load:	4.6 A

Efficiency

for $I_L > 0.5$ A: 87%

Ambient Temperature Range

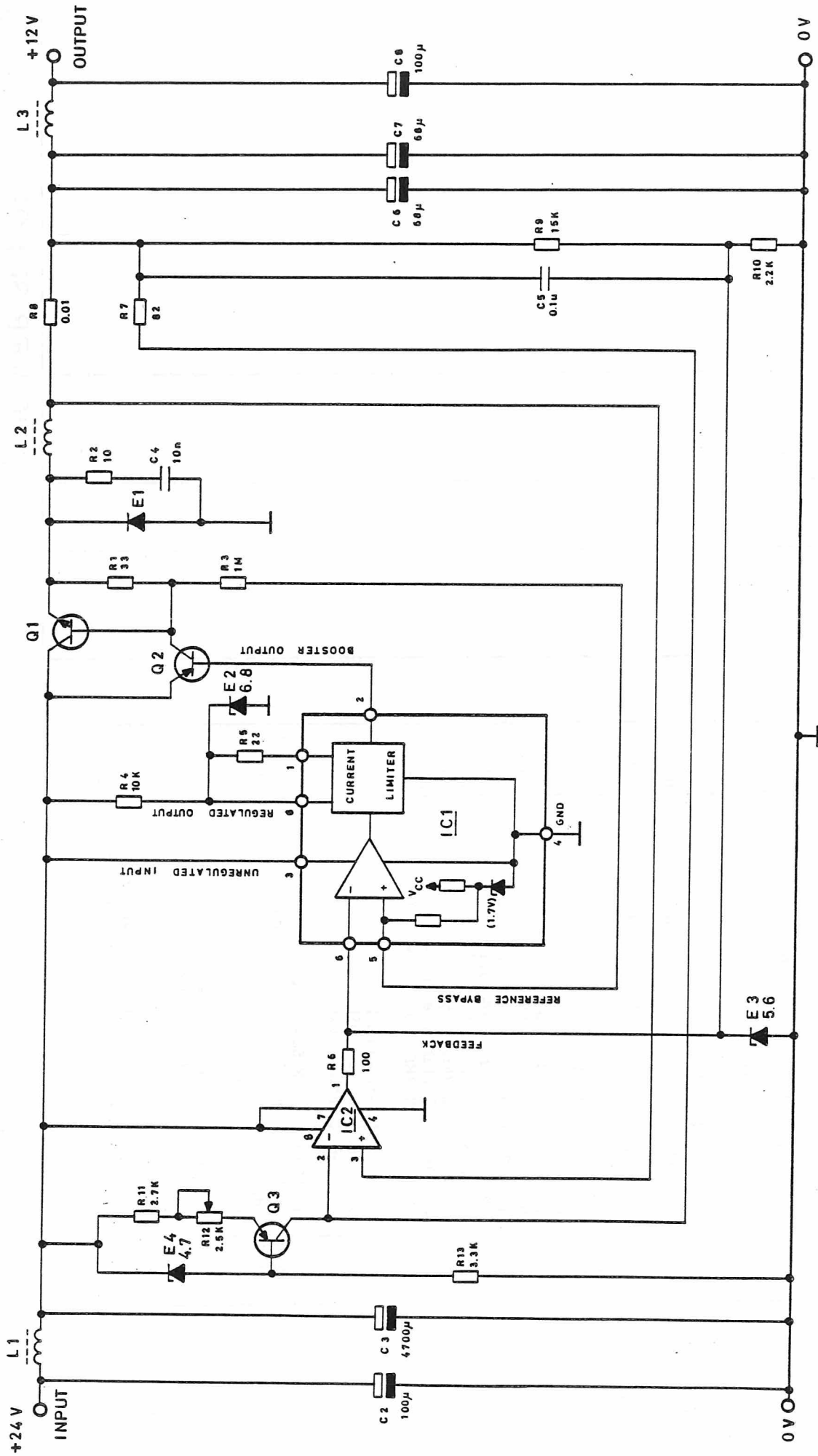
(for continuous duty at 8 A)

operating range:	-25°C to +40°C
functioning range:	-25°C to +80°C

(for intermittent duty,

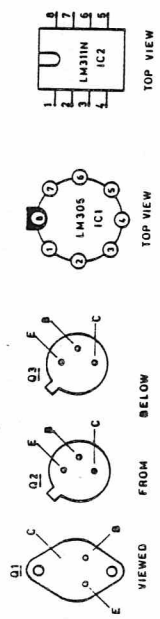
average load ≤ 4 A and duty period ≤ 20 min.)

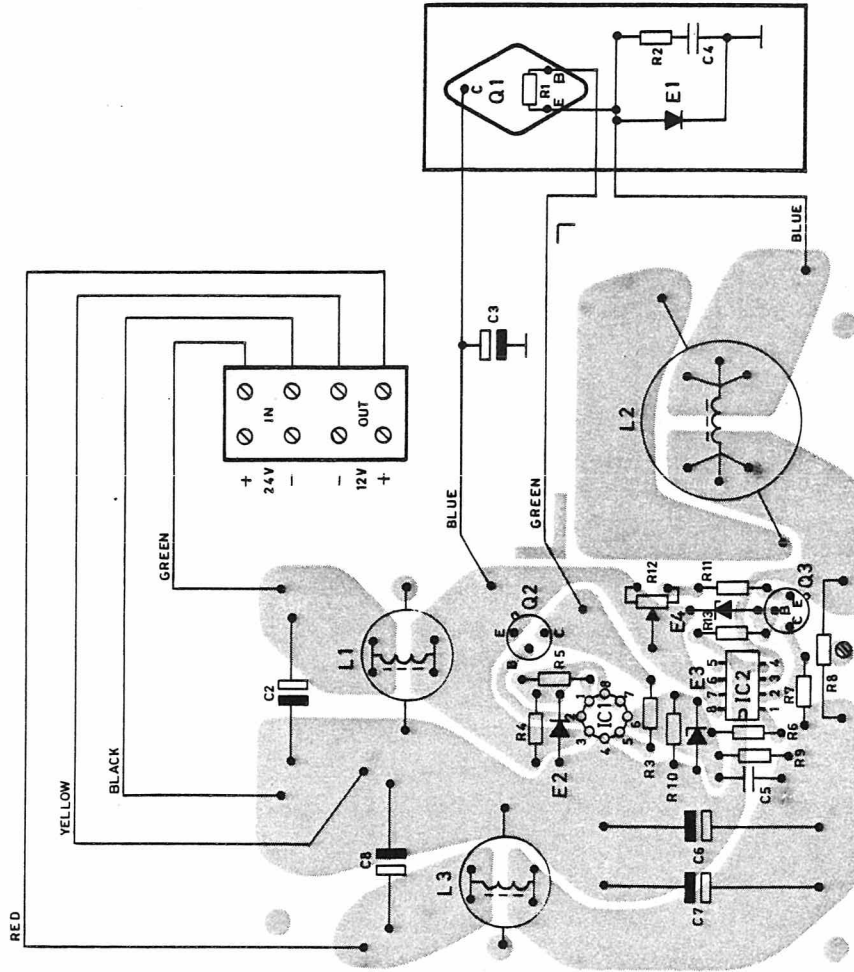
operating range:	-25°C to +60°C
functioning range:	-25°C to +80°C



POWER SUPPLY PS702

D401.870/2





POWER SUPPLY PS702
STRØMFORSYNING

D402.096

POWER SUPPLY UNIT PS703

Circuit Description

The power supply unit PS703 is operated from the mains. It converts 220 V AC to 13.5 V stabilized DC.

The PS703 consists of the following:

- Power transformer
- Rectifier
- Filter
- Series regulator
- Current Limiter

The power regulator is of the conventional series type with Q1 as the series pass element. Transistors Q2 and Q3 are driving Q1 in a three stage darlington configuration. The base voltage of Q3 is controlled by the error voltage amplifier Q5.

The reference voltage is provided by zener diode E6 and compared to the voltage derived from resistor chain R11, R12, and R13. The output voltage is adjusted by means of potentiometer R12. The circuit will oppose any change in the output voltage by regulating the voltage across the series transistor at a value that will keep the output voltage constant.

To reduce output ripple capacitor C5 provides AC feedback.

The current limiter is of the fold back type and consists of transistor Q4 and current sense resistor R7. Capacitors C3 and C4 introduce phase compensation to prevent instability.

Diode E3 protects the unit against reverse current due to incorrect connection and against transients from an inductive load.

Technical Specifications

Supply voltage

220 V AC \pm 20%, 50 Hz.

Output Voltage

13.5 V DC.

Output current

max. 3.5 A.

Load regulation 0 - 3.5 A

< 200 mV (200 V AC).

< 1 V (175 V AC).

Line regulation

< 200 mV for 220 V \pm 10%

< 1 V for 220 V \pm 20%

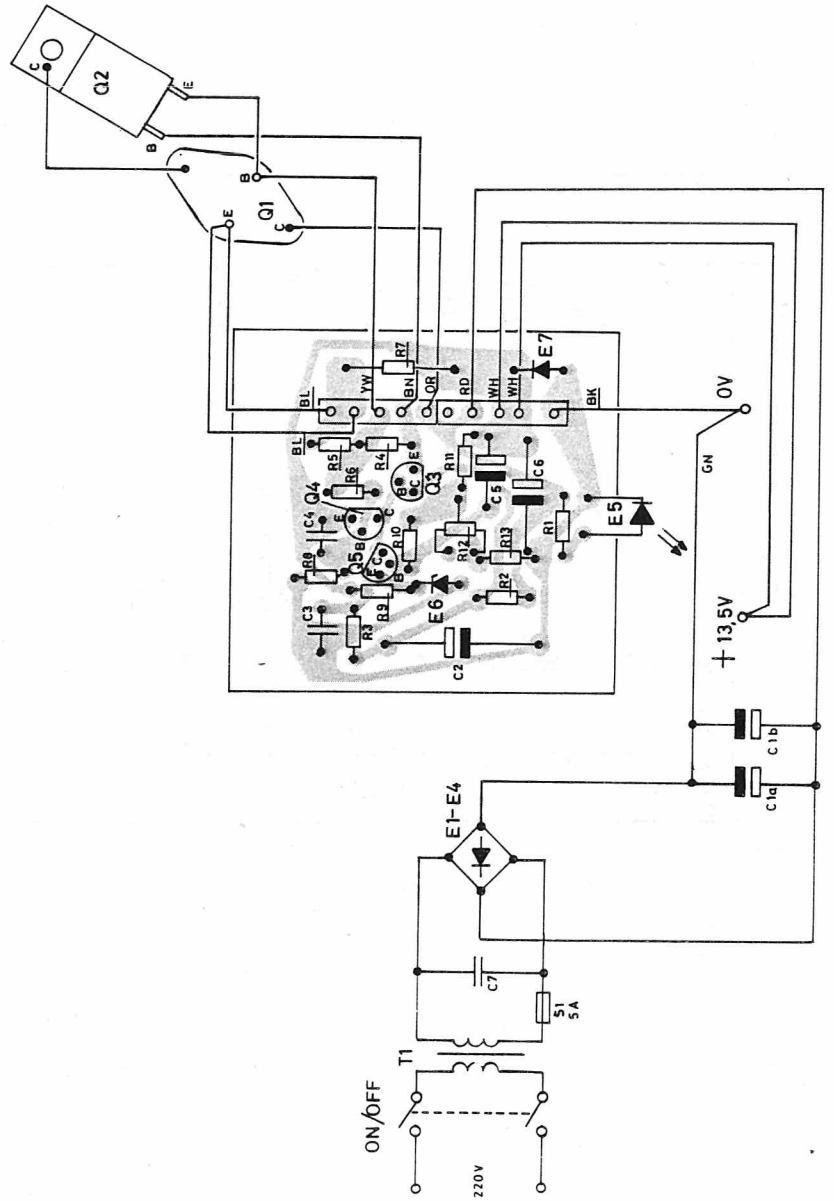
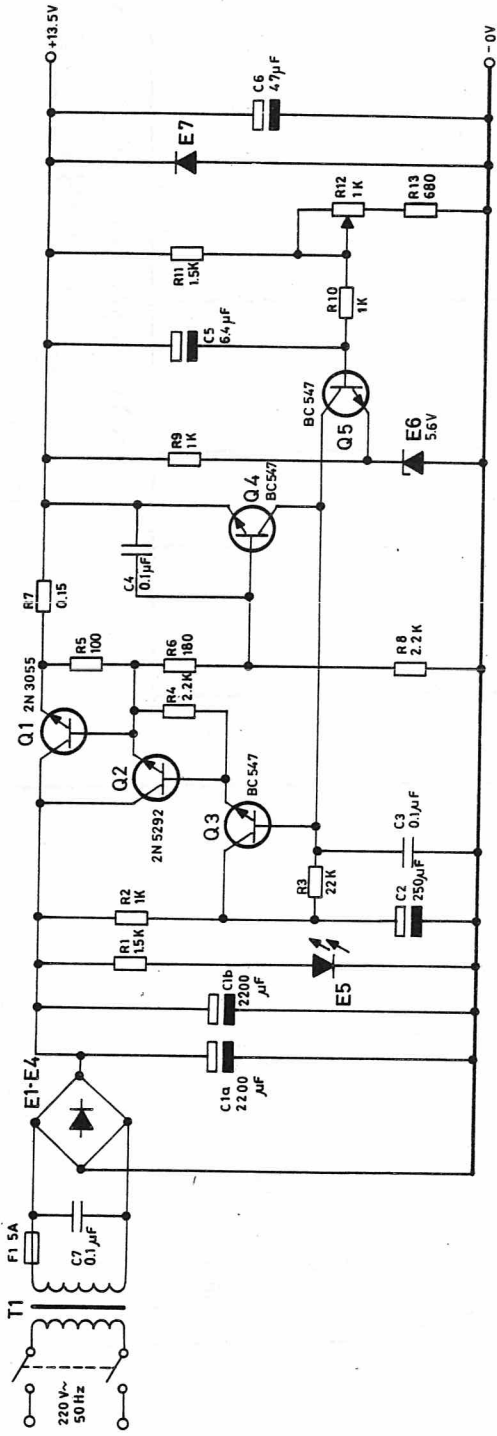
Output voltage ripple

< 0.5 mV RMS at 3.5 A, 220 VAC \pm 10%.

< 100 mV pp at 3.5 A, 175 VAC.

Short circuit current

< 1 A.



POWER SUPPLY
STRØMFORSYNING

PS703

D402.009

POWER SUPPLY UNIT PS704

Circuit Description

The power supply unit PS704 is used in 24 Volt installations to reduce the battery voltage to 12 Volt for the radiotelephone.

The PS704 uses the series regulator principle with two transistors, Q1 and Q2, connected in parallel as the series element.

The transistors are driven by Q3 in a darlington configuration. Resistors R7 and R8 equalize the load current between Q1 and Q2.

The base voltage of driver transistor Q3 is controlled by the error amplifier Q4, the reference voltage of which is provided by zener diode E3. Diode E5 protects the unit against reverse current due to incorrect connection and against transients from an inductive load.

In case of failure of the series transistors zener diode E4 will conduct and protect the load against excessive voltage.

Zener diode E1 protects the input against excessive voltage and against transients on the supply voltage.

In both cases fuse F1 will blow and must be replaced.

Technical Specifications

Input voltage

21 V - 32 V DC.

Polarity

Negative chassis.

Output Voltage

13.5 V

No load current

< 30 mA

Continuous load

1.5 A

Load duty cycle

5.5 A (1 min).

0.8 A (1 min).

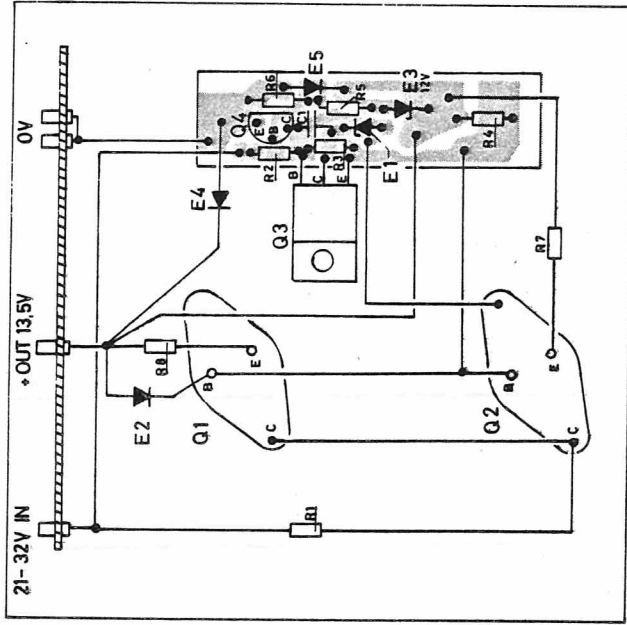
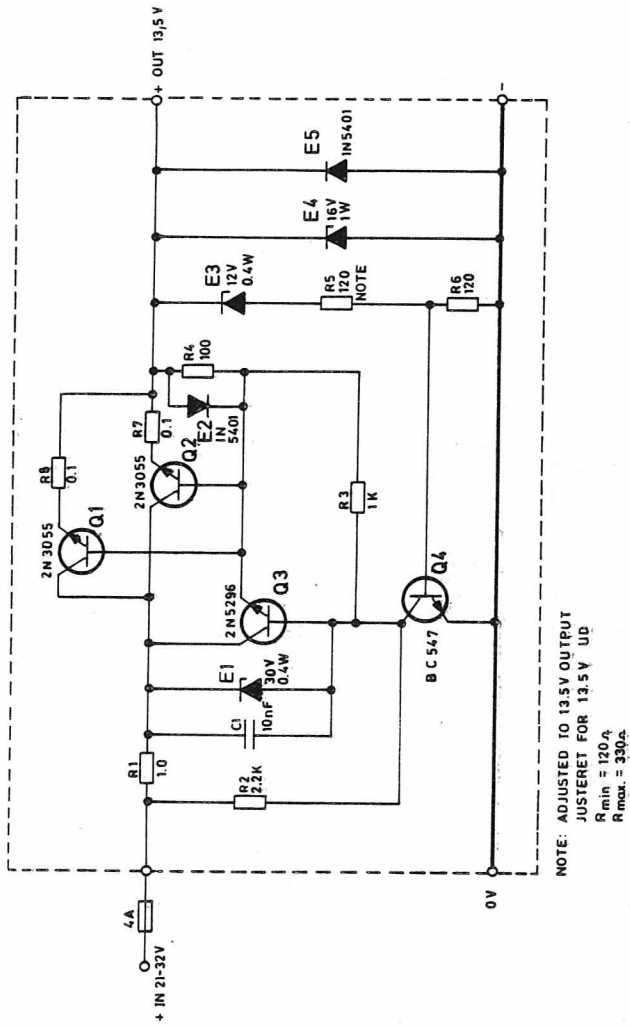
0.4 A (3 min).

Output Overvoltage protection

Activated at voltages >16V.

Temperature Range

-30°C - +55°C.



**POWER SUPPLY
 STRØMFORSYNING PS704**

D402.044

Storno

Storno

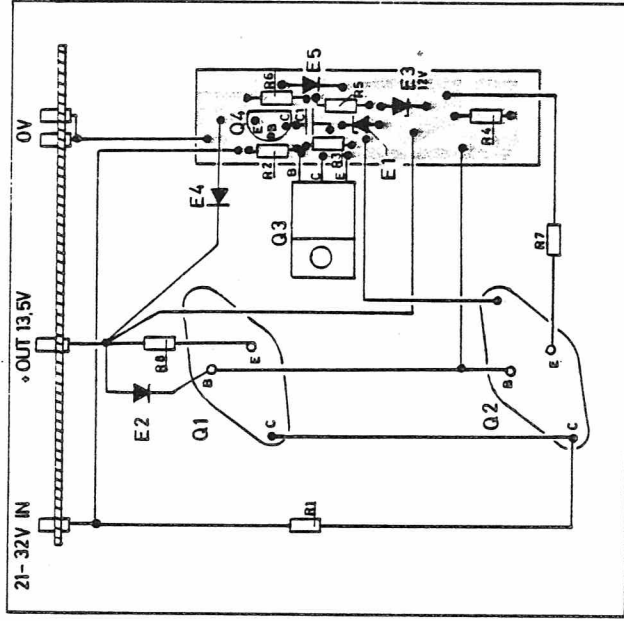
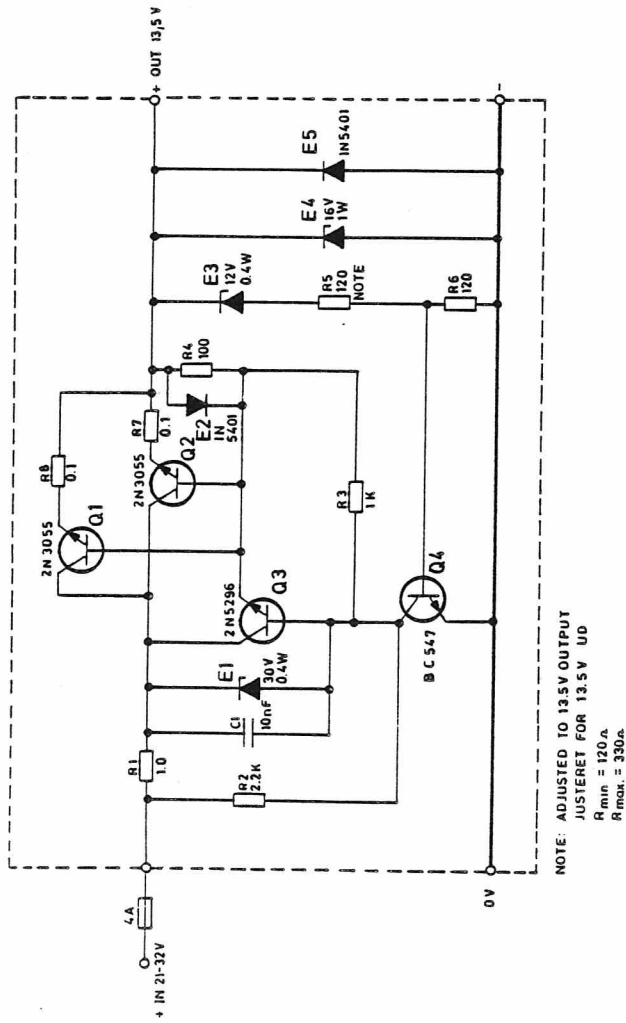
TYPE	Nº	CODE	DATA
PS704		10. 3049	Voltagereregulator 24 V DC/13. 5 V DC
	C1		10 nF 10% polyester.
	R1	80. 5453	1 Ω Resistance wire
	R2	80. 5449	2.2 KΩ carbon film
	R3	80. 5437	1 KΩ " "
	R4	80. 5437	100 Ω " "
	R5	80. 54XX	120-330 Ω " "
	R6	80. 5438	120 Ω " "
	R7		0.1 Ω Resistance wire
	R8		0.1 Ω " "
	E1		30 V Zenerdiode
	E2	99. 5220	1 N 5401 Diode
	E3		12 V Zenerdiode
	E4		16 V Zenerdiode
	E5	99. 5220	1 N 5401 Diode
	Q1	99. 5171	2 N 3055 Transistor
	Q2	99. 5171	" "
	Q3		2 N 5296 " "
	Q4		BC 547 " "
			Fuse 4 A
			1/4 W
			1/4 W
			1/4 W
			1/4 W
			1/4 W
			0.4 W
			0.4 W
			1 W

TYPE	Nº	CODE	DATA

POWER SUPPLY UNIT
STRØMFORSYNING

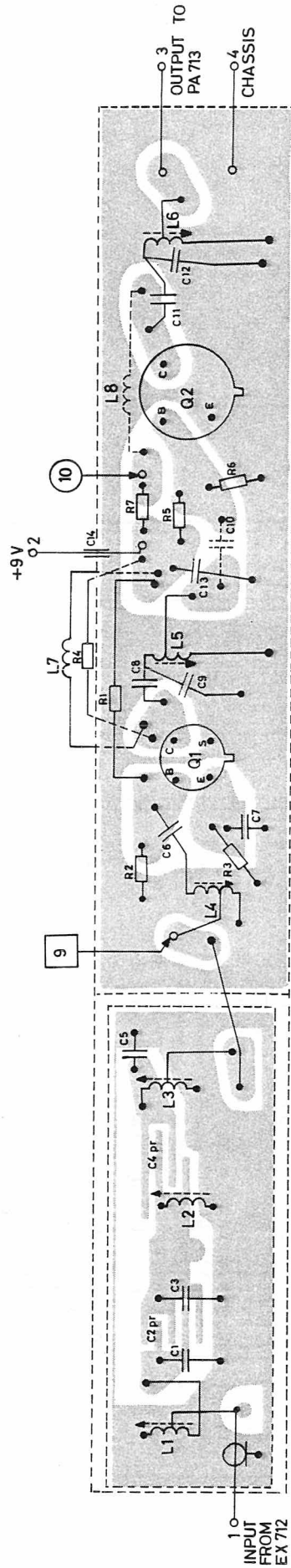
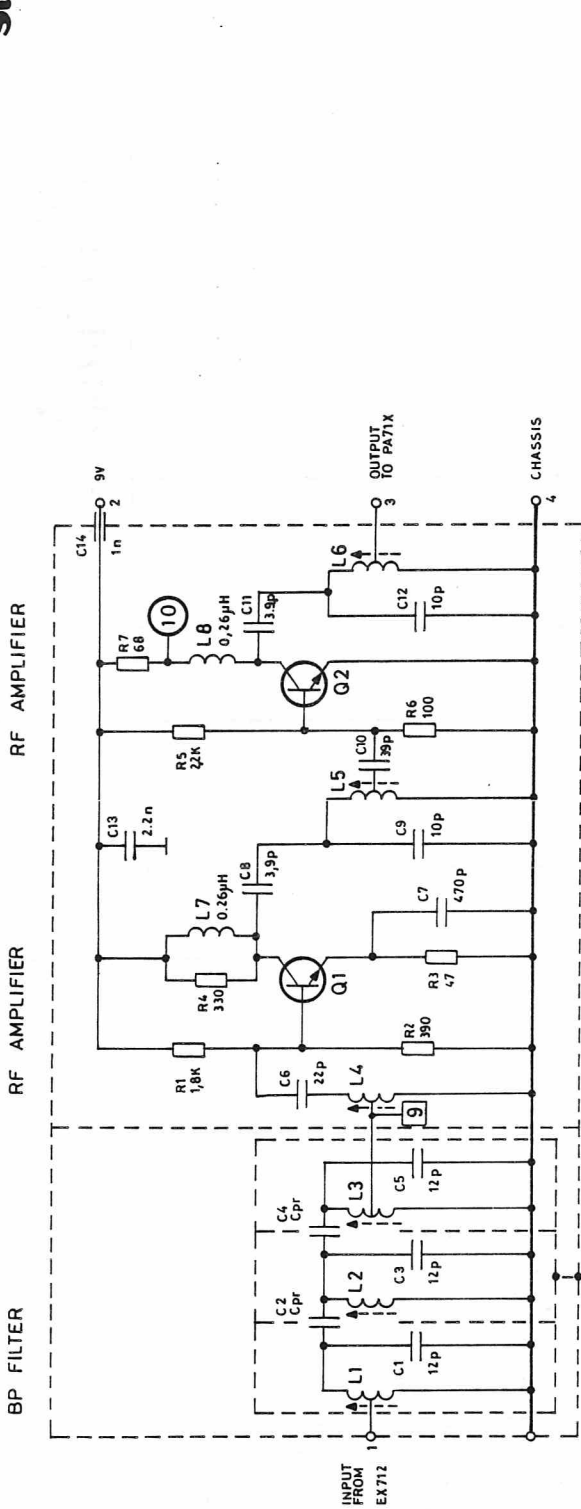
PS704

X402. 397



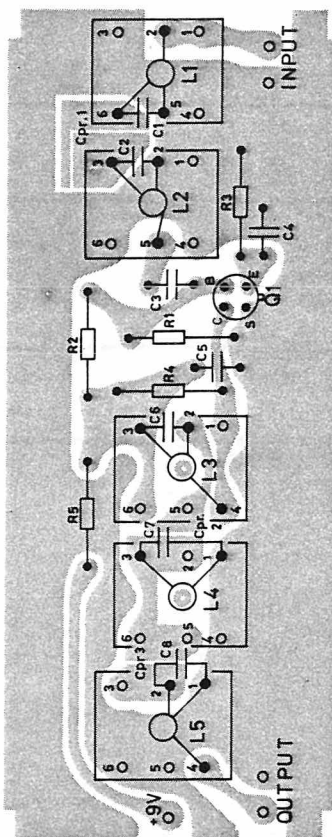
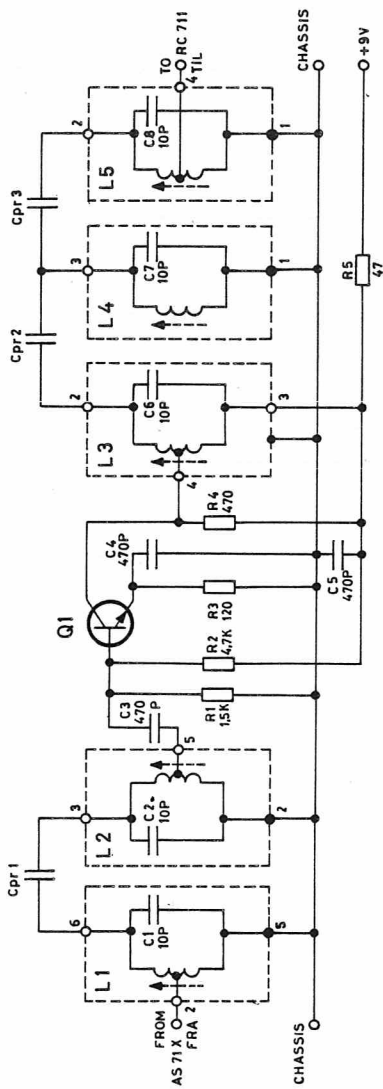
POWER SUPPLY
 STRØMFORSYNING PS704

D402.044

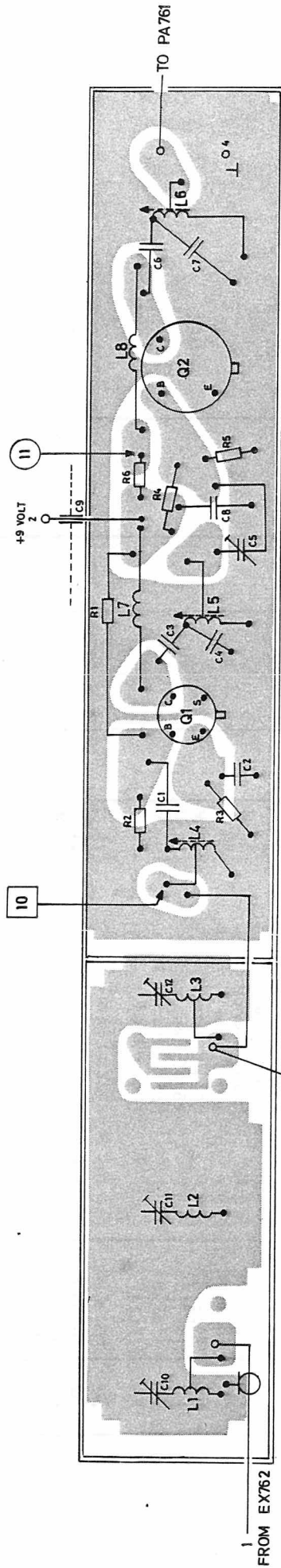
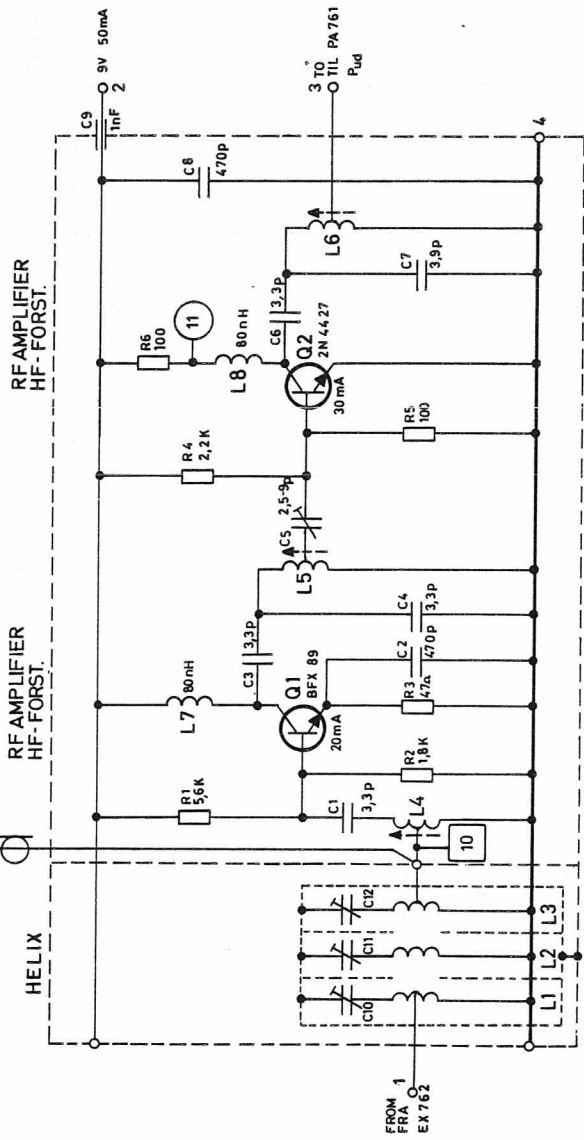


RF AMPLIFIER RA711
HF FORSTÆRKER

D401.84.8/2



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE



RF AMPLIFIER
HF FORSTÆRKER

RA761

Storno

Storno

TYPE	NO.	CODE	DATA
RA761		10.2925	RF Amplifier
	C1	74.5129	3.3 pF ± 0.25 pF ceram DI
	C2	74.5162	470 pF-20+50% ceram DI
	C3	74.5129	3.3 pF ± 0.25 pF ceram DI
	C4	74.5129	3.3 pF ± 0.25 pF ceram DI
	C5	78.5055	2.5 - 9 pF trimmer
	C6	74.5129	3.3 pF ± 0.25 pF ceram DI
	C7	74.5130	3.9 pF ± 0.25 pF ceram DI
	C8	74.5161	470 pF-20 +80% ceram PL
	C9	74.5198	1 nF -20+50% ceram FT
	R1	80.5058	5.6 KΩ 5% carbon film
	R2	80.5052	1.8 KΩ 5%
	R3	80.5033	47 Ω 5%
	R4	80.5053	2.2 KΩ 5%
	R5	80.5037	100Ω 5%
	R6	80.5237	100 Ω 5%
	L1	61.	Helix coil 420-470 MHz
	L2	61.	Helix Coil 420-470 MHz
	L3	61.	Helix Coil 420-470 MHz
	L4	61.1223	RF-Coil 420-470 MHz
	L5	61.1224	RF Coil 420-470 MHz
	L6	61.1224	RF Coil 420-470 MHz
	L7	62.0651	0.08 μH RF choke
	L8	62.0651	0.08 μH RF choke
	Q1	99.5240	BFX89 Transistor
	Q2	99.5229	2N4427 Transistor

TYPE NO. CODE DATA

RF AMPLIFIER
HF FORSTÆRKER

RA761

X 401.860

Storno

The schematic diagram shows the RF amplifier section, divided into three main stages:

- HELIX:** The input stage, featuring a helix resonator with components L1, L2, L3, C10, C11, and C12. It is connected to terminals 1 and 2.
- RF AMPLIFIER HF-FORST (First Stage):** The first amplification stage, centered around a 20mA BFX 89 tube (Q1). It includes a 5.6K resistor (R1), an 80nH inductor (L7), a 3.3pF capacitor (C3), a 1.8K resistor (R2), a 470pF capacitor (C2), a 470pF capacitor (C4), a 3.3pF capacitor (C1), and a 3.3pF capacitor (L4). It is connected to terminal 10.
- RF AMPLIFIER HF-FORST (Second Stage):** The second amplification stage, centered around a 30mA 2N4427 tube (Q2). It includes a 2.2K resistor (R4), an 80nH inductor (L8), a 3.3pF capacitor (C6), a 3.3pF capacitor (C7), a 470pF capacitor (C8), and a 3.3pF capacitor (L6). It is connected to terminal 4.

Additional components include a 1nF capacitor (C9) connected to a 9V 50mA source, and a 3 TO 0111 PA761 output stage connected to terminal 3.

Storno

The schematic diagram shows the PA761 output stage, including a +9VOLT source connected to terminal 11. The stage is divided into two main sections:

- Driver Stage:** Features a 5S tube (Q1) with a 1.8K resistor (R2), a 470pF capacitor (C1), a 470pF capacitor (C2), a 3.3pF capacitor (C3), a 3.3pF capacitor (L5), a 3.3pF capacitor (C4), a 3.3pF capacitor (L7), a 3.3pF capacitor (R1), and a 3.3pF capacitor (C5). It is connected to terminal 10.
- Output Stage:** Features a 30mA 2N4427 tube (Q2) with an 80nH inductor (L8), a 3.3pF capacitor (C6), a 3.3pF capacitor (C7), a 470pF capacitor (C8), and a 3.3pF capacitor (L6). It is connected to terminal 4.

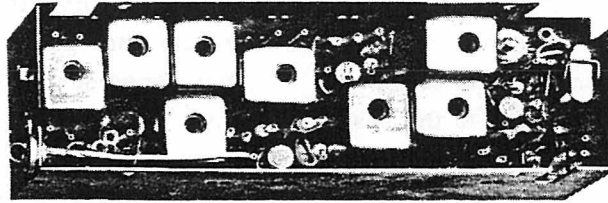
The output stage is connected to a 3 TO 0111 PA761 output stage, which is connected to terminal 3. The output is connected to a 10.4 ohm load.

RF AMPLIFIER
HF FORSTÆRKER

RA761

D401.778/2

RECEIVER CONVERTER RC711



Description

General

The RC711 consists of an oscillator/tripler stage, two frequency doublers and a mixer; it receives the incoming antenna signal from the band-pass filter BP711, and its output works into the 10.7 MHz crystal filter found in the input of the IF converter, IC700.

This unit is designed for use in equipment belonging to the CQM700 series and operating in the frequency range of 146 to 174 MHz. The receiver converter, as its name implies, converts the receiver VHF frequencies to 10.7 MHz, which is the first intermediate frequency. To suppress spurious radiation the unit is enclosed in a metal shielding.

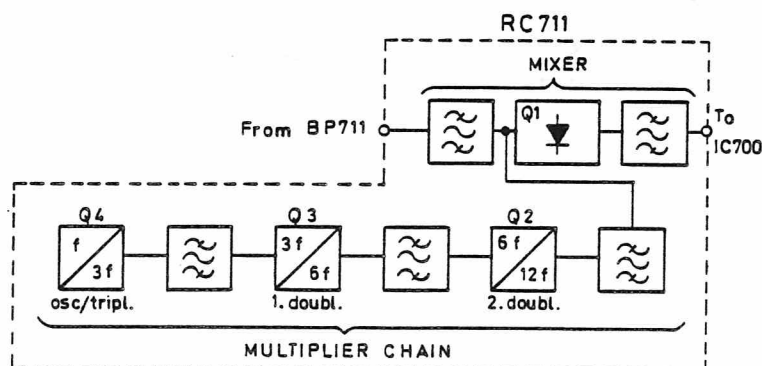
The Oscillator and Frequency Multiplier Stages

The oscillator included in the RC stage is sufficient for single channel service, but multi-channel operation requires a separate oscilla-

tor for each additional channel. These are to be found in the XS701 module. A function of the channel switch causes any oscillator signal selected from XS701 to be fed directly to the collector circuit of Q4 via the p-c board terminal connection. Of course, when an oscillator in XS701 is operating, the oscillator in RC711 is made inoperative by disconnecting its emitter return through the channel switch. For single channel operation the emitter of Q4 will be tied to chassis ground as shown on the schematic diagram.

The LC circuit incorporating L7 in the collector of oscillator Q4 is tuned to the 3rd harmonic of the oscillator frequency(ies), as is the tuned circuit of L8 which forwards the signal to the base of Q3.

Two tuned circuits are required to suppress spurious frequencies since the composite product of the 14th harmonic of the oscillator frequency lies within the radiotelephone's VHF pass-band.



The signal is amplified in Q3 and here the LC circuit incorporating L6 in its collector is tuned to the 2nd harmonic of the signal at its base. This, then, is the first doubler. The resistor in series with the collector ensures circuit stability.

The signal is taken off from the joint of the capacitive divider network and fed to the base of Q2, the second frequency doubler. Again, the collector circuit is tuned to the 2nd harmonic of the signal at the base. The signal available to the mixer stage, Q1, is 12 times the frequency of the oscillator.

Three tuned circuits are employed between the collector of Q2 and the mixer gate; L5, L4, and L3. High selectivity is necessary here as spurious signals from the frequency multipliers can otherwise have an effect on the mixer sensitivity.

The transistor types employed were selected because of their high gain characteristics and, at the same time, minimum noise figure.

When checking the drive voltage to the transistors the collector current is used as an indication of drive signal level (an increase in drive signal results in an increase in collector current).

The Mixer

The antenna signal is applied to the gate of the J-FET transistor, Q1, through the matching network, L1, which is designed for negligible insertion loss and whereby the matching to the mixer is accomplished so as to achieve the best possible noise figure.

A field-effect transistor, having good intermodulation and blocking characteristics, is used as the mixer.

The capacitor inserted between Q1's drain and ground is to improve circuit gain and stability. The capacitor is intended to make up a series resonant trap at the antenna frequency.

The output circuit, L2, is tuned to 10.7 MHz and the inductance is tapped down to match the impedance of the crystal filter in the IC700 input.

Technical Specifications

Frequency Range

146 to 174 MHz

Bandwidth

Input circuit: 15 MHz

output circuit: 0.3 MHz

Multiplier (at the output frequency): 1.5 MHz

Impedances

Nominal input impedance at L1: 50 Ω

Output impedance at L2: 910 Ω 20 pF

Oscillator Frequency

$$f_x = \frac{f_s - 10.7}{12} : 11.3 \text{ to } 13.6 \text{ MHz}$$

Frequency Multiplication Factor

3 x 2 x 2 : 12 times

Supply Voltage

Nominal: + 9 V

Current Consumption

20 mA

Ambient Temperature Range

operating range: -25° to $+65^{\circ}$ C

functioning range: -30° to $+75^{\circ}$ C

Mechanical Dimensions

Width = 28 mm, length = 92 mm, height = 24 mm

Weight

40 g

Storno

TYPE	NO.	CODE	DATA
RC711		10.2557	Receiver Converter
	C1	74.5131	4.7 pF ±0.25 pF ceram DI
	C2	74.5109	10 nF -20 +80% ceram PL
	C3	74.5117	39 pF 5% ceram TB
	C4	74.5133	6.8 pF ±0.25pF ceram DI
	C5	74.5109	10 nF -20 +80% ceram PL
	C6	74.5111	56 pF 5% ceram TB
	C7	76.5103	150 pF 2.5% polystyr. TB
	C8	74.5134	8.2 pF ±0.25 pF ceram DI
	C9	74.5134	8.2 pF ±0.25 pF ceram DI
	C10	74.5133	6.8 pF ±0.25 pF ceram DI
	C12	74.5155	1 nF -20 +80% ceram PL
	C13	74.5137	15 pF 5% ceram DI
	C14	74.5111	56 pF 5% ceram TB
	C15	74.5116	33 pF 5% ceram TB
	C16	74.5161	470 pF -20 +80% ceram PL
	C17	74.5109	10 nF -20 +80% ceram PL
	C18	76.5103	150 pF 2.5% polystyr TB
	C19	74.5116	33 pF 5% ceram TB
	C20	74.5116	33 pF 5% ceram TB
	C21	76.5059	2.2 nF 10% polyester FL
	C22	76.5061	4.7 nF 10% polyester FL
	C23	76.5102	100 pF 2.5% polystyr TB
	C24	76.5106	470 pF 2.5%
	C25	76.5059	2.2 nF 10% polyester FL
	C26	74.5191	33 pF 5% ceram TB
	C27	78.5044	2-18 pF trimmer
	C28	74.5135	10 pF 5% ceram DI
	R1	80.5255	3.3 kΩ 5% carbon film
	R2	80.5243	330 Ω 5%
	R3	80.5237	100 Ω 5%
	R4	80.5271	68 kΩ 5%
	R5	80.5259	6.8 kΩ 5%
	R6	80.5237	100 Ω 5%
	R7	80.5237	100 Ω 5%
	R8	80.5237	100 Ω 5%
	R9	80.5273	0.1 MΩ 5%
	R10	80.5263	15 kΩ 5%
	R11	80.5237	100 Ω 5%
	R12	80.5247	680 Ω 5%
	R13	80.5237	100 Ω 5%
	R14	80.5243	330 Ω 5%
	R15	80.5265	22 kΩ 5%
	R16	80.5262	12 kΩ 5%

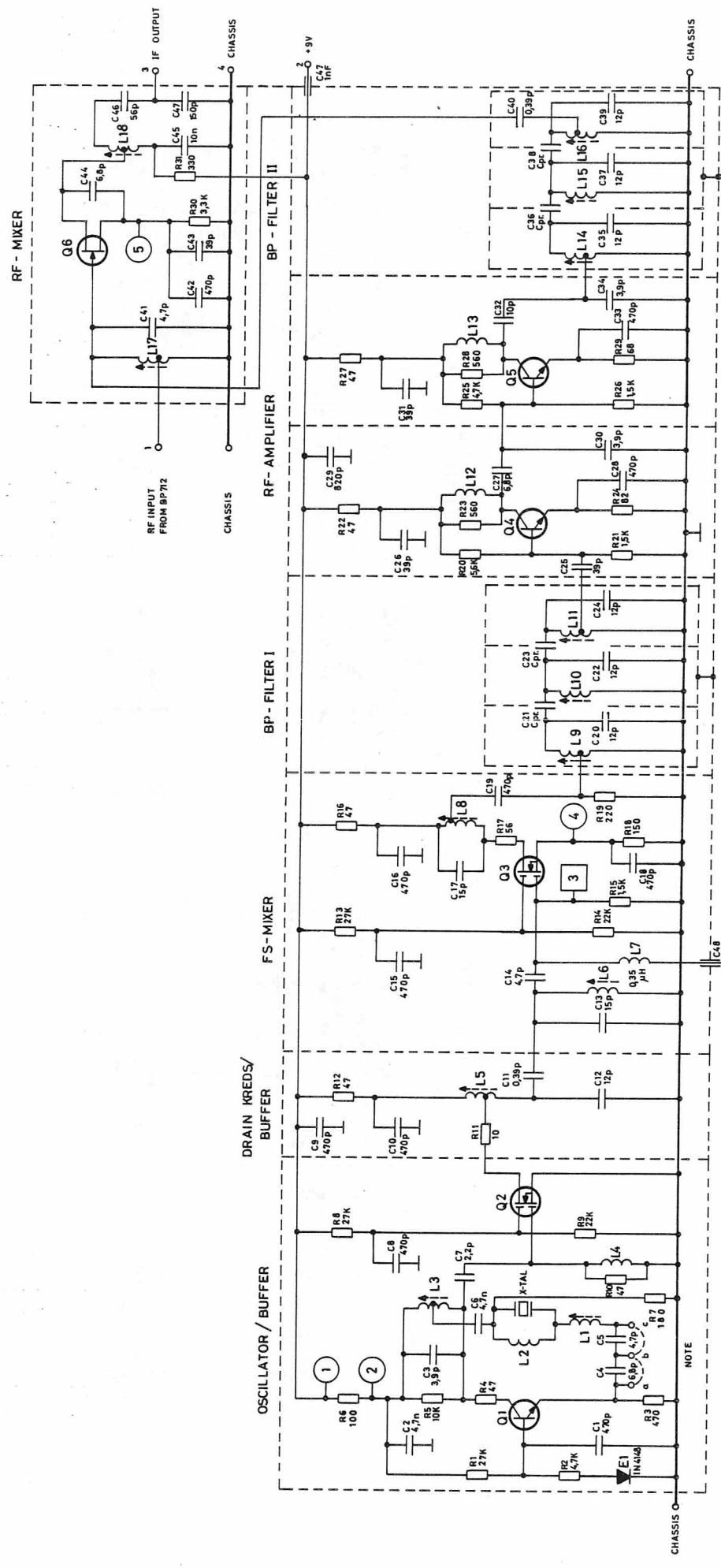
Storno

TYPE	NO.	CODE	DATA
	L1	61.1142	RF coil 146-174 MHz
	L2	61.1143	IF coil 10.7 MHz
	L3	61.1144	RF coil 135.3 - 163.3 MHz
	L4	61.1144	RF coil 135.3 - 163.3 MHz
	L5	61.1146	RF coil 135.3 - 163.3 MHz
	L6	61.1147	RF coil 67.65 - 81.65 MHz
	L7	61.1145	RF coil 33.8 - 40.8 MHz
	L8	61.1149	RF coil 33.8 - 40.8 MHz
	Q1	99.5245	2N5245 Transistor J-FET
	Q2	99.5217	2N918 Transistor
	Q3	99.5168	BF173 Transistor
	Q4	99.5139	BSX19 Transistor

**RECEIVER CONVERTER
MODTAGERKONVERTER**

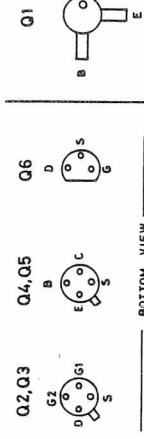
RC711

X401.382



NOTE:

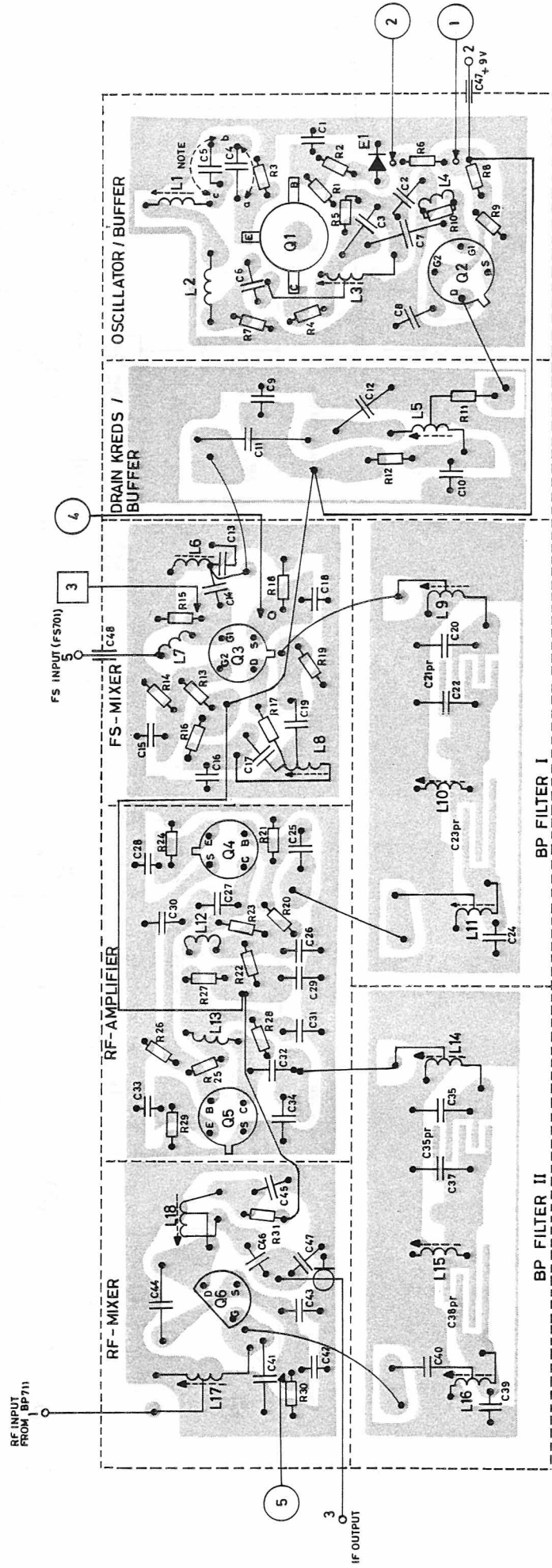
FREQUENCY FREKVENNS	STRAP STRÄPPNING
UP / OP NORMAL	NONE / INGEN a-b
DOWN / NED	b-c



RECEIVER CONVERTER RC712
MODTAGGERKONVERTER

D401.846/2

BOTTOM VIEW



RECEIVER CONVERTER RC712
MODTAGERKONVERTER

D401976

TYPE	NO.	CODE	DATA
RC712		10.2935	Receiver Converter
	C1	74.5162	ceram DI 400V
	C2	74.5108	ceram PL 20V
	C3	74.5302	ceram PL 63V
	C4	74.5321	ceram PL 100V
	C5	74.5318	ceram PL 20V
	C6	74.5108	ceram PL 63V
	C7	74.5299	ceram PL 63V
	C8	74.5161	ceram DI 400V
	C9	74.5162	ceram DI 400V
	C10	74.5162	ceram BD 250V
	C11	74.5120	ceram DI 250V
	C12	74.5136	ceram DI 250V
	C13	74.5137	ceram DI 250V
	C14	74.5131	ceram DI 250V
	C15	74.5162	ceram DI 400V
	C16	74.5162	ceram DI 400V
	C17	74.5137	ceram DI 250V
	C18	74.5162	ceram DI 400V
	C19	74.5161	ceram PL 63V
	C20	74.5308	ceram PL 63V
	C21	74.5308	ceram PL 63V
	C22	74.5308	ceram PL 63V
	C23	74.5308	ceram PL 63V
	C24	74.5308	ceram PL 63V
	C25	74.5316	ceram PL 63V
	C26	74.5316	ceram PL 63V
	C27	74.5305	ceram PL 63V
	C28	74.5162	ceram DI 400V
	C29	74.5314	ceram PL 63V
	C30	74.5302	ceram PL 63V
	C31	74.5316	ceram PL 63V
	C32	74.5307	ceram PL 63V
	C33	74.5162	ceram DI 400V
	C34	74.5302	ceram PL 63V
	C35	74.5308	ceram PL 63V
	C36	74.5308	ceram PL 63V
	C37	74.5308	ceram PL 63V
	C38	74.5308	ceram PL 63V
	C39	74.5120	ceram PL 63V
	C40	74.5131	ceram BD 250V
	C41	74.5131	ceram BD 250V
	C42	74.5162	ceram DI 400V
	C43	74.5117	ceram TB160V
	C44	74.5133	ceram BD250V
	C45	74.5109	ceram PL 20V

TYPE	NO.	CODE	DATA
	C46	74.5111	56pF 5%
	C47	76.5103	150pF 2.5%
	C48	74.5323	47pF 20%
	C49	74.5198	1nF -20/+50%
	R1	80.5066	27 KΩ 5%
	R2	80.5057	4.7 KΩ 5%
	R3	80.5045	470 Ω 5%
	R4	80.5033	47 Ω 5%
	R5	80.5061	10 KΩ 5%
	R6	80.5237	100 Ω 5%
	R7	80.5041	220 Ω 5%
	R8	80.5066	27 KΩ 5%
	R9	80.5065	22 KΩ 5%
	R10	80.5033	47 Ω 5%
	R11	80.5025	10 Ω 5%
	R12	80.5233	47 Ω 5%
	R13	80.5066	27 Ω 5%
	R14	80.5065	22 KΩ 5%
	R15	80.5051	1.5 KΩ 5%
	R16	80.5033	47 Ω 5%
	R17	80.5034	56 Ω 5%
	R18	80.5039	150 Ω 5%
	R19	80.5041	220 Ω 5%
	R20	80.5058	5.6 KΩ 5%
	R21	80.5051	1.5 KΩ 5%
	R22	80.5033	47 Ω 5%
	R23	80.5054	560 Ω 5%
	R24	80.5036	82 Ω 5%
	R25	80.5057	4.7 KΩ 5%
	R26	80.5051	1.5 KΩ 5%
	R27	80.5033	47 Ω 5%
	R28	80.5046	560 Ω 5%
	R29	80.5035	68 Ω 5%
	R30	80.5243	330 Ω 5%
	R31	80.5255	3.3 KΩ 5%
	L1	61.1234	RF coil
	L2	61.1230	RF coil
	L3	61.1229	RF coil 119 - 159 MHz
	L4	61.1231	RF choke (R10)

**RECEIVER CONVERTER
MODTAGERKONVERTER**

RC712

X401.942/2

Storno

TYPE	NO.	CODE	DATA
L5		61.1253	RF coil
L6		61.1252	RF coil
L7		62.0659	0.35 μ H RF choke
L8		61.1251	RF coil
L9		61.1250	RF coil
L10		61.1249	RF coil
L11		61.1248	RF coil
L12		62.0651	0.08 μ H RF choke
L13		62.0651	0.08 μ H RF choke
L14		61.1250	RF coil
L15		61.1249	RF coil
L16		61.1247	RF coil
L17		61.1246	RF coil 146-174 MHz
L18		61.1117	IF coil 10.7 MHz
E1		99.5237	1N4148 Diode
Q1		99.5290	BFR90 Transistor
Q2		99.5291	3N205 Transistor FET
Q3		99.5291	3N205 Transistor FET
Q4		99.5240	BFX89 Transistor
Q5		99.5240	BFX89 Transistor
Q6		99.5245	2N5245 Transistor J-FET

Storno

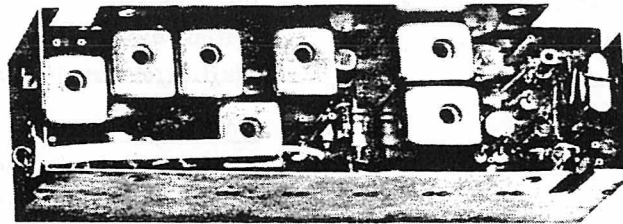
TYPE	NO.	CODE	DATA
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RECEIVER CONVERTER
MODTAGERKONVERTER

RC712

X401.942

RECEIVER CONVERTER RC731



Description

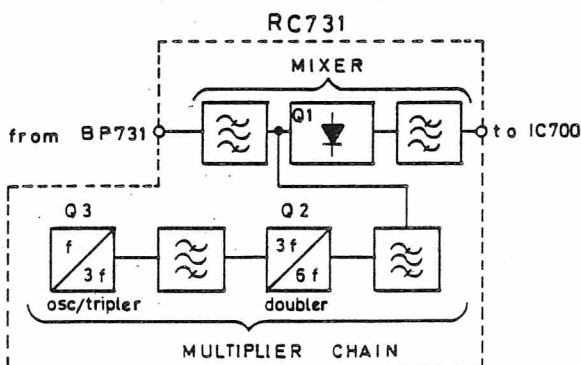
General

The RC731 consists of an oscillator/tripler stage, a frequency doubler and a mixer; it receives the incoming antenna signal from the band-pass filter BP731 and its output works into the 10.7 MHz crystal filter found in the input of the IF converter, IC700.

This unit is designed for use in equipment belonging to the CQM700 series and operating in the frequency range of 68 to 88 MHz. The receiver converter, as its name implies, converts the receiver VHF frequencies to 10.7 MHz, which is the first intermediate frequency. To suppress spurious radiation the unit is enclosed in a metal shielding.

The Oscillator and Frequency Multiplier Stages

The oscillator included in the RC stage is sufficient for single channel service, but multichannel operation requires a separate oscillator for each additional channel.



These are to be found in the XS701 module. A function of the channel switch causes any oscillator signal selected from XS701 to be fed directly to the collector circuit of Q3 via the p-c board terminal connection. Of course, when an oscillator in XS701 is operating, the oscillator in RC731 is made inoperative. This is done by disconnecting its emitter return through the channel switch. For single channel operation the emitter of Q3 will be tied to chassis ground as shown on the schematic diagram.

The LC circuit incorporating L6 in the collector of oscillator Q3 is tuned to the 3rd harmonic of the oscillator frequency(ies), as is the tuned circuit of L7 which forwards the signal to the base of Q2.

Two tuned circuits are required to suppress spurious frequencies since the composite product of the 8th harmonic of the oscillator frequency lies within the radiotelephone's VHF pass-band.

The signal is amplified in Q2 and here the LC circuit incorporating L5 in its collector is tuned to the 2nd harmonic of the signal at its base. This is the doubler. The signal available to the mixer, Q1, is 6 times the frequency of the oscillator.

Three tuned circuits are employed between the collector of Q2 and the mixer gate; L5, L4, and L3. High selectivity is necessary here as spurious signals from the frequency multipliers can otherwise have an effect on the mixer sensitivity.

The transistor types employed were selected because of their high gain characteristics and, at the same time, minimum noise figure.

When checking the drive voltage to the transistors the collector current is used as an indication of drive signal level (an increase in drive signal results in an increase in collector current).

The Mixer

The antenna signal is applied to the gate of the J-FET transistor, Q1, through the matching network, L1, which is designed for negligible insertion loss and whereby the matching to the mixer is accomplished so as to achieve the best possible noise figure.

A field-effect transistor, having good intermodulation and blocking characteristics, is used as the mixer.

The capacitor inserted between Q1's drain and source is to improve circuit gain and stability. The capacitor is intended to make up a series resonant trap at the antenna frequency.

The output circuit, L2, is tuned to 10.7 MHz and the inductance is tapped down to match the impedance of the crystal filter in the IC700 input.

Technical Specifications

Frequency Range

68 to 88 MHz

Bandwidth

Input circuit L1: 5 MHz

Output circuit L2: 0.3 MHz

Multiplier (at the output frequency: 1.2 MHz)

Impedances

Nominal input impedance at L1: 50 Ω

Output impedance at L2: 910 Ω // 20 pF

Oscillator Frequency

$f_x = \frac{f_s - 10.7}{6}$: 9.55 to 12.9 MHz

Frequency Multiplication Factor

$3 \times 2 = 6$ times

Supply Voltage

Nominal: + 9 V

Current Consumption

15 mA

Ambient Temperature Range

Operating range: -25° to $+65^{\circ}$ C

Functioning range: -30° to $+75^{\circ}$ C

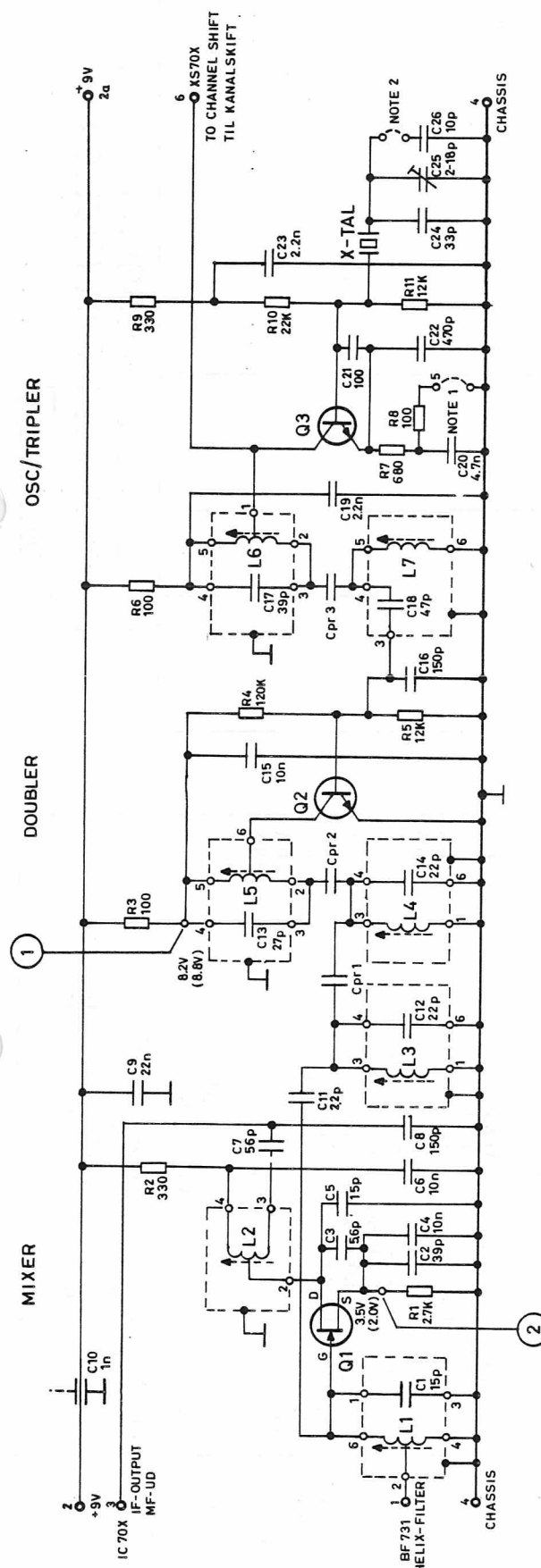
Mechanical Dimensions

width = 28 mm, length = 92 mm,

length = 24 mm

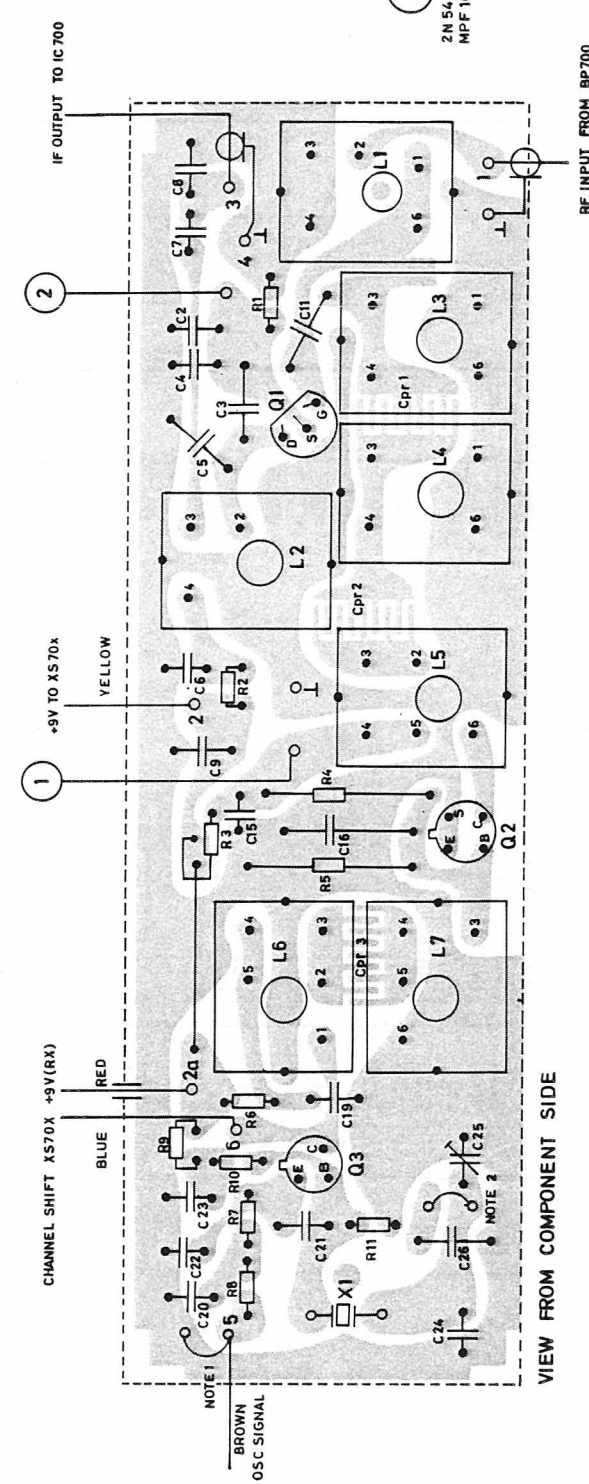
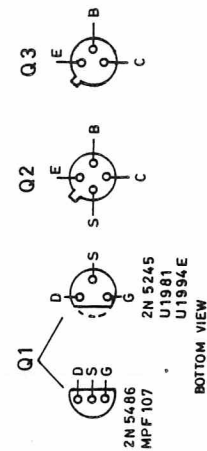
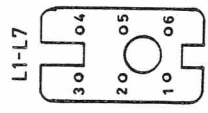
Weight

40 g



Cpr 1 - 3 printed capacitors
 DC voltages without paranthesis measured with signal
 DC voltages with paranthesis measured without signal

Note 1: Strap for 1 channel
 Note 2: Insert strap to extend lower frequency pulling range



RECEIVER CONVERTER
 MODTAGERKONVERTER

RC731

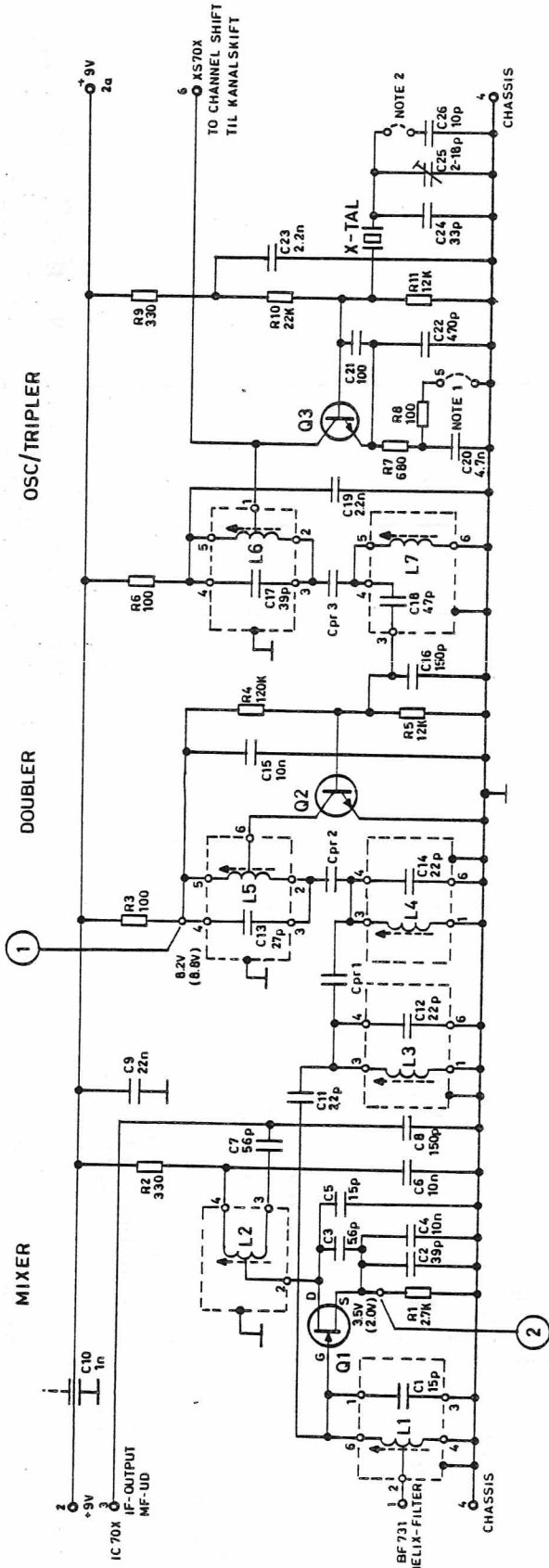
D401.341/3

TYPE	NO.	CODE	DATA
RC731		10.2631-00	RECEIVER CONVERTER
	C1	74.5105	15pF 5% ceram TB 160V
	C2	74.5117	39pF 5% ceram TB 160V
	C3	74.5132	5.6pF ±0.25pF ceram DI 250V
	C4	74.5109	10nF -20/+80% ceram PL 20V
	C5	74.5137	15pF 5% ceram TB 160V
	C6	74.5109	10nF -20/+80% ceram PL 20V
	C7	74.5111	56pF 5% ceram TB 160V
	C8	76.5103	150pF 2.5% polystyr TB 25V
	C9	76.5071	22nF 10% polystyr FL 50V
	C10	74.5198	1nF -20/+50% ceram FT 30V
	C11	74.5127	2.2pF ±0.25pF ceram DI 250V
	C12	74.5106	22pF 5% ceram TB 160V
	C14	74.5106	22pF 5% ceram TB 160V
	C15	74.5109	10nF -20/+80% PL 20V
	C16	76.5103	150pF 2.5% polystyr TB 25V
	C17	74.5117	39pF 5% ceram TB 160V
	C18	74.5118	47pF 5% ceram TB 160V
	C19	76.5059	2.2nF 10% polvest. FL 50V
	C20	76.5061	4.7nF 10% polvest. FL 50V
	C21	76.5102	100pF 2.5% polystyr TB 25V
	C22	76.5106	470pF 2.5% polystyr TB 25V
	C23	76.5059	2.2nF 10% polvest. FL 50V
	C24	74.5191	33pF 5% ceram TB 160V
	C25	78.5044	2-18pF trimmer 300V
	C26	74.5135	10pF 5% ceram DI 125V
	R1	80.5254	2.7kΩ 5% carbon film 1/8W
	R2	80.5243	330Ω 5% carbon film 1/8W
	R3	80.5237	100Ω 5% carbon film 1/8W
	R4	80.5274	0.12MΩ 5% carbon film 1/8W
	R5	80.5262	12kΩ 5% carbon film 1/8W
	R6	80.5237	100Ω 5% carbon film 1/8W
	R7	80.5247	680Ω 5% carbon film 1/8W
	R8	80.5237	100Ω 5% carbon film 1/8W
	R9	80.5243	330Ω 5% carbon film 1/8W
	R10	80.5265	22kΩ 5% carbon film 1/8W
	R11	80.5262	12kΩ 5% carbon film 1/8W
	L1	61.1159	RF coil 68-88 MHz
	L2	61.1143	IF coil 10.7 MHz
	L3	61.1161	RF coil 57.3-77.3 MHz
	L4	61.1162	RF coil 57.3-77.3 MHz
	L5	61.1163	RF coil 57.3-77.3 MHz
	L6	61.1164	RF coil 28.65-38.65 MHz
	L7	61.1165	RF coil 28.65-38.65 MHz

TYPE	NO.	CODE	DATA
	Q1	99.5245	Transistor 2N5245 FET
	Q2	99.5217	Transistor 2N918
	Q3	99.5139	Transistor BSX19

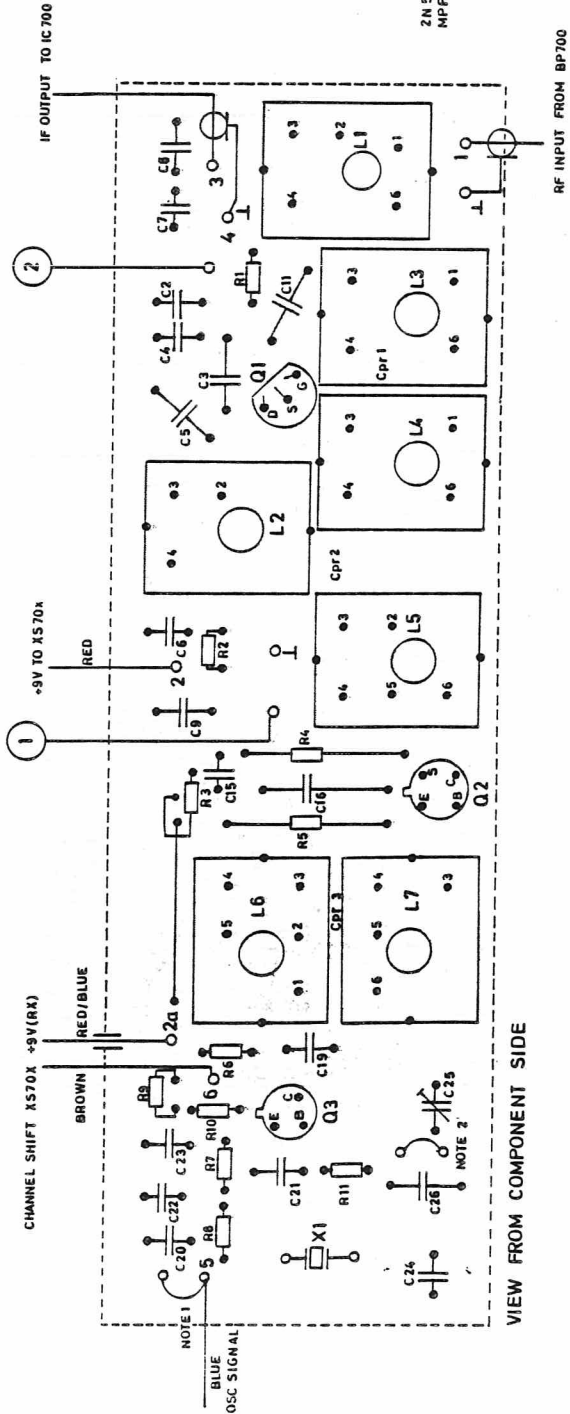
RECEIVER CONVERTER RC731
 MODTAGERKONVERTER

X401.537



Cpr 1 - 3 printed capacitors
 DC voltages without paranthesis
 measured with signal
 DC voltages with paranthesis
 measured without signal

Note 1: Strap for 1 channel
 Note 2: Insert strap to extend lower
 frequency pulling range



RECEIVER CONVERTER
 MODTAGERKONVERTER

RC731

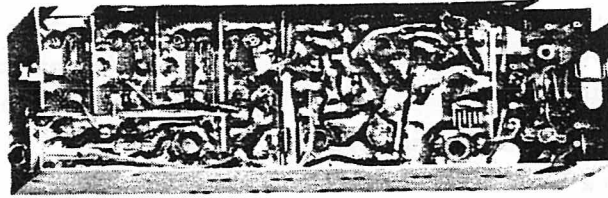
D4013A12

TYPE	NO.	CODE	DATA
RC731		10.2631-00	RECEIVER CONVERTER
	C1	74.5105	15pF 5% ceram TB 160V
	C2	74.5117	39pF 5% ceram TB 160V
	C3	74.5132	5.6pF ± 0.25pF ceram DI 250V
	C4	74.5109	10nF -20/+80% ceram PL 20V
	C5	74.5137	15pF 5% ceram TB 160V
	C6	74.5109	10nF -20/+80% ceram PL 20V
	C7	74.5111	56pF 5% ceram TB 160V
	C8	76.5103	150pF 2.5% polystyr TB 25V
	C9	76.5071	22nF 10% polystyr FL 50V
	C10	74.5198	1nF -20/+50% ceram FT 30V
	C11	74.5127	2.2pF ± 0.25pF ceram DI 250V
	C12	74.5106	22pF 5% ceram TB 160V
	C14	74.5106	22pF 5% ceram TB 160V
	C15	74.5109	10nF -20/+80% PL 20V
	C16	76.5103	150pF 2.5% polystyr TB 25V
	C17	74.5117	39pF 5% ceram TB 160V
	C18	74.5118	47pF 5% ceram TB 160V
	C19	76.5059	2.2nF 10% polyest. FL 50V
	C20	76.5061	4.7nF 10% polyest. FL 50V
	C21	76.5102	100pF 2.5% polystyr TB 25V
	C22	76.5106	470pF 2.5% polystyr TB 25V
	C23	76.5059	2.2nF 10% polyest. FL 50V
	C24	74.5191	33pF 5% ceram TB 160V
	C25	78.5044	2-18pF trimmer 300V
	C26	74.5135	10pF 5% ceram DI 125V
	R1	80.5254	2.7kΩ 5% carbon film 1/8W
	R2	80.5243	330Ω 5% carbon film 1/8W
	R3	80.5237	100Ω 5% carbon film 1/8W
	R4	80.5274	0.12MΩ 5% carbon film 1/8W
	R5	80.5262	12kΩ 5% carbon film 1/8W
	R6	80.5237	100Ω 5% carbon film 1/8W
	R7	80.5247	680Ω 5% carbon film 1/8W
	R8	80.5237	100Ω 5% carbon film 1/8W
	R9	80.5243	330Ω 5% carbon film 1/8W
	R10	80.5265	22kΩ 5% carbon film 1/8W
	R11	80.5262	12kΩ 5% carbon film 1/8W
	L1	61.1159	RF coil 68-88 MHz
	L2	61.1143	IF coil 10.7 MHz
	L3	61.1161	RF coil 57.3-77.3 MHz
	L4	61.1162	RF coil 57.3-77.3 MHz
	L5	61.1163	RF coil 57.3-77.3 MHz
	L6	61.1164	RF coil 28.65-38.65 MHz
	L7	61.1165	RF coil 28.65-38.65 MHz

RECEIVER CONVERTER RC731
 MODTAGERKONVERTER

X401.537

RECEIVER CONVERTER RC761



Description

General

The RC761 consists of an oscillator/tripler stage, another frequency tripler, two frequency doublers and a mixer; it receives the incoming antenna signal from the band-pass filter BP761 and its output works into the 10.7 MHz crystal filter found in the input of the IF converter, IC700.

This unit is designed for use in equipment belonging to the CQM700 series and operating in the frequency range of 420 to 470 MHz. The receiver converter, as its name implies, converts the receiver UHF frequencies to 10.7 MHz, which is the first intermediate frequency. To suppress spurious radiation the unit is enclosed in a metal shielding.

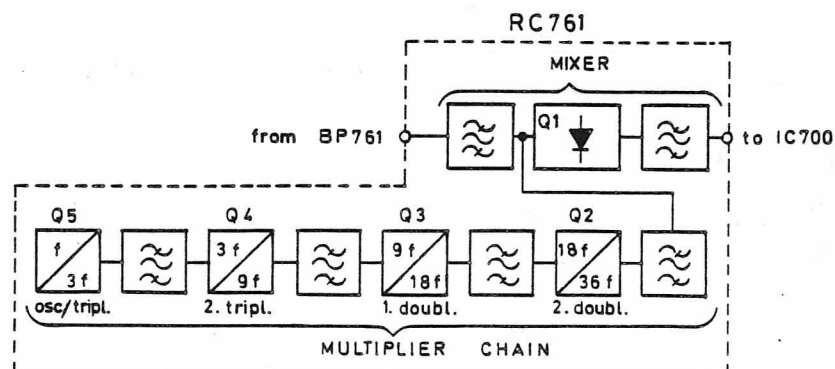
The Oscillator and Frequency Multiplier Stages.

The oscillator included in the RC stage is sufficient for single channel service, but multichannel operation requires a separate

oscillator for each additional channel. These are to be found in the XS701 module. A function of the channel switch causes any oscillator signal selected from XS701 to be fed directly to the collector circuit of Q5 via the p-c board terminal connection. Of course, when an oscillator in XS701 is operating, the oscillator in RC711 is made inoperative by disconnecting its emitter return through the channel switch. For single channel operation the emitter of Q5 will be tied to chassis ground as shown on the schematic diagram.

The LC circuit incorporating L8 in the collector of oscillator Q5 is tuned to be 3rd harmonic of the oscillator frequency(ies), as is the tuned circuit of L9 which forwards the signal to the base of Q4.

Two tuned circuits are required to suppress spurious frequencies since the composite product of 38th harmonic of the oscillator frequency lies within the radiotelephone's VHF pass-band.



The LC circuit of L7, C26 and C27 is tuned to the third harmonic of the signal applied to and amplified in Q4. The signal, now at 9 times the oscillator frequency, is fed to base of Q3. The signal take off point is at the junction of the capacitors. The resistor in series with the collector ensures circuit stability.

The signal is next amplified in Q3 and here the LC circuit incorporating L6 in its collector is tuned to the 2nd harmonic of the signal at its base. This, then, is the first doubler.

The signal is taken off from the joint of the capacitive divider network and fed to the base of Q2, the second frequency doubler. Again, the collector circuit is tuned to the 2nd harmonic of the signal at the base. The signal available to the mixer stage, Q1, is 36 times the frequency of the oscillator.

Three tuned circuits are employed between the collector of Q2 and the mixer gate; L5, L4, and L3. High selectivity is necessary here as spurious signals from the frequency multipliers can otherwise have an effect on the mixer sensitivity.

The transistor types employed were selected because of their high gain characteristics and, at the same time, minimum noise figure.

When checking the drive voltage to the transistors the collector current is used as an indication of drive signal level (an increase in drive signal results in an increase in collector current).

The mixer

The antenna signal is applied to the gate of the J-FET transistor, Q1, through the matching network, L1, which is designed for negligible insertion loss and whereby the matching to the mixer is accomplished so as to achieve the best possible noise figure.

A field-effect transistor, having good intermodulation and blocking characteristics, is used as the mixer.

Two parallel capacitors placed between drain and source of Q1 improve circuit gain and stability. They make up a series resonant trap at the antenna frequency.

The output circuit, L2, is tuned to 10.7 MHz and the inductance is tapped down to match the impedance of the crystal filter in the IC700 input.

Technical Specifications

Frequency Range

420 to 470 MHz

Bandwidth

Input Circuit: 20 MHz

Output circuit: 0.3 MHz

Multiplier: 4 MHz

Impedances

Nominal input impedance at L1: 50 Ω

Output impedance at L2: 910 Ω // 20 pF

Oscillator Frequency

$$f_x = \frac{f_s - 10.7}{36} = 11.35 \text{ to } 12.75 \text{ MHz}$$

Frequency Multiplication Factor

3 x 3 x 2 x 2 = 36 times

Supply Voltage

Nominal: +9 V

Current Consumption

30 mA

Ambient Temperature Range

Operating range: -25^o to +65^oC

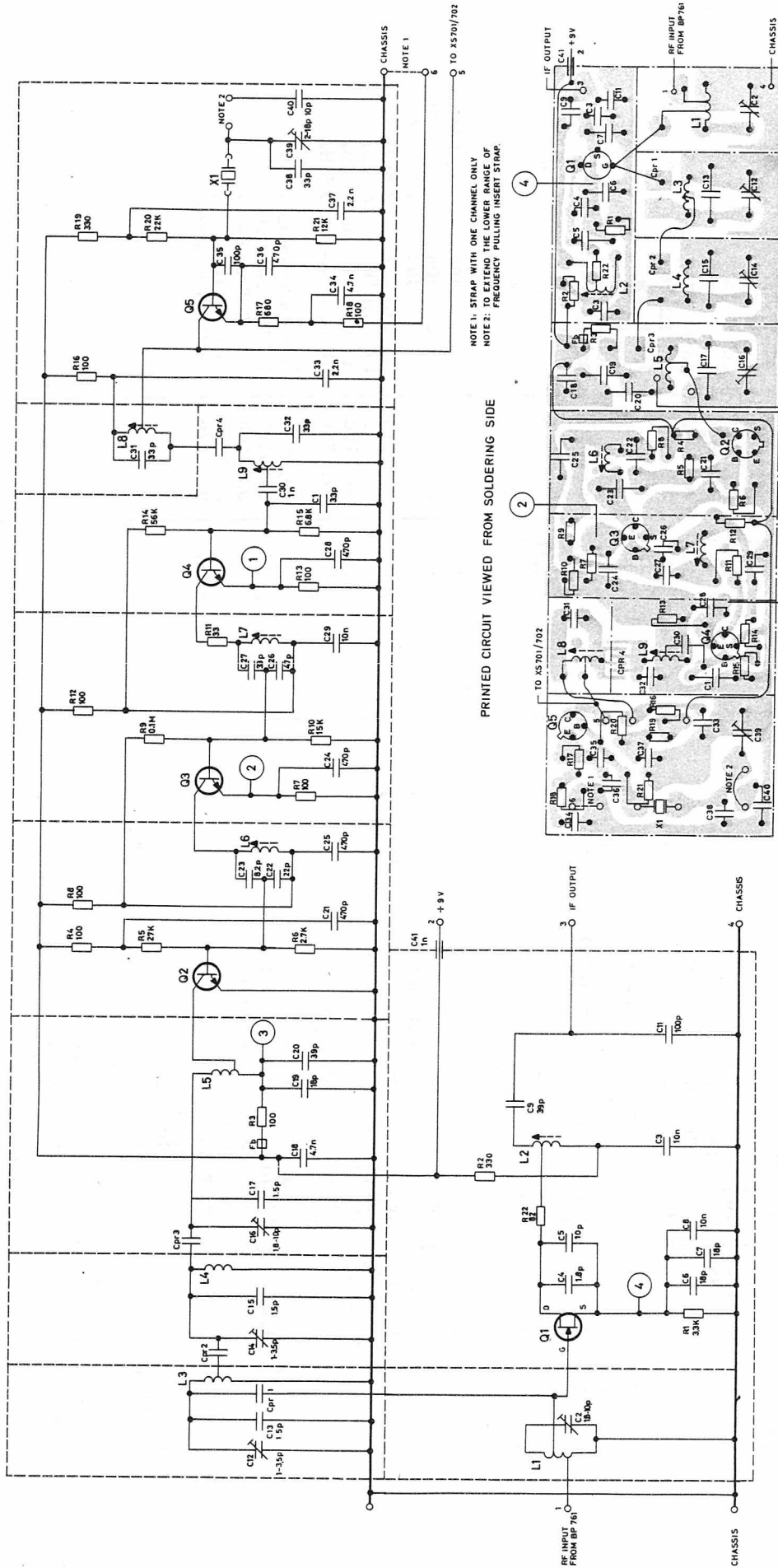
Functioning range: -30^o to +75^oC

Mechanical Dimensions

Width = 29 mm, length = 92 mm,
height = 23.5 mm

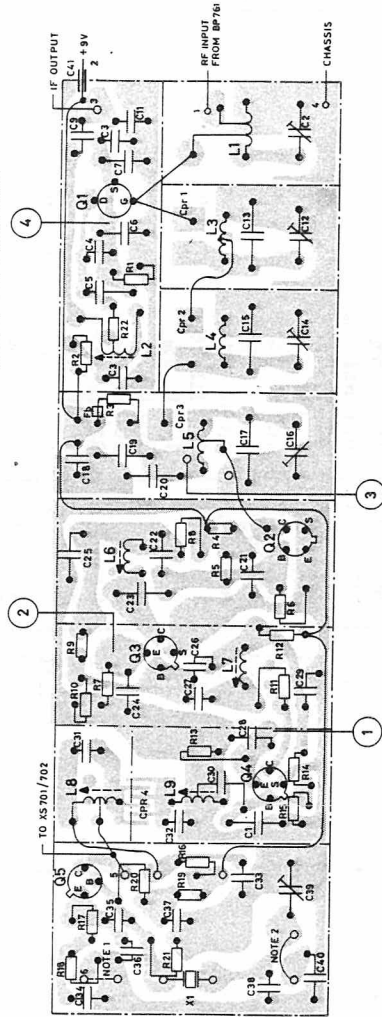
Weight

66 g



NOTE 1: STRAP WITH ONE CHANNEL ONLY
 NOTE 2: TO EXTEND THE LOWER RANGE OF
 FREQUENCY PULLING INSERT STRIP.

PRINTED CIRCUIT VIEWED FROM SOLDERING SIDE



RECEIVER CONVERTER RC761

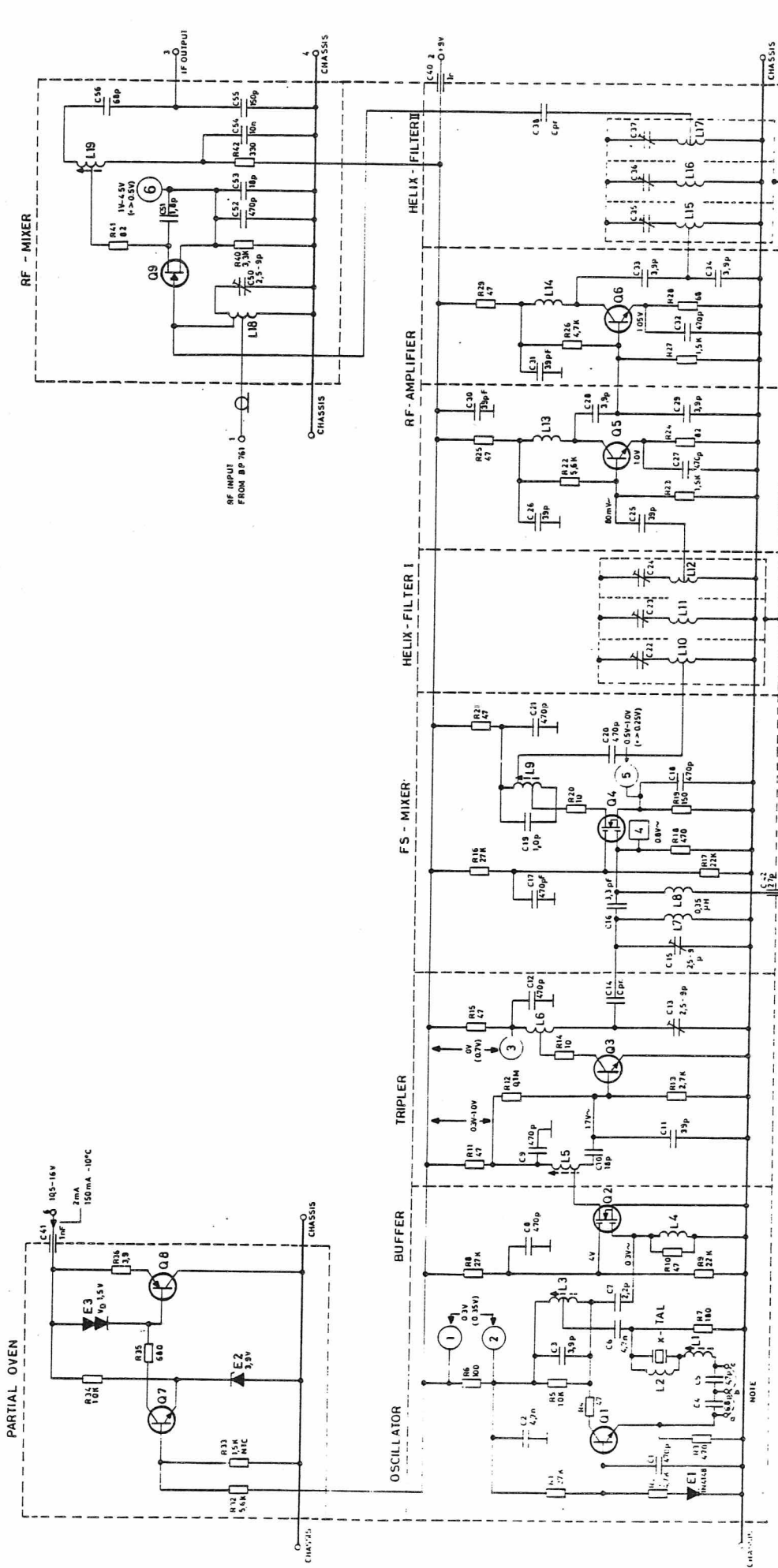
D401.333/2

TYPE	NO.	CODE	DATA
RC761		10.2430	Receiver Converter
	C1	74.5129	3.3 pF ± 0.25 pF ceram DI
	C2	78.5048	1.8 - 10 pF trimmer
	C3	74.5109	10 nF -20 +80% ceram PL
	C4	74.5126	1.8 pF ± 0.25 pF ceram BD
	C5	74.5135	10 pF 5% ceram DI
	C6	74.5138	18 pF 5% ceram DI
	C7	74.5138	18 pF 5% ceram DI
	C8	74.5109	10 nF -20 +80% ceram PL
	C9	74.5195	39 pF 5% ceram TB
	C11	76.5102	100 pF 2.5 pF polystyr TB
	C12	78.5047	1-3.5 pF trimmer
	C13	74.5189	1.5 pF ± 0.25 pF ceram BD
	C14	78.5047	1-3.5 pF trimmer
	C15	74.5189	1.5 pF ± 0.25 pF ceram BD
	C16	78.5048	1.8-10 pF trimmer
	C17	74.5189	1.5 pF ± 0.25 pF ceram BD
	C18	76.5061	4.7 nF 10% polyester, FL
	C19	74.5138	18 pF 5% ceram DI
	C20	74.5117	39 pF 5% ceram TB
	C21	74.5161	470 pF -20 +80% ceram PL
	C22	74.5106	22 pF 5% ceram TB
	C23	74.5134	8.2 pF ± 0.25 pF ceram DI
	C24	74.5161	470 pF -20 +80% ceram PL
	C25	74.5161	470 pF -20 +80% ceram PL
	C26	74.5118	47 pF 5% ceram TB
	C27	74.5116	33 pF 5% ceram TB
	C28	74.5161	470 pF -20 +80% ceram PL
	C29	74.5109	10 nF -20 +80% ceram PL
	C30	74.5155	1 nF -20 +80% ceram PL
	C31	74.5116	33 pF 5% ceram TB
	C32	74.5116	33 pF 5% ceram TB
	C33	76.5059	2.2 nF 10% polyester, FL
	C34	76.5061	4.7 nF 10% polyester, FL
	C35	76.5102	100 pF 2.5% polystyr TB
	C36	76.5106	470 pF 2.5% polystyr TB
	C37	76.5059	2.2 nF 10% polyester, FL
	C38	74.5191	33 pF 5% ceram TB
	C39	78.5044	2-18 pF trimmer
	C40	74.5135	10 pF 5% ceram DI
	C41	74.5198	1 nF -20 +50% ceram FT
	R1	80.5255	3.3 kΩ 5% carbon film
	R2	80.5243	330 Ω 5% " "
	R3	80.5237	100 Ω 5% " "
	R4	80.5237	100 Ω 5% " "

TYPE	NO.	CODE	DATA
	R5	80.5266	27 kΩ 5% carbon film
	R6	80.5254	2.7 kΩ 5% " "
	R7	80.5237	100 Ω 5% " "
	R8	80.5237	100 Ω 5% " "
	R9	80.5273	0.1 MΩ 5% " "
	R10	80.5263	15 kΩ 5% " "
	R11	80.5231	33 Ω 5% " "
	R12	80.5237	100 Ω 5% " "
	R13	80.5237	100 Ω 5% " "
	R14	80.5270	56 kΩ 5% " "
	R15	80.5259	6.8 kΩ 5% " "
	R16	80.5237	100 Ω 5% " "
	R17	80.5247	680 Ω 5% " "
	R18	80.5237	100 Ω 5% " "
	R19	80.5243	330 Ω 5% " "
	R20	80.5265	22 kΩ 5% " "
	R21	80.5262	12 kΩ 5% " "
	R22	80.5036	82Ω 5% " "
	L1	62.0814	RF coil 420 - 470 MHz
	L2	61.1117	IF coil 10.7 MHz
	L3	62.0812	RF coil 409.3 - 459.3 MHz
	L4	62.0815	RF coil 409.3 - 459.3 MHz
	L5	62.0813	RF coil 409.3 - 459.3 MHz
	L6	61.1118	RF coil 204 - 230 MHz
	L7	61.1119	RF coil 102 - 115 MHz
	L8	61.1120	RF coil 34 - 38.5 MHz
	L9	61.1121	RF coil 34 - 38.5 MHz
	Q1	99.5245	2N5245 Transistor FET
	Q2	99.5217	2N918 Transistor
	Q3	99.5168	BF173 Transistor
	Q4	99.5168	BF173 Transistor
	Q5	99.5139	BSX19 Transistor

RECEIVER CONVERTER RC761

X401.332/2

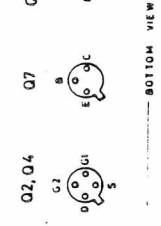


NOTE

FREQ. FNCY	STRAP
UP/OP	NONE/ANGEN
NORMAL	a - b
DOWN/RED	b - c

() MEASURED WITH DRIVE
MULTI MILD SUBSTRING

5.0 0.330mV
INPUT FROM FS 701



BOTTOM VIEW

RECEIVER CONVERTER
MODTAGERKONVERTER

RC762

D.401.785

TYPE	NO.	CODE	DATA
RC762		10.2922	Receiver Converter
	C1	74.5162	470 pF -20+50% ceram DI
	C2	74.5108	4.7 nF -20+80% ceram PL
	C3	74.5302	3.9 pF ± 0.25 pF ceram PL
	C4	74.5321	6.8 pF ± 0.25 pF ceram PL
	C5	74.5318	4.7 pF ± 0.25 pF ceram PL
	C6	74.5108	4.7 nF -20+80% ceram PL
	C7	74.5299	2.2 pF ± 0.25 pF ceram PL
	C8	74.5161	470 pF -20+80% ceram PL
	C9	74.5162	470 pF -20 +50% ceram DI
	C10	74.5310	18 pF 5% ceram PL
	C11	74.5316	39 pF 5% ceram PL
	C12	74.5162	470 pF -20+50% ceram DI
	C13	78.5055	2.5 - 9 pF trimmer DI
	C14		Printed capacitor
	C15		2.5 - 9 pF trimmer DI
	C16	74.5301	3.3 pF ± 0.25 pF ceram PL
	C17	74.5162	470 pF -20+50% ceram DI
	C18	74.5162	470 pF -20+50% ceram DI
	C19	74.5123	1.6 pF ± 0.25 pF ceram DI
	C20	74.5161	470 pF -20+80% ceram PL
	C21	74.5162	470 pF -20+50% ceram DI
	C22		Helix Coil Adjustor
	C23		Helix Coil Adjustor
	C24	Heli	Helic Coil Adjustor
	C25	74.5316	39 pF 5% ceram PL
	C26	74.5316	39 pF 5% ceram PL
	C27	74.5162	470 pF -20+50% ceram DI
	C28	74.5302	30 pF ± 0.25 pF ceram PL
	C29	74.5302	3.9 pF ± 0.25 pF ceram PL
	C30	74.5316	39 pF 5% ceram PL
	C31	74.5316	39 pF 5% ceram PL
	C32	74.5162	470 pF -20+50% ceram DI
	C33	74.5302	3.9 pF ± 0.25 pF ceram PL
	C34	74.5302	3.9 pF ± 0.25 pF ceram PL
	C35		Helix Coil Adjustor
	C36		Helix Coil Adjustor
	C37		Helix Coil Adjustor
	C38		Printed Capacitor
	C40	74.5198	1 nF -20+50% ceram FT
	C41	74.5198	1 nF -20+50% ceram FT
	C42	74.5322	27 pF 20% ceram FT
	C50	78.5055	2.5 - 9 pF trimmer DI
	C51	74.5126	1.8 pF ± 0.25 pF ceram BD
	C52	74.5162	470 pF -20+50% ceram DI
	C53	74.5138	18 pF 5% ceram DI
	C54	74.5109	10 nF -20+80% ceram PL

TYPE	NO.	CODE	DATA
	C55	76.5103	150 pF 2.5 % polystyr. TB
	C56	76.5101	68 pF 2.5 % polystyr. TB
	R1	80.5066	27 KΩ 5% carbon film
	R2	80.5057	4.7 KΩ 5%
	R3	80.5045	470 Ω 5%
	R4	80.5033	47 Ω 5%
	R5	80.5061	10 KΩ 5%
	R6	80.5237	100 Ω 5%
	R7	80.5040	180 Ω 5%
	R8	80.5066	27 KΩ 5%
	R9	80.5065	22 KΩ 5%
	R10	80.5033	47 Ω 5%
	R11	80.5033	47 Ω 5%
	R12	80.5073	100 KΩ 5%
	R13	80.5054	2.7 KΩ 5%
	R14	80.5025	10 Ω 5%
	R15	80.5033	47 Ω 5%
	R16	80.5066	27 KΩ 5%
	R17	80.5065	22 KΩ 5%
	R18	80.5045	470 Ω 5%
	R19	80.5239	150Ω 5%
	R20	80.5025	10 Ω 5%
	R21	80.5033	47Ω 5%
	R22	80.5058	5.8 KΩ 5%
	R23	80.5051	1.5 KΩ 5%
	R24	80.5036	82 Ω 5%
	R25	80.5033	47 Ω 5%
	R26	80.5057	4.7 KΩ 5%
	R27	80.5051	1.5 KΩ 5%
	R28	80.5035	68Ω 5%
	R29	80.5033	47Ω 5%
	R32	80.5058	5.6 KΩ 5%
	R33	89.5060	1.5 KΩ 5% NTC
	R34	80.5061	10 KΩ 5% carbon film
	R35	80.5047	680 Ω 5%
	R40	80.5255	3.3 KΩ 5%
	R41	80.5036	82 Ω 5%
	R42	80.5243	330 Ω 5%
	L1	61.1234	RF Coil
	L2	61.1230	RF Coil

**RECEIVER CONVERTER
MODTAGERKONVERTER**

RC762

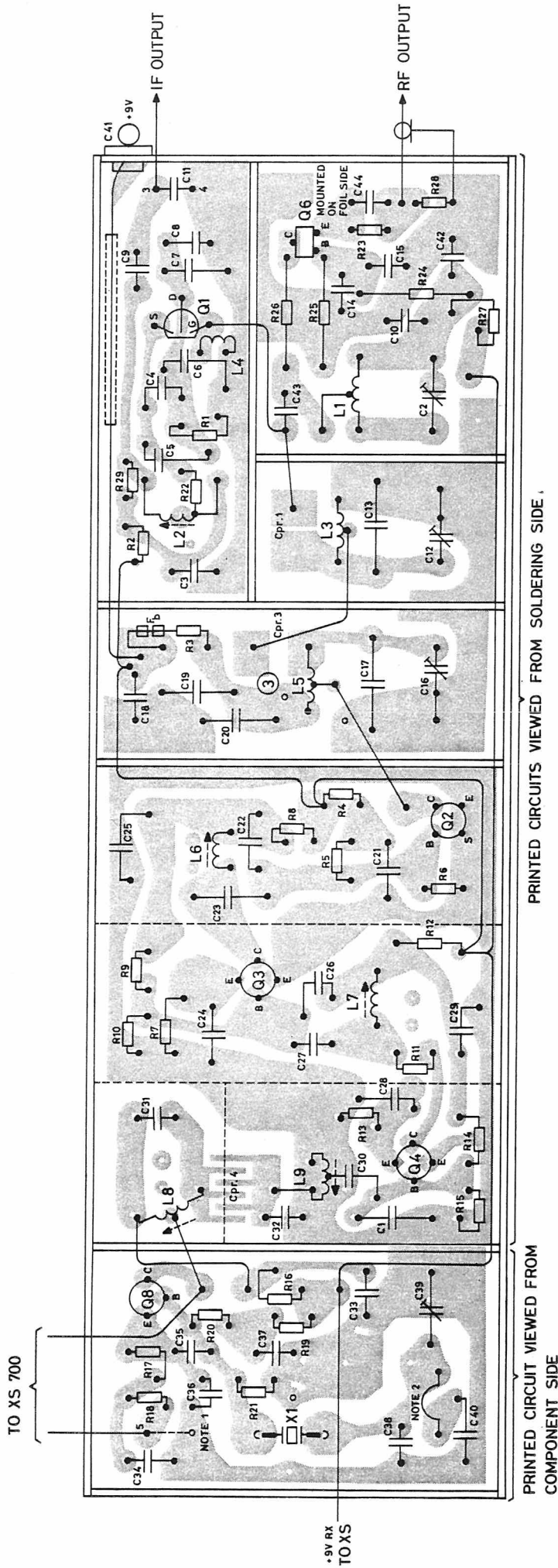
X 401.865

TYPE	NO	CODE	DATA
RC763		10. 3432-00	Receiver Converter
C1		74. 5338	100 pF 5%
C2		78. 5048	1. 8/10 pF
C3		74. 5109	10 nF -20 + 80%
C4		74. 5126	1. 8 pF 0. 25 pF
C5		74. 5135	10 pF 5%
C6		74. 5138	18 pF 5%
C7		74. 5138	18 pF 5%
C8		74. 5109	10 nF -20 + 80%
C9		74. 5348	82 pF 2%
C10		74. 5338	39 pF 5%
C11		74. 5349	100 pF 2%
C12		78. 5047	1/3. 5 pF
C13		74. 5189	1. 5 pF 0. 25 pF
C14		74. 5338	39 pF 5%
C15		74. 5312	470 pF -20 + 80%
C16		78. 5048	1. 8/10 pF
C17		74. 5189	1. 5 pF 0. 25 pF
C18		76. 5061	4. 7 nF 10%
C19		74. 5138	18 pF 5%
C20		74. 5117	39 pF 5%
C21		74. 5161	470 pF -20 + 80%
C22		74. 5338	39 pF 5%
C23		74. 5134	8. 2 pF 0. 25 pF
C24		74. 5161	470 pF -20 + 80%
C25		74. 5161	470 pF -20 + 80%
C26		74. 5118	47 pF 5%
C27		74. 5116	33 pF 5%
C28		74. 5161	470 pF -20 + 80%
C29		74. 5109	10 nF -20 + 80%
C30		74. 5155	1 nF -20 + 80%
C31		74. 5116	33 pF 5%
C32		74. 5116	33 pF 5%
C33		76. 5059	2. 2 nF 10%
C34		76. 5061	4. 7 nF 10%
C35		76. 5102	100 pF 2. 5%
C36		76. 5106	470 pF 2. 5%
C37		76. 5059	2. 2 nF 10%
C38		74. 5191	33 pF 5%
C39		76. 5044	2/18 pF
C40		74. 5135	10 pF 5%
C41		74. 5198	1 nF -20 + 80%
R1		80. 5255	3. 3 K Ω 5%
R2		80. 5243	330 Ω 5%
R3		80. 5237	100 Ω 5%
R4		80. 5237	100 Ω 5%

TYPE	NO	CODE	DATA
	R5	80. 5266	27 K Ω 5%
	R6	80. 5254	2. 7 K Ω 5%
	R7	80. 5237	100 Ω 5%
	R8	80. 5237	100 Ω 5%
	R9	80. 5273	100 K Ω 5%
	R10	80. 5263	15 K Ω 5%
	R11	80. 5231	33 Ω 5%
	R12	80. 5237	100 Ω 5%
	R13	80. 5237	100 Ω 5%
	R14	80. 5270	56 K Ω 5%
	R15	80. 5259	6. 8 K Ω 5%
	R16	80. 5237	100 Ω 5%
	R17	80. 5247	680 Ω 5%
	R18	80. 5237	100 Ω 5%
	R19	80. 5243	330 Ω 5%
	R20	80. 5265	22 K Ω 5%
	R21	80. 5262	12 K Ω 5%
	R22	80. 5036	82 Ω 5%
	R23	80. 5039	150 Ω 5%
	R24	80. 5059	6. 8 K Ω 5%
	R25	80. 5051	1. 5 K Ω 5%
	R26	80. 5038	120 Ω 5%
	R27	80. 5037	100 Ω 5%
	R28	80. 5042	270 Ω 5%
	R29	80. 5061	10 K Ω 5%
	L1	62. 0936	RF coil 420 - 470 MHz
	L2	61. 1117	IF coil 10. 7 MHz
	L3	62. 0812	RF coil 409. 3 - 459. 3 MHz
	L4	62. 0935	RF coil 420 - 470 MHz
	L5	62. 0813	RF coil 409. 3 - 459. 3 MHz
	L6	61. 1118	RF coil 204 - 230 MHz
	L7	61. 1119	RF coil 102 - 115 MHz
	L8	61. 1120	RF coil 34 - 38. 5 MHz
	L9	61. 1121	RF coil 34 - 28. 5 MHz
	Q1	99. 5245	Transistor 2 N 5245
	Q2	99. 5240	Transistor BFX 89
	Q3	99. 5168	Transistor BF 173
	Q4	99. 5168	Transistor BF 173
	Q5	99. 5294	Transistor 2 N 2369 A
	Q6	99. 5320	Transistor BFR 93 / BFR 35 A

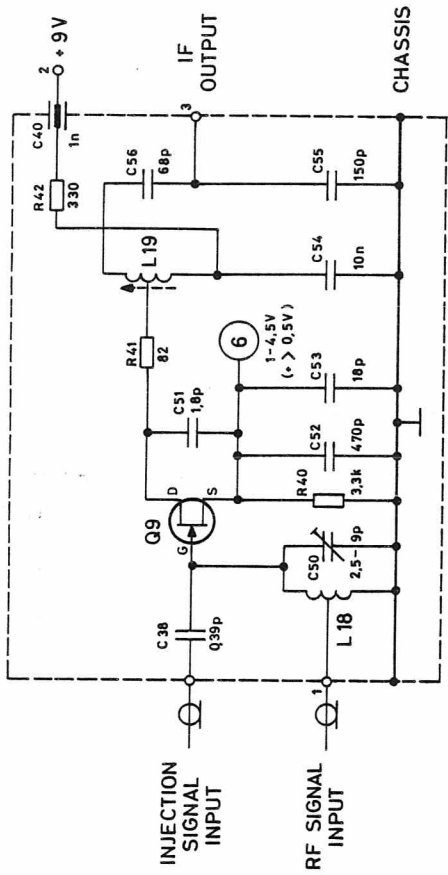
RECEIVER CONVERTER RC763

X402.366

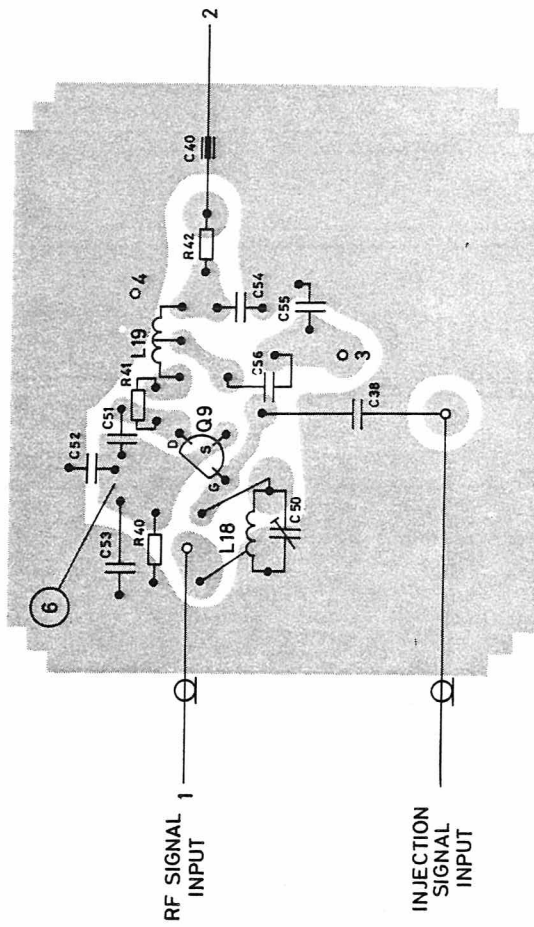


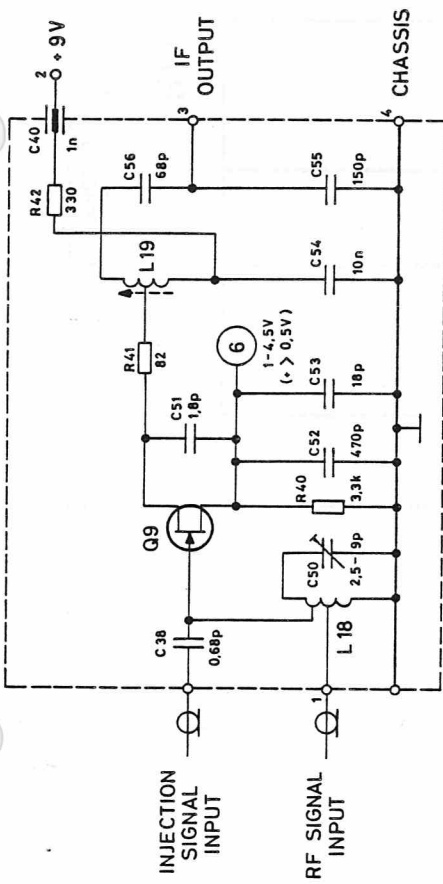
RECEIVER CONVERTER RC763

D402.422



Q9
BOTTOM VIEW

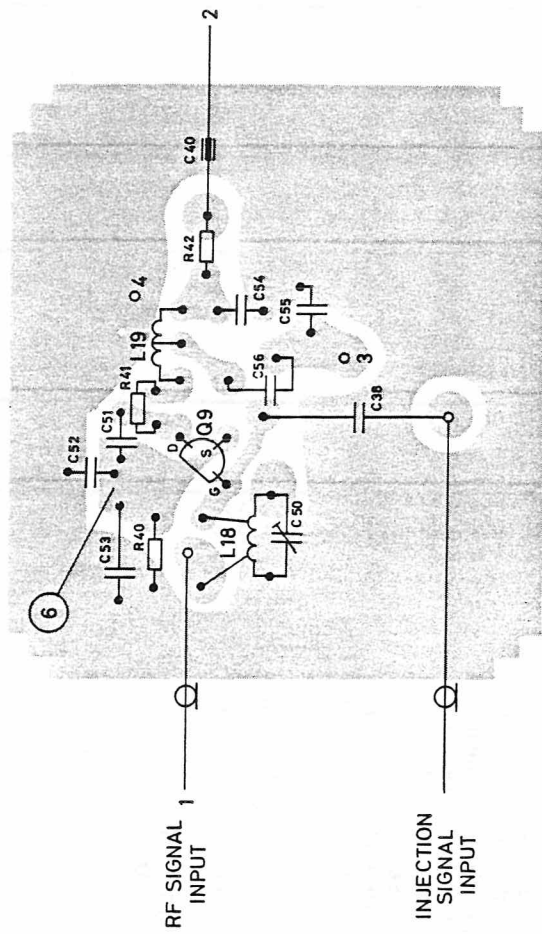




() VOLTAGE INCREASE MEASURED WITH INJECTION SIGNAL APPLIED.



Q9
BOTTOM VIEW



RECEIVER CONVERTER RC764

STORNOPHONE 700
 MAINTENANCE MANUAL
 VOLUME II
 Section 7

TITLE		Code
SR781	Description 1 - 7	60.253-E1
	Functional Diagram	D402.111
	Schematic	D401.825
	Component Lay-out	D402.353
	Part List	X401.962
SR783	Schematic	D402.372
	Component Lay-out	D402.511
	Part List	X402.453
SR785	Description 1 - 8	60.218-E1
	Schematic	D401.722
	Component Lay-out	D401.978
	Part List 1 - 2	X401.701
SR785a	Description 1 - 7	60.232-E1
	Functional Diagram	D401.977/2
	Schematic	D401.894
	Component Lay-out	D402.159
	Part List 1 - 2	X401.963
SR7841	Description 1 -11	60.219-E1
	Schematic	D401.706/2
	Component Lay-out	D401.711/2
	Part List 1 - 1	X401.695/2
SR7841a	Description	60.347-E1
	Schematic	D402.056
	Component Lay-out	D402.468
	Part List 1 - 3	X402.184
ST7845	Description 1 - 3	60.230-E1
	Functional Diagram	D401.966
	Schematic	D401.583/4
	Component Lay-out	D401.686
SU704	Part List	X401.689/2
	Installation	D402.371

Service Coordination

STORNOPHONE 700
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 Section 7

TITLE		Code
Cont.		
TR780	Description 1 - 5	60. 210-E1
TR782	Schematic	D401. 161/6
	Part List 1 - 2	X401. 650/2
TR783	Schematic	D401. 231/3
	Part List 1 - 2	X401. 699/2
TR785	Schematic	D401. 230/3
	Part List 1 - 2	X401. 700/2
TR786	Schematic	D402. 251
	Component Lay-out	D402. 510
	Part List	X402. 466
TT781/783	Description 1 - 2	60. 228-E1
TT781	Schematic	D402. 161
	Part List	X401. 162
TT783	Schematic	D401. 557/3
	Part List	X401. 687/2
TT784	Description	60. 349-E1
	Schematic	D402. 242
	Part List	X402. 543
TT7812/13/14	Description 1 - 2	60. 229-E1
TT7812	Schematic	D401. 556/3
	Part List	X401. 688/3
TT7813	Schematic	D401. 774/2
	Part List	X401. 688/3
TT7814	Schematic	D401. 775/2
	Part List	X401. 688/3

SEQUENTIAL TONE RECEIVER

SR781

Description

SR781 is a sequential tone receiver for selective calling. It was developed for use in Stornophone 700 radiotelephone equipment. The frequencies employed are the standard CCIR series: 960 Hz to 2110 Hz.

SR781 is designed to operate on a 5-tone sequence, but can also be set to accommodate a 4-tone sequence.

GENERAL DESCRIPTION

Upon reception of a signal having the correct tones in the proper sequence the following events take place (in the receiver):

The call Lamp lights, the AF Muting is cancelled and the Key Lock function "unlocks". An audio alarm signal of about 1.5 seconds in duration can be sent out over the radiotelephone's loudspeaker, and when the vehicle's traffic horn is connected to the tone receiver via an auxilliary relay, the horn will also sound for the same length of time.

There is also a provision for automatically turning off the car's broadcast band receiver when a call arrives.

The audio circuit and the Key Lock are both turned on and off manually by means of the LS IN/OUT push button. Since the switch that "unlocks" the Key Lock also turns on the loudspeaker, the operator is forced to check for the presence of another signal on the channel before being able to key his transmitter.

In addition, the tone receiver is equipped with an Occupied Lamp controlled by the

squelch circuit in the radiotelephone receiver. Thus, if an RF signal having that channel's frequency is present at the antenna input it will cause the Occupied Lamp to light as an indication that the channel is not free.

After reception of a correct call the speaker will remain open until the LS IN/OUT button is depressed.

Logic Terms

Positive logic is employed in SR781, logical references are:

1. low voltage level ($\sim 0V$) = logic state "0" (LO)
2. high voltage level ($\sim 5V$) = logic state "1" (HI)

Tone Signalling

The first tone of a sequential signal, arriving from input terminal 35, passes through the Amplifier/Limiter, IC1, where it becomes suitable for applying to the tuned circuit of L1 and C8.

In stand by the resonant frequency of the tuned Circuit is set up by the first Tone Gate, Q4, for the first tone of its code. If the first tone received corresponds to the circuit resonant frequency, it becomes selected, is then amplified by IC2 and detected by E1.

The correct tone will thus fire the Schmitt Trigger, IC3a, whose output drives the Clock Delay (CP Delay) circuit, IC3b. This circuit produces a Clock Pulse whose leading (positive going) edge is delayed

approximately 15 msec. from the Schmitt Trigger output signal.

The clock pulse is applied to the Counter circuit, IC6a, IC7a and IC6b. The counter is arranged as a Synchronous, divide-by-5 counter whose binary states are read out in BCD (binary coded decimal) mode in the Decoders, IC4a-d and IC5a-b.

The first five Decoders drive the Tone Gates, Q4-Q8. The output of the sixth Decoder, IC5b, is applied to the Readout circuit, IC7b.

The Readout flip-flop is also timed by the same clock pulses that toggle the Counter flip-flops.

At the end of a tone pulse, the Schmitt Trigger reverts to its quiescent state and the resultant trailing (negative going) pulse edge from the CP Delay output causes the Counter flip-flops to change state. (So far, with just the first pulse completed, only Counter IC6a is affected.)

The Decoders sense the new binary state and turn Tone Gate Q4 OFF and Tone Gate Q5 ON, thus setting the resonant circuit up for the second tone in the sequential code.

Suppose that the next tone received does not match the receiver's code. It will not be selected by the resonant circuit and no signal will be available to fire the Schmitt Trigger. When the Schmitt Trigger was fired the first time, it also turned Q1 ON and activated the Clear Delay circuit, IC3c. The output of IC3c then enabled the Counters by applying a HI logical state to their Clear inputs. The Clear Delay output remains HI for about 220 msec. after the Schmitt Trigger has returned to "0". If the second tone does not activate the Schmitt Trigger by then, Q1 goes OFF and the Clear Delay output goes LO, clearing the counter and setting the Decoders back

to the stand by position, i. e. ready to receive the first tone again. This is what happens if the second, or any consequent tone fails (for instance, if the tone is not the correct one for the particular receiver under consideration).

The 2nd, 3rd, 4th and 5th tones of a sequence occur like the 1st, each time stepping the Decoder one position forward until the final tone has been received.

When all five tones have been received, at the end of the 5th tone, IC7b clears the Holding Circuit, IC8, and turns transistor Q2 ON.

Q2 drives the Alarm Delay circuit.

All the functions mentioned in the beginning of this description, i. e. Call Lamp, AF Muting, Key Lock, Alarm Tone Generator, etc. occur at this time.

The Call Lamp and the speaker will remain ON until switched OFF manually with the LS IN/OUT push button (via terminal 32).

If the operator later wants to make a call he must first "unlock" the Key Lock function with the LS IN/OUT push button again, thus turning the loudspeaker ON. If there is any traffic on his channel, he will hear it and be warned before he can key his transmitter.

CIRCUIT DESCRIPTION

Input Stage (IC1)

Input terminal 35 can be wired in either of two positions (marked DK and SV on schematic diagram D401.825):

DK = input signal through C2 and R1, linear response

SV = input signal differentiated through C1 to match the modulation index used in Sweden and by Storno.

The amplifier circuit incorporates amplitude limiting for signal levels above the minimum required to activate the Schmitt Trigger.

Resistor R6 sets the amplifier sensitivity.

Amplifier Stage (IC2)

The signal is inductively coupled to the Amplifier via the parallel resonant circuit, L1 and C8.

Five of the taps on tone coil L1 are wired to Tone Gates Q4 to Q8, respectively (with a 4-tone code, Q8 is not used). When a Tone Gate is ON, i. e. conducting, it completes a path from its coil tap to chassis ground and the parallel resonant circuit for that particular tone frequency is formed.

NTC resistor R13 compensates for variations in circuit Q caused by changes in ambient temperature.

The selected signal passes to operational amplifier IC2, which is bootstrapped so as not to load the resonant circuit. Amplifier gain is determined by the ratio of R17 to R19.

Detector and Schmitt Trigger (E1, E2, IC3a)

The amplified tone signal is then rectified by the forward-biased diode, E1, and filtered by C13. The resultant DC voltage is present at the inverting input of IC3a.

When the rectified voltage exceeds the threshold level set by R21, R22, R25, R26 and diode E2, the output of the Schmitt Trigger switches from LO ($\sim 0V$) to HI ($\sim 5V$) and remains in that state for the duration of the tone pulse.

Feedback to the non-inverting input via R27 produces a circuit hysteresis of circa 0.2 V.

When the tone ends the Schmitt Trigger switches back to its quiescent state, i. e. : output LO.

Feedback through C14 and R29 will hold the Schmitt Trigger output LO for approx. 10 msec.

Clock Delay (E4, IC3b)

In stand by the Schmitt Trigger output state is LO, C15 is discharged through E4, and the potential at the non-inverting input is also LO (IC3b output is also LO).

Notice that the voltage divider network of R41 and R42 determines the threshold voltage at the inverting inputs of all 3 "delay" circuits, IC3b, IC3c and IC3d.

Now, when the Schmitt Trigger output goes HI, it reverse-biases diode E4 and capacitor C15 begins to charge through resistors R31 and R32. The moment the charge on C15, as seen at the non-inverting input of the comparator, reaches the threshold level, the output switches to the HI state.

It takes C15 approx. 15 msec. to charge up to the threshold level of IC3b. This is what determines the Clock Delay time, removing the short circuit across R30 lengthens the delay time.

At the end of the tone the Schmitt Trigger output returns to its LO state and C15 can once again discharge through E4 and R32. The time constant of this circuit provides a delay at the negative going trailing edge of the pulse, too. These delays prevent random noise pulses from operating the circuit erratically.

Clear Delay (Q1, IC3c)

In stand by, Q1 is OFF and C16 has no charge on it. When the Schmitt Trigger output goes HI it drives Q1 ON, and C16

builds up a charge via R37 and Q1, triggering comparator IC3c so its output goes HI.

The clear Delay circuit operates similarly to the Clock Delay circuit.

As long as the Schmitt Trigger keeps operating at the normal tone intervals, Q1 can maintain the charge on C16. At the end of the 5th tone, the Schmitt Trigger reverts to its quiescent state (output LO) and turns Q1 OFF, as the emitter of Q1 will be biased by the charge on C16. The discharge path for C16 is through R36 and R37. In about 220 msec. the voltage at the non-inverting input of IC3c will fall back to the threshold level and the comparator output switches state. The LO potential at the Clear Delay output clears the Counter and the Readout circuits. Since the interval between tones is normally much less than 220 msec., the Clear Delay will remain OFF (output HI) throughout the entire tone sequence.

Counter (IC6a, IC7a, IC6b)

The Counter elements are J-K master-slave flip-flops arranged as a synchronous, divide-by-five counter that is clocked by the Clock Delay output and is cleared by the Clear Delay output. All of the normal (Q) and complement (\bar{Q}) Counter outputs are wired to appropriate Decoder inputs (IC4 and IC5).

The binary information present at each flip-flop input when a clock pulse arrives will be transferred to the output by the trailing edge of the clock pulse. A 5-tone code sequence correct for the receiver in question, produces 5 clock pulses, one for each tone pulse.

220 msec. after the 5th tone ends, the logical "0" (LO) state at the Clear Delay output clears the Counter flip-flops. However, the Counter will not be able to start counting again until the flip-flops are enabled by the Clear Delay output being switched to logical "1" again by the Schmitt Trigger action.

Decoder (IC4a-d, IC5a) and Tone Gates (Q4 - Q8)

The wiring between the Counter outputs and Decoder NOR gate inputs is arranged to drive the Tone Gates one at a time.

The output of a NOR gate is HI (logical state "1") only when all of its inputs are LO (logical state "0"). If either or both of its inputs are HI, the NOR gate output will be LO.

In stand by, both inputs to IC4a are LO and the output is therefore HI. The other 5 Decoder NOR gates have at least one of their inputs HI, so their outputs will all be LO. Tone Gate Q4 is thus held ON by IC4a, while Q5-Q8 are held OFF by IC4b - IC5a.

Transistor Q4, conducting hard, acts as a virtual short circuit from chassis ground to whichever tone coil tap is specified for the first tone of the code sequence. At the end of the first clock pulse, one of the inputs to IC4a goes HI, the NOR gate output goes LO, and Q4 cuts off. At the same time both inputs to IC4b are now LO, its output goes HI, and Q5 goes ON to tune the resonant circuit for the 2nd tone of the code sequence.

One special consideration here is that the actual maximum HI potential measurable at the NOR gate output is limited to approx. 0.7 V by the conducting Tone Gate transistor's emitter-base junction.

With each correct pulse the Counter steps the Decoder one position forward until the final tone has been received.

Readout Circuit (IC5b, IC7b)

At the end of the 4th tone of a 5-tone signal (or the 3rd tone of a 4-tone signal) both inputs to IC5b will be LO, and the NOR gate output will go HI, driving the J input of IC7b HI, as well.

Now, with its J input driven HI and its K input held as chassis ground potential, IC7b can switch output states when the trailing (negative going) edge of the 5th (or 4th) tone pulse arrives. The normal (Q) output activates the Alarm Delay circuit, and the complement (\bar{Q}) output clears the Holding Circuit, IC8.

220 msec. later the Clear Delay, IC3c, clears the Counter and Readout circuits, and the Tone Receiver is set up for the first tone again by the Decoder and Tone Gate circuits.

A strapping arrangement at the input of IC5b allows for either 4 or 5-tone codes.

Alarm Delay (IC3d, Q2, Q3)

Transistor Q2 is normally OFF and the output of IC3d is HI, Q3, a PNP transistor, is held OFF, and so is Q13.

When the Q output of IC7b in the Readout circuit goes HI at the end of the last tone pulse, it drives Q2 ON. Then capacitor C18 quickly charges through the conducting transistor Q2. When the charge reaches the threshold established by the resistive divider circuit of R41 and R42 the output of IC3d goes LO, turning Q3, then Q13 ON.

Q13 acts as a switch capable of carrying 100 mA of current between ground and terminal 37, the connection for an auxiliary alarm relay.

As long as the Clear Delay, IC3c, output remains HI, Q2 is held ON by IC7b and maintains the charge across C18. 220 msec. after the last pulse from the Clock Delay, IC3b, ends, IC3c switches state and clears the Counter and Readout IC's. The Q output of IC7b returns to logical "0", turning Q2 OFF. C 18 now discharges slowly through R43 and R44.

The time constant of C18, R43 and R44 is calculated so that the Alarm Delay,

IC3d, output switches back to logical "1" approx. 1.3 sec. after the end of the final clock pulse.

The Alarm Delay is a comparator circuit that operates in the same manner as the Clock Delay.

Holding Circuit (IC8, Q9, Q11) Call Lamp + Key Lock Switches (Q10, Q11)

The Holding Circuit is an integrated flip-flop with its J and K inputs both tied to logical "1" through R64. With both the J and the K inputs HI, the flip-flop output will complement itself for each clock pulse arriving at the CP (toggle) input. Notice that the CP input is also tied to +Vcc, through R62. This simulates the flat top portion of a clock pulse.

Now, whenever the LS IN/OUT push button on the radiotelephone control panel is pressed, terminal 32 is grounded. C30 at the CP input discharges quickly through the 27 Ω resistor, R63, and the flip-flop sees a negative going trailing edge of a "clock pulse" and switches state. When the push button is released again, C30 charges up to +Vcc through R62, forming the positive going leading edge of the next "clock pulse".

Only the normal (Q) output is used in this circuit, it switches Q11 ON and OFF.

As just seen, IC8 is designed so that it can only be toggled manually by means of the LS IN/OUT switch. However, the Clear input is operated electronically from the \bar{Q} output of Readout flip-flop IC7b.

C32 provides a drive pulse to the base of Q9, saturating the transistor as soon as the radiotelephone is turned on. This pulls the collector of Q9 down to ground, presetting IC8. In the preset state, the Q output is HI and Q11 is held OFF, and Q10 and Q12 are likewise OFF.

With the collector of Q9 LO, diode E3 keeps the Schmitt Trigger output at logical "0", as well, inhibiting both the Clock and the Clear Delay circuits.

As capacitor C32 accumulates a charge, the charging current decreases until it no longer can forward bias Q9. The transistor goes OFF, its collector voltage goes HI, and IC8 becomes enabled.

Diode E6 serves to discharge C32 when the equipment is turned off.

Each time the LS IN/OUT button is pressed, IC8 changes state, switching Q11 ON or OFF and, in turn, driving Q10 and Q12 into saturation or cut-off.

When Q10 conducts it provides a ground connection to light the Call Lamp and, when applicable to operate a relay for muting the car's broadcast band radio.

Q12, conducting simultaneously, turns the loudspeaker ON and also unlocks the Key Lock function.

At the end of the last tone pulse in a sequence, the complement output (\bar{Q}) of IC7b clears IC8, whose output goes LO and turns Q11 ON. Q10 and Q12 are then driven into saturation. 220 msec. after, the Clear Delay clears the Counter and Readout circuits and \bar{Q} of IC7b goes HI again. IC8 can be manually toggled via terminal 32 any time afterwards.

Note that whenever the speaker is in operation, whether turned on manually or by an incoming call, the Call Lamp will light.

Occupied Lamp Switch (Q14)

Whenever the channel is occupied a DC voltage from the Squelch circuit, via terminal 41, turns Q14 ON and establishes a ground connection to the Occupied Lamp, so it can light.

Alarm Tone Generator (IC5c, IC5d)

Two NOR gates, coupled to operate as a free-running (astable) multivibrator, generate an audio signal that is available at terminal 20. The Generator can be strapped to the output of IC3d or to +Vcc through R61.

In stand by, IC3d has a HI output, which would inhibit NOR gate IC5d. When a selective call comes through, the Alarm Delay output goes LO for approx. 1.5 sec. During that interval the multivibrator can oscillate at a frequency determined by the time constants of R57 / C27 and R58 / C26. When Alarm Delay output goes HI again the oscillator stops.

Regardless of the state of IC8 a correct tone signal will clear the flip-flop and turn Q11, then Q10 and Q12 ON. Thus, a tone call has higher priority than the manual switch.

Clock Pulse	Clear Delay	IC6a				IC7a				IC8b				IC4a	IC4b	IC4c	IC4d	IC5a	IC5b	IC7b \bar{Q}
		J	K	Q	\bar{Q}	J	K	Q	\bar{Q}	J	K	Q	\bar{Q}							
0	0	1	0	0	1	0	0	0	1	0	0	0	1	1	0	0	0	0	0	1
1	1	1	0	1	0	1	0	0	1	0	0	0	1	0	1	0	0	0	0	1
2	1	1	0	1	0	1	0	1	0	1	0	0	1	0	0	1	0	0	0	1
3	1	0	1	1	0	1	0	1	0	1	0	0	0	0	0	0	1	0	0	1
4	1	0	1	0	1	0	0	1	0	1	0	1	0	0	0	0	0	1	1	1
5	1	0	1	0	1	0	0	1	0	1	0	1	0	0	0	0	0	1	1	0
Δ	0	1	0	0	1	0	0	0	1	0	0	0	1	1	0	0	0	0	0	1

NOTE: Δ = 220 msec. after the end of the 5th tone

Technical SpecificationsSupply Power

Nominal : 13.6 V
 Minimum : 10.5 V
 Maximum : 16.0 V

Current Drain

Stand by: 24 mA \pm 4 mA

Regulated Voltage

Nominal 4.9 V

Temperature Range

Operating range: -25°C to $+60^{\circ}\text{C}$
 Functioning range: -30°C to $+60^{\circ}\text{C}$

Maximum Load Currents

Terminal 37 ALARM 100 mA (for 1.5 sec.)
 Terminal 47 CALL 100 mA
 Terminal 45 OCCUPIED 100 mA
 Terminal 51
 and 43 KEY LOCK 10 mA
 Terminal 34 AF MUTING I_{load} min. 0.75 mA
 for $V_{\text{out}} = 8 \text{ V}$

Input Impedance

$\geq 6\text{K}\Omega$

Signal Input Level

Nominal at 1000 Hz: 110 mV

AF Muting

In conjunction with terminal 18 of CF701 or CF702:
 $\geq 60 \text{ dB}$.

Signalling Code

Sequence of 4 or 5 tone bursts of 100 ms
 $\pm 10 \text{ ms}$ duration with maximum 10 ms
 interval between tone bursts.

Tone Signal Frequencies

<u>Coil terminal</u>	<u>Tone frequency</u>
1	960Hz
2	1022Hz
3	1124Hz
4	1197Hz
5	1275Hz
6	1358Hz
7	1446Hz
8	1540Hz
9	1640Hz
10	1747Hz
11	1860Hz
12	1981Hz
13	2110Hz

Frequency Accuracy

Coil tuned for 1022Hz: $\leq 0.3\%$ for all tones

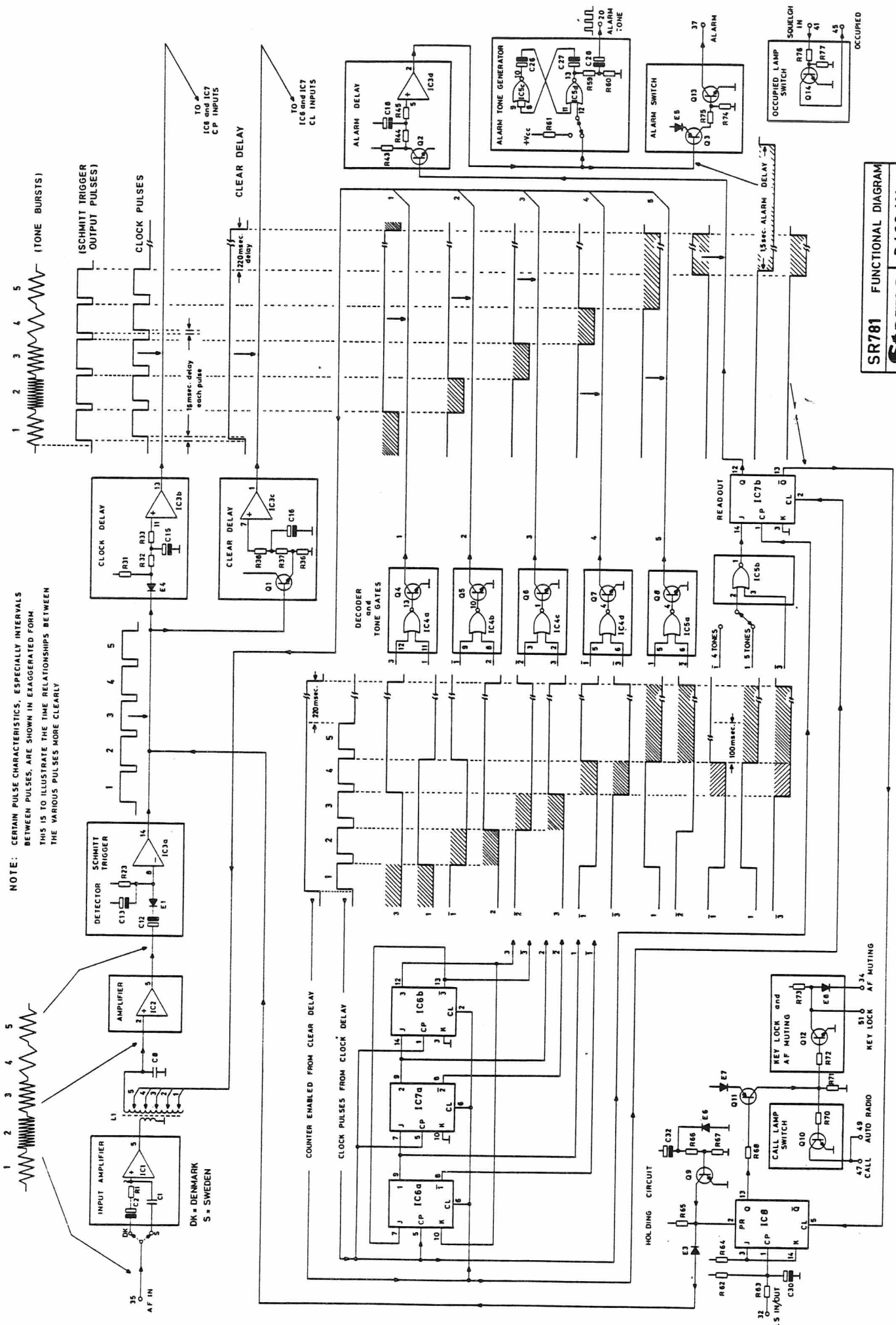
Frequency Stability

(typically $\leq 0.5\%$) $\leq 1.0\%$

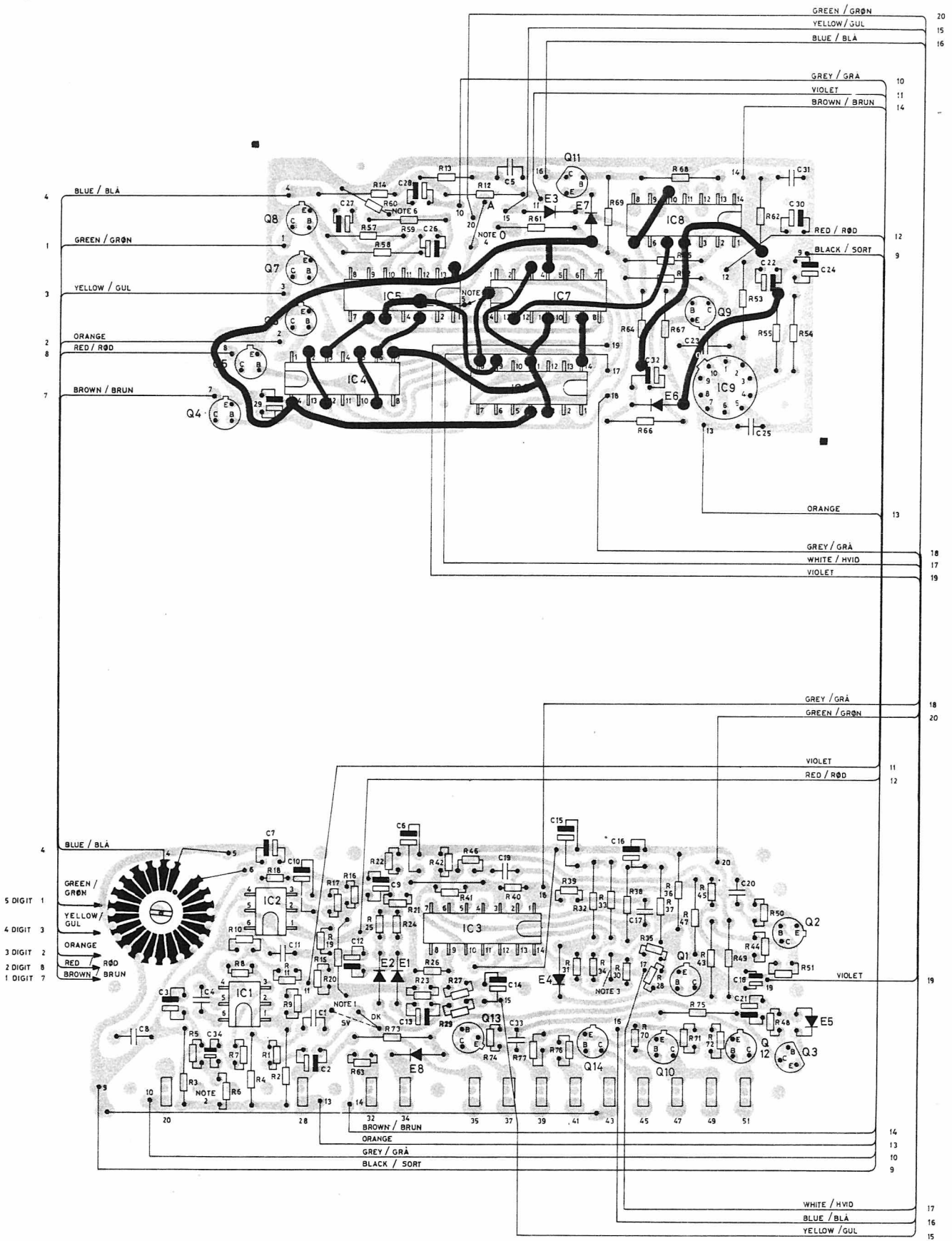
Selectivity

Frequencies differing from f_0 by 3% or more are unable to trigger the tone receiver.

NOTE: CERTAIN PULSE CHARACTERISTICS, ESPECIALLY INTERVALS BETWEEN PULSES, ARE SHOWN IN EXAGGERATED FORM THIS IS TO ILLUSTRATE THE TIME RELATIONSHIPS BETWEEN THE VARIOUS PULSES MORE CLEARLY



SR781 FUNCTIONAL DIAGRAM
Storno D402.111



SEQUENTIAL TONE RECEIVER SR781
 SEKVENSTONEMODTAGER

D402.353

TYPE	NO.	CODE	DATA
SR781		10.2965	Sequential Tone Receiver
	C1	74.5061	4.7nF 10% polyester. FL 50V
	C2	73.5118	0.22μF 20% tantal 35V
	C3	73.5102	2.2μF 20% tantal 35V
	C4	74.5116	33pF 5% ceram TB 160V
	C5	76.5059	2.2nF 10% polyester. FL 50V
	C6	73.5109	10μF 20% tantal 16V
	C7	73.5089	0.1μF 20% tantal 35V
	C8	76.5068	0.1μF 1% polystyry TB 63V
	C9	73.5102	2.2μF 20% tantal 35V
	C10	73.5114	1μF 20% tantal 35V
	C11	74.5116	33pF 5% ceram TB 160V
	C12	73.5114	1μF 20% tantal 35V
	C13	73.5118	0.22μF 20% tantal 35V
	C14	73.5089	0.1μF 20% tantal 35V
	C15	73.5102	2.2μF 20% tantal 35V
	C16	73.5102	2.2μF 20% tantal 35%
	C17	76.5071	22nF 10% polyester. FL 50V
	C18	73.5109	10μF 20% tantal 16V
	C19	76.5071	22nF 10% polyester. FL 50V
	C20	76.5070	10nF 10% polyester. FL 50V
	C21	73.5114	1μF 20% tantal 35V
	C22	73.5124	47μF 20% tantal 6.3V
	C23	74.5165	100pF 10% ceram PL 63V
	C24	73.5126	4.7μF 20% tantal 35V
	C25	76.5070	10nF 10% polyester. FL 50V
	C26	73.5118	0.22μF 20% tantal 35V
	C27	73.5118	0.22μF 20% tantal 35V
	C28	73.5089	0.1μF 20% tantal 35V
	C29	73.5109	10μF 20% tantal 16V
	C30	73.5126	4.7μF 20% tantal 35V
	C31	74.5155	1nF -20+80% ceram PL 63V
	C32	73.5126	4.7μF 20% tantal 35V
	C33	76.5070	10nF 10% polyester. FL 50V
	C34	73.5114	1μF 20% tantal 35V
	R1	80.5262	12kΩ 5% carbon film 1/8W
	R2	80.5268	39kΩ 5% carbon film 1/8W
	R3	80.5264	18kΩ 5% carbon film 1/8W
	R4	80.5261	10kΩ 5% carbon film 1/8W
	R5	80.5261	10kΩ 5% carbon film 1/8W
	R6	80.52xx	Adjusted 1/8W
	R7	80.5253	2.2kΩ 5% carbon film 1/8W
	R8	80.5279	0.33 MΩ 5% carbon film 1/8W
	R9	80.5259	6.8kΩ 5% carbon film 1/8W
	R10	80.5261	10kΩ 5% carbon film 1/8W
	R11	80.5265	22kΩ 5% carbon film 1/8W

TYPE	NO.	CODE	DATA
	R12	80.5264	18kΩ 5% carbon film 1/8W
	R13	89.5009	15kΩ 20% NTC 0.6W
	R14	80.5262	12kΩ 5% carbon film 1/8W
	R15	80.5264	18kΩ 5% carbon film 1/8W
	R16	80.5265	22kΩ 5% carbon film 1/8W
	R17	80.5260	8.2kΩ 5% carbon film 1/8W
	R18	80.5273	0.1 MΩ 5% carbon film 1/8W
	R19	80.5274	0.12 MΩ 5% carbon film 1/8W
	R20	80.5258	5.6kΩ 5% carbon film 1/8W
	R21	80.5256	3.9kΩ 5% carbon film 1/8W
	R22	80.5249	1kΩ 5% carbon film 1/8W
	R23	80.5278	0.27MΩ 5% carbon film 1/8W
	R24	80.5271	68kΩ 5% carbon film 1/8W
	R25	80.5258	5.6kΩ 5% carbon film 1/8W
	R26	80.5276	0.18 MΩ 5% carbon film 1/8W
	R27	80.5274	0.12 MΩ 5% carbon film 1/8W
	R28	80.5261	10kΩ 5% carbon film 1/8W
	R29	80.5276	0.18 MΩ 5% carbon film 1/8W
	R30	80.5259	6.8kΩ 5% carbon film 1/8W
	R31	80.5261	10kΩ 5% carbon film 1/8W
	R32	80.5251	1.5kΩ 5% carbon film 1/8W
	R33	80.5264	18kΩ 5% carbon film 1/8W
	R34	80.5278	0.27 MΩ 5% carbon film 1/8W
	R35	80.5261	10kΩ 5% carbon film 1/8W
	R36	80.5276	0.18 MΩ 5% carbon film 1/8W
	R37	80.5253	2.2kΩ 5% carbon film 1/8W
	R38	80.5264	18kΩ 5% carbon film 1/8W
	R39	80.5276	0.18 MΩ 5% carbon film 1/8W
	R40	80.5261	10kΩ 5% carbon film 1/8W
	R41	80.5261	10kΩ 5% carbon film 1/8W
	R42	80.5261	10kΩ 5% carbon film 1/8W
	R43	80.5276	0.18 MΩ 5% carbon film 1/8W
	R44	80.5250	1.2kΩ 5% carbon film 1/8W
	R45	80.5264	18kΩ 5% carbon film 1/8W
	R46	80.5276	0.18 MΩ 5% carbon film 1/8W
	R47	80.5261	10kΩ 5% carbon film 1/8W
	R48	80.5262	12kΩ 5% carbon film 1/8W
	R49	80.5261	10kΩ 5% carbon film 1/8W
	R50	80.5261	10kΩ 5% carbon film 1/8W
	R51	80.5262	12kΩ 5% carbon film 1/8W
	R52	80.5226	12Ω 5% carbon film 1/8W
	R53	80.5251	1.5kΩ 5% carbon film 1/8W

**SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER**

SR781

X401.962

Storno

TYPE	NO.	CODE	DATA
	R54	80. 5253	2. 2kΩ 5% carbon film
	R55	80. 5258	5. 6kΩ 5% carbon film
	R56		Not used
	R57	80. 5251	1. 5kΩ 5% carbon film
	R58	80. 5251	1. 5kΩ 5% carbon film
	R59	80. 5269	47kΩ 5% carbon film
	R60	80. 5061	10kΩ 5% carbon film
	R61	80. 5268	39kΩ 5% carbon film
	R62	80. 5268	39kΩ 5% carbon film
	R63	80. 5230	27Ω 5% carbon film
	R64	80. 5268	39kΩ 5% carbon film
	R65	80. 5263	15kΩ 5% carbon film
	R66	80. 5265	22kΩ 5% carbon film
	R67	80. 5268	39kΩ 5% carbon film
	R68	80. 5257	4. 7kΩ 5% carbon film
	R69	80. 5257	4. 7kΩ 5% carbon film
	R70	80. 5246	680Ω 5% carbon film
	R71	80. 5261	10kΩ 5% carbon film
	R72	80. 5255	3. 3kΩ 5% carbon film
	R73	80. 5253	2. 2kΩ 5% carbon film
	R74	80. 5261	10kΩ 5% carbon film
	R75	80. 5246	680Ω 5% carbon film
	R76	80. 5246	680Ω 5% carbon film
	R77	80. 5261	10kΩ 5% carbon film
	L1	61. 1172	Tone coil
	E1	99. 5237	1N4148 Diode
	E2	99. 5237	1N4148 Diode
	E3	99. 5237	1N4148 Diode
	E4	99. 5237	1N4148 Diode
	E5	99. 5237	1N4148 Diode
	E6	99. 5237	1N4148 Diode
	E7	99. 5237	1N4148 Diode
	E8	99. 5237	1N4148 Diode
	Q1	99. 5143	BC108 Transistor
	Q2	99. 5143	BC108 Transistor
	Q3	99. 5144	S5144 Transistor
	Q4	99. 5201	BC109 Transistor
	Q5	99. 5201	BC109 Transistor
	Q6	99. 5201	BC109 Transistor
	Q7	99. 5201	BC109 Transistor
	Q8	99. 5201	BC109 Transistor
	Q9	99. 5143	BC108 Transistor
	Q10	99. 5143	BC108 Transistor
	Q11	99. 5144	S5144 Transistor
	Q12	99. 5143	BC108 Transistor

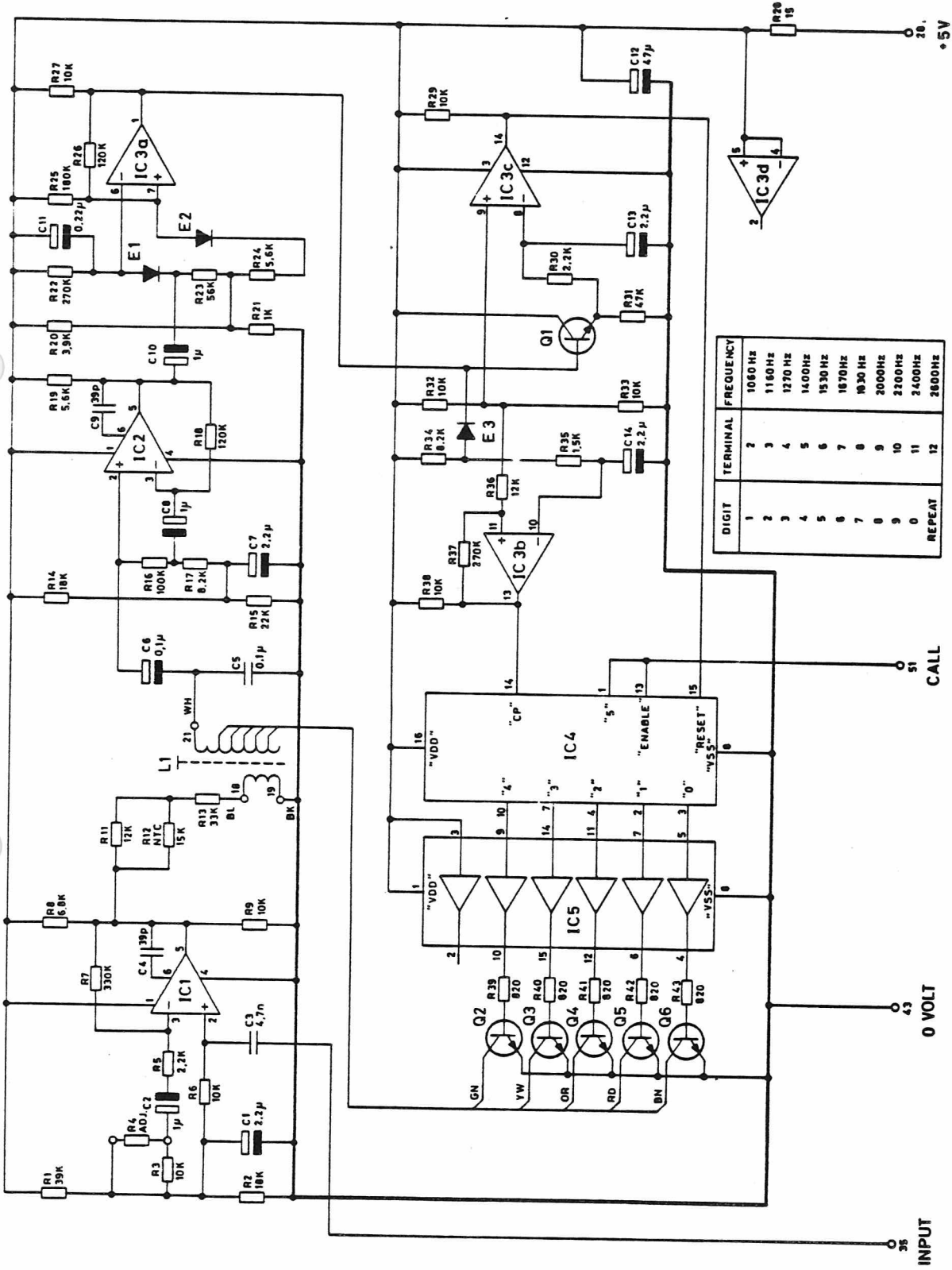
Storno

TYPE	NO.	CODE	DATA
	Q13	99. 5143	BC108 Transistor
	Q14	99. 5143	BC108 Transistor
	IC1	14. 5017	Operational Amplifier
	IC2	14. 5017	Operational Amplifier
	IC3	14. 5019	Quadruple comparator
	IC4	14. 5018	Quadruple 2-input pos. NOR Gate
	IC5	14. 5018	Quadruple 2-input pos. NOR Gate
	IC6	14. 5008	Dual J-K master-Slave Flip-Flop
	IC7	14. 5008	Dual J-K master-Slave Flip-Flop
	IC8	14. 5056	Dual J-K master-Slave Flip-Flop
	IC9	14. 5055	Voltage regulator

**SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER**

SR781

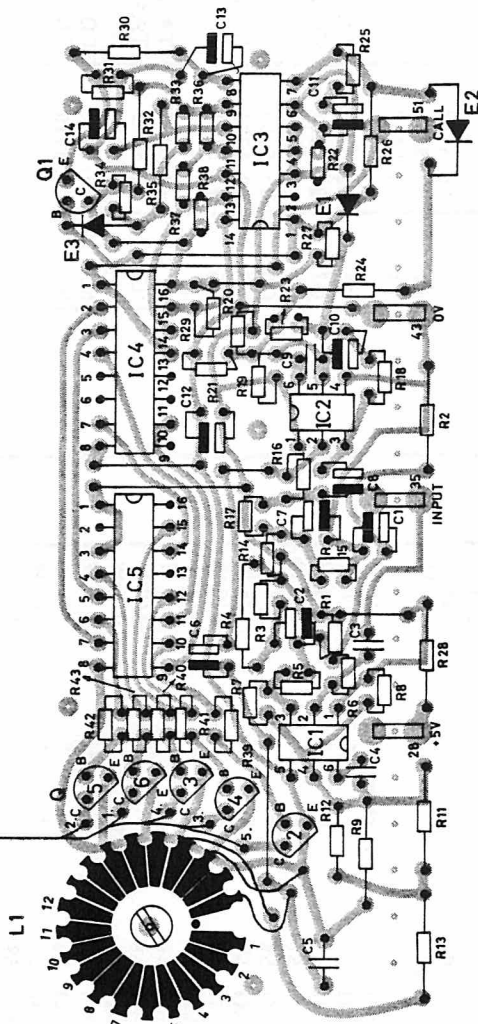
X401. 962



SEQUENTIAL TONE RECEIVER SR783

D402.372

- DIGIT
- | | |
|----|-----|
| 1. | BN. |
| 2. | RD. |
| 3. | OR. |
| 4. | YW. |
| 5. | GN. |



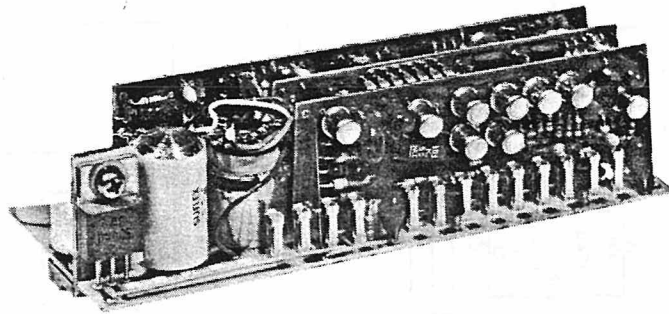
PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE.

SEQUENTIAL TONE RECEIVER SR783

D4C2.511

SEQUENTIAL TONE RECEIVER

SR785



Introduction

SR785 is a sequential tone receiver for selective calling. It was developed for use in Stornophone 700 radiotelephone equipment. The frequencies employed are the standard Storno series: 970 Hz to 2800 Hz.

SR785 is designed to operate on a 5-tone sequence, but can also be set to accommodate a 4-tone sequence.

General Description

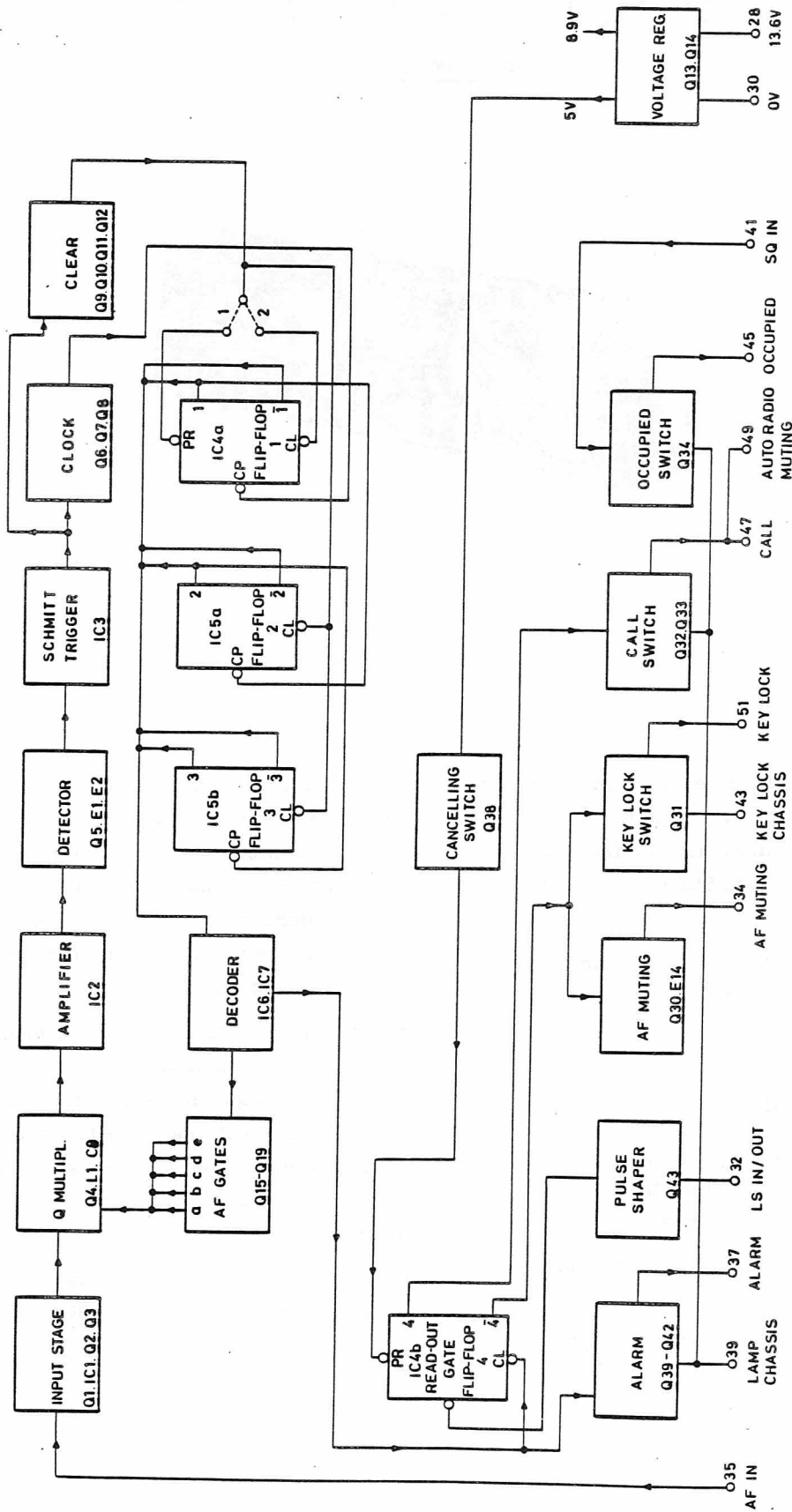
Upon reception of a signal having the correct tones in the proper sequence the following events take place (in the receiver):

The Call Lamp lights, the AF Muting is cancelled and the Key Lock function "unlocks". When the vehicle's traffic horn is connected to the tone receiver via an auxiliary relay, the horn will also sound for about one second.

The audio circuit and the Key Lock are both turned on and off manually by means of the LS IN/OUT push button. Since the switch that "unlocks" the Key Lock also turns on the loudspeaker, the operator is forced to check for the presence of another signal on the channel before being able to key his transmitter.

In addition, the tone receiver is equipped with an Occupied Lamp controlled by the squelch circuit in the radiotelephone receiver. Thus, if an RF signal having that channel's frequency is present at the antenna input it will cause the Occupied Lamp to light as an indication that the channel is not free.

After reception of a correct call the speaker will remain open until the LS IN/OUT button is depressed.



NOTE:
 FOR 4-TONE CALLING: INSERT STRAP 1.
 FOR 5-TONE CALLING: INSERT STRAP 2.

SR785

Logic Terms

Positive logic is employed in SR785; logical references are:

1. low voltage level ($\sim 0\text{ V}$) = logic state "0" (LO)
2. high voltage level ($\sim 5\text{ V}$) = logic state "1" (HI)

5-tone Signalling

The Input Stage includes Q1, IC1, Q2 and Q3. The first tone of a sequential tone signal, arriving from input terminal 35, passes through the input stage, where it becomes suitable for applying to the Q Multiplier.

In stand by the Q Multiplier is tuned, via AF Gate a, for the first tone of its code. If the first tone received corresponds to the circuit resonant frequency, it becomes selected, is then amplified in IC2 and rectified at the Detector, Q5, E1, and E2.

The rectified signal turns the Schmitt Trigger, IC3, ON. The output of IC3 becomes logic "1" and suspends the Clear function (Q9 - Q12). Binary Counters FF1 to FF3 are then ready to count.

A 25 ms delay is introduced between the time that the Schmitt Trigger output becomes logic "1" and the clock pulse from the Clock stage goes "1".

When the 1st tone ends, the Schmitt Trigger output goes "0" again, bringing the Clock output to logic "0". Counter FF1 then switches state, also causing the Decoder (IC6 and IC7) to step to the next AF gate, which is b.

The output of the Clear stage remains at logic "1" for about 40 ms after the Schmitt Trigger has returned to "0". The next (2nd) tone must be received within that time or the Clear function will reset the Counter and the Decoder will go back to stand by, i. e. ready to receive the 1st tone again.

The 2nd, 3rd, 4th, and 5th tones of a sequence occur like the 1st, each time stepping the Decoder one position forward until the final tone is received. At the end of the 5th tone the IC7_c output goes "0" which causes the Alarm circuit to ground terminal 37. A relay connected here will sound the traffic horn for approximately 1 second.

IC7_c also clears the Read-out Gate, FF4. This lights the Call Lamp via FF4 output 4 and terminal 47 while turning the speaker ON via output $\bar{4}$ and terminal 34.

The Call Lamp and the speaker will remain ON until switched OFF manually with the LS IN/OUT push button (via terminal 32).

When the channel is occupied (a carrier wave being received) the receiver squelch circuit feeds a voltage to terminal 41 (SQUELCH IN). The Occupied Lamp lights via terminal 45.

The Key Lock disables the transmitter via terminal 51. The voltage regulator will only supply power to the transmitter section when terminal 51 (KEY LOCK) from SR785 is at chassis ground potential.

Conditions for transmitting are:

- AF Muting cancelled (term. 34 LO)
- Call Lamp ON (term. 47 to ground)
- Key Lock cancelled (term. 51 to ground)

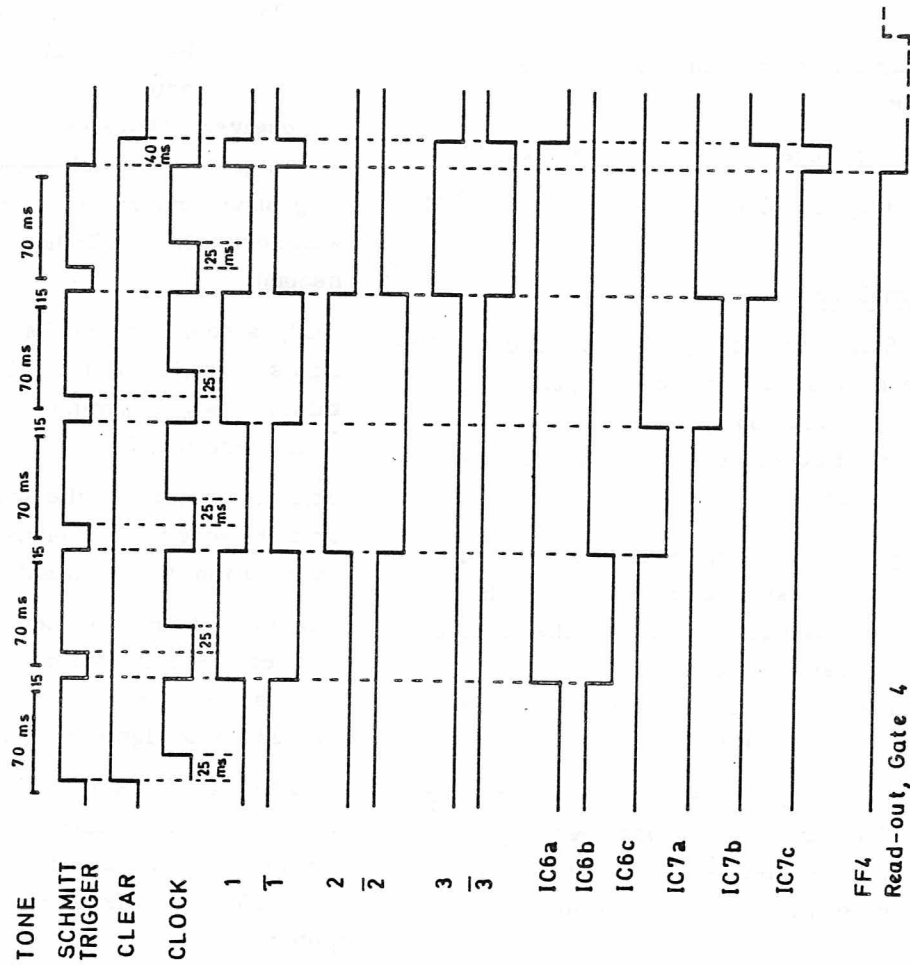
Approximately 40 ms after the last tone in the sequence, the Clear output goes "0", clearing Counter FF1 - FF3. AF Gate a is then set to wait for the 1st tone of a new call.

4-tone Signals

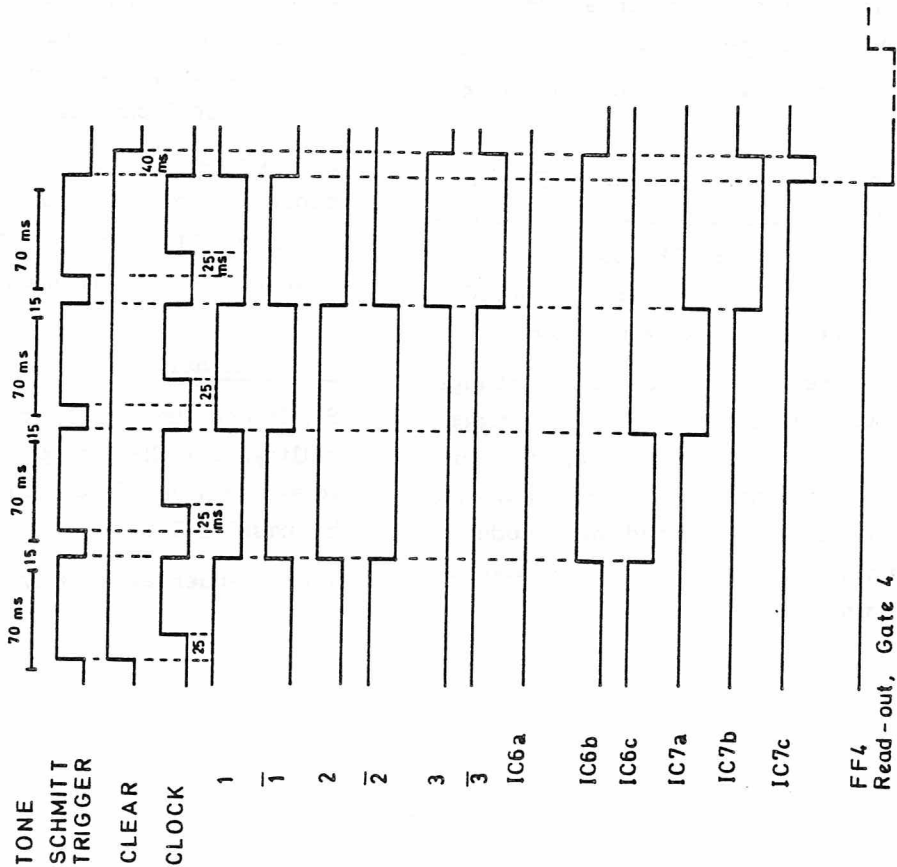
SR785 can also be strapped for 4-tone code signalling. The Clear output will then preset FF1 to switch in AF Gate b when in stand by, thus by-passing Gate a.

Pulse sequences for 4 and 5-tone signals follow:

5-TONE PULSE SEQUENCE



4-TONE PULSE SEQUENCE



Input Stage (Q1, IC1, Q2, Q3)

The pre-emphasis network includes Q1, R4 and C4.

IC1 is a linear amplifier. Signal clipping begins when the signal amplitude approaches the supply voltage level (5V). Full amplitude limiting occurs when the input signal is 6 dB above the nominal 110 mV value.

R5 and R8 determine the amplifier gain. Voltage divider R6 and R7 sets the DC output level.

The limiting action and the narrow pass-band of the subsequent Q Multiplier ensure selectivity. Tones differing by at least 4.5 % from the resonant frequency will not be able to trigger the tone receiver.

Transistors Q2 and Q3 are arranged so that they present an extremely low output impedance (on the order of 1Ω) which is suitable as a common return connection for the resonant circuit in the following stage.

Q Multiplier (Q4)

The Q Multiplier involves a parallel resonant circuit, L1 and C8. This is very loosely coupled to the transistor, Q4, in order to maintain a constant Q over the entire tone range. C8 in the resonant circuit is grounded through the output impedances of the driver transistors while the relevant terminals of coil L1 are alternately grounded through the AF Gates, a - e (Q15 - Q19).

A portion of the tone signal is reapplied to L1 in phase by means of a feedback winding in the collector circuit of Q4, approximately doubling the Q of L1.

To offset the effect of temperature upon the Q of L1 an NTC resistor, R19, is inserted in the emitter circuit of Q4. R19, aided by R17 and R18, maintains a nearly flat temperature response from -30°C to $+80^{\circ}\text{C}$.

Amplifier (IC2)

The signal from the Q Multiplier is DC coupled to the non-inverting input of IC2. Amplifier gain, and thus trigger level for the Schmitt Trigger, is adjustable by changing the value of R20.

Detector (Q5, E1, E2)

Emitter follower Q5 drives the voltage doubling rectifier circuit.

Schmitt Trigger (IC3)

The Schmitt Trigger is an operational amplifier working as a threshold detector to control the Clock and the Clear settings. The threshold voltage is set by network R29, E3, and R30.

In stand by the state of the non-inverting input is logic "0", thus the trigger output is also "0". When the rectified DC voltage from the Detector surpasses the threshold the Schmitt Trigger switches state and the output goes "1".

Clock (Q6, Q7, Q8)

The Clock toggles Counter FF1 after first introducing a 25 ms delay in order to prevent erratic operation. The Clock output pulse is delayed until the Schmitt Trigger has displayed a logic "1" output state for approx. 25 ms. Delay time is adjustable by means of R35.

In stand by the output state of IC3 is "0", holding Q6, Q7, and Q8 ON. Clock output is also "0". When IC3 triggers, its output goes logic "1". This cuts off Q6, and C16 begins charging through R34 in parallel with R35. After the set delay time, Q7 becomes reverse biased and cuts off, turning Q8 OFF. Clock output at the collector of Q8 goes "1".

When the tone ends, the Schmitt Trigger returns to its quiescent state and Q6 goes ON and C16 discharges rapidly through Q6 and R36, turning Q7, then Q8 ON. Clock output switches to logic state "0", and FF1 toggles.

Clear Circuit (Q9 - Q12, E5, E6)

The Clear circuit sets the Counter to stand by approx. 40 ms after the last correct tone arrives. Where the tone code is correct for the receiver setting the last tone will, of course, be the 5th tone (4th tone with 4-tone signalling). In the event of an incorrect tone code, the tone receiver will respond normally until one of the tones in the false sequence fails to match the resonant frequency set up by the AF Gates. Since each

tone lasts for about 70 ms, the Clear circuit will have reset the Counter to stand by before the incorrect tone expires and prior to the arrival of the next tone.

Emitter follower Q9 is driven by the Schmitt Trigger output through diode E5. In stand by, E5 cannot conduct, and Q9 is OFF. Q10, Q11, and Q12 are all ON, and output is at logic "0".

When the Schmitt Trigger output goes "1", E5 conducts, turning Q9 ON. C18 discharges through Q9, whereby Q10, Q11, and Q12 go OFF (output state "1"). The Counter is now able to start counting.

At the end of a tone E5 stops conducting (trigger output at "0" again) and C18 charges through R42 and R43. The charge building up on C18 eventually overcomes the emitter bias and turns Q10 ON. Emitter voltage for Q10, and thus the time elapsing before the Clear circuit returns to its quiescent state, is determined by voltage divider R45 and R46. When Q10 conducts, it turns Q11 and Q12 ON, as well, resetting the Counter to stand by.

The 40 ms delay is measured as the time elapsed between the Schmitt Trigger output "0" and when the Clear output goes "0".

Tones in a sequence arrive with maximum 15 ms interval between them, which is fast enough to keep the Clear output at "1".

When battery voltage is initially applied to the circuit a positive pulse is fed through E6 to the base of Q11, driving Q12 into saturation and ensuring that the Counter is cleared and ready to accommodate an incoming call.

Counter FF1 - FF3 (IC4_a, IC5_a, IC5_b)

The Counter is composed of three J-K master-slave flip-flops with their J-K inputs all tied to logic state "1" through resistor R87. Each FF will thus toggle whenever it receives a clock pulse at the same time that its Clear input is held at "1". The Clock stage toggles FF1, FF1 toggles FF2, and FF2 toggles FF3.

FF1 has a Preset as well as a Clear function, allowing the tone receiver to be strapped to either 4-tone or 5-tone sequences.

Truth tables for these two modes follow:

Truth Table for the Counter

5-tone

	1	$\bar{1}$	2	$\bar{2}$	3	$\bar{3}$
Cleared (pending call)	0	1	0	1	0	1
After the first tone	1	0	0	1	0	1
After the second tone	0	1	1	0	0	1
After the third tone	1	0	1	0	0	1
After the fourth tone	0	1	0	1	1	0
After the fifth tone	1	0	0	1	1	0
40 ms after the last tone (cleared pending call)	0	1	0	1	0	1

4-tone

	1	$\bar{1}$	2	$\bar{2}$	3	$\bar{3}$
Preset (pending call)	1	0	0	1	0	1
After the first tone	0	1	1	0	0	1
After the second tone	1	0	1	0	0	1
After the third tone	0	1	0	1	1	0
After the fourth tone	1	0	0	1	1	0
40 ms after the last tone (cleared pending call)	1	0	0	1	0	1

Decoder (IC6, IC7)

Each Decoder IC contains 3 separate, 3-input TTL NAND gates.

The output of a NAND gate is LO (logic "0") only when all of its inputs are HI (logic "1").

In stand by, 5-tone mode, the output of IC6_a is always "0". In the 4-tone mode, the output of IC6_b will be "0", instead.

At the end of a correct tone call IC7_c presents a logic "0" to the Read-out Gate and to the Alarm circuit. The Alarm output, terminal 37, goes "0" through Q42.

AF Gates a, b, c, d, e (Q15 - Q19)

The AF Gates are controlled from the Decoder NAND gates, IC6_a - IC7_b. When a transistor

base is driven L0 (logic "0") by a NAND gate, that transistor will conduct and ground the coil terminal connected to its collector.

Alarm Circuit (Q39 - Q42, E18)

In stand by, Q39 is ON and E18 cannot conduct. Q40 and Q41 are both ON, and Q42 is OFF.

A correct call turns Q39 OFF and C46 charges through E18, causing Q40 and Q41 to turn OFF, driving Q42 ON, and connecting terminal 37 (ALARM) to chassis ground.

After approximately 40 ms (the clear delay) IC7_c goes "1" and turns Q39 ON again. E18 can no longer conduct and C46 discharges through R114. After the delay caused by the time constant of C46 - R114, Q40 and Q41 turn ON and disconnect the Alarm circuit common return through Q42. The Alarm stays ON for approximately 1 second.

AF Muting and Key Lock Switch (Q30, Q31, E14)

The AF Muting and the Key Lock are controlled by the output of Read-out Gate IC4_b (output $\bar{4}$).

In stand by the outputs of Q30 and Q31 are HI ($\sim +10V$), E14 conducts and the loudspeaker is muted through terminal 34.

As long as the potential at terminal 51 is HI, the transmitter keying function is also disabled.

When the Read-out Gate is activated, output $\bar{4}$ goes "1", and Q30 and Q31 conduct, suspending the AF Muting and Key Lock functions.

Call and Occupied Lamp Switches (Q32, Q33, Q34)

The Call Lamp Switch, Q33, lights the Call Lamp by grounding it through terminal 47.

Terminal 49, in parallel with terminal 47, is provided for automatic muting of the vehicle's broadcast band radio, and requires an auxiliary relay.

At the end of a tone sequence, output 4 of FF4 goes "0", cutting Q32 OFF and turning Q33 ON, to complete the common return path for terminals 47 and 49.

Whenever the channel is occupied a DC voltage, from the Squelch circuit, via terminal 41, turns Q34 ON, grounding the Occupied Lamp through terminal 45.

Cancelling Switch (Q38)

When the radiotelephone is turned ON the output functions must not be activated. To ensure this, Q38 feeds a negative pulse ("0") to the Preset of the Read-out Gate. When the battery voltage is switched ON, C41 discharges through Q38 which goes ON briefly, presetting the Read-out Gate.

Technical Specifications

Supply Power

Nominal: 13.6 V
Minimum: 10.5 V
Maximum: 16.0 V

Current Drain

Stand by: 100 mA \pm 15 mA

Regulated Voltages

Nominal: 8.9 V and 4.9 V

Temperature Range

Operating range: $-25^{\circ}C$ to $+60^{\circ}C$
Functioning range: $-30^{\circ}C$ to $+80^{\circ}C$

Input Impedance

$\geq 6 K\Omega$

Signal Input Level

Nominal at 1000 Hz: 110 mV

Equalization

Preemphasis (by RC function) $f_c = 1000$ Hz

Signalling Code

Sequence of 4 or 5 tone bursts of 70 ms \pm 15 ms duration with maximum 15 ms interval between tone bursts.

Tone Signal Frequencies

<u>Coil terminal</u>	<u>Tone frequency</u>
1	970 Hz
2	1060 Hz
3	1160 Hz
4	1270 Hz
5	1400 Hz
6	1530 Hz
7	1670 Hz
8	1830 Hz
9	2000 Hz
10	2200 Hz
11	2400 Hz
12	2600 Hz
13	2800 Hz

Frequency Accuracy

Coil tuned for 1060 Hz: $\leq 0.4\%$ for all tones

Frequency Stability

(typically $\leq 0.5\%$): $\leq 1.0\%$

Selectivity

Frequencies differing from f_0 by 4.5% or more are unable to trigger the tone receiver.

Maximum Load Currents

Terminal 37 ALARM 100 mA (for 1.2 sec)

Terminal 47 CALL 100 mA

Terminal 45 OCCUPIED 100 mA

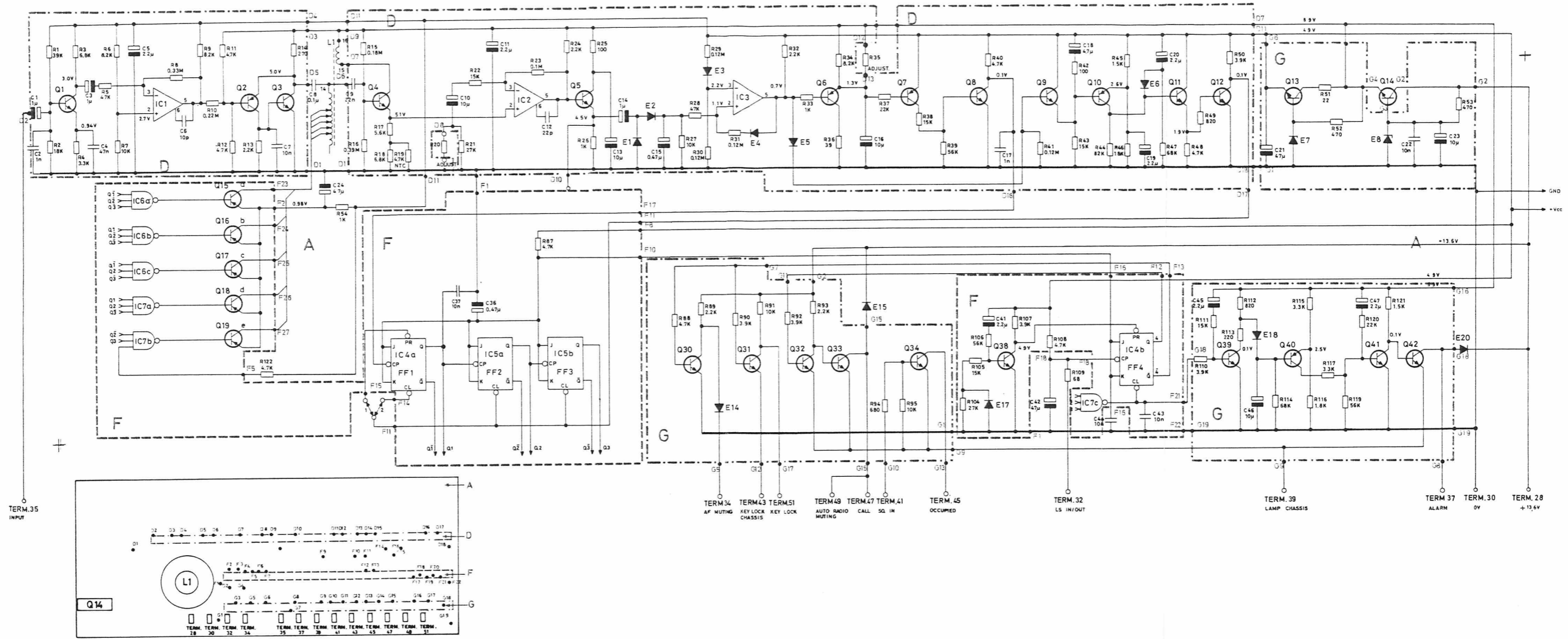
Terminal 51

and 43 KEY LOCK 10 mA

Terminal 34 AF MUTING I_{load} min. 0.75 mA
for $V_{out} = 8 V$

AF Muting

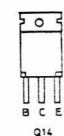
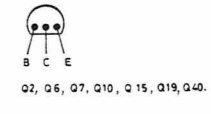
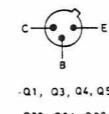
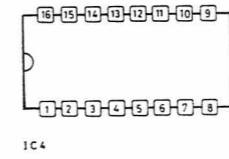
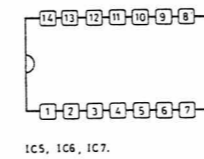
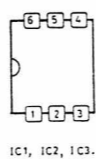
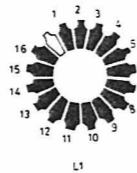
In conjunction with terminal 18 of CF701:
 ≥ 60 dB.



4-TONE SEQUENTIAL RECEIVER: INSERT STRAP 1
 5-TONE SEQUENTIAL RECEIVER: INSERT STRAP 2

TERM.	DIGIT	FREQ.
1	X	970 Hz
2	1	1060 -
3	2	1160 -
4	3	1270 -
5	4	1400 -
6	5	1530 -
7	6	1670 -
8	7	1830 -
9	8	2000 -
10	9	2200 -
11	0	2400 -
12	REPEAT	2600 -
13	ALARM	2800 -

IC	Vcc PIN	GND PIN
IC1	2	6
IC2	2	6
IC3	2	6
IC4	5	13
IC5	4	11
IC6	14	7
IC7	14	7

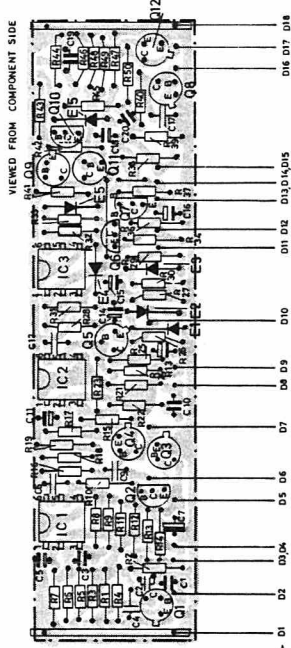


Q1, Q3, Q4, Q5, Q8, Q9, Q11, Q12, Q13, Q30, Q34, Q38, Q39, Q41, Q42.

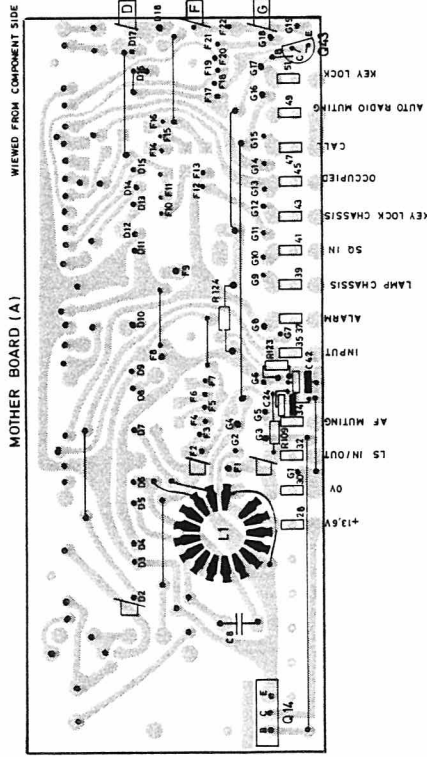
BOTTOM VIEW

TOP VIEW

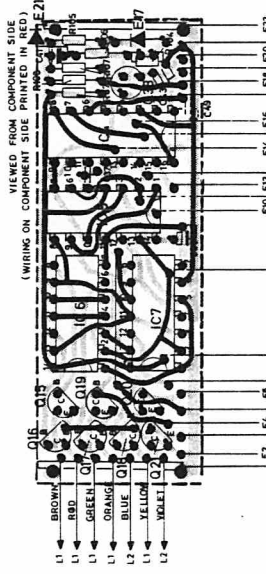
INDIVIDUAL CHAIN (D)



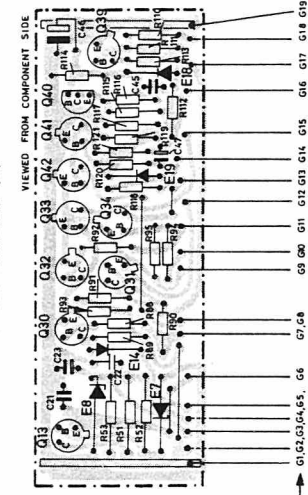
MOTHER BOARD (A)



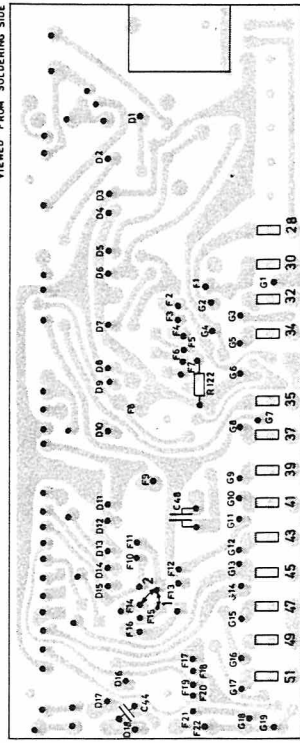
COUNTER AND DECODER (F)



OUTLET SWITCHES (G)



VIEWED FROM SOLDERING SIDE



TYPE	NO.	CODE	DATA
SR785		10. 2541	Sequential Tone Receiver
	C1	73. 5135	1μF -20 + 50% tantal
	C2	76. 5069	1nF 10% polyester, FL
	C3	73. 5135	1μF -20 + 50% tantal
	C4	76. 5072	47nF 10% polyester, FL
	C5	73. 5129	2. 2μF -20 + 50% tantal
	C6	74. 5135	10pF 5% ceram
	C7	76. 5070	10nF 10% polyester, FL
	C8	76. 5068	0. 1μF 1% polystyr TB
	C9	76. 5071	22nF 10% polyester, FL
	C10	73. 5109	10μF 20% tantal
	C11	73. 5129	2. 2μF -20 + 50% tantal
	C12	74. 5106	22pF ± 0. 5pF ceram
	C13	73. 5109	10μF 20% tantal
	C14	73. 5114	1μF 20% tantal
	C15	73. 5125	0. 47μF 20% tantal
	C16	73. 5109	10μF 20% tantal
	C17	76. 5069	1nF 10% polyester, FL
	C18	73. 5126	4. 7μF 20% tantal
	C19	73. 5129	2. 2μF -20 + 50% tantal
	C20	73. 5129	2. 2μF -20 + 50% tantal
	C21	73. 5124	47μF 20% tantal
	C22	76. 5070	10nF 10% polyester, FL
	C23	73. 2109	10μF 20% tantal
	C24	73. 5124	47μF 20% tantal
	C36	73. 5134	0. 47μF -20 + 50% tantal
	C37	74. 5109	10nF -20 + 80% ceram PL
	C41	73. 5129	2. 2μF -20 + 50% tantal
	C42	73. 5124	47μF 20% tantal
	C43	74. 5109	10nF -20 + 80% ceram PL
	C44	74. 5109	10nF -20 + 80% ceram PL
	C45	73. 5129	2. 2μF -20 + 50% tantal
	C46	73. 5109	10μF 20% tantal
	C47	73. 5129	2. 2μF -20 + 50% tantal
	R1	80. 5068	39kΩ 5% carbon film
	R2	80. 5064	18kΩ 5% carbon film
	R3	80. 5059	6. 8kΩ 5% carbon film
	R4	80. 5055	3. 3kΩ 5% carbon film
	R5	80. 5059	47kΩ 5% carbon film
	R6	80. 5060	8. 2kΩ 5% carbon film
	R7	80. 5061	10kΩ 5% carbon film
	R8	80. 5079	0. 39MΩ 5% carbon film
	R9	80. 5060	8. 2kΩ 5% carbon film
	R10	80. 5077	0. 22MΩ 5% carbon film
	R11	80. 5057	4. 7kΩ 5% carbon film

TYPE	NO.	CODE	DATA
	R12	80. 5057	4. 7kΩ 5% carbon film
	R13	80. 5053	2. 2kΩ 5% carbon film
	R14	80. 5042	270Ω 5% carbon film
	R15	80. 5076	0. 18MΩ 5% carbon film
	R16	80. 5080	0. 39MΩ 5% carbon film
	R17	80. 5058	5. 6kΩ 5% carbon film
	R18	80. 5059	6. 8kΩ 5% carbon film
	R19	89. 5009	4. 7kΩ 20% NTC
	R20	80. 50xx	Adjusted 5% carbon film
	R21	80. 5066	27kΩ 5% carbon film
	R22	80. 5063	15kΩ 5% carbon film
	R23	80. 5073	0. 1MΩ 5% carbon film
	R24	80. 5053	2. 2kΩ 5% carbon film
	R25	80. 5037	100Ω 5% carbon film
	R26	80. 5049	1kΩ 5% carbon film
	R27	80. 5061	10kΩ 5% carbon film
	R28	80. 5069	47kΩ 5% carbon film
	R29	80. 5074	0. 12MΩ 5% carbon film
	R30	80. 5074	0. 12MΩ 5% carbon film
	R31	80. 5074	0. 12MΩ 5% carbon film
	R32	80. 5053	2. 2kΩ 5% carbon film
	R33	80. 5049	1kΩ 5% carbon film
	R34	80. 5060	8. 2kΩ 5% carbon film
	R35	80. 50xx	Adjusted 5% carbon film
	R36	80. 5032	39Ω 5% carbon film
	R37	80. 5065	22kΩ 5% carbon film
	R38	80. 5063	15kΩ 5% carbon film
	R39	80. 5070	56kΩ 5% carbon film
	R40	80. 5057	4. 7kΩ 5% carbon film
	R41	80. 5074	0. 12MΩ 5% carbon film
	R42	80. 5037	100Ω 5% carbon film
	R43	80. 5063	15kΩ 5% carbon film
	R44	80. 5072	82kΩ 5% carbon film
	R45	80. 5051	1. 5kΩ 5% carbon film
	R46	80. 5052	1. 8kΩ 5% carbon film
	R47	80. 5071	68kΩ 5% carbon film
	R48	80. 5057	4. 7kΩ 5% carbon film
	R49	80. 5048	820Ω 5% carbon film
	R50	80. 5056	3. 9kΩ 5% carbon film
	R51	80. 5229	22Ω 5% carbon film
	R52	80. 5245	470Ω 5% carbon film
	R53	80. 5245	470Ω 5% carbon film

**SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER**

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X401. 701

TYPE	NO.	CODE	DATA
	R54	80. 5049	1k Ω 5% carbon film
	R87	80. 5057	4. 7k Ω 5% carbon film
	R88	80. 5057	4. 7k Ω 5% carbon film
	R89	80. 5053	2. 2k Ω 5% carbon film
	R90	80. 5056	3. 9k Ω 5% carbon film
	R91	80. 5061	10k Ω 5% carbon film
	R92	80. 5056	3. 9k Ω 5% carbon film
	R93	80. 5053	2. 2k Ω 5% carbon film
	R94	80. 5047	680 Ω 5% carbon film
	R95	80. 5061	10k Ω 5% carbon film
	R104	80. 5066	27k Ω 5% carbon film
	R105	80. 5063	15k Ω 5% carbon film
	R106	80. 5070	56k Ω 5% carbon film
	R107	80. 5056	3. 9k Ω 5% carbon film
	R108	80. 5057	4. 7k Ω 5% carbon film
	R109	80. 5035	68 Ω 5% carbon film
	R110	80. 5056	3. 9k Ω 5% carbon film
	R111	80. 5063	15k Ω 5% carbon film
	R112	80. 5048	820 Ω 5% carbon film
	R113	80. 5041	220 Ω 5% carbon film
	R114	80. 5071	68k Ω 5% carbon film
	R115	80. 5055	3. 3k Ω 5% carbon film
	R116	80. 5052	1. 8k Ω 5% carbon film
	R117	80. 5055	3. 3k Ω 5% carbon film
	R119	80. 5070	56k Ω 5% carbon film
	R120	80. 5065	22k Ω 5% carbon film
	R121	80. 5051	1. 5k Ω 5% carbon film
	R122	80. 5057	4. 7k Ω 5% carbon film
	L1	61. 1148	Tone coil
	E1	99. 5237	1N4148 Diode
	E2	99. 5237	1N4148 Diode
	E3	99. 5237	1N4148 Diode
	E4	99. 5237	1N4148 Diode
	E5	99. 5237	1N4148 Diode
	E6	99. 5237	1N4148 Diode
	E7	99. 5114	5. 6V 5% Zenerdiode
	E8	99. 5042	9. 1V 5% Zenerdiode
	E14	99. 5237	1N4148 Diode
	E15	99. 5020	1N4004 Diode
	E17	99. 5237	1N4148 Diode
	E18	99. 5237	1N4148 Diode
	E20	99. 5020	1N4004 Diode
	Q1	99. 5143	BC108 Transistor
	Q2	99. 5144	BC214L Transistor

TYPE	NO.	CODE	DATA
	Q3	99. 5143	BC108 Transistor
	Q4	99. 5143	BC108 Transistor
	Q5	99. 5143	BC108 Transistor
	Q6	99. 5144	BC214L Transistor
	Q7	99. 5144	BC214L Transistor
	Q8	99. 5143	BC108 Transistor
	Q9	99. 5143	BC108 Transistor
	Q10	99. 5144	BC214L Transistor
	Q11	99. 5143	BC108 Transistor
	Q12	99. 5143	BC108 Transistor
	Q13	99. 5143	BC108 Transistor
	Q14	99. 5246	TIP31 Transistor
	Q15	99. 5144	BC214L Transistor
	Q16	99. 5144	BC214L Transistor
	Q17	99. 5144	BC214L Transistor
	Q18	99. 5144	BC214L Transistor
	Q19	99. 5144	BC214L Transistor
	Q30	99. 5143	BC108 Transistor
	Q31	99. 5143	BC108 Transistor
	Q32	99. 5143	BC108 Transistor
	Q33	99. 5143	BC108 Transistor
	Q34	99. 5143	BC108 Transistor
	Q38	99. 5143	BC108 Transistor
	Q39	99. 5143	BC108 Transistor
	Q40	99. 5143	BC108 Transistor
	Q41	99. 5143	BC108 Transistor
	Q42	99. 5143	BC108 Transistor
	IC1	14. 5017	TAA861 Operational Amplifier
	IC2	14. 5017	TAA861 Operational Amplifier
	IC3	14. 5017	TAA861 Operational Amplifier
	IC4	14. 5009	Dual J-K Master-slave F. F. Clear/pres.
	IC5	14. 5008	Dual J-K Master-slave F. F. Clear
	IC6	14. 5007	Triple 3-input NAND Gate
	IC7	14. 5007	Triple 3-input NAND Gate

**SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER**

SR785

X401.701

TYPE	NO.	CODE	DATA
SR785		10.2541	Sequential Tone Receiver
	C1	73.5135	1μF -20 + 50% tantal
	C2	76.5069	1nF 10% polyest. FL
	C3	73.5135	1μF -20 + 50% tantal
	C4	76.5072	47nF 10% polyest. FL
	C5	73.5129	2.2μF -20 + 50% tantal
	C6	74.5135	10pF 5% ceram
	C7	76.5070	10nF 10% polyest. FL
	C8	76.5068	0.1μF 1% polystyr TB
	C9	76.5071	22nF 10% polyest. FL
	C10	73.5109	10μF 20% tantal
	C11	73.5129	2.2μF -20 + 50% tantal
	C12	74.5106	22pF ± 0.5pF ceram
	C13	73.5109	10μF 20% tantal
	C14	73.5114	1μF 20% tantal
	C15	73.5125	0.47μF 20% tantal
	C16	73.5109	10μF 20% tantal
	C17	76.5069	1nF 10% polyest. FL
	C18	73.5126	4.7μF 20% tantal
	C19	73.5129	2.2μF -20 + 50% tantal
	C20	73.5129	2.2μF -20 + 50% tantal
	C21	73.5124	47μF 20% tantal
	C22	76.5070	10nF 10% polyest. FL
	C23	73.2109	1μF 20% tantal
	C24	73.5124	47μF 20% tantal
	C36	74.5134	0.47μF -20+50% tantal
	C37	74.5109	10 nF -20+80% ceram PL
	C41	73.5129	2.2μF -20+50% tantal
	C42	73.5129	2.2μF -20+50% tantal
	C43	74.5109	10nF -20+80% ceram PL
	C44	74.5109	10nF -20+80% ceram PL
	C45	73.5129	2.2μF -20+50% tantal
	C46	73.5109	10μF 20% tantal
	C47	73.5129	2.2μF -20+50% tantal
	C48	76.5070	10 nF 10% polyest. FL
	C49	74.5155	1 nF -20+80% ceram PL
	R1	80.5068	39 kΩ 5% carbon film
	R2	80.5064	18 kΩ 5% carbon film
	R3	80.5059	6.8kΩ 5% carbon film
	R4	80.5055	3.3kΩ 5% carbon film
	R5	80.5069	47kΩ 5% carbon film
	R6	80.5060	8.2kΩ 5% carbon film
	R7	80.5061	10kΩ 5% carbon film
	R8	80.5079	0.39 MΩ 5% carbon film
	R9	80.5060	8.2kΩ 5% carbon film
	R10	80.5077	0.22 MΩ 5% carbon film
	R11	80.5057	4.7kΩ 5% carbon film

TYPE	NO.	CODE	DATA
	R12	80.5057	4.7kΩ 5% carbon film
	R13	80.5053	2.2kΩ 5% carbon film
	R14	80.5042	270Ω 5% carbon film
	R15	80.5076	0.18MΩ 5% carbon film
	R16	80.5080	0.39MΩ 5% carbon film
	R17	80.5058	5.6kΩ 5% carbon film
	R18	80.5059	6.8kΩ 5% carbon film
	R19	89.5009	4.7kΩ 20% NTC
	R20	80.50xx	Adjusted 5% carbon film
	R21	80.5066	27kΩ 5% carbon film
	R22	80.5063	15kΩ 5% carbon film
	R23	80.5073	0.1MΩ 5% carbon film
	R24	80.5053	2.2kΩ 5% carbon film
	R25	80.5037	100Ω 5% carbon film
	R26	80.5049	1kΩ 5% carbon film
	R27	80.5061	10kΩ 5% carbon film
	R28	80.5069	47kΩ 5% carbon film
	R29	80.5074	0.12MΩ 5% carbon film
	R30	80.5074	0.12MΩ 5% carbon film
	R31	80.5074	0.12MΩ 5% carbon film
	R32	80.5053	2.2kΩ 5% carbon film
	R33	80.5049	1kΩ 5% carbon film
	R34	80.5060	8.2kΩ 5% carbon film
	R35	80.50xx	Adjusted 5% carbon film
	R36	80.5032	3Ω 5% carbon film
	R37	80.5065	22kΩ 5% carbon film
	R38	80.5063	15kΩ 5% carbon film
	R39	80.5070	56kΩ 5% carbon film
	R40	80.5057	4.7kΩ 5% carbon film
	R41	80.5074	0.12MΩ 5% carbon film
	R42	80.5037	100Ω 5% carbon film
	R43	80.5063	15kΩ 5% carbon film
	R44	80.5072	82kΩ 5% carbon film
	R45	80.5051	1.5kΩ 5% carbon film
	R46	80.5052	1.8kΩ 5% carbon film
	R47	80.5071	68kΩ 5% carbon film
	R48	80.5057	4.7kΩ 5% carbon film
	R49	80.5048	820Ω 5% carbon film
	R50	80.5056	3.9kΩ 5% carbon film
	R51	80.5229	22Ω 5% carbon film
	R52	80.5245	470Ω 5% carbon film
	R53	80.5245	470Ω 5% carbon film

SEQUENTIAL TONE RECEIVER
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TYPE	NO.	CODE	DATA
	R54	80.5049	1k Ω 5% carbon film
	R87	80.5057	4.7k Ω 5% carbon film
	R88	80.5057	4.7k Ω 5% carbon film
	R89	80.5053	2.2k Ω 5% carbon film
	R90	80.5056	3.9k Ω 5% carbon film
	R91	80.5061	10k Ω 5% carbon film
	R92	80.5056	3.9k Ω 5% carbon film
	R93	80.5053	2.2k Ω 5% carbon film
	R94	80.5047	680 Ω 5% carbon film
	R95	80.5061	10k Ω 5% carbon film
	R104	80.5066	27k Ω 5% carbon film
	R105	80.5063	15k Ω 5% carbon film
	R106	80.5070	56k Ω 5% carbon film
	R107	80.5056	3.9k Ω 5% carbon film
	R108	80.5057	4.7k Ω 5% carbon film
	R109	80.5027	15 Ω 5% carbon film
	R110	80.5056	3.9k Ω 5% carbon film
	R111	80.5063	15k Ω 5% carbon film
	R112	80.5048	820 Ω 5% carbon film
	R113	80.5041	220 Ω 5% carbon film
	R114	80.5071	68k Ω 5% carbon film
	R115	80.5055	3.3k Ω 5% carbon film
	R116	80.5052	1.8k Ω 5% carbon film
	R117	80.5055	3.3k Ω 5% carbon film
	R119	80.5070	56k Ω 5% carbon film
	R120	80.5065	22k Ω 5% carbon film
	R121	80.5051	1.5k Ω 5% carbon film
	R122	80.5057	4.7k Ω 5% carbon film
	R123	80.5072	82 K Ω 5% carbon film
	R124	80.5064	18 K Ω 5% carbon film
	L1	61.1148	Tone coil
	E1	99.5237	1N4148 Diode
	E2	99.5237	1N4148 Diode
	E3	99.5237	1N4148 Diode
	E4	99.5237	1N4148 Diode
	E5	99.5237	1N4148 Diode
	E6	99.5237	1N4148 Diode
	E7	99.5114	5.6V 5% Zenerdiode
	E8	99.5042	9.1V 5% Zenerdiode
	E14	99.5237	1N4148 Diode
	E17	99.5237	1N4148 Diode
	E18	99.5237	1N4148 Diode
	Q1	99.5143	BC108 Transistor
	Q2	99.5144	BC214L Transistor

TYPE	NO.	CODE	DATA
	Q3	99.5143	BC108 Transistor
	Q4	99.5143	BC108 Transistor
	Q5	99.5143	BC108 Transistor
	Q6	99.5144	BC214L Transistor
	Q7	99.5144	BC214L Transistor
	Q8	99.5143	BC108 Transistor
	Q9	99.5143	BC108 Transistor
	Q10	99.5144	BC214L Transistor
	Q11	99.5143	BC108 Transistor
	Q12	99.5143	BC108 Transistor
	Q13	99.5143	BC108 Transistor
	Q14	99.5246	TIP31 Transistor
	Q15	99.5144	BC214L Transistor
	Q16	99.5144	BC214L Transistor
	Q17	99.5144	BC214L Transistor
	Q18	99.5144	BC214L Transistor
	Q19	99.5144	BC214L Transistor
	Q30	99.5143	BC108 Transistor
	Q31	99.5143	BC108 Transistor
	Q32	99.5143	BC108 Transistor
	Q33	99.5143	BC108 Transistor
	Q34	99.5143	BC108 Transistor
	Q38	99.5143	BC108 Transistor
	Q39	99.5143	BC108 Transistor
	Q40	99.5143	BC108 Transistor
	Q41	99.5143	BC108 Transistor
	Q42	99.5143	BC108 Transistor
	Q43	99.5117	BC167 Transistor
	IC1	14.5017	TAA861 Operational Amplifier
	IC2	14.5017	TAA861 Operational Amplifier
	IC3	14.5017	TAA861 Operational Amplifier
	IC4	14.5009	Dual J-K Master-slave F. F. Clear/pres.
	IC5	14.5008	Dual J-K Master-slave F. F. Clear
	IC6	14.5007	Triple 3-input NAND Gate
	IC7	14.5007	Triple 3-input NAND Gate

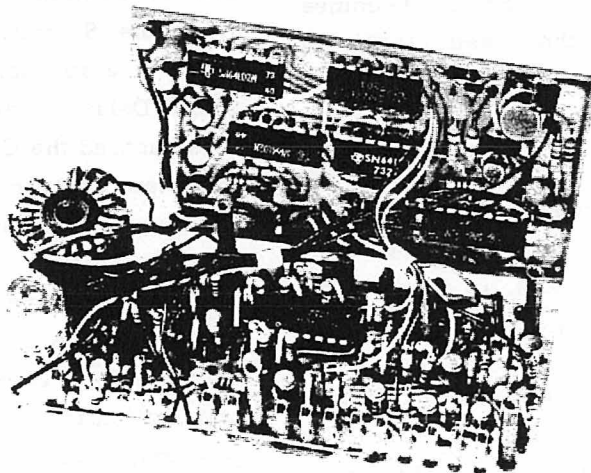
SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER

SR785

X401.701/2

SEQUENTIAL TONE RECEIVER

SR785a



Description

SR785a is a sequential tone receiver for selective calling. It was developed for use in Stornophone 700 radiotelephone equipment. The frequencies employed are the standard Storno series: 970 Hz to 2800 Hz.

SR785a is designed to operate on a 5-tone sequence, but can also be set to accommodate a 4-tone sequence.

GENERAL DESCRIPTION

Upon reception of a signal having the correct tones in the proper sequence the following events take place (in the receiver):

The Call Lamp lights, the AF Muting is cancelled and the Key Lock function "unlocks". An audio alarm signal of about 1.3 seconds in duration can be sent out over the radiotelephone's loudspeaker, and when the vehicle's traffic horn is connected to the tone receiver via an auxiliary relay, the horn will also sound for the same length of time.

There is also a provision for automatically turning off the car's broadcast band receiver when a call arrives.

The audio circuit and the Key Lock are both turned on and off manually by means of the LS IN/OUT push button. Since the switch that "unlocks" the Key Lock also turns on the loudspeaker, the operator is forced to check for the presence of another signal on the channel before being able to key his transmitter.

In addition, the tone receiver is equipped with an Occupied Lamp controlled by the squelch circuit in the radiotelephone receiver. Thus, if an RF signal having that channel's frequency is present at the antenna input it will cause the Occupied Lamp to light as an indication that the channel is not free.

After reception of a correct call the speaker will remain open until the LS IN/OUT button is depressed.

Logic Terms

Positive logic is employed in SR785a; logical references are:

1. low voltage level ($\sim 0V$) = logic state "0" (LO)
2. high voltage level ($\sim 5V$) = logic state "1" (HI)

Tone Signalling

The first tone of a sequential signal, arriving from input terminal 35, passes through the Amplifier/Limiter, IC1, where it becomes suitable for applying to the tuned circuit of L1 and C8.

In stand by the resonant frequency of the tuned Circuit is set up by the first Tone Gate, Q4, for the first tone of its code. If the first tone received corresponds to the circuit resonant frequency, it becomes selected, is then amplified by IC2 and detected by E1.

The correct tone will thus fire the Schmitt Trigger, IC3a, whose output drives the Clock Delay (CP Delay) circuit, IC3b. This circuit produces a Clock Pulse whose leading (positive going) edge is delayed approximately 15 msec. from the Schmitt Trigger output signal.

The clock pulse is applied to the Counter circuit, IC6a, IC7a and IC6b. The Counter is arranged as a synchronous, divide-by-5 counter whose binary states are read out in BCD (binary coded decimal) mode in the Decoders, IC4a-d and IC5a-b.

The first five Decoders drive the Tone Gates, Q4-Q8. The output of the sixth Decoder, IC5b, is applied to the Readout circuit, IC7b.

The Readout flip-flop is also timed by the same clock pulses that toggle the Counter flip-flops.

At the end of a tone pulse, the Schmitt Trigger reverts to its quiescent state and the resultant trailing (negative going) pulse edge from the CP Delay output causes the Counter flip-flops to change state. (So far, with just the first pulse completed, only Counter IC6a is affected.)

The Decoders sense the new binary state and turn Tone Gate Q4 OFF and Tone Gate Q5 ON, thus setting the resonant circuit up for the second tone in the sequential code.

Suppose that the next tone received does not match the receiver's code. It will not be selected by the resonant circuit and no signal will be available to fire the Schmitt Trigger. When the Schmitt Trigger was fired the first time, it also turned Q1 ON and activated the Clear Delay circuit, IC3c. The output of IC3c then enabled the Counters by applying a HI logical state to their Clear inputs. The Clear Delay output remains HI for about 70 msec. after the Schmitt Trigger has returned to "0". If the second tone does not activate the Schmitt Trigger by then, Q1 goes OFF and the Clear Delay output goes LO, clearing the counter and setting the Decoders back to the stand by position, i.e. ready to receive the first tone again. This is what happens if the second, or any consequent tone fails (for instance, if the tone is not the correct one for the particular receiver under consideration).

The 2nd, 3rd, 4th and 5th tones of a sequence occur like the 1st, each time stepping the Decoder one position forward until the final tone has been received.

When all five tones have been received, at the end of the 5th tone, IC7b clears the Holding Circuit, IC8, and turns transistor Q2 ON.

Q2 drives the Alarm Delay circuit.

All the functions mentioned in the beginning of this description, i.e. Call Lamp, AF Muting, Key Lock, Alarm Tone Generator, etc. occur at this time.

The Call Lamp and the speaker will remain ON until switched OFF manually with the LS IN/OUT push button (via terminal 32).

If the operator later wants to make a call, he must first "unlock" the Key Lock function with the LS IN/OUT push button again, thus turning the loudspeaker ON. If there is any traffic on his channel, he will hear it and be warned before he can key his transmitter.

CIRCUIT DESCRIPTIONInput Stage (IC1)

Input terminal 35 can be wired in either of two positions (marked DK and SV on schematic diagram D401.894):

DK = input signal through C2 and R1, linear response

SV = input signal differentiated through C1 to match the modulation index used in Sweden and by Storno.

The amplifier circuit incorporates amplitude limiting for signal levels above the minimum required to activate the Schmitt Trigger.

Resistor R6 sets the amplifier sensitivity.

Amplifier Stage (IC2)

The signal is inductively coupled to the Amplifier via the parallel resonant circuit, L1 and C8.

Five of the taps on tone coil L1 are wired to Tone Gates Q4 to Q8, respectively (with a 4-tone code, Q8 is not used). When a Tone Gate is ON, i.e. conducting, it completes a path from its coil tap to chassis ground and the parallel resonant circuit for that particular tone frequency is formed.

NTC resistor R13 compensates for variations in circuit Q caused by changes in ambient temperature.

The selected signal passes to operational amplifier IC2, which is bootstrapped so as not to load the resonant circuit. Amplifier gain is determined by the ratio of R17 to R19.

Detector and Schmitt Trigger (E1, E2, IC3a)

The amplified tone signal is then rectified by the forward-biased diode, E1, and filtered by C13. The resultant DC voltage is present at the inverting input of IC3a.

When the rectified voltage exceeds the threshold level set by R21, R22, R25, R26 and diode E2, the output of the Schmitt Trigger

switches from LO ($\sim 0V$) to HI ($\sim 5V$) and remains in that state for the duration of the tone pulse.

Feedback to the non-inverting input via R27 produces a circuit hysteresis of circa 0.2 V.

When the tone ends the Schmitt Trigger switches back to its quiescent state, i.e.: output LO.

Clock Delay (E4, IC3b)

In stand by the Schmitt Trigger output state is LO, C15 is discharged through E4, and the potential at the non-inverting input is also LO (IC3b output is also LO).

Notice that the voltage divider network of R41 and R42 determines the threshold voltage at the inverting inputs of all 3 "delay" circuits, IC3b, IC3c and IC3d.

Now, when the Schmitt Trigger output goes HI, it reverse-biases diode E4 and capacitor C15 begins to charge through resistors R31 and R32. The moment the charge on C15, as seen at the non-inverting input of the comparator, reaches the threshold level, the output switches to the HI state.

It takes C15 approx. 15 msec. to charge up to the threshold level of IC3b. This is what determines the Clock Delay time; removing the short circuit across R30 lengthens the delay time.

At the end of the tone the Schmitt Trigger output returns to its LO state and C15 can once again discharge through E4 and R32. The time constant of this circuit provides a delay at the negative going trailing edge of the pulse, too. These delays prevent random noise pulses from operating the circuit erratically.

Clear Delay (Q1, IC3c)

In stand by, Q1 is OFF and C16 has no charge on it. When the Schmitt Trigger output goes HI it drives Q1 ON, and C16 builds up a charge via R37 and Q1, triggering comparator IC3c so its output goes HI. The Clear Delay circuit operates similarly to the Clock Delay circuit.

As long as the Schmitt Trigger keeps operating at the normal tone intervals, Q1 can maintain the charge on C16. At the end of the 5th tone, the Schmitt Trigger reverts to its quiescent state (output LO) and turns Q1 OFF, as the emitter of Q1 will be biased by the charge on C16. The discharge path for C16 is through R36 and R37. In about 70 msec. the voltage at the non-inverting input of IC3c will fall back to the threshold level and the comparator output switches state. The LO potential at the Clear Delay output clears the Counter and the Readout circuits. Since the interval between tones is normally much less than 70 msec., the Clear Delay will remain OFF (output HI) throughout the entire tone sequence.

Counter (IC6a, IC7a, IC6b)

The Counter elements are J-K master-slave flip-flops arranged as a synchronous, divide-by-five counter that is clocked by the Clock Delay output and is cleared by the Clear Delay output. All of the normal (Q) and complement (\bar{Q}) Counter outputs are wired to appropriate Decoder inputs (IC4 and IC5).

The binary information present at each flip-flop input when a clock pulse arrives will be transferred to the output by the trailing edge of the clock pulse. A 5-tone code sequence, correct for the receiver in question, produces 5 clock pulses, one for each tone pulse.

70 msec. after the 5th tone ends, the logical "0" (LO) state at the Clear Delay output clears the Counter flip-flops. However, the Counter will not be able to start counting again until the flip-flops are enabled by the Clear Delay output being switched to logical "1" again by the Schmitt Trigger action.

Decoder (IC4a-d, IC5a) and Tone Gates (Q4-Q8)

The wiring between the Counter outputs and the Decoder NOR gate inputs is arranged to drive the Tone Gates one at a time.

The output of a NOR gate is HI (logical state "1") only when all of its inputs are LO (logical state "0"). If either or both of its inputs are HI, the NOR gate output will be LO.

In stand by, both inputs to IC4a are LO and the output is therefore HI. The other 5 Decoder NOR gates have at least one of their inputs HI, so their outputs will all be LO. Tone Gate Q4 is thus held ON by IC4a, while Q5-Q8 are held OFF by IC4b - IC5a.

Transistor Q4, conducting hard, acts as a virtual short circuit from chassis ground to whichever tone coil tap is specified for the first tone of the code sequence. At the end of the first clock pulse, one of the inputs to IC4a goes HI, the NOR gate output goes LO, and Q4 cuts off. At the same time both inputs to IC4b are now LO, its output goes HI, and Q5 goes ON to tune the resonant circuit for the 2nd tone of the code sequence.

One special consideration here is that the actual maximum HI potential measurable at the NOR gate output is limited to approx. 0.7 V by the conducting Tone Gate transistor's emitter-base junction.

With each correct pulse the Counter steps the Decoder one position forward until the final tone has been received.

Readout Circuit (IC5b, IC7b)

At the end of the 4th tone of a 5-tone signal (or the 3rd tone of a 4-tone signal) both inputs to IC5b will be LO, and the NOR gate output will go HI, driving the J input of IC7b HI, as well.

Now, with its J input driven HI and its K input held at chassis ground potential, IC7b can switch output states when the trailing (negative going) edge of the 5th (or 4th) tone pulse arrives. The normal (Q) output activates the Alarm Delay circuit, and the complement (\bar{Q}) output clears the Holding Circuit, IC8.

70 msec. later the Clear Delay, IC3c, clears the Counter and Readout circuits, and the Tone

Receiver is set up for the first tone again by the Decoder and Tone Gate circuits.

A strapping arrangement at the input of IC5b allows for either 4 or 5-tone codes.

Alarm Delay (IC3d, Q2, Q3)

Transistor Q2 is normally OFF and the output of IC3d is HI; Q3, a PNP transistor, is held OFF, and so is Q13.

When the Q output of IC7b in the Readout circuit goes HI at the end of the last tone pulse, it drives Q2 ON. Then capacitor C18 quickly charges through the conducting transistor Q2. When the charge reaches the threshold established by the resistive divider circuit of R41 and R42 the output of IC3d goes LO, turning Q3, then Q13 ON.

Q13 acts as a switch capable of carrying 100 mA of current between ground and terminal 37, the connection for an auxiliary alarm relay.

As long as the Clear Delay, IC3c, output remains HI, Q2 is held ON by IC7b and maintains the charge across C18. 70 msec. after the last pulse from the Clock Delay, IC3b, ends, IC3c switches state and clears the Counter and Readout IC's. The Q output of IC7b returns to logical "0", turning Q2 OFF. C18 now discharges slowly through R43 and R44.

The time constant of C18, R43 and R44 is calculated so that the Alarm Delay, IC3d, output switches back to logical "1" approx. 1, 3 sec. after the end of the final clock pulse.

The Alarm Delay is a comparator circuit that operates in the same manner as the Clock Delay.

Holding Circuit (IC8, Q9, Q11)

Call Lamp + Key Lock Switches (Q10, Q11)

The Holding Circuit is an integrated flip-flop with its J and K inputs both tied to logical "1" through R64. With both the J and the K inputs HI, the flip-flop output will complement itself for each clock pulse arriving at the CP

(toggle) input. Notice that the CP input is also tied to +Vcc, through R62. This simulates the flat top portion of a clock pulse. Now whenever the LS IN/OUT push button on the radiotelephone control panel is pressed, terminal 32 is grounded. C30 at the CP input discharges quickly through the 27 Ω resistor, R63, and the flip-flop sees a negative going trailing edge of a "clock pulse" and switches state. When the push button is released again, C30 charges up to +Vcc through R62, forming the positive going leading edge of the next "clock pulse".

Only the normal (Q) output is used in this circuit; it switches Q11 ON and OFF.

As just seen, IC8 is designed so that it can only be toggled manually by means of the LS IN/OUT switch. However, the Clear input is operated electronically from the \bar{Q} output of Readout flip-flop IC7b.

C32 provides a drive pulse to the base of Q9, saturating the transistor as soon as the radiotelephone is turned on. This pulls the collector of Q9 down to ground, presetting IC8. In the preset state, the Q output is HI and Q11 is held OFF, and Q10 and Q12 are likewise OFF.

With the collector of Q9 LO, diode E3 keeps the Schmitt Trigger output at logical "0", as well, inhibiting both the Clock and the Clear Delay circuits.

As capacitor C32 accumulates a charge, the charging current decreases until it no longer can forward bias Q9. The transistor goes OFF, its collector voltage goes HI, and IC8 becomes enabled.

Diode E6 serves to discharge C32 when the equipment is turned off.

Each time the LS IN/OUT button is pressed, IC8 changes state, switching Q11 ON or OFF and, in turn, driving Q10 and Q12 into saturation or cut-off.

When Q10 conducts it provides a ground connection to light the Call Lamp and, when ap-

plicable, to operate a relay for muting the car's broadcast band radio.

Q12, conducting simultaneously, turns the loud-speaker ON and also unlocks the Key Lock function.

At the end of the last tone pulse in a sequence, the complement output (\bar{Q}) of IC7b clears IC8, whose output goes LO and turns Q11 ON. Q10 and Q12 are then driven into saturation. 70 msec. after, the Clear Delay clears the Counter and Readout circuits and \bar{Q} of IC7b goes HI again. IC8 can be manually toggled via terminal 32 any time afterwards.

Note that whenever the speaker is in operation, whether turned on manually or by an incoming call, the Call Lamp will light.

Occupied Lamp Switch (Q14)

Whenever the channel is occupied a DC voltage from the Squelch circuit, via terminal 41, turns Q14 ON and establishes a ground connection to the Occupied Lamp, so it can light.

Alarm Tone Generator (IC5c, IC5d)

Two NOR gates, coupled to operate as a free-running (astable) multivibrator, generate an audio signal that is available at terminal 20. The Generator can be strapped to the output of IC3d or to +Vcc through R61.

In stand by, IC3d has a HI output, which would inhibit NOR gate IC5d. When a selective call comes through, the Alarm Delay output goes LO for approx. 1.3 sec. During that interval the multivibrator can oscillate at a frequency determined by the time constants of R57 / C27 and R58 / C26. When the Alarm Delay output goes HI again the oscillator stops.

On the other hand, if its input is tied to +Vcc, IC5d would be permanently inhibited and no audio signal could be generated, at all.

Output signal level can be regulated by resistor R60.

Regardless of the state of IC8 a correct tone signal will clear the flip-flop and turn Q11, then Q10 and Q12 ON. Thus, a tone call has higher priority than the manual switch.

T R U T H T A B L E
for Counter, Readout, and Decoder Circuits

Clock Pulse	Clear Delay	IC6a				IC7a				IC6b				IC4a	IC4b	IC4c	IC4d	IC5a	IC5b	IC7b \bar{Q}
		J	K	Q	\bar{Q}	J	K	Q	\bar{Q}	J	K	Q	\bar{Q}							
0	0	1	0	0	1	0	0	0	1	0	0	0	1	1	0	0	0	0	0	1
1	1	1	0	1	0	1	0	0	1	0	0	0	1	0	1	0	0	0	0	1
2	1	1	0	1	0	1	0	1	0	1	0	0	1	0	0	1	0	0	0	1
3	1	0	1	1	0	1	0	1	0	1	0	1	0	0	0	0	1	0	0	1
4	1	0	1	0	1	0	0	1	0	1	0	1	0	0	0	0	0	1	1	1
5	1	0	1	0	1	0	0	1	0	1	0	1	0	0	0	0	0	1	1	0
Δ	0	1	0	0	1	0	0	0	1	0	0	0	1	1	0	0	0	0	0	1

NOTE: Δ = 70 msec. after the end of the 5th tone

SEQUENTIAL TONE RECEIVER

SR785a

Technical Specification

Supply Power

Nominal: 13.6 V
 Minimum: 10.5 V
 Maximum: 16.0 V

Current Drain

Stand by: 24 mA \pm 4 mA

Regulated Voltage

Nominal 4.9 V

Temperature Range

Operating range: -25°C to $+60^{\circ}\text{C}$
 Functioning range: -30°C to $+80^{\circ}\text{C}$

Maximum Load Currents

Terminal 37 ALARM 100 mA (for 1.3 sec.)
 Terminal 47 Call 100 mA
 Terminal 45 OCCUPIED 100 mA
 Terminal 51
 and 43 KEY LOCK 10 mA
 Terminal 34 AF MUTING I_{load} min. 0.75 mA

for $V_{\text{out}} = 8 \text{ V}$

Input Impedance

$\geq 6 \text{ K}\Omega$

Signal Input Level

Nominal at 1000 Hz: 110 mV

AF Muting

In conjunction with terminal 18 of CF701 or CF702:
 $\geq 60 \text{ dB}$.

Signalling Code

Sequence of 4 or 5 tone bursts of 70 ms \pm 15 ms duration with maximum 15 ms interval between tone bursts.

Tone Signal Frequencies

<u>Coil terminal</u>	<u>Tone frequency</u>
1	970 Hz
2	1060 Hz
3	1160 Hz
4	1270 Hz
5	1400 Hz
6	1530 Hz
7	1670 Hz
8	1830 Hz
9	2000 Hz
10	2200 Hz
11	2400 Hz
12	2600 Hz
13	2800 Hz

Frequency Accuracy

Coil tuned for 1060 Hz: $\leq 0.3\%$ for all tones

Frequency Stability

(typically $\leq 0.5\%$) $\leq 1.0\%$

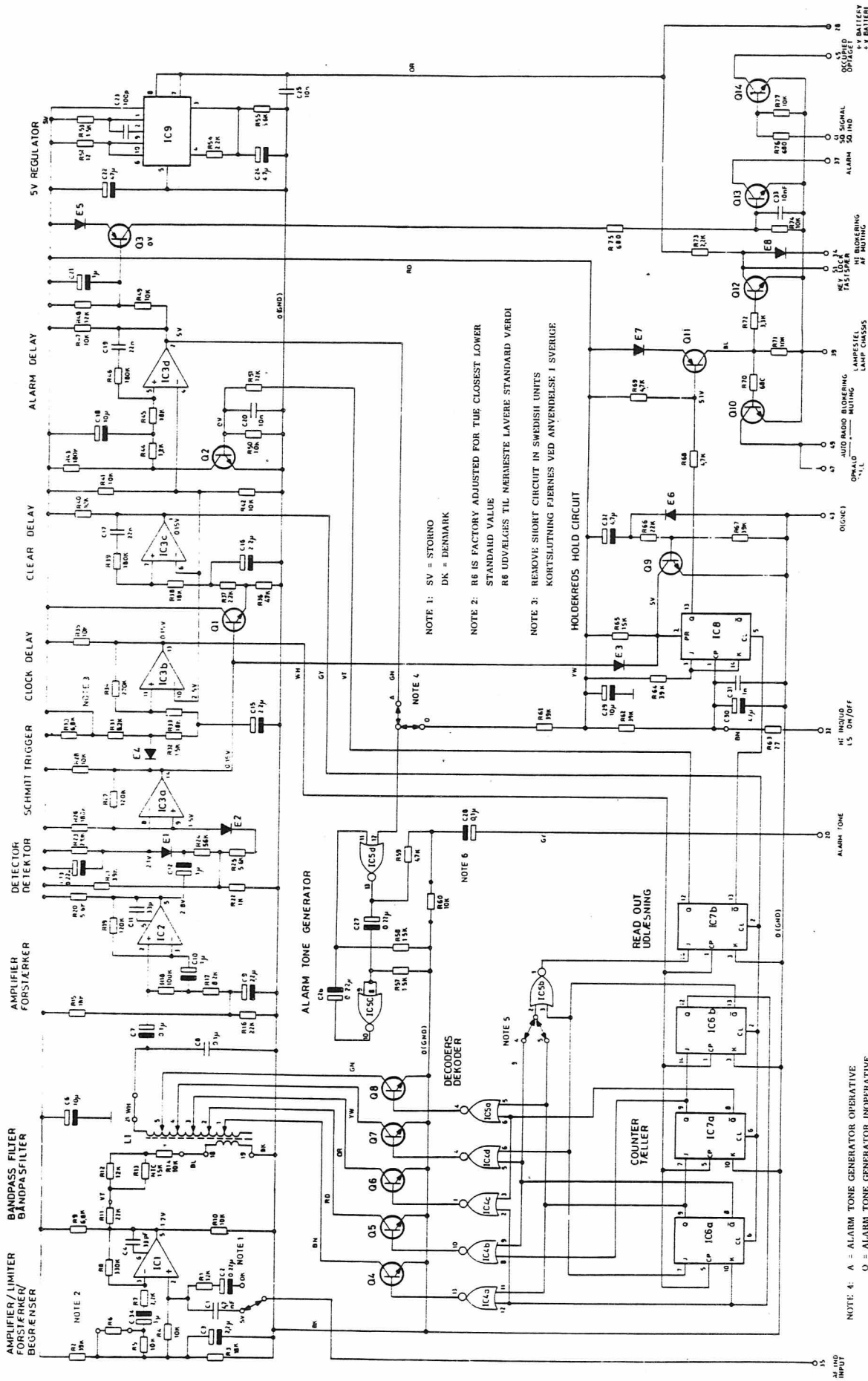
Selectivity

Frequencies differing from f_0 by 4% or more are unable to trigger the tone receiver.

NOTE: CERTAIN PULSE CHARACTERISTICS, ESPECIALLY INTERVALS BETWEEN PULSES, ARE SHOWN IN EXAGGERATED FORM. THIS IS TO ILLUSTRATE THE TIME RELATIONSHIPS BETWEEN THE VARIOUS PULSES MORE CLEARLY.

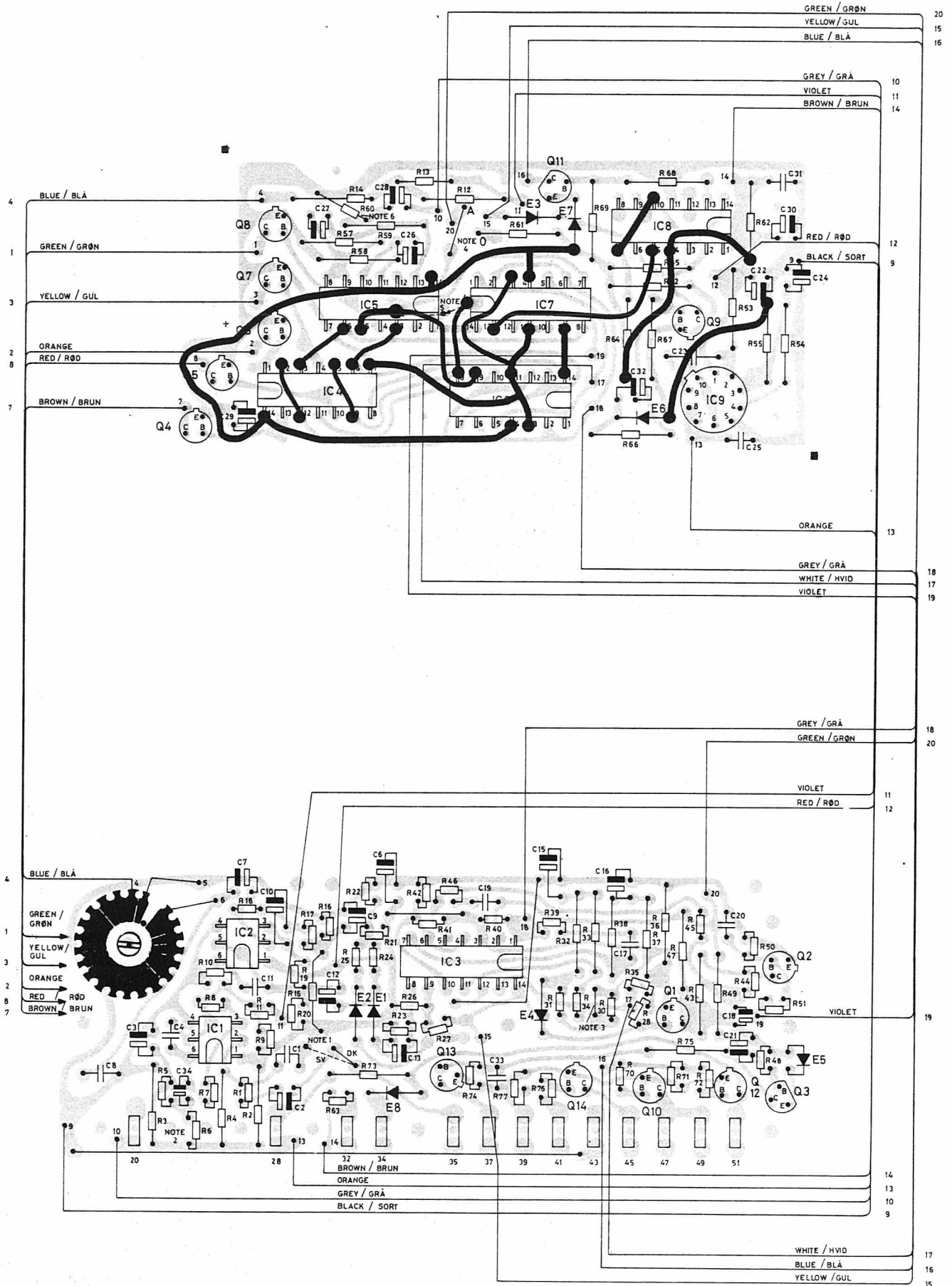


SR785a FUNCTIONAL DIAGRAM
Sorno D401.977/2



SEQUENTIAL TONE RECEIVER SR785a
SEKVENSTONEMODTAGER

D401.894



SEQUENTIAL TONE RECEIVER SR785a
 SEKVENSTONEMODTAGER

D402.159

TYPE	NO.	CODE	DATA
SR785a		10.2541-01	Sequential Tone Receiver
	C1	74.5061	4.7nF 10% polyest. FL
	C2	73.5118	0.22μF 20% tantal
	C3	73.5102	2.2μF 20% tantal
	C4	74.5116	33pF 5% ceram TB
	C5		not used
	C6	73.5109	10μF 20% tantal
	C7	73.5089	0.1μF 20% tantal
	C8	76.5068	0.1μF 1% polystyr TB
	C9	73.5102	2.2μF 20% tantal
	C10	73.5114	1μF 20% tantal
	C11	74.5116	33pF 5% ceram TB
	C12	73.5114	1μF 20% tantal
	C13	73.5118	0.22μF 20% tantal
	C14		not used
	C15	73.5102	2.2μF 20% tantal
	C16	73.5102	2.2μF 20% tantal
	C17	76.5071	22nF 10% polyest. FL
	C18	73.5109	10μF 20% tantal
	C19	76.5071	22nF 10% polyest. FL
	C20	76.5070	10nF 10% polyest. FL
	C21	73.5114	1μF 20% tantal
	C22	73.5124	47nF 20% tantal
	C23	74.5165	100pF 10% ceram
	C24	73.5126	4.7μF 20% tantal
	C25	76.5070	10nF 10% polyest. FL
	C26	73.5118	0.22μF 20% tantal
	C27	73.5118	0.22μF 20% tantal
	C28	73.5089	0.1μF 20% tantal
	C29	73.5109	10μF 20% tantal
	C30	73.5126	4.7μF 20% tantal
	C31	74.5155	1nF -20+80% ceram PL
	C32	73.5126	4.7μF 20% tantal
	C33	76.5070	10nF 10% polyest. FL
	C34	73.5114	1μF 20% tantal
	R1	80.5262	12kΩ 5% carbon film
	R2	80.5268	39kΩ 5% carbon film
	R3	80.5264	18kΩ 5% carbon film
	R4	80.5261	10kΩ 5% carbon film
	R5	80.5261	10kΩ 5% carbon film
	R6	80.52xx	Adjusted
	R7	80.5253	2.2kΩ 5% carbon film
	R8	80.5279	0.33 MΩ 5% carbon film
	R9	80.5259	6.8kΩ 5% carbon film
	R10	80.5261	10kΩ 5% carbon film
	R11	80.5265	22kΩ 5% carbon film

TYPE	NO.	CODE	DATA
	R12	80.5262	12kΩ 5% carbon film
	R13	89.5009	15kΩ 20% NTC
	R14	80.5261	10kΩ 5% carbon film
	R15	80.5264	18kΩ 5% carbon film
	R16	80.5265	22kΩ 5% carbon film
	R17	80.5260	8.2kΩ 5% carbon film
	R18	80.5273	0.1 MΩ 5% carbon film
	R19	80.5273	0.12 MΩ 5% carbon film
	R20	80.5258	5.6kΩ 5% carbon film
	R21	80.5256	3.9kΩ 5% carbon film
	R22	80.5249	1kΩ 5% carbon film
	R23	80.5278	0.2 MΩ 5% carbon film
	R24	80.5270	56kΩ 5% carbon film
	R25	80.5258	5.6kΩ 5% carbon film
	R26	80.5276	0.18 MΩ 5% carbon film
	R27	80.5274	0.12 MΩ 5% carbon film
	R28	80.5261	10kΩ 5% carbon film
	R29		Not used
	R30	80.5259	6.8kΩ 5% carbon film
	R31	80.5260	8.2kΩ 5% carbon film
	R32	80.5251	1.5kΩ 5% carbon film
	R33	80.5264	18kΩ 5% carbon film
	R34	80.5278	0.27 MΩ 5% carbon film
	R35	80.5261	10kΩ 5% carbon film
	R36	80.5269	47kΩ 5% carbon film
	R37	80.5253	2.2kΩ 5% carbon film
	R38	80.5264	18kΩ 5% carbon film
	R39	80.5276	0.18 MΩ 5% carbon film
	R40	80.5261	10kΩ 5% carbon film
	R41	80.5261	10kΩ 5% carbon film
	R42	80.5261	10kΩ 5% carbon film
	R43	80.5276	0.18 MΩ 5% carbon film
	R44	80.5250	1.2kΩ 5% carbon film
	R45	80.5264	18kΩ 5% carbon film
	R46	80.5276	0.18 MΩ 5% carbon film
	R47	80.5261	10kΩ 5% carbon film
	R48	80.5262	12kΩ 5% carbon film
	R49	80.5261	10kΩ 5% carbon film
	R50	80.5261	10kΩ 5% carbon film
	R51	80.5262	12kΩ 5% carbon film
	R52	80.5226	12Ω 5% carbon film
	R53	80.5251	1.5Ω 5% carbon film

SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER

SR785a

X401.963

TYPE	NO.	CODE	DATA
R54	80.5253	2.2kΩ	5% carbon film
R55	80.5258	5.6kΩ	5% carbon film
R56		Not used	
R57	80.5251	1.5kΩ	5% carbon film
R58	80.5251	1.5kΩ	5% carbon film
R59	80.5269	47kΩ	5% carbon film
R60	80.5061	10kΩ	5% carbon film
R61	80.5268	39kΩ	5% carbon film
R62	80.5268	39kΩ	5% carbon film
R63	27Ω	5% carbon film	
R64	80.5268	39kΩ	5% carbon film
R65	80.5263	15kΩ	5% carbon film
R66	80.5265	22kΩ	5% carbon film
R67	80.5268	39kΩ	5% carbon film
R68	80.5257	4.7kΩ	5% carbon film
R69	80.5257	4.7kΩ	5% carbon film
R70	80.5246	680Ω	5% carbon film
R71	80.5261	10kΩ	5% carbon film
R72	80.5255	3.3kΩ	5% carbon film
R73	80.5253	2.2kΩ	5% carbon film
R74	80.5261	10kΩ	5% carbon film
R75	80.5246	680Ω	5% carbon film
R76	80.5246	680Ω	5% carbon film
R77	80.5261	10kΩ	5% carbon film
L1	61.1259	Tone coil	
E1	99.5237	1N4148 Diode	
E2	99.5237	1N4148 Diode	
E3	99.5237	1N4148 Diode	
E4	99.5237	1N4148 Diode	
E5	99.5237	1N4148 Diode	
E6	99.5237	1N4148 Diode	
E7	99.5237	1N4148 Diode	
E8	99.5237	1N4148 Diode	
Q1	99.5143	BC108 Transistor	
Q2	99.5143	BC108 Transistor	
Q3	99.5144	S5144 Transistor	
Q4	99.5201	BC109 Transistor	
Q5	99.5201	BC109 Transistor	
Q6	99.5201	BC109 Transistor	
Q7	99.5201	BC109 Transistor	
Q8	99.5201	BC109 Transistor	
Q9	99.5143	BC108 Transistor	
Q10	99.5143	BC108 Transistor	
Q11	99.5144	S5144 Transistor	
Q12	99.5143	BC108 Transistor	

TYPE	NO.	CODE	DATA
	Q13	99.5143	BC108 Transistor
	Q14	99.5143	BC108 Transistor
	IC1	14.5017	Operational Amplifier
	IC2	14.5017	Operational Amplifier
	IC3	14.5019	Operational Amplifier
	IC4	14.5018	Quadruple comparator
	IC5	14.5018	Quadruple 2-input pos. NOR Gate
	IC6	14.5008	Quadruple 2-input pos. NOR Gate
	IC7	14.5008	Dual J-K master-slave Flip-Flop
	IC8	14.5056	Dual J-K master-slave Flip-Flop
	IC9	14.5055	Dual J-K master-slave Flip-Flop
			Voltage regulator

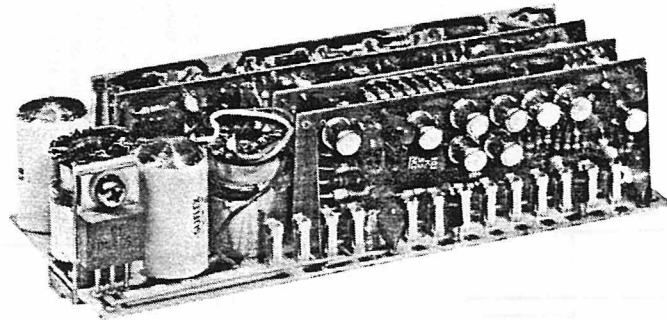
SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER

SR785a

X401.963

SEQUENTIAL TONE RECEIVER

SR7841



Introduction

SR7841 is a sequential tone receiver for selective calling. It was developed for use in Storno-phone 700 radiotelephone equipment. The frequencies employed are the standard Storno series: 970 Hz to 2800 Hz.

The SR7841 tone receiver can be coded for any of the following operating modes:

- 4 or 5 tones, individual call, only
- 4 or 5 tones, including one group call digit
- 4 or 5 tones, including two group call digits

General Description

Individual Call

Upon reception of a signal having the correct tones in the proper sequence the following events take place (in the receiver):

The Call Lamp lights, the AF Muting is cancelled and the Key Lock function "unlocks". When the vehicle's traffic horn is connected to the tone receiver via an auxiliary relay, the horn will also sound for about one second.

The audio circuit and the Key Lock are both turned on and off manually by means of the LS

IN / OUT push button. Since the switch that "unlocks" the Key Lock also turns on the loudspeaker, the operator is forced to check for the presence of another signal on the channel before being able to key his transmitter.

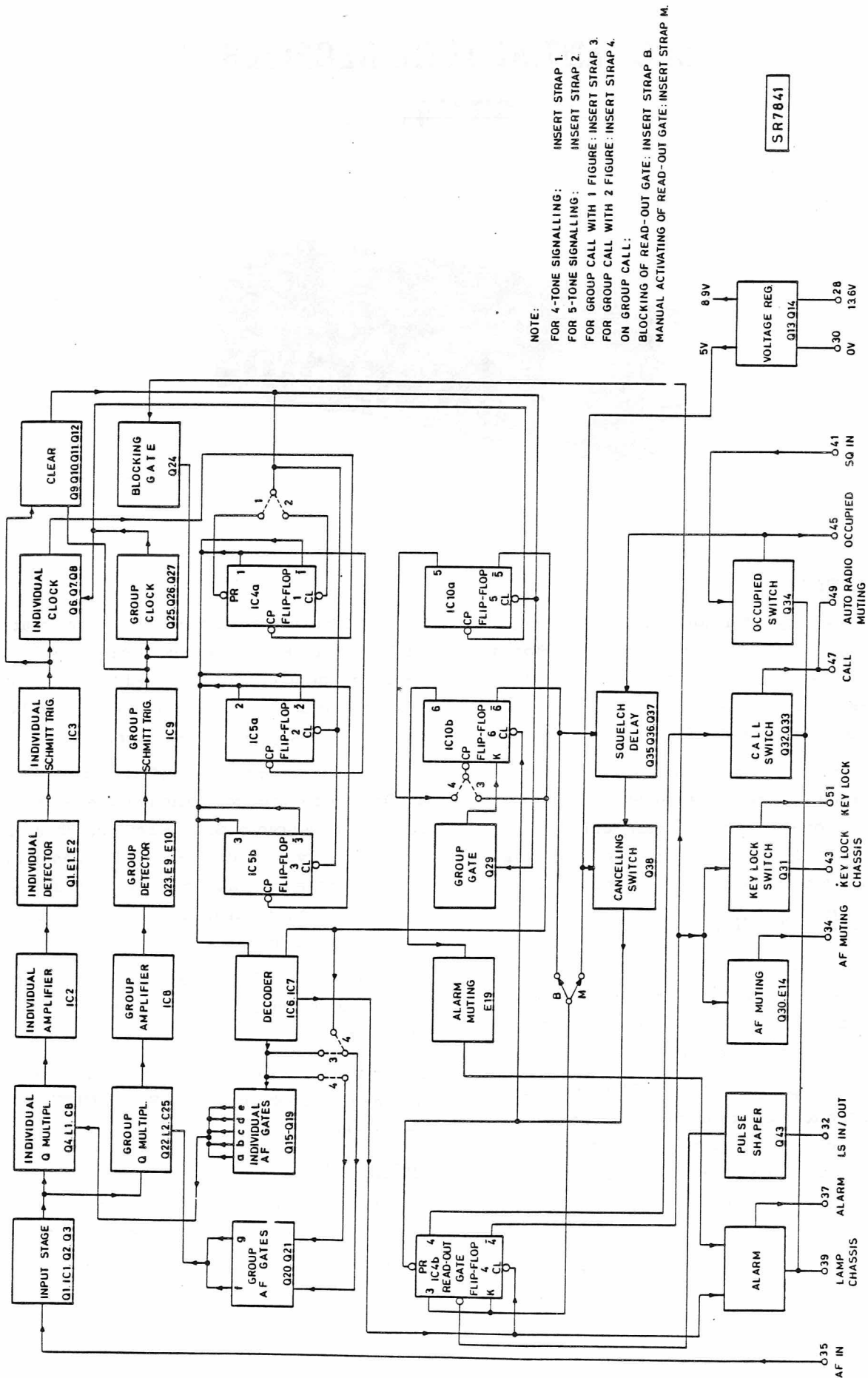
In addition, the tone receiver is equipped with an Occupied Lamp controlled by the squelch circuit in the radiotelephone receiver. Thus, if an RF signal having that channel's frequency is present at the antenna input it will cause the Occupied Lamp to light as an indication that the channel is not free.

At the end of a call the Call Lamp, governed by the receiver Squelch, goes out when the carrier disappears.

After reception of a correct call the speaker will remain open until the LS IN / OUT button is depressed.

Group Call

Group calls do not activate the Alarm circuit. Also, the loudspeaker becomes automatically muted again at the end of a group call.



NOTE:
 FOR 4-TONE SIGNALLING: INSERT STRAP 1.
 FOR 5-TONE SIGNALLING: INSERT STRAP 2.
 FOR GROUP CALL WITH 1 FIGURE: INSERT STRAP 3.
 FOR GROUP CALL WITH 2 FIGURE: INSERT STRAP 4.
 ON GROUP CALL:
 BLOCKING OF READ-OUT GATE: INSERT STRAP B.
 MANUAL ACTIVATING OF READ-OUT GATE: INSERT STRAP M.

SR7841

Logic Terms

Positive logic is employed in SR7841; logical references are:

1. low voltage level ($\sim 0V$) = logic state "0" (LO)
2. high voltage level ($\sim 5V$) = logic state "1" (HI)

Mode of Operation5-tone Individual Signalling

The Input Stage includes Q1, IC1, Q2 and Q3. The first tone of a sequential tone signal, arriving from input terminal 35, passes through the input stage, where it becomes suitable for applying to the Q Multiplier.

In stand by the Q Multiplier is tuned, via Individual AF Gate a, for the first tone of its code. If the first tone received corresponds to the circuit resonant frequency, it becomes selected, is then amplified in IC2 and rectified at the Detector, Q5, E1, and E2.

The rectified signal turns the Individual Schmitt Trigger, IC3, ON. The output of IC3 becomes logic "1" and suspends the Clear function (Q9 - Q12). Individual Counters FF1 to FF3 and Group Counter FF5 are then ready to count.

A 25 ms delay is introduced between the time that the Schmitt Trigger output becomes logic "1" and the clock pulse from the Clock stage goes "1". When the 1st tone ends, the Schmitt Trigger output goes "0" again, bringing the Clock output to logic "0". Counter FF1 then switches state, also causing the Decoder (IC6 and IC7) to step to the next AF Gate, which is b.

The output of the Clear stage remains at logic "1" for about 40 ms after the Schmitt Trigger has returned to "0". The next (2nd) tone must be received within that time or the Clear function will reset the Counter and the Decoder will go back to stand by, i. e. ready to receive the 1st tone again.

The 2nd, 3rd, 4th, and 5th tones of a sequence occur like the 1st, each time stepping the Decoder one position forward until the final tone is received. At the end of the 5th tone the IC7_c output goes "0" which causes the Alarm circuit to ground terminal 37. A relay connected here will sound the traffic horn for approximately 1 second.

IC7_c also clears the Read-out Gate, FF4. This lights the Call Lamp via FF4 output 4 and terminal 47 while turning the speaker ON via output 4 and terminal 34.

The Call Lamp and the speaker will remain ON until switched OFF manually with the LS IN/OUT push button (via terminal 32).

When the channel is occupied (a carrier wave being received) the receiver squelch circuit feeds a DC voltage to terminal 41 (SQUELCH IN). The Occupied Lamp lights via terminal 45.

The Key Lock disables the transmitter via terminal 51. The voltage regulator will only supply power to the transmitter section when terminal 51 (KEY LOCK) from SR7841 is at chassis ground potential.

Conditions for transmitting are:

- AF Muting cancelled (term. 34 LO)
- Call Lamp ON (term. 47 to ground)
- Key Lock cancelled (term. 51 to ground)

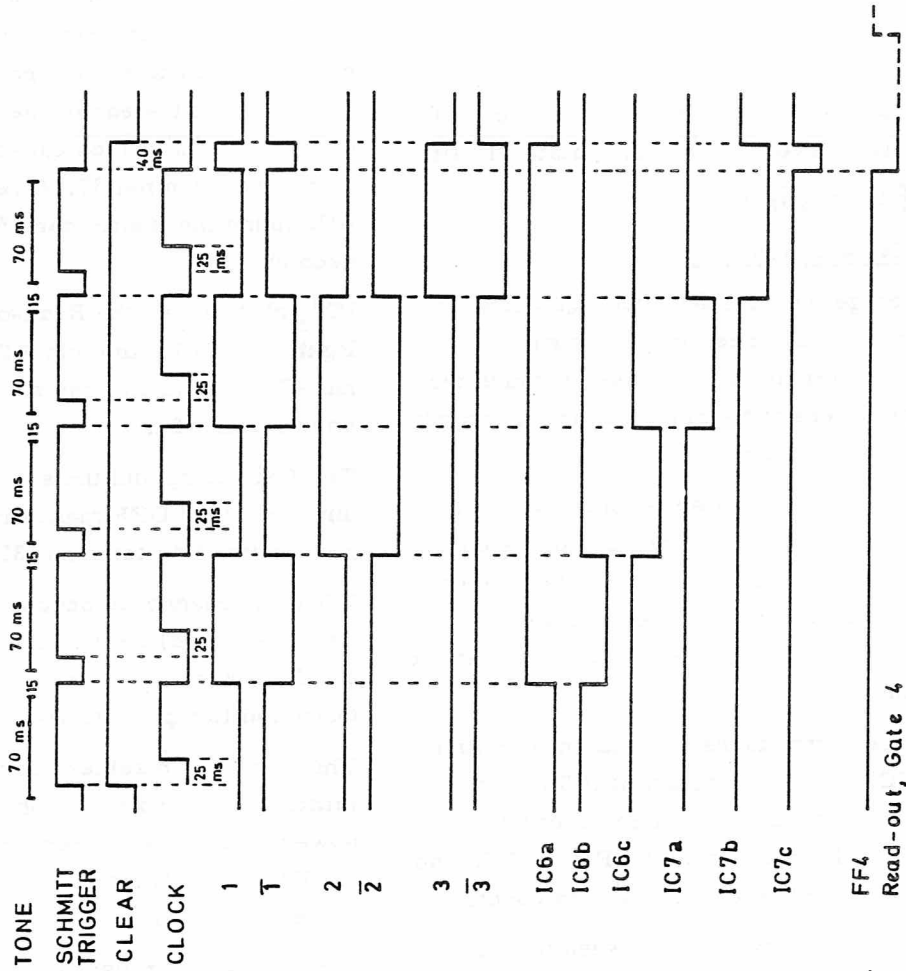
Approximately 40 ms after the last tone in the sequence, the Clear output goes "0", clearing Counter FF1 - FF3. AF Gate a is then set to wait for the 1st tone of a new call.

4-tone Signals

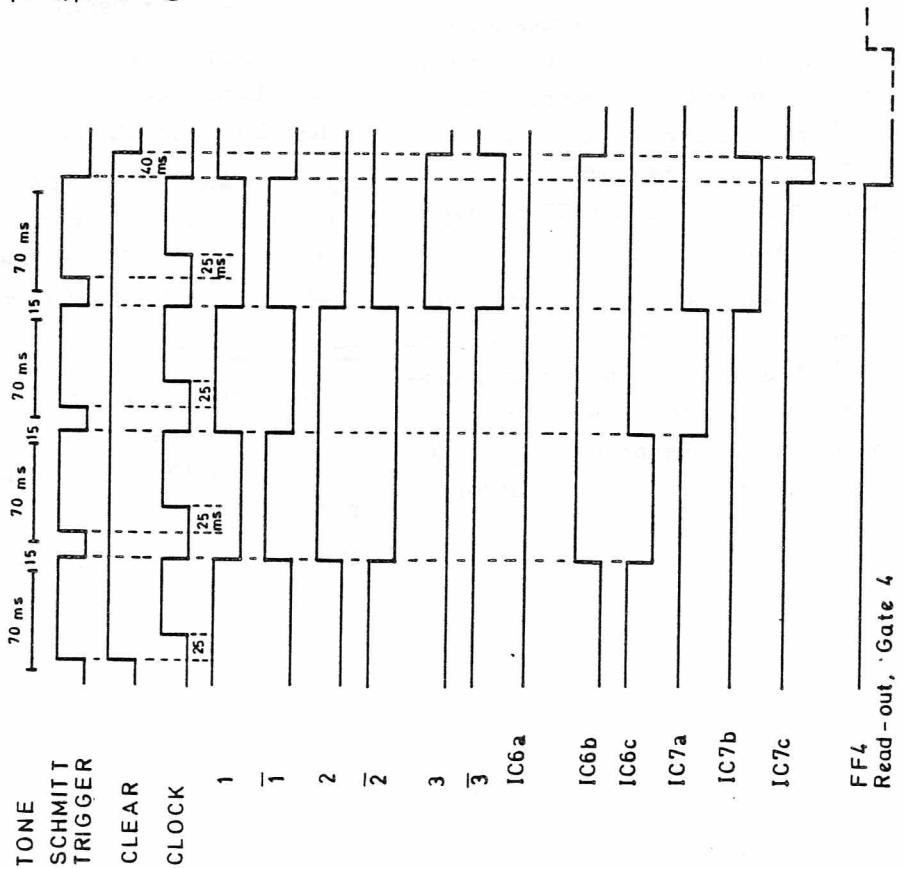
SR7841 can also be strapped for 4-tone code signalling. The Clear output will then preset FF1 to switch in AF Gate b when in stand by, thus bypassing Gate a.

Pulse sequences for 4 and 5-tone signals follow:

5-TONE PULSE SEQUENCE



4-TONE PULSE SEQUENCE



Group Calls, One Group Digit

The first 4 tones of a 5-tone signal take place just as described for individual calling. Now the receiver is ready for the final tone (digit).

Preparing for the final digit, AF Gate e sets coil L1 for the frequency that would normally be the 5th tone of the sequence. At the same time, AF Gate g sets coil L2 for the group tone. The two Q Multiplier inputs are parallel connected.

If the incoming tone has the frequency for an individual call the Individual Q Multiplier will respond, resulting in a normal individual call. However, if the 5th tone matches the group digit frequency the Group Q Multiplier will respond.

The chain of circuits consisting of the Group Q Multiplier, Group Amplifier, Group Detector, Group Schmitt Trigger, and Group Clock are identical with the Individual chain.

The signal proceeds through the Group chain to the output of the Group Schmitt Trigger. The trigger output goes "1", so the Clear circuit function will still be suspended and Individual Counters FF1 - FF3 as well as Group Counter FF5 can count.

After the 25 ms delay the Group Clock output goes "1". The Group Clock drives the Individual Clock via transistor Q28, forcing the Individual Clock output to follow the Group Clock Output; i. e. when the Group Clock output goes logic "1", so does the Individual Clock output.

When the 5th tone ends, the output of the Group Schmitt Trigger goes "0". The Group Counter toggles and reads:

output $\bar{5}$ = "0"
 output 6 = "1"
 output $\bar{6}$ = "0"

The k input of FF6 receives its signal from the Group Gate, Q29. Since Q29's base is driven by the Clear output, FF6 input k is held at logic level "0" as long as the Clear output is at logic "1". The j input is tied to logic "1" through R86.

The FF6 outputs do not change state when the group call ends, but remain at:

6 = "1"
 $\bar{6}$ = "0"

until the carrier falls away and a cancelling pulse clears FF6.

Decoder IC7_c goes "0" at the end of the last tone, clearing Read-out Gate FF4: $\bar{4}$ = "0"
 4 = "1"

Approx. 40 ms later, the Clear output returns to "0".

The Call Lamp lights and the AF Muting is cancelled (terminals 34 and 47 grounded). The Alarm, however, does not go ON for a group call as the logic "1" at FF6 output 6 keeps Q41 ON (and Q42 OFF).

Individual Counter FF1 - FF3 and Group Counter FF5 clear.

AF Gate a is set for a new call.

When an RF carrier is occupying the channel, Q34 holds terminal 45 (OCCUPIED) at chassis ground potential and Q36 is held OFF through E16. In the case of a group call, FF6 output $\bar{6}$ goes "0" after the last digit is received and the L0 signal holds Q35 OFF. Collector of Q35 tends to go H1, but Q34 and E16 prevent this.

When the RF carrier disappears terminal 45 goes HI, reverse biasing E16; with Q35 OFF, Q36 and Q37 can go ON, sending a positive pulse to Q38 whose collector then goes L0, presetting FF4.

output 4 goes "1"
 output $\bar{4}$ goes "0"

The Call Lamp turns OFF and the AF Muting ON.

The negative pulse from Q38 also clears FF6.

output 6 goes "0"
 output $\bar{6}$ goes "1"

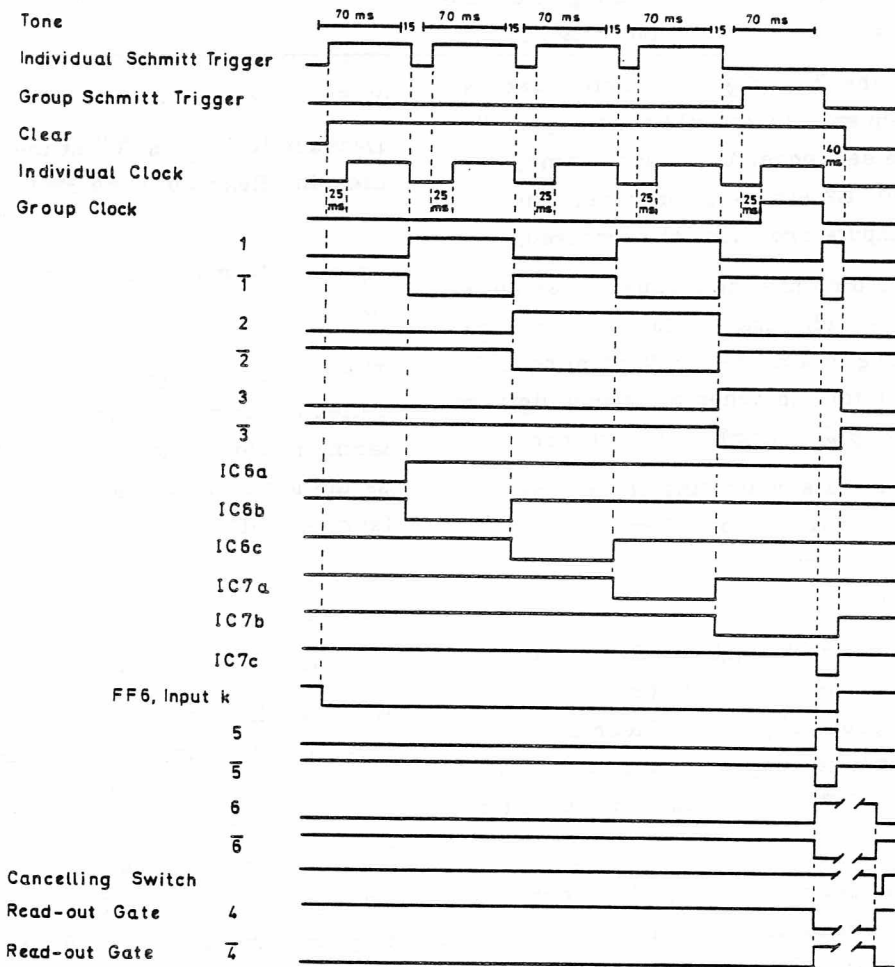
A delay of about 300 ms is introduced in order to avoid possible problems due to fading.

The tone receiver is now ready for a new call.

Pulse sequences for 5-tone signals with one group digit are as follows:

SR7841

PULSE SEQUENCE, 5 Tones with 1 Group Digit



Group Call, Two Group Digits

The first 3 tones of a 5-tone signal take place just as described for individual calling. Now the receiver is ready for the fourth tone (digit). Notice the change between strapping lugs 3 and 4.

AF Gate d sets coil L1 for the frequency that would normally be the 4th tone of the sequence. At the same time, AF gate f sets coil L2 for the first group tone.

If the last two tones have the same frequencies as the 4th and 5th tone of the individual code, the result will be a normal individual call. However, if they have the group digit frequencies, the Group Q Multiplier will respond to them.

The Group circuits take over from the Individual circuits; the Group Schmitt Trigger drives the Clear circuit and the Group Clock. The Individual Clock follows the Group Clock, as just described in the preceding section.

When the 4th tone ends, IC7_a goes "1", inhibiting AF Gates d and f. FF5 output 5-bar will be at logic state "0", inhibiting Decoder IC7_b and thereby also AF Gate e (which only functions for individual calls).

The logic "0" from output 5-bar is also present at the base of Q21, so AF Gate g is open for the 2nd group digit (5th tone of the sequence).

When the final tone ceases FF6 outputs go:

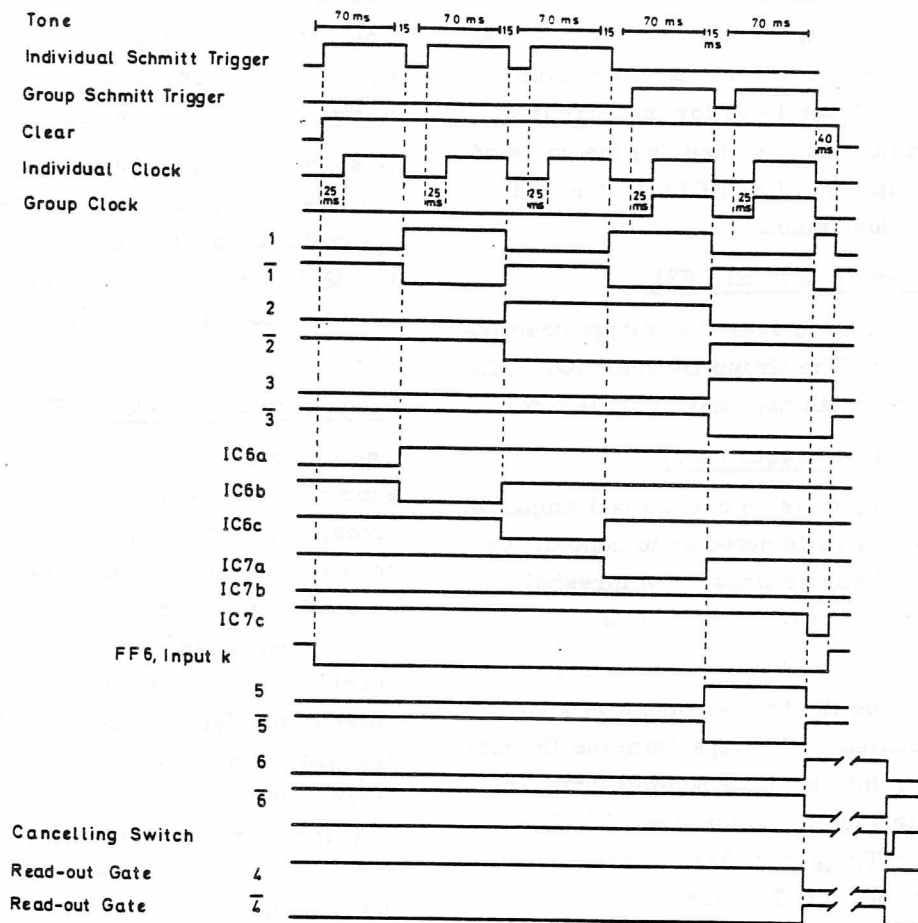
$$\begin{aligned} \text{output } 6 &= "1" \\ \text{output } \bar{6} &= "0" \end{aligned}$$

Clearing circuit action, Alarm suspension as well as clearing and resetting of the Counters, Read-out Gate, AF Gates, etc. all occur as previously described in the section on group calling with only one group digit.

Pulse sequences for 5-tone signals with two group digits are as follows:

SR7841

PULSE SEQUENCE, 5 Tones with 2 Group Digits



Circuit Description

Input Stage (Q1, IC1, Q2, Q3)

The pre-emphasis network includes Q1, R4, and C4.

IC1 is a linear amplifier. Signal clipping begins when the signal amplitude approaches the supply voltage level (5 V). Full amplitude limiting occurs when the input signal is 6 dB above the nominal 110 mV value.

R5 and R8 determine the amplifier gain. Voltage divider R6 and R7 sets the DC output level.

The limiting action and the narrow pass-band of the subsequent Q Multiplier ensure selectivity. Tones differing by at least 4.5% from the resonant frequency will not be able to trigger the tone receiver.

Transistors Q2 and Q3 are arranged so that they present an extremely low output impedance (on the order of 1Ω) which is suitable as a common return connection for the resonant circuit in the following stage.

Individual Q Multiplier (Q4)

The Q Multiplier involves a parallel resonant circuit, L1 and C8. This is very loosely coupled to the transistor, Q4, in order to maintain a constant Q over the entire tone range. C8 in the resonant circuit is grounded through the output impedances of the driver transistors while the relevant terminals of coil L1 are alternately grounded through the AF Gates, a - e (Q15 - Q19)

A portion of the tone signal is reapplied to L1 in phase by means of a feedback winding in the collector circuit of Q4, approximately doubling the Q of L1.

To offset the effect of temperature upon the Q of L1 an NTC resistor, R19, is inserted in the emitter circuit of Q4. R19, aided by R17 and R18, maintains a nearly flat temperature response from -30°C to $+80^{\circ}\text{C}$. The Group Q Multiplier (Q22) is identical with the Individual Q Multiplier.

Individual Amplifier (IC2)

The signal from the Q Multiplier is DC coupled to the non-inverting input of IC2. Amplifier gain, and thus trigger level for the Schmitt Trigger, is adjustable by changing the value of R20. The Group Amplifier (IC8) is identical with the Individual Amplifier.

Individual Detector (Q5, E1, E2)

Emitter follower Q5 drives the voltage doubling rectifier circuit. The Group Detector (Q23, E9, E10) is identical with the Individual Detector.

Individual Schmitt Trigger (IC3)

The Schmitt Trigger is an operational amplifier working as a threshold detector to control the Clock and the Clear settings. The threshold voltage is set by network R29, E3, and R30.

In stand by the state of the non-inverting input is logic "0", thus the trigger output is also "0". When the rectified DC voltage from the Detector surpasses the threshold the Schmitt Trigger switches state and the output goes "1". The Group Schmitt Trigger (IC9) is identical with the Individual Schmitt Trigger.

Individual Clock (Q6, Q7, Q8)

The Individual Clock toggles Counter FF1 after first introducing a 25 ms delay in order to prevent erratic operation. The Clock output pulse is delayed until the Schmitt Trigger has displayed a logic "1" output state for approx. 25 ms. Delay time is adjustable by means of R35.

In stand by the output state of IC3 is "0", holding Q6, Q7, and Q8 ON. Clock output is also "0". When IC3 triggers, its output goes logic "1". This cuts off Q6, and C16 begins charging through R34 in parallel with R35. After the set delay time, Q7 becomes reverse biased and cuts off, turning Q8 OFF. Clock output at the collector of Q8 goes "1".

When the tone ends, the Schmitt Trigger returns to its quiescent state and Q6 goes ON and C16 discharges rapidly through Q6 and R36, turning Q7, then Q8 ON. Clock output switches to logic state "0" and FF1 toggles.

Group Clock (Q25 - Q27)

The Group Clock toggles Group Counter FF5. Circuit operation, including the 25 ms delay, is the same as for the Individual Clock.

Q28 drives the Individual Clock so that its output follows the output of the Group Clock. When the collector of Q27 (Group Clock output) goes HI, Q28 conducts, grounding the base of Q8 whose collector (Individual Clock output) goes HI.

Clear Circuit (Q9 - Q12, E5, E6, E13)

The Clear circuit sets the Counter to stand by approx. 40 ms after the last correct tone arrives. Where the tone code is correct for the receiver setting the last tone will, of course, be the 5th tone (4th tone with 4-tone signalling). In the event of an incorrect tone code, the tone receiver will respond normally until one of the tones in the false sequence fails to match the resonant frequency set up by the AF Gates. Since each tone lasts for about 70 ms, the Clear circuit will have reset the Counter to stand by before the incorrect tone expires and prior to the arrival of the next tone.

Emitter follower Q9 is driven by the Schmitt Trigger outputs through diode E5 or through E13. In stand by, E5 (E13) cannot conduct, and Q9 is OFF. Q10, Q11, and Q12 are all ON, and output is at logic "0".

When one of the Schmitt Trigger outputs goes "1", E5 or E13 conducts, turning Q9 ON. C18 discharges through Q9, whereby Q10, Q11, and Q12 go OFF (output state "1"). The Counter is now able to start counting.

At the end of a tone E5 (E13) stops conducting (trigger output at "0" again) and C18 charges through R42 and R43. The charge building up on C18 eventually overcomes the emitter bias and turns Q10 ON. Emitter voltage for Q10, and thus the time elapsing before the Clear circuit returns to its quiescent state, is determined by voltage divider R45 and R46. When Q10 conducts, it turns Q11 and Q12 ON, as well, resetting the counter to stand by.

The 40 ms delay is measured as the time elapsed between the Schmitt Trigger output "0" and when the Clear output goes "1".

Tones in a sequence arrive with maximum 15 ms interval between them, which is fast enough to keep the Clear output at "1".

When battery voltage is initially applied to the circuit a positive pulse is fed through E6 to the base of Q11, driving Q12 into saturation and ensuring that the Counter is cleared and ready to accommodate an incoming call.

Individual Counter FF1 - FF3
(IC4_a, IC5_a, IC5_b)

The Individual Counter is composed of three J-K master-slave flip-flops with their J-K inputs all tied to logic state "1" through resistor R87. Each FF will thus toggle whenever it receives a clock pulse at the same time that its Clear input is held at "1". The Clock stage toggles FF1, FF1 toggles FF2, and FF2 toggles FF3.

FF1 has a Preset as well as a Clear function, allowing the tone receiver to be strapped to either 4-tone or 5-tone sequences.

Truth tables for these two models follow:

Truth Table for the Individual Counter

<u>5-tone</u>	<u>1</u>	<u>$\bar{1}$</u>	<u>2</u>	<u>$\bar{2}$</u>	<u>3</u>	<u>$\bar{3}$</u>
Cleared (pending call)	0	1	0	1	0	1
After first tone	1	0	0	1	0	1
After second tone	0	1	1	0	0	1
After third tone	1	0	1	0	0	1
After fourth tone	0	1	0	1	1	0
After fifth tone	1	0	0	1	1	0
40 mS after last tone (cleared, pending call)	0	1	0	1	0	1

<u>4-tone</u>	<u>1</u>	<u>$\bar{1}$</u>	<u>2</u>	<u>$\bar{2}$</u>	<u>3</u>	<u>$\bar{3}$</u>
Preset (pending call)	1	0	0	1	0	1
After first tone	0	1	1	0	0	1
After second tone	1	0	1	0	0	1
After third tone	0	1	0	1	1	0
After fourth tone	1	0	0	1	1	0
40 mS after last tone (cleared, pending call)	1	0	0	1	0	1

The truth table for group calls will be similar.

Group Counter FF5 - FF6 (IC10_a, IC10_b)

The Group Counter comprises two J-K master-slave flip-flops which are coupled quite similarly to FF1 - FF3 in the Individual Counter except that the K input of FF6 is controlled by Group Gate Q29.

Group Gate (Q29) and Blocking Gate (Q24)

These two gates prevent inadvertent cancelling of the group call set-up when or if the group call tone sequence is retransmitted.

During the tone signalling sequence, inverter Q29 holds the FF6 K input at logic state "0" to inhibit the Counter from switching output states and thus cancelling the call set-up.

After the group call is set up, Q24 will be held ON by FF4 output $\bar{4}$. The logic "1" level at this output turns Q24 ON, placing a short circuit across the Group Schmitt Trigger output so that no new group signal can reach the clock circuits.

The Blocking Gate has another function; when the loudspeaker is turned ON, an incoming group call must not be able to interrupt the connection. Since FF4 output $\bar{4}$ is at logic state "1" whenever the speaker is ON (as when a call comes through or when set up by the LS IN / OUT push button via terminal 32), Q24 short circuits the Group Schmitt Trigger as just explained.

Truth Tables for Group Counter

<u>One Group Digit</u>	<u>5</u>	<u>$\bar{5}$</u>	<u>6</u>	<u>$\bar{6}$</u>
Cleared (pending call)	0	1	0	1
After first tone	1	0	1	0
40 ms later (Clear circuit output returns to "0")	0	1	1	0
300 ms after carrier disappears (Squelch Delay triggers Cancelling Switch)	0	1	0	1

<u>Two Group Digits</u>	<u>5</u>	<u>$\bar{5}$</u>	<u>6</u>	<u>$\bar{6}$</u>
Cleared (pending call)	0	1	0	1
After first tone	1	0	0	1
After second tone	0	1	1	0
40 ms later (Clear circuit output returns to "0")	0	1	1	0
300 ms after carrier disappears (Squelch Delay triggers Cancelling Switch)	0	1	0	1

Decoder (IC6, IC7)

Each Decoder IC contains 3 separate, 3-input TTL NAND gates.

The output of a NAND gate is L0 (logic "0") only when all of its inputs are HI (logic "1").

In stand by, 5-tone mode, the output of IC6_a is always "0". In the 4-tone mode, the output of IC6_b will be "0", instead.

At the end of a correct tone call IC7_c presents a logic "0" to the Read-out Gate and to the Alarm circuit. The Alarm output, terminal 37, goes "0" through Q42, but only for individual calls. Group calls do not activate the Alarm circuit.

Individual AF Gates a, b, c, d, e (Q15 - Q19)

The AF Gates are controlled from the Decoder NAND gates, IC6_a - IC7_b. When a transistor base is driven L0 (logic "0") by a NAND gate, that transistor will conduct and ground the coil terminal connected to its collector.

Group AF Gates f and g (Q20, Q21)

For tone signals with only one group digit, Q21 is controlled from IC7_b. Q20 is not connected.

For signals having two group digits, the first Group AF Gate, Q20, is connected in parallel with the fourth Individual AF Gate, Q18. Both gates are driven by IC7_a. The second (last) Group AF Gate, Q21, is driven directly by FF5 output 5̄.

Alarm Circuit (Q39 - Q42, E18)

In stand by, Q39 is ON and E18 cannot conduct. Q40 and Q41 are both ON, and Q42 is OFF.

A correct call turns Q39 OFF and C46 charges through E18, causing Q40 and Q41 to turn OFF, driving Q42 ON, and connecting terminal 37 (ALARM) to chassis ground.

After approximately 40 ms (the clear delay) IC7_c goes "1" and turns Q39 ON again. E18 can no longer conduct and C46 discharges through R114. After the delay caused by the time constant of C46 - R114, Q40 and Q41 turn ON and disconnect the Alarm circuit common return through Q42. The Alarm stays ON for approximately 1 second.

Group calls, however, do not activate the Alarm circuit. After receipt of the last group tone, FF6

output 6 goes "1". E19 then conducts, holding Q41 ON, thus Q42 stays cut off.

AF Muting and Key Lock Switch (Q30, Q31, E14)

The AF Muting and the Key Lock are controlled by the output of Read-out Gate IC4_b (output 4̄).

In stand by the outputs of Q30 and Q31 are HI (~+10 V), E14 conducts and the loudspeaker is muted through terminal 34.

As long as the potential at terminal 51 is HI, the transmitter keying function is also disabled.

When the Read-out Gate is activated, output 4̄ goes "1", and Q30 and Q31 conduct, suspending the AF Muting and Key Lock functions.

Call and Occupied Lamp Switches (Q32, Q33, Q34)

The Call Lamp Switch, Q33, lights the Call Lamp by grounding it through terminal 47.

Terminal 49, in parallel with terminal 47, is provided for automatic muting of the vehicle's broadcast band radio, and requires an auxiliary relay.

At the end of a tone sequence, output 4 of FF4 goes "0", cutting Q32 OFF and turning Q33 ON, to complete the common return path for terminals 47 and 49.

Whenever the channel is occupied a DC voltage from the Squelch circuit, via terminal 41, turns Q34 ON, grounding the Occupied Lamp through terminal 45.

Cancelling Switch (Q38)

When the radiotelephone is turned ON the output functions must not be activated. To ensure this, Q38 feeds a negative pulse ("0") to the Preset of the Read-out Gate. When the battery voltage is switched ON, C41 discharges through Q38 which goes ON briefly, presetting the Read-out Gate.

The Cancelling Switch also serves to cancel out the call set-up when a group call expires. Receiving a pulse from the Delay circuit, Q38 then forwards a logic "0" to the preset input of FF4, the Read-out Gate.

Squelch Delay (Q35 - Q37)

Fading can be a problem when receiving a group call. To ensure uninterrupted reception, a time delay of approx. 300 ms is introduced before

allowing the Cancelling Switch to clear down the connection. The delay is measured from the time that terminal 45 goes HI to when Q38 Collector goes LO.

After a group call is set up, FF6 output $\bar{6}$ goes "0" and Q35 goes OFF. As long as the RF carrier is present, Q34 is still ON and E16 conducts, keeping Q36 OFF. When the carrier disappears, Q34 goes OFF, E16 can no longer conduct, and C39 begins to charge through R98. Approx. 300 ms later, Q36 goes ON, turning Q37 ON. Q37 feeds a positive pulse to Q38, which in turn applies a negative pulse ("0") to the Read-out Gate preset, cancelling the group call.

This same pulse from Q38 also clears FF6, and the tone receiver is ready for a new call.

Technical Specifications

Supply Power

Nominal: 13.6 V
Minimum: 10.5 V
Maximum: 16.0 V

Current Drain

Stand by: 115 mA \pm 15 mA

Regulated Voltages

Nominal 8.9 V and 4.9 V

Temperature Range

Operating range: -25°C to $+60^{\circ}\text{C}$
Functioning range: -30°C to $+80^{\circ}\text{C}$

Input Impedance

$\geq 6 \text{ K}\Omega$

Equalization

Preemphasis (by RC function) $f_c = 1000\text{Hz}$

Signal Input Level

Nominal at 1000 Hz: 110 mV

Signalling Code

Sequence of 4 or 5 tone bursts of 70 ms \pm 15 ms duration with maximum 15 ms interval between tone bursts.

Tone Signal Frequencies

<u>Coil terminal</u>	<u>Tone frequency</u>
1	970 Hz
2	1060 Hz
3	1160 Hz
4	1270 Hz
5	1400 Hz
6	1530 Hz
7	1670 Hz
8	1830 Hz
9	2000 Hz
10	2200 Hz
11	2400 Hz
12	2600 Hz
13	2800 Hz

Frequency Accuracy

Coil tuned for 1060 Hz: $\leq 0.4\%$ for all tones

Frequency Stability

(typically $\leq 0.5\%$) $\leq 1.0\%$

Selectivity

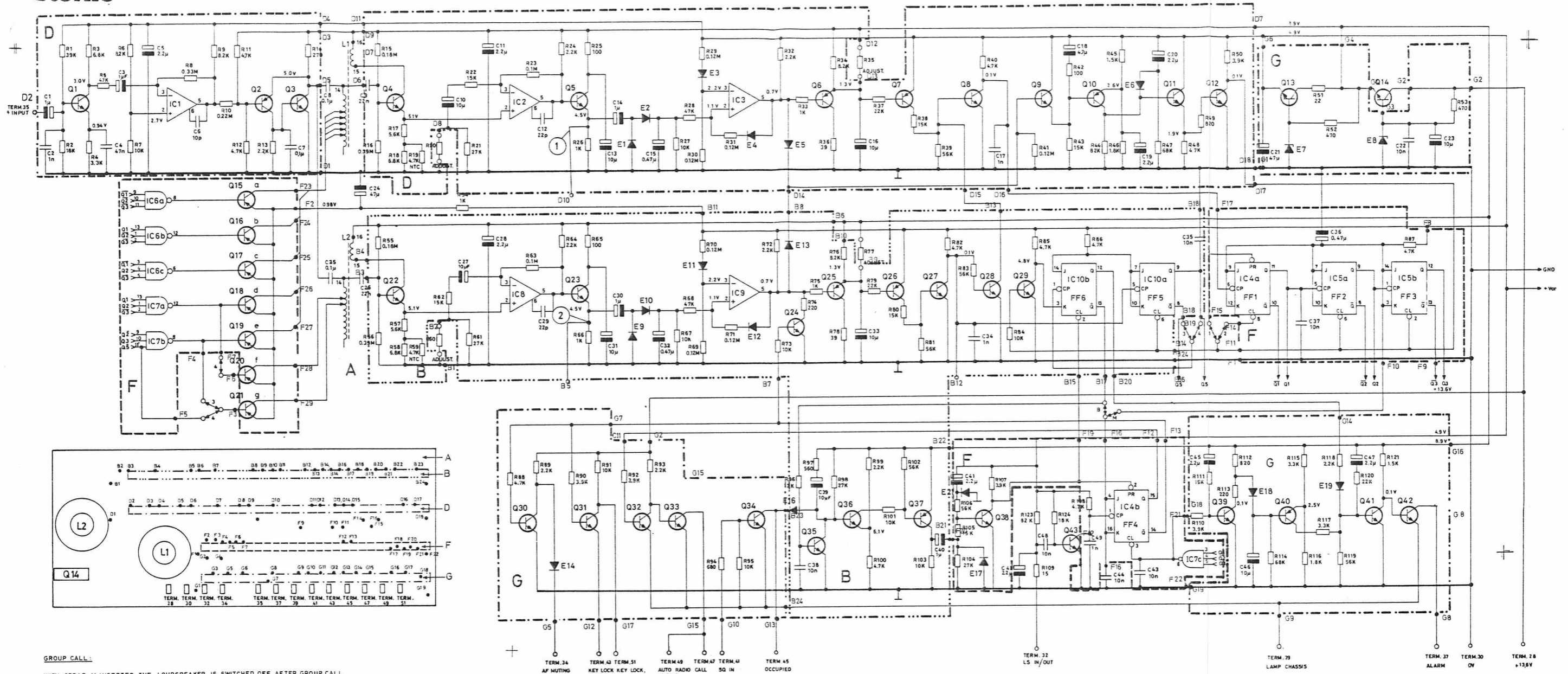
Frequencies differing from f_0 by 4.5% or more are unable to trigger the tone receiver.

Maximum Load Currents

Terminal 37	ALARM	100 mA (for 1.2 sec)
Terminal 47	CALL	100 mA
Terminal 45	OCCUPIED	100 mA
Terminal 51		
and 43	KEY LOCK	10 mA
Terminal 34	AF MUTING	I_{load} min. 0.75 mA for $V_{\text{out}} = 8 \text{ V}$

AF Muting

In conjunction with terminal 18 of CF701: $\geq 60 \text{ dB}$

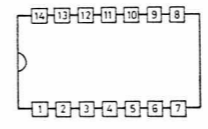
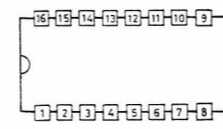
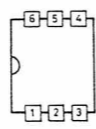
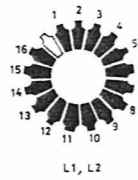


GROUP CALL:

WITH STRAP M INSERTED, THE LOUDSPEAKER IS SWITCHED OFF AFTER GROUP CALL.
 WITH STRAP B INSERTED, THE LOUDSPEAKER REMAINS ON AFTER THE GROUP CALL.

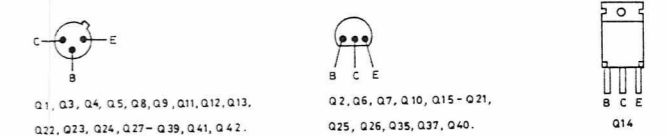
TERM.	DIGIT	FREQ.
1	X	970 Hz
2	1	1060 -
3	2	1160 -
4	3	1270 -
5	4	1400 -
6	5	1530 -
7	6	1670 -
8	7	1830 -
9	8	2000 -
10	9	2200 -
11	0	2400 -
12	REPEAT	2600 -
13	ALARM	2800 -

IC	Vcc PIN	GND PIN
IC1	2	6
IC2	2	6
IC3	2	6
IC4	5	13
IC5	4	11
IC6	14	7
IC7	14	7
IC8	2	6
IC9	2	6
IC10	4	11



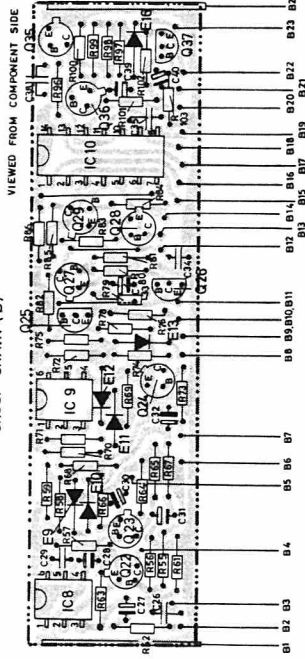
TOP VIEW

- 4-TONE SEQUENTIAL RECEIVER: INSERT STRAP 1
- 5-TONE SEQUENTIAL RECEIVER: INSERT STRAP 2
- 4-TONE SEQUENTIAL RECEIVER WITH 1-TONE GROUP CALL: INSERT STRAPS 1 AND 3
- 4-TONE SEQUENTIAL RECEIVER WITH 2-TONE GROUP CALL: INSERT STRAPS 1 AND 4
- 5-TONE SEQUENTIAL RECEIVER WITH 1-TONE GROUP CALL: INSERT STRAPS 2 AND 3
- 5-TONE SEQUENTIAL RECEIVER WITH 2-TONE GROUP CALL: INSERT STRAPS 2 AND 4

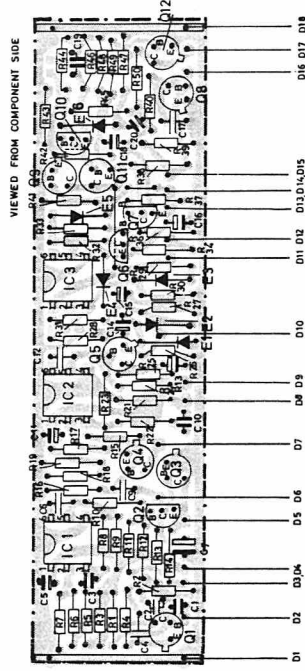


BOTTOM VIEW

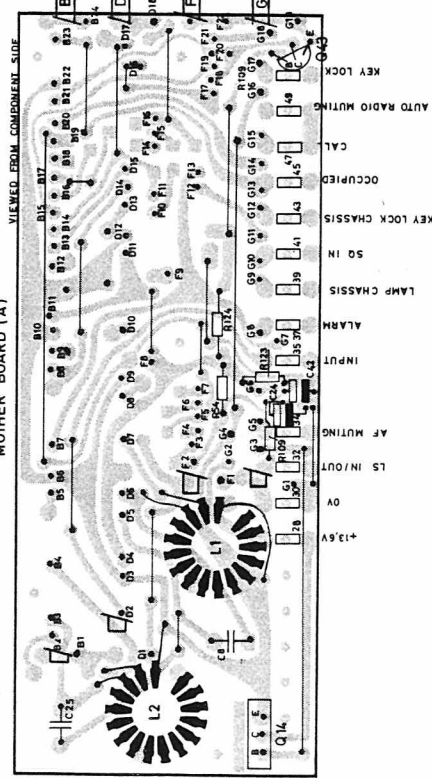
GROUP CHAIN (B)



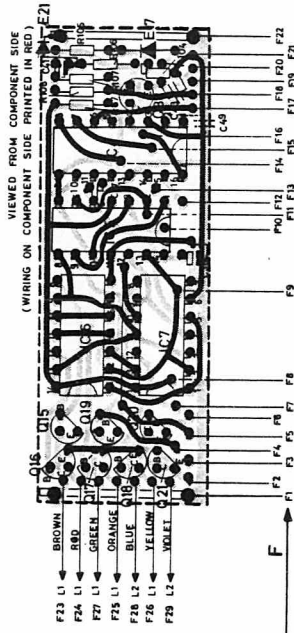
INDIVIDUAL CHAIN (D)



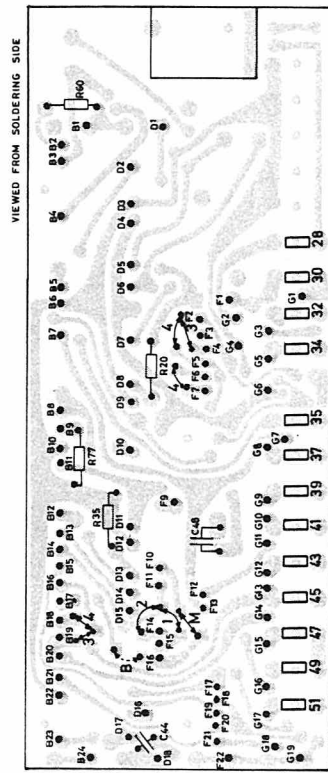
MOTHER BOARD (A)



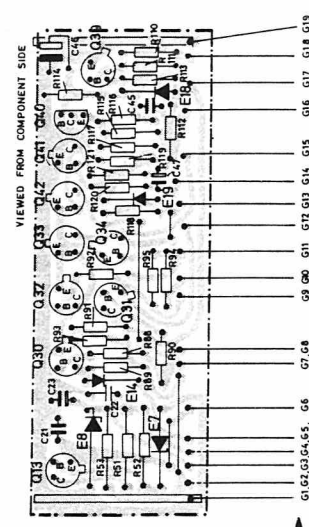
COUNTER AND DECODER (F)



MOTHER BOARD (A)



OUTLET SWITCHES (G)



SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER

SR7841

D401.711/2

TYPE	NO.	CODE	DATA
SR7841		10.2456	Sequential Tone Receiver
	C1	73.5135	1μF -20+50% tantal
	C2	76.5069	1nF 10% polyester, FL
	C3	73.5135	1μF -20+50% tantal
	C4	76.5072	47nF 10% polyester, FL
	C5	73.5129	2.2μF -20+50% tantal
	C6	74.5135	10pF 5% ceram
	C7	76.5070	10nF 10% polyester, FL
	C8	76.5068	0.1μF 1% polystyren TB
	C9	76.5071	22nF 10% polyester, FL
	C10	73.5109	10μF 20% tantal
	C11	73.5129	2.2μF -20+50% tantal
	C12	74.5106	22pF ± 0.5pF ceram
	C13	73.5109	10μF 20% tantal
	C14	73.5114	1μF 20% tantal
	C15	73.5125	0.47μF 20% tantal
	C16	73.5109	10μF 20% tantal
	C17	76.5069	1nF 10% polyester, FL
	C18	73.5126	4.7μF 20% tantal
	C19	73.5129	2.2μF -20+50% tantal
	C20	73.5129	2.2μF -20+50% tantal
	C21	73.5124	47μF 20% tantal
	C22	76.5070	10nF 10% polyester, FL
	C23	73.5109	10μF 20% tantal
	C24	73.5124	47μF 20% tantal
	C25	76.5068	0.1μF 1% polystyr TB
	C26	76.5071	22nF 10% polyester, FL
	C27	73.5109	10μF 20% tantal
	C28	73.5129	2.2μF -20+50% tantal
	C29	74.5106	22pF ± 0.5pF ceram
	C30	73.5114	1μF 20% tantal
	C31	73.5109	10μF 20% tantal
	C32	73.5125	0.47μF 20% tantal
	C33	73.5109	10μF 20% tantal
	C34	76.5069	1nF 10% polyester, FL
	C35	74.5109	10nF -20/+80% ceram PL
	C36	73.5134	0.47μF -20+50% tantal
	C37	74.5109	10nF -20/+80% ceram PL
	C38	74.5109	10nF -20/+80% ceram PL
	C39	73.5109	10μF 20% tantal
	C40	73.5135	1μF -20/+50% tantal
	C41	73.5129	2.2μF -20+50% tantal
	C42	73.5129	2.2μF -20+50% tantal
	C43	74.5109	10nF -20+80% ceram PL
	C44	74.5109	10nF -20+80% ceram PL
	C45	73.5129	2.2μF -20+50% tantal
	C46	73.5109	10μF 20% tantal

TYPE	NO.	CODE	DATA
	C47	73.5129	2.2μF -20+50% tantal
	R1	80.5068	39kΩ 5% carbon film
	R2	80.5064	18kΩ 5% carbon film
	R3	80.5059	6.8kΩ 5% carbon film
	R4	80.5055	3.3kΩ 5% carbon film
	R5	80.5069	47kΩ 5% carbon film
	R6	80.5060	8.2kΩ 5% carbon film
	R7	80.5061	10kΩ 5% carbon film
	R8	80.5079	0.33MΩ 5% carbon film
	R9	80.5060	8.2kΩ 5% carbon film
	R10	80.5077	0.22MΩ 5% carbon film
	R11	80.5057	4.7kΩ 5% carbon film
	R12	80.5057	4.7kΩ 5% carbon film
	R13	80.5053	2.2kΩ 5% carbon film
	R14	80.5042	270Ω 5% carbon film
	R15	80.5076	0.18MΩ 5% carbon film
	R16	80.5080	0.39MΩ 5% carbon film
	R17	80.5058	5.6kΩ 5% carbon film
	R18	80.5059	6.8kΩ 5% carbon film
	R19	89.5009	4.7kΩ 20% NTC
	R20	80.50xx	Adjusted 5% carbon film
	R21	80.5066	27kΩ 5% carbon film
	R22	80.5063	15kΩ 5% carbon film
	R23	80.5073	0.1MΩ 5% carbon film
	R24	80.5053	2.2kΩ 5% carbon film
	R25	80.5037	100Ω 5% carbon film
	R26	80.5049	1kΩ 5% carbon film
	R27	80.5061	10kΩ 5% carbon film
	R28	80.5069	47kΩ 5% carbon film
	R29	80.5074	0.12MΩ 5% carbon film
	R30	80.5074	0.12MΩ 5% carbon film
	R31	80.5074	0.12MΩ 5% carbon film
	R32	80.5053	2.2kΩ 5% carbon film
	R33	80.5049	1kΩ 5% carbon film
	R34	80.5060	8.2kΩ 5% carbon film
	R35	80.50xx	Adjusted 5% carbon film
	R36	80.5032	39Ω 5% carbon film
	R37	80.5065	22kΩ 5% carbon film
	R38	80.5063	15kΩ 5% carbon film
	R39	80.5070	56kΩ 5% carbon film
	R40	80.5057	4.7kΩ 5% carbon film

SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER

SR7841

X401.695/2

TYPE	NO.	CODE	DATA
	R41	80.5074	0.12M Ω 5%
	R42	80.5037	carbon film
	R43	80.5063	carbon film
	R44	80.5072	carbon film
	R45	80.5051	carbon film
	R46	80.5052	carbon film
	R47	80.5071	carbon film
	R48	80.5057	carbon film
	R49	80.5048	carbon film
	R50	80.5056	carbon film
	R51	80.5229	carbon film
	R52	80.5245	22 Ω 5%
	R53	80.5245	carbon film
	R54	80.5049	carbon film
	R55	80.5076	1k Ω 5%
	R56	80.5080	0.18M Ω 5%
	R57	80.5058	0.39M Ω 5%
	R58	80.5059	5.6k Ω 5%
	R59	89.5009	6.8k Ω 5%
	R60	80.50xx	4.7k Ω NTC 20%
	R61	80.5066	Adjusted 5%
	R62	80.5063	27k Ω 5%
	R63	80.5073	15k Ω 5%
	R64	80.5053	0.1M Ω 5%
	R65	80.5037	2.2k Ω 5%
	R66	80.5049	100 Ω 5%
	R67	80.5061	1k Ω 5%
	R68	80.5069	10k Ω 5%
	R69	80.5074	47k Ω 5%
	R70	80.5074	0.12M Ω 5%
	R71	80.5074	0.12M Ω 5%
	R72	80.5053	2.2k Ω 5%
	R73	80.5041	10k Ω 5%
	R74	80.5049	220 Ω 5%
	R75	80.5049	1k Ω 5%
	R76	80.5060	8.2k Ω 5%
	R77	80.50xx	Adjusted 5%
	R78	80.5032	39 Ω 5%
	R79	80.5065	22k Ω 5%
	R80	80.5063	15k Ω 5%
	R81	80.5070	56k Ω 5%
	R82	80.5057	4.7k Ω 5%
	R83	80.5070	56k Ω 5%
	R84	80.5061	10k Ω 5%
	R85	80.5057	4.7k Ω 5%
	R86	80.5057	4.7k Ω 5%
	R87	80.5057	4.7k Ω 5%
	R88	80.5057	4.7k Ω 5%

TYPE	NO.	CODE	DATA
	R89	80.5053	2.2k Ω 5%
	R90	80.5056	carbon film
	R91	80.5061	carbon film
	R92	80.5056	carbon film
	R93	80.5053	carbon film
	R94	80.5047	carbon film
	R95	80.5061	680 Ω 5%
	R96	80.5062	10k Ω 5%
	R97	80.5046	12k Ω 5%
	R98	80.5066	560 Ω 5%
	R99	80.5053	27k Ω 5%
	R100	80.5057	2.2k Ω 5%
	R101	80.5061	4.7k Ω 5%
	R102	80.5070	10k Ω 5%
	R103	80.5061	56k Ω 5%
	R104	80.5066	10k Ω 5%
	R105	80.5063	27k Ω 5%
	R106	80.5070	15k Ω 5%
	R107	80.5056	56k Ω 5%
	R108	80.5057	3.9k Ω 5%
	R109	80.5027	4.7k Ω 5%
	R110	80.5056	15.2 5%
	R111	80.5063	3.9k Ω 5%
	R112	80.5048	15k Ω 5%
	R113	80.5041	820 Ω 5%
	R114	80.5071	220 Ω 5%
	R115	80.5055	68 Ω 5%
	R116	80.5052	3.3k Ω 5%
	R117	80.5055	1.8k Ω 5%
	R118	80.5053	3.3k Ω 5%
	R119	80.5053	2.2k Ω 5%
	R120	80.5065	carbon film
	R121	80.5051	carbon film
	R123	80.5072	56k Ω 5%
	R124	80.5064	1.5k Ω 5%
	L1	61.1148	82 K Ω 5%
	L2	61.1148	18 K Ω 5%
	E1	99.5237	Tone coil
	E2	99.5237	Tone coil
	E3	99.5237	1N4148 Diode
	E4	99.5237	1N4148 Diode
	E5	99.5237	1N4148 Diode

SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER

SR7841

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TYPE	NO.	CODE	DATA
	E6	99. 5237	1N4148 Diode
	E7	99. 5114	5. 6V 5% Zenerdiode
	E8	99. 5042	9. 1V 5% Zenerdiode
	E9	99. 5237	1N4148 Diode
	E10	99. 5237	1N4148 Diode
	E11	99. 5237	1N4148 Diode
	E12	99. 5237	1N4148 Diode
	E13	99. 5237	1N4148 Diode
	E14	99. 5237	1N4148 Diode
	E16	99. 5237	1N4148 Diode
	E17	99. 5237	1N4148 Diode
	E18	99. 5237	1N4148 Diode
	E19	99. 5237	1N4148 Diode
	Q1	99. 5143	BC108 Transistor
	Q2	99. 5144	BC214L Transistor
	Q3	99. 5743	BC108 Transistor
	Q4	99. 5143	BC108 Transistor
	Q5	99. 5143	BC108 Transistor
	Q6	99. 5144	BC214L Transistor
	Q7	99. 5144	BC214L Transistor
	Q8	99. 5143	BC108 Transistor
	Q9	99. 5143	BC108 Transistor
	Q10	99. 5144	BC214L Transistor
	Q11	99. 5143	BC108 Transistor
	Q12	99. 5143	BC108 Transistor
	Q13	99. 5143	BC108 Transistor
	Q14	99. 5246	TIP31 Transistor
	Q15	99. 5144	BC214L Transistor
	Q16	99. 5144	BC214L Transistor
	Q17	99. 5144	BC214L Transistor
	Q18	99. 5144	BC214L Transistor
	Q19	99. 5144	BC214L Transistor
	Q20	99. 5144	BC214L Transistor
	Q21	99. 5144	BC214L Transistor
	Q22	99. 5143	BC108 Transistor
	Q23	99. 5143	BC108 Transistor
	Q24	99. 5143	BC108 Transistor
	Q25	99. 5144	BC214L Transistor
	Q26	99. 5144	BC214L Transistor
	Q27	99. 5143	BC108 Transistor
	Q28	99. 5143	BC108 Transistor
	Q29	99. 5143	BC108 Transistor
	Q30	99. 5143	BC108 Transistor
	Q31	99. 5143	BC108 Transistor
	Q32	99. 5143	BC108 Transistor

0. 25W
0. 25W

TYPE	NO.	CODE	DATA
	Q33	99. 5143	BC108 Transistor
	Q34	99. 5143	BC108 Transistor
	Q35	99. 5143	BC108 Transistor
	Q36	99. 5143	BC108 Transistor
	Q37	99. 5144	BC214L Transistor
	Q38	99. 5143	BC108 Transistor
	Q39	99. 5143	BC108 Transistor
	Q40	99. 5144	BC214L Transistor
	Q41	99. 5143	BC108 Transistor
	Q42	99. 5143	BC108 Transistor
	Q43	99. 5117	BC167 Transistor
	IC1	14. 5017	1AA861 Operational Amplifier
	IC2	14. 5017	TAA861 Operational Amplifier
	IC3	14. 5017	TAA861 Operational Amplifier
	IC4	14. 5009	Dual J-K, master slave FF/clear-- preset
	IC5	14. 5008	Dual J-K, master slave FF/clear
	IC6	14. 5007	Triple 3-input NAND-gate
	IC7	14. 5007	Triple 3-input NAND-gate
	IC8	14. 5017	TAA861 Operational Amplifier
	IC9	14. 5017	TAA861 Operational Amplifier
	IC10	14. 5008	Dual J-K, master slave FF/clear

SEQUENTIAL TONE RECEIVER SR7841
SEKVENSTONEMODTAGER

X401. 695 / 2

TYPE	NO.	CODE	DATA
SR7841		10. 2456	Sequential Tone Receiver
	C1	73. 5135	1μF -20+50% tantal
	C2	76. 5069	1nF 10% polyester, FL
	C3	73. 5135	1μF -20+50% tantal
	C4	76. 5072	47nF 10% polyester, FL
	C5	73. 5129	2. 2μF -20+50% tantal
	C6	74. 5135	10pF 5% ceram
	C7	76. 5070	10nF 10% polyester, FL
	C8	76. 5068	0. 1μF 1% polystyren TB
	C9	76. 5071	22nF 10% polyester, FL
	C10	73. 5109	10μF 20% tantal
	C11	73. 5129	2. 2μF -20+50% tantal
	C12	74. 5106	22pF ± 0. 5pF ceram
	C13	73. 5109	10μF 20% tantal
	C14	73. 5114	1μF 20% tantal
	C15	73. 5125	0. 47μF 20% tantal
	C16	73. 5109	10μF 20% tantal
	C17	76. 5069	1nF 10% polyester, FL
	C18	73. 5126	4. 7μF 20% tantal
	C19	73. 5129	2. 2μF -20+50% tantal
	C20	73. 5129	2. 2μF -20+50% tantal
	C21	73. 5124	47μF 20% tantal
	C22	76. 5070	10nF 10% polyester, FL
	C23	73. 5109	10μF 20% tantal
	C24	73. 5124	47μF 20% tantal
	C25	76. 5068	0. 1μF 1% polystyr TB
	C26	76. 5071	22nF 10% polyester, FL
	C27	73. 5109	10μF 20% tantal
	C28	73. 5129	2. 2μF -20/+50% tantal
	C29	74. 5106	22pF ± 0. 5pF ceram
	C30	73. 5114	1μF 20% tantal
	C31	73. 5109	10μF 20% tantal
	C32	73. 5125	0. 47μF 20% tantal
	C33	73. 5109	10μF 20% tantal
	C34	76. 5069	1nF 10% polyester, FL
	C35	74. 5109	10nF -20/+80% ceram PL
	C36	73. 5134	0. 47μF -20+50% tantal
	C37	74. 5109	10nF -20/+80% ceram PL
	C38	74. 5109	10nF -20/+80% ceram PL
	C39	73. 5109	10μF 20% tantal
	C40	73. 5135	1μF -20/+50% tantal
	C41	73. 5129	2. 2μF -20+50% tantal
	C42	73. 5124	47μF 20% tantal
	C43	74. 5109	10nF -20+80% ceram PL
	C44	74. 5109	10nF -20+80% ceram PL
	C45	73. 5129	2. 2μF -20+50% tantal
	C46	73. 5109	10μF 20% tantal

TYPE	NO.	CODE	DATA
	C47	73. 5129	2. 2μF -20+50% tantal
	R1	80. 5068	39kΩ 5% carbon film
	R2	80. 5064	18kΩ 5% carbon film
	R3	80. 5059	6. 8kΩ 5% carbon film
	R4	80. 5055	3. 3kΩ 5% carbon film
	R5	80. 5069	47kΩ 5% carbon film
	R6	80. 5060	8. 2kΩ 5% carbon film
	R7	80. 5061	10kΩ 5% carbon film
	R8	80. 5079	0. 33MΩ 5% carbon film
	R9	80. 5060	8. 2kΩ 5% carbon film
	R10	80. 5077	0. 22MΩ 5% carbon film
	R11	80. 5057	4. 7kΩ 5% carbon film
	R12	80. 5057	4. 7kΩ 5% carbon film
	R13	80. 5053	2. 2kΩ 5% carbon film
	R14	80. 5042	270Ω 5% carbon film
	R15	80. 5076	0. 18MΩ 5% carbon film
	R16	80. 5080	0. 39MΩ 5% carbon film
	R17	80. 5058	5. 6kΩ 5% carbon film
	R18	80. 5059	6. 8kΩ 5% carbon film
	R19	89. 5009	4. 7kΩ 20% NTC
	R20	80. 50xx	Adjusted 5% carbon film
	R21	80. 5066	27kΩ 5% carbon film
	R22	80. 5063	15kΩ 5% carbon film
	R23	80. 5073	0. 1MΩ 5% carbon film
	R24	80. 5053	2. 2kΩ 5% carbon film
	R25	80. 5037	100Ω 5% carbon film
	R26	80. 5049	1kΩ 5% carbon film
	R27	80. 5061	10kΩ 5% carbon film
	R28	80. 5059	47kΩ 5% carbon film
	R29	80. 5074	0. 12MΩ 5% carbon film
	R30	80. 5074	0. 12MΩ 5% carbon film
	R31	80. 5074	0. 12mΩ 5% carbon film
	R32	80. 5053	2. 2kΩ 5% carbon film
	R33	80. 5049	1kΩ 5% carbon film
	R34	80. 5060	8. 2kΩ 5% carbon film
	R35	80. 50xx	Adjusted 5% carbon film
	R36	80. 5032	3Ω 5% carbon film
	R37	80. 5065	22kΩ 5% carbon film
	R38	80. 5063	15kΩ 5% carbon film
	R39	80. 5070	56kΩ 5% carbon film
	R40	80. 5057	4. 7kΩ 5% carbon film

SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER

SR7841

X401. 695

TYPE	NO.	CODE	DATA
	R41	80.5074	0.12M Ω 5%
	R42	80.5037	100 Ω 5%
	R43	80.5063	15k Ω 5%
	R44	80.5072	82k Ω 5%
	R45	80.5051	1.5k Ω 5%
	R46	80.5052	1.8k Ω 5%
	R47	80.5071	68k Ω 5%
	R48	80.5057	4.7k Ω 5%
	R49	80.5048	820 Ω 5%
	R50	80.5056	3.9k Ω 5%
	R51	80.5229	22 Ω 5%
	R52	80.5245	470 Ω 5%
	R53	80.5245	470 Ω 5%
	R54	80.5049	1k Ω 5%
	R55	80.5076	0.18M Ω 5%
	R56	80.5080	0.39M Ω 5%
	R57	80.5058	5.6k Ω 5%
	R58	80.5059	6.8k Ω 5%
	R59	89.5009	4.7k Ω NTC 20%
	R60	80.50xx	Adjusted 5%
	R61	80.5066	27k Ω 5%
	R62	80.5063	15k Ω 5%
	R63	80.5073	0.1M Ω 5%
	R64	80.5053	2.2k Ω 5%
	R65	80.5037	100 Ω 5%
	R66	80.5049	1k Ω 5%
	R67	80.5061	10k Ω 5%
	R68	80.5069	47k Ω 5%
	R69	80.5074	0.12M Ω 5%
	R70	80.5074	0.12M Ω 5%
	R71	80.5074	0.12M Ω 5%
	R72	80.5053	2.2k Ω 5%
	R73	80.5061	10k Ω 5%
	R74	80.5041	220 Ω 5%
	R75	80.5049	1k Ω 5%
	R76	80.5060	8.2k Ω 5%
	R77	80.50xx	Adjusted 5%
	R78	80.5032	39 Ω 5%
	R79	80.5065	22k Ω 5%
	R80	80.5063	15k Ω 5%
	R81	80.5070	56k Ω 5%
	R82	80.5057	4.7k Ω 5%
	R83	80.5070	56k Ω 5%
	R84	80.5061	10k Ω 5%
	R85	80.5057	4.7k Ω 5%
	R86	80.5057	4.7k Ω 5%
	R87	80.5057	4.7k Ω 5%
	R88	80.5057	4.7k Ω 5%

TYPE	NO.	CODE	DATA
	R89	80.5053	2.2k Ω 5%
	R90	80.5056	3.9k Ω 5%
	R91	80.5061	10k Ω 5%
	R92	80.5056	3.9k Ω 5%
	R93	80.5053	2.2k Ω 5%
	R94	80.5047	680 Ω 5%
	R95	80.5061	10k Ω 5%
	R96	80.5062	12k Ω 5%
	R97	80.5046	560 Ω 5%
	R98	80.5066	27k Ω 5%
	R99	80.5053	2.2k Ω 5%
	R100	80.5057	4.7k Ω 5%
	R101	80.5061	10k Ω 5%
	R102	80.5070	56k Ω 5%
	R103	80.5061	10k Ω 5%
	R104	80.5066	27k Ω 5%
	R105	80.5063	15k Ω 5%
	R106	80.5070	56k Ω 5%
	R107	80.5056	3.9k Ω 5%
	R108	80.5057	4.7k Ω 5%
	R109	80.5035	68 Ω 5%
	R110	80.5056	3.9k Ω 5%
	R111	80.5063	15k Ω 5%
	R112	80.5048	820 Ω 5%
	R113	80.5041	220 Ω 5%
	R114	80.5071	68k Ω 5%
	R115	80.5055	3.3k Ω 5%
	R116	80.5052	1.8k Ω 5%
	R117	80.5055	3.3k Ω 5%
	R118	80.5053	2.2k Ω 5%
	R119	80.5070	56k Ω 5%
	R120	80.5065	22k Ω 5%
	R121	80.5051	1.5k Ω 5%
	L1	61.1148	Tone coil
	L2	61.1148	Tone coil
	E1	99.5237	1N4148 Diode
	E2	99.5237	1N4148 Diode
	E3	99.5237	1N4148 Diode
	E4	99.5237	1N4148 Diode
	E5	99.5237	1N4148 Diode

**SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER**

SR7841

X401.695

TYPE	NO.	CODE	DATA
	E6	99. 5237	1N4148 Diode
	E7	99. 5114	5. 6V 5% Zenerdiode
	E8	99. 5042	9. 1V 5% Zenerdiode
	E9	99. 5237	1N4148 Diode
	E10	99. 5237	1N4148 Diode
	E11	99. 5237	1N4148 Diode
	E12	99. 5237	1N4148 Diode
	E13	99. 5237	1N4148 Diode
	E14	99. 5237	1N4148 Diode
	E15	99. 5020	1N4004 Diode
	E16	99. 5237	1N4148 Diode
	E17	99. 5237	1N4148 Diode
	E18	99. 5237	1N4148 Diode
	E19	99. 5237	1N4148 Diode
	E20	99. 5020	1N4004 Diode
	Q1	99. 5143	BC108 Transistor
	Q2	99. 5144	BC214L Transistor
	Q3	99. 5743	BC108 Transistor
	Q4	99. 5143	BC108 Transistor
	Q5	99. 5143	BC108 Transistor
	Q6	99. 5144	BC214L Transistor
	Q7	99. 5144	BC214L Transistor
	Q8	99. 5143	BC108 Transistor
	Q9	99. 5143	BC108 Transistor
	Q10	99. 5144	BC214L Transistor
	Q11	99. 5143	BC108 Transistor
	Q12	99. 5143	BC108 Transistor
	Q13	99. 5143	BC108 Transistor
	Q14	99. 5246	TIP31 Transistor
	Q15	99. 5144	BC214L Transistor
	Q16	99. 5144	BC214L Transistor
	Q17	99. 5144	BC214L Transistor
	Q18	99. 5144	BC214L Transistor
	Q19	99. 5144	BC214L Transistor
	Q20	99. 5144	BC214L Transistor
	Q21	99. 5144	BC214L Transistor
	Q22	99. 5143	BC108 Transistor
	Q23	99. 5143	BC108 Transistor
	Q24	99. 5143	BC108 Transistor
	Q25	99. 5144	BC214L Transistor
	Q26	99. 5144	BC214L Transistor
	Q27	99. 5143	BC108 Transistor
	Q28	99. 5143	BC108 Transistor
	Q29	99. 5143	BC108 Transistor
	Q30	99. 5143	BC108 Transistor
	Q31	99. 5143	BC108 Transistor
	Q32	99. 5143	BC108 Transistor

0. 25W
0. 25W

TYPE	NO.	CODE	DATA
	Q33	99. 5143	BC108 Transistor
	Q34	99. 5143	BC108 Transistor
	Q35	99. 5143	BC108 Transistor
	Q36	99. 5143	BC108 Transistor
	Q37	99. 5144	BC214L Transistor
	Q38	99. 5143	BC108 Transistor
	Q39	99. 5143	BC108 Transistor
	Q40	99. 5144	BC214L Transistor
	Q41	99. 5143	BC108 Transistor
	Q42	99. 5143	BC108 Transistor
	IC1	14. 5017	TAA861 Operational Amplifier
	IC2	14. 5017	TAA861 Operational Amplifier
	IC3	14. 5017	TAA861 Operational Amplifier
	IC4	14. 5009	Dual J-K, master slave FF/clear- preset
	IC5	14. 5008	Dual J-K, master slave FF/clear
	IC6	14. 5007	Triple 3-input NAND-gate
	IC7	14. 5007	Triple 3-input NAND-gate
	IC8	14. 5017	TAA861 Operational Amplifier
	IC9	14. 5017	TAA861 Operational Amplifier
	IC10	14. 5008	Dual J-K, master slave FF/clear

**SEQUENTIAL TONE RECEIVER
SEKVENSTONEMODTAGER**

SR7841

X401. 695

SEQUENTIAL TONE RECEIVER

SR7841a

Introduction

SR7841a is a sequential tone receiver for selective calling in Stornophone 700 radiotelephone equipment. The frequencies employed are the standard Storno series: 970 Hz to 2800 Hz.

The SR7841a tone receiver can be coded for any of the following operating modes:

- 4 or 5 tones, individual call, only
- 4 or 5 tones, including one group call digit
- 4 or 5 tones, including two group call digits.

General Description

Individual Call

Upon reception of a signal having the correct tones in the proper sequence the following events take place (in the receiver):

The Call Lamp lights, the AF Muting is cancelled and the Key Lock function "unlocks". When the vehicle's traffic horn is connected to the tone receiver via an auxiliary relay, the horn will also sound for about one second.

The audio circuit and the Key Lock are both turned on and off manually by means of the LS IN/OUT push button. Since the switch that "unlocks" the Key Lock also turns on the loudspeaker, the operator is forced to check for the presence of another signal on the channel before being able to key his transmitter.

In addition, the tone receiver is equipped with an Occupied Lamp controlled by the squelch circuit of the radiotelephone receiver. Thus, if an RF signal on the channel frequency is present at the antenna input it will cause the Occupied Lamp to light as an indication that the channel is not free.

At the end of a call the Call Lamp, governed by the receiver Squelch, goes out when the carrier disappears.

After reception of a correct call the speaker will remain open until the LS IN/OUT button is depressed.

Group Call

Group calls do not activate the Alarm circuit and the transmitter lock does not "unlock". The Call Lamp and the loudspeaker are both turned on. During the call the Occupied Lamp is on and 300 ms after it goes off the loudspeaker is turned off as it is controlled by the squelch circuit. If, what will not be normal procedures, the call is to be answered the Loudspeaker and the key lock must be released manually.

Mode of Operation

Logic Terms

Low voltage (~ 0 V) = logic state '0'.

High voltage ($\sim > 7$ V) = logic state '1'.

(refer to block diagram).

5-tone Individual Call Signalling

The first tone of a sequential tone signal passes through the input stage and limiter, which provide the frequency response, level, and impedance transformation, and becomes suitable for applying to the resonant circuit and Q-multiplier.

In stand by the Q-multiplier is tuned, via gate "a" to the first of its code. If the first tone corresponds to the circuit resonant frequency, it be-

comes selected and rectified by the Individual Call Detector.

The detector output is, in stand by, approx. 9 V, i. e. logic '1'. A received tone causes the detector output to become 0 V, i. e. logic '0'.

The clock delay circuit is activated via the OR-gate and after the elapse of 20 ms the voltage on the counter's clock input goes logic '0'. Simultaneous the clear delay circuit is activated.

In stand by the counter's clear input is logic '1', and the counter is inhibited.

Activating the clear circuit causes the voltage to go logic '0', delay approx. 7 ms, and the counter inhibit disappears. This condition remains unchanged as long as the detector receives a signal. When the 1st tone ends, the detector output voltage goes logic '1'. Also the counter input (delay approx. 3 ms) changes and the counter steps one position forward and, via an inverter and gate b, tunes the circuit to the second tone.

The 2nd, 3rd, 4th, and 5th tones of a sequence occur like the 1st, each time stepping the counter one position forward until the final tone disappears.

At the end of the 5th tone the counter steps to position 6 and an output signal is applied to both inputs on the Read Out circuit (AA and BB) via the logic part of the circuit. This releases the individual call functions.

The clear input of the counter remains logic '0', but 150 ms after the last tone of the sequence the clear delay output goes logic '1' and the counter is reset to stand by position, i. e. ready to receive the 1st tone again. If one tone of the sequence is lacking, or the frequency does not correspond to the code to which the tone receiver is set, the clear input likewise goes to logic '1', and 150 ms after the last of the correctly received tones the receiver is set to receive the first tone of a new call.

Group Call

A group call takes place just as described for individual calling, as the resonant circuit, Q-mul-

tiplier, and detector circuits are identical. When the counter is in position 4 (in the case of a 5 digit call with 2 group digits) and gate d sets the individual tone coil via gate f. Likewise, the 5th tone and the 2nd group tone is selected by gates e and g, respectively. The two output circuits are joined in the OR-gate.

The call will proceed through, regardless of the tones being the frequencies of an individual call or group call. The logic circuits alone decide the type of call and apply the output of the counter to the Read Out circuit.

Signals on both inputs, AA and BB, give the functions of an individual call, and signal on BB alone gives a group call.

Logic Circuit

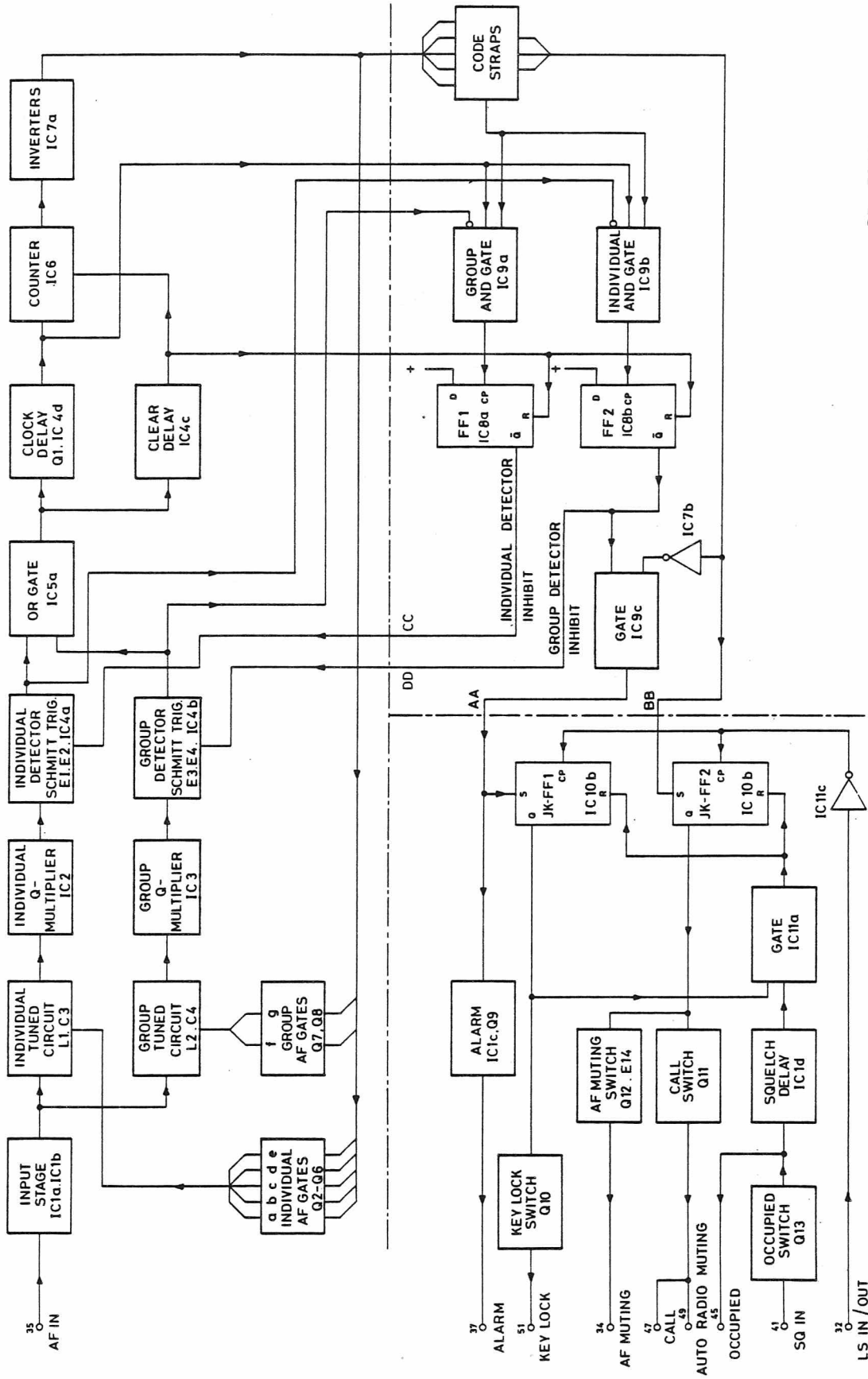
The logic circuit has two functions. It controls the signals as they proceed through the two signal channels, the individual call channel and the group call channel, and it controls the output pulse from the counter to the Read Out Circuit in order to release the proper functions.

The individual call detector and the group call detector may be inhibited by the logic circuit.

The first 3 tones of a 5-tone signal take place just as described. Now the tone receiver is ready for the 4th tone of the individual call and the 1st tone of the group tones.

If the last two tones have the same frequencies as the 4th and 5th tone of the individual code, the result will be a normal individual call, and the group tone detector is inhibited as soon as the 4th tone is accepted (after 20 ms). However, if they have the group call frequencies, the individual tone detector is inhibited when the tone is accepted.

When the 5th tone appears, only one circuit is functioning and hence a group call is recognized only if the 4th tone is a group call. The call will not be transferred to the output circuit before also the 5th tone is accepted and the counter has stepped to its 6th position.



SR 7841a

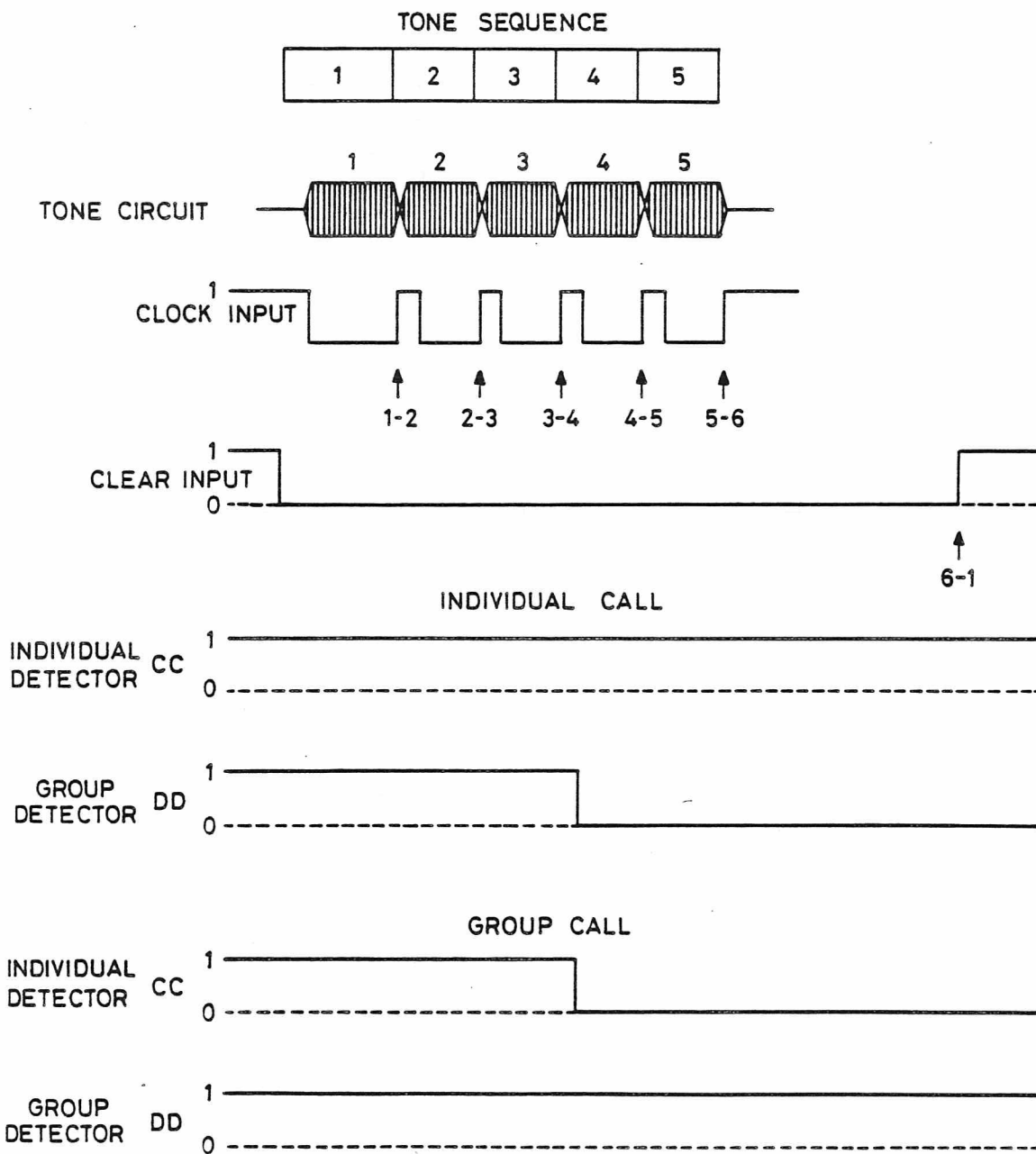
Controlling the Counter Output

When all 5 tones are correctly received the counter produces an output (output 6 is logic '1'). This condition occurs regardless of the call being individual or group.

If the 4th tone is received by the group circuit it toggles D flip-flop 1; if it is an individual tone D flip-flop 2 is toggled. The output pulse

from the counter is applied directly to BB, but to AA it passes through gate 9a which is controlled by the \bar{Q} output of D flip-flop DFF2. For an individual call the \bar{Q} is logic '0' and the gate is open applying the signal to both the AA and BB outputs.

For a group call \bar{Q} is logic '1' which inhibits the gate and the signal is applied to BB only.



TIMING DIAGRAM

SR 7841a

The amplifier output is applied to the detector and a portion of the signal is reapplied in phase to the feed-back winding via compensating networks, R11 - R12 - R13 (R15 - R16 - R17), thereby increasing the circuit Q. This configuration enables a relatively small coil form to be used without loss of temperature stability and deterioration of circuit Q.

To offset the effect of temperature upon the signal level an NTC resistor is inserted in the compensation network.

Detectors

The detector includes the rectifiers E1 - E2 (E3 - E4) and the Schmitt trigger IC4a (IC4b). The trigger level is set by the bias difference between the inverting and non-inverting inputs of IC4a (IC4b) and the hysteresis by resistor R32 (R37).

The trigger level is adjusted to be approx. 6 dB below the point of full limiting by selection of R7 (R8), and thus differences in trigger levels and amplification can be equalized. This adjustment does not influence on the sensitivity which is not adjustable, as minor variations are not important.

NOR Circuit

Joining the detector output signals for individual call and group call is by means of a NOR gate, IC5a. A tone signal produces a positive voltage (logic '1') at the detector output. An output signal from one detector only, applied to the NOR gate, causes the output to be logic '0'. The detector output signals are applied to the logic circuit, too.

Clock Delay

The Clock Delay Circuit includes Q1 and IC4d. When the IC5a NOR output goes logic '0' transistor Q1 cuts off and C14, which in stand by has charged to 9 V, begins discharging through R46-R47, the time constant being 29.7 ms.

IC4d is controlled by the voltage of C14 and the output goes logic '0' after approx. 22 ms. When

the signal disappears and the NOR gate goes logic '1', Q1 goes ON and C14 charges via R47 with a time constant of 3.3 ms. IC4d changes state to logic '1' and the counter is toggled at the positive edge. If the signal disappears before the elapse of the 22 ms, IC4d has not changed to logic '0', and hence the counter is not toggled. This prevents the counter from being toggled by noise pulses.

Clear Delay

The Clear Delay circuit includes E5, IC4c, and their associated components.

In stand by diode E5 is reverse biased and C13 charged to 9 V. The IC4c output is logic '1' and the counter reset to position 1 and cannot be toggled.

When the NOR gate, IC5a, goes logic '0' diode E5 conducts and C13 discharge via R42. The time constant is 7 ms which is less than the clock delay (22 ms). IC4c changes state, logic '1' to logic '0', and the counter is now ready to count.

When the signal disappears the NOR gate, IC5a, reverts to logic '1', diode E5 is reverse biased, and C13 charges to 9 V via R41-R42 the time constant being 190 ms. When the charge building up eventually overcomes the reference voltage, 4.5 V, IC4c goes logic '1' (approx. 150 ms) whereby the counter is reset to position 1 (stand by). Since the intervals between tones are only few milliseconds, the resetting to stand by first takes place when all tones contained in the signal have passed or if one of the tones fails to match the code.

Counter

The counter, IC6, is a 8 bit Johnson Counter toggled at the positive edge of the clock pulse and reset by applying a logic '1' to the reset input. Both the clock input and the reset input may be isolated by removing straps on the printed wiring board in order to control the counter manually during service and fault tracing.

4-tone Signals, or One Group Digit

If the signal code contains 4 tones the counter is strapped to produce the output signal in the 5th position. If two group digits are used, the 3rd tone becomes the first group tone, and the logic control circuit is strapped to enable the counter's 3rd position to control gates 9 a and 9 b.

Using 5 tones and 1 group digit the gates are controlled by the 5th position of the counter.

Using 4 tones and 1 group digit the gates are controlled by the 4th position of the counter.

(refer to the diagram for strapping combinations.)

Read Out Functions

The Read Out functions are controlled by two J - K flip-flops, FF1 and FF2, of which the FF1 controls the Key Lock function and the FF2 the Call Lamp and the AF Muting.

The FF1 is preset via the AA input, the FF2 via the BB input. The LS IN/OUT terminal toggles both flip-flops via the clock input, and the FF1 J - K inputs are controlled by FF2 in order to be complementary when toggled via the clock input (refer to truth table).

The AA input also controls the Alarm Delay Circuit, which produces an alarm signal for approx. 1 sec. after the AA input changes from logic '0' to logic '1'.

The Squelch In voltage (terminal 41) controls, partly the Occupied Lamp via a transistor, partly a delay circuit which resets FF1 and FF2 approx. 300 ms after the Occupied Lamp turns off. This resetting of FF1 and FF2 takes place via a gate,

IC11a, which is controlled by FF1. The reset will only be effective when the FF1 is off (Q = 1), i. e. after a group call.

When turning the equipment on it must be ensured that the alarm function is not activated and that the flip-flops remain in the reset position. A transistor, Q14, short circuits the alarm and reset circuits when the supply voltage is applied. After charging of a capacitor the transistor turns off.

Circuit Description

The input circuit includes an RC-circuit (R2-C1) to offset the de-emphasis of the sequential tone generator, a preamplifier, IC1a, and a limiter stage, IC1b.

The nominal input level is -17 dBm, but the desired sensitivity is -27 dBm. The preamplifier is necessary in order to achieve this, but strong feed-back is introduced to avoid overload at levels lower than specified.





A series resistor, R4, between the preamplifier and the limiter determines the sensitivity.

The output is applied to the selective circuits via series resistors.

Resonant Circuits and Q-multipliers

The selective circuits involve coils and capacitors, 47 nF, to which the signals and the feed-back are applied by means of separate windings.

The top of the L - C circuit is coupled to the amplifier, IC2 (IC3), via an RC circuit, R14-C5 (R18 - C6).

Clock	Q _{2m}	Q _{2m+1}	J ₁	K ₁	Q _{1m}	Q _{1m+1}
	0	1	1	0	0	1
	1	0	0	1	0	0
	0	1	1	0	1	1
	1	0	0	1	1	0

Inverters and AF Gate Transistors

The AF gates connect to the counter, IC6, via inverters. When a transistor base is driven logic '0' by an inverter, that transistor will conduct and ground the coil terminal. The PNP transistors have their collectors connected to the tone coil terminals and their emitters to a +1.5 V d. c. voltage, which is a. c. bypassed to chassis ground.

As the counter produces a positive voltage (logic '1'), and the transistors turn on for logic '0', inverters are inserted. They also function as buffer circuits in order to provide adequate drive for the transistor.

Resistor R78 prevents high voltage transients across L2 when the first group tone is selected.

Logic Circuit

The Logic Circuit includes two D flip-flops, IC8a and IC8b, two NOR gates, IC9a and IC9b, and three inverters, IC5a, IC5b, and IC7b.

The D flip-flop IC8a is toggled by the IC9a output which is logic '1' when the group detector output is logic '1', the clock pulse output is logic '0', and the counter output 4 is logic '1'.

As the D input of IC8a connects to $+V_B$ the Q output stays logic '1' after the flip-flop has been toggled. Likewise, D flip-flop IC8b is toggled by the individual detector, the clock pulse output, and the counter's 4th output.

Whenever the IC8a flip-flop is toggled the individual detector is inhibited as the voltage at the Schmitt trigger's non-inverting (+) input goes logic '0'.

If IC8b is toggled the Q output goes logic '0', and NOR gate IC9c will apply logic '1' to the AA when the BB goes logic '1'; the BB signal is applied to the IC9a NOR gate via an inverter.

Alarm Circuit

The Alarm Circuit includes IC1c, Q9, and their associated components.

The output voltage of the logic circuit (AA = logic '1') charges C17 in 150 ms. This causes the output of IC1c to go logic '1' and this positive voltage is applied to the input via R55. When the voltage charging C17 disappears, the capacitor begins discharging through R58; the time constant is 846 ms. When the capacitor voltage has decreased to below trigger level the circuit reverts to stand by. Logic '1' at the IC1c output drives Q9 ON and grounds terminal 37.

Squelch Delay

Whenever the RF channel is occupied the receiver squelch feeds a positive voltage to terminal 41. This voltage turns Q13 ON, grounding the Occupied Lamp through terminal 45. Q13 also causes E11 to conduct and C18 to discharge through E11-Q13, and thus the Schmitt trigger output, IC1d, goes logic '0'.

When the RF carrier disappears Q13 turns off, and E11 is no longer conducting. Now C18 is allowed to charge through 180 k Ω ; time constant 390 ms. At the Schmitt trigger threshold the output voltage goes logic '1', and a positive pulse is fed, via C20, gate IC11a and inverter IC11b to the flip-flop reset inputs.

Flip-flop Trigger Circuit

As IC10a and IC11b trigger on a positive edge IC11c is inserted to invert the LS IN/OUT function. The IC11c input connect to $+V_B$ through R72 causing the clock inputs on IC10a and IC11b to be logic '0' in stand by. Grounding the LS IN/OUT, terminal 32, via R73 and bypass capacitor C19, triggers the flip-flops. C19 protects the input against transients and prevents malfunction due to contact bouncing. The R-C values, 100 Ω - 0.1 μ F, are optimum with respect to the pulse rise time.

Start Circuit

When battery voltage is initially applied C21 charges and transistor Q14 opens momentarily. Via diodes

E13 and E14 the Alarm Delay is inhibited, and the flip-flops, IC10a - IC10b, are reset via inverter IC11b. As the charging of C21 proceeds (time constant approx. 1 sec.) the voltage at Q14's base decreases and eventually Q14 turns off. When turning the equipment off, C21 discharges via diode E12 giving a very short delay time. This makes the circuit passive for repeated operations of the on/off switch.

Read Out Circuits

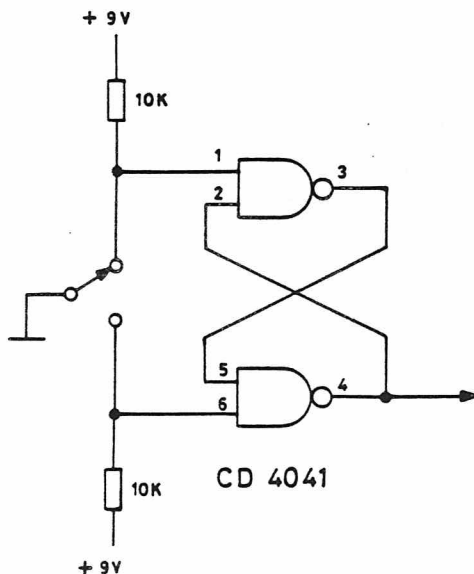
The Key Lock function is controlled by the output of IC10a and Q10, the Call Lamp by the output of IC10b and Q11, and the AF Muting by Q12. Terminal 49 is provided for automatic muting of the vehicle's broadcast band radio, and requires an auxiliary relay.

Voltage Regulator

The digital Cosmos circuits requires an internal supply voltage which is 9 V. The low current drain, 30 mA maximum, enables a simple voltage regulation circuit to be used (Q15 - E15).

Fault Tracing

To ease fault tracing the counter's clock and clear inputs, pin 14 and 15, may be isolated from the detectors when removing two straps on the printed circuit board. The counter may now be controlled by two auxiliary switches



with antibounce circuits, see diagram, enabling proper switching of tones, test of the selective circuits, and the detector functions to be checked. Likewise, the inhibiting voltages to the detector circuits may be removed from IC8, pin 2 and pin 12, and connected to +V_B (= logic '1'). Disabling the detector inhibit circuit will ease checking of the circuits in case of faults in the logic system.

Before initiating a systematic fault finding procedure the tone receiver is inspected for correct tone frequencies and setting of the code.

If the fault is not obviously located to one part of the circuit, most of the circuits on the lower printed board can be tested by applying pulses to AA and BB using a switch circuit as shown in the diagram.

The detector circuits and the logic circuits are tested by applying an input and tracing the signal through the channels to BB. If a static receiver test applying one tone at the time shows no fault, and the signal levels are correct, but the receiver refuses to accept a call, the Clock Delay circuit and the Clear Delay circuit must be investigated.

A tone signalling generator, Storno type TS-G13 and a storage oscilloscope will facilitate tests and fault tracing.

SPECIFICATIONS

Supply Voltage

Nominal:	13.6 V
Minimum:	10.5 V
Maximum:	16.0 V

Current Drain

Stand by: 25 mA ± 5 mA

Temperature Range

Operating range	: -25°C to +60°C
Functioning range	: -30°C to +80°C

Input Impedance

> 6 kΩ asymmetrical

Signal Input Level

Nominal at 1000 Hz : 110 mV r.m.s. (~ -17 dBm).

Equalization

Deemphasis (by RC function) $f_c = 1000$ Hz.

Signalling Code

Sequence of 4 or 5 tone bursts of 70 ms \pm 15 ms duration with maximum 15 ms interval between tone bursts.

Frequency Accuracy

Coil tuned to 1060 Hz: $\leq 0.4\%$

Frequency Stability

(typically $\leq 0.5\%$) $\leq 1\%$

Selectivity

Frequencies differing from f_o by 4.5% or more are unable to trigger the tone receiver.

Tone Signal Frequencies

<u>Coil terminal</u>	<u>Tone frequency</u>
1	(885) do not comply with specifications
2	970
3	1060
4	1160
5	1270
6	1400
7	1530
8	1670
9	1830
10	2000
11	2200
12	2400
13	2600
14	2800
15	(2900) do not comply with specifications

Maximum Load Currents

Terminal 37	ALARM	100 mA (for 1 sec.)
Terminal 47	CALL	100 mA
Terminal 45	OCCUPIED	100 mA
Terminal 51 and 43	KEY LOCK	10 mA
Terminal 34	AF MUTING	I_{load} min. 0.75 mA for $V_{OUT} = 8$ V.

Maximum Sensitivity

-27 dBm

Clear Down Delay (after group call)

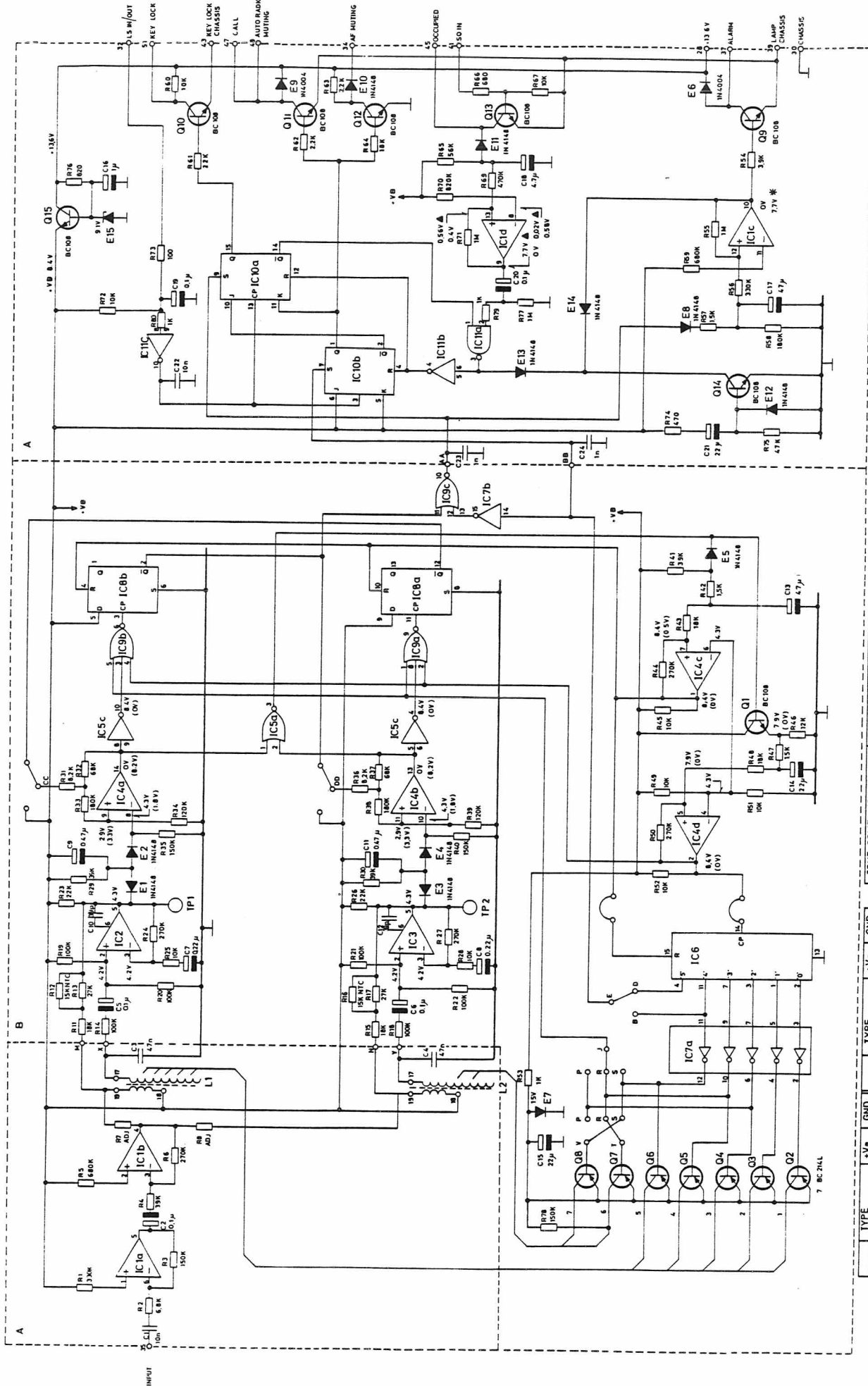
approx. 300 ms.

Failure Rate for 3 dB SINAD

$< 10^{-3}$

AF Muting

In conjunction with terminal 18 of CF701: ≥ 60 dB

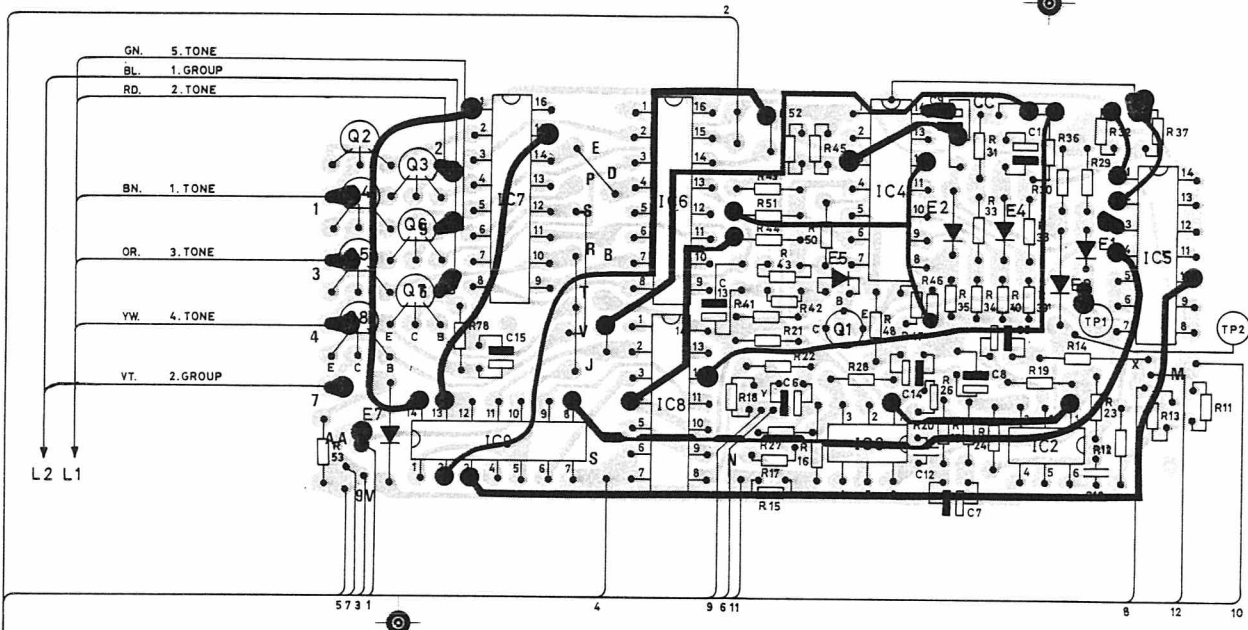


VOLTAGE WITHIN () MEASURED WITH SIGNAL APPLIED.
 VOLTAGE MARKED # MEASURED WITH ALARM SIGNAL.
 VOLTAGE MARKED ▲ MEASURED WITH THE RECEIVER SQUELCHED.

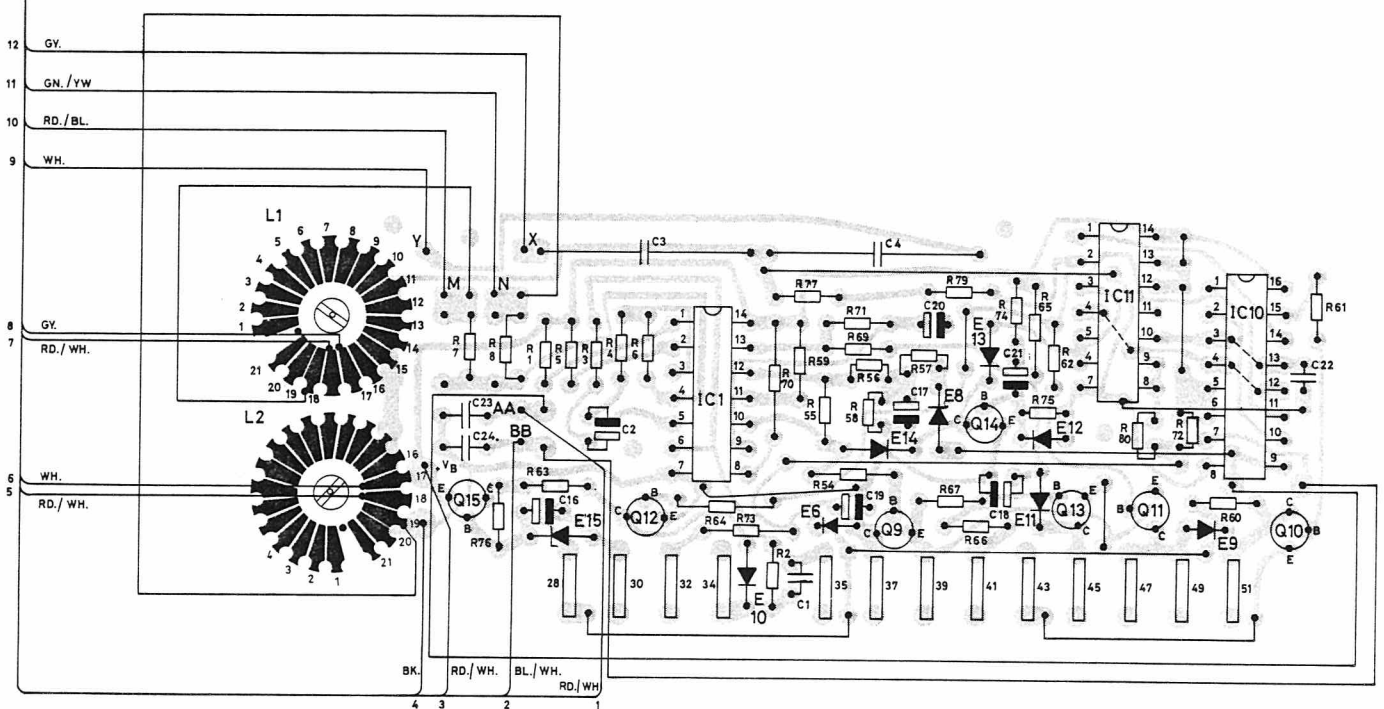
TONE COMBINATIONS		CONNECTIONS	
5 INDIVIDUAL	2 GROUP	E-D	J-R
5	1	E-D	R-T
4	2	E-D	J-S
4	1	E-B	J-P
4	1	E-B	J-R

IC1	TYPE	+Vb	GND	+Vb	GND
IC1	LM 2300	14	7	14	8
IC2	TAA 865A	1	4	14	7
IC3	TAA 865A	1	4	14	7
IC4	MC 3302	3	12	16	8
IC5	CD 4001	14	7	14	7
IC6	CD 4022	16	8	14	7

SEQUENTIAL TONE RECEIVER
 SR 7841a



PRINTED CIRCUITS VIEWED FROM COMPONENT SIDE.



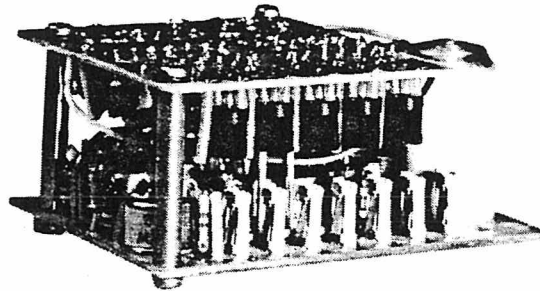
TYPE	NO.	CODE	DATA
SR7841a		19. 2456-01	Sequential Tone Receiver
	C1	76. 5070	10 nF 10% polyester FL 50V
	C2	73. 5089	0.1 μF 20% tantal
	C3	76. 5123	47 nF 2.5% polystyr
	C4	76. 5123	47 nF 2.5% polystyr
	C5	73. 5089	0.1 μF 20% tantal
	C6	73. 5089	0.1 μF 20% tantal
	C7	73. 5118	0.22 μF 20% tantal
	C8	73. 5118	0.22 μF 20% tantal
	C9	73. 5125	0.47 μF 20% tantal
	C10	74. 5316	39 pF 5% PL
	C11	73. 5125	0.47 μF 20% tantal
	C12	74. 5316	39 pF 5% PL
	C13	73. 5126	4.7 μF 20% tantal
	C14	73. 5102	2.2 μF 20% tantal
	C15	73. 5127	22 μF 20% tantal
	C16	73. 5114	1 μF 20% tantal
	C17	73. 5126	4.7 μF 20% tantal
	C18	73. 5126	4.7 μF 20% tantal
	C19	73. 5089	0.1 μF 20% tantal
	C20	73. 5089	0.1 μF 20% tantal
	C21	73. 5127	22 μF 20% tantal
	C22	76. 5070	10 nF 10% polyester FL 50V
	C23	74. 5155	1 nF -20% +80% PL 63V
	C24	74. 5155	1 nF -20% +80% PL 63V
	R1	80. 5079	330KΩ 5% carbon film 0.1W
	R2	80. 5079	6.8KΩ 5% " " 0.1W
	R3	80. 5075	150KΩ 5% " " 0.1W
	R4	80. 5068	39KΩ 5% " " 0.1W
	R5	80. 5083	680KΩ 5% " " 0.1W
	R6	80. 5078	270KΩ 5% " " 0.1W
	R7	80. 50xx	Adjusted 33KΩ - 68KΩ 0.1W
	R8	80. 50xx	Adjusted 33KΩ - 68KΩ 0.1W
	R9		Not used
	R10		Not used
	R11	80. 5064	18KΩ 5% carbon film 0.1W
	R12	89. 5010	15KΩ 20% NTC 0.6W
	R13	80. 5066	27KΩ 5% carbon film 0.1W
	R14	80. 5073	100KΩ 5% " " 0.1W
	R15	80. 5064	18KΩ 5% " " 0.1W
	R16	89. 5010	15KΩ 20% NTC 0.6W
	R17	80. 5066	27KΩ 5% carbon film 0.1W
	R18	80. 5073	100KΩ 5% " " 0.1W
	R19	80. 5073	100KΩ 5% " " 0.1W
	R20	80. 5073	100KΩ 5% " " 0.1W
	R21	80. 5073	100KΩ 5% " " 0.1W
	R22	80. 5073	100KΩ 5% " " 0.1W

TYPE	NO.	CODE	DATA
	R23	80. 5065	22KΩ 5% carbon film 0.1W
	R24	80. 5078	270KΩ 5% " " 0.1W
	R25	80. 5061	10KΩ 5% " " 0.1W
	R26	80. 5065	22KΩ 5% " " 0.1W
	R27	80. 5078	270KΩ 5% " " 0.1W
	R28	80. 5061	10KΩ 5% " " 0.1W
	R29	80. 5068	39KΩ 5% " " 0.1W
	R30	80. 5068	39KΩ 5% " " 0.1W
	R31	80. 5060	8.2KΩ 5% " " 0.1W
	R32	80. 5071	68KΩ 5% " " 0.1W
	R33	80. 5076	180KΩ 5% " " 0.1W
	R34	80. 5074	120KΩ 5% " " 0.1W
	R35	80. 5075	150KΩ 5% " " 0.1W
	R36	80. 5060	8.2KΩ 5% " " 0.1W
	R37	80. 5071	68KΩ 5% " " 0.1W
	R38	80. 5076	180KΩ 5% " " 0.1W
	R39	80. 5074	120KΩ 5% " " 0.1W
	R40	80. 5075	150KΩ 5% " " 0.1W
	R41	80. 5068	39KΩ 5% " " 0.1W
	R42	80. 5051	1.5KΩ 5% " " 0.1W
	R43	80. 5064	18KΩ 5% " " 0.1W
	R44	80. 5078	270KΩ 5% " " 0.1W
	R45	80. 5061	10KΩ 5% " " 0.1W
	R46	80. 5062	12KΩ 5% " " 0.1W
	R47	80. 5051	1.5KΩ 5% " " 0.1W
	R48	80. 5064	18KΩ 5% " " 0.1W
	R49	80. 5061	10KΩ 5% " " 0.1W
	R50	80. 5078	270KΩ 5% " " 0.1W
	R51	80. 5061	10KΩ 5% " " 0.1W
	R52	80. 5061	10KΩ 5% " " 0.1W
	R53	80. 5049	1KΩ 5% " " 0.1W
	R54	80. 5056	3.9KΩ 5% " " 0.1W
	R55	80. 5085	1MΩ 5% " " 0.1W
	R56	80. 5079	330KΩ 5% " " 0.1W
	R57	80. 5051	1.5KΩ 5% " " 0.1W
	R58	80. 5076	180KΩ 5% " " 0.1W
	R59	80. 5083	680KΩ 5% " " 0.1W
	R60	80. 5061	10KΩ 5% " " 0.1W
	R61	80. 5053	2.2KΩ 5% " " 0.1W
	R62	80. 5053	2.2KΩ 5% " " 0.1W
	R63	80. 5053	2.2KΩ 5% " " 0.1W
	R64	80. 5064	18KΩ 5% " " 0.1W

SEQUENTIAL TONE RECEIVER SR7841a

X402.184

SEQUENTIAL TONE TRANSMITTER ST7845

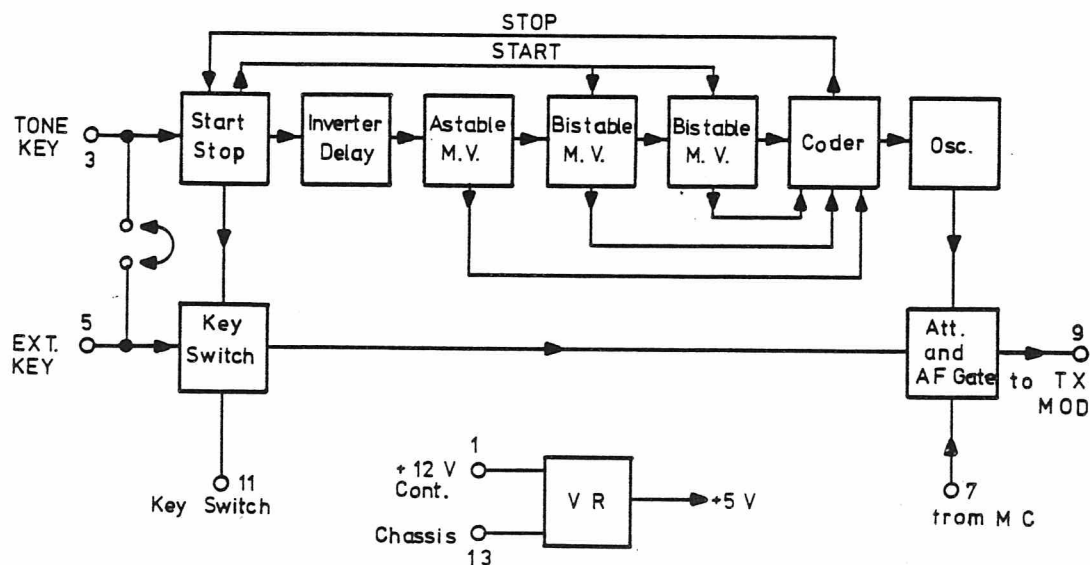


Description

General

ST7845 is a sequential tone transmitter developed for the Stornophone 700 series radiotelephones. ST7845 generates a five (or four) tone sequence code. When the Tone Key button is depressed ST7845 generates seven consecutive pulses, each of 70 msec. duration. The first two (or three) pulses are unmodulated and the last five (or four) pulses are modulated by the tone oscillator.

An AF Gate blocks the voice modulation during the tone sequence and the transmitter is keyed through the Key Switch. After generating all seven pulses of the sequence, approximately 490 msec., the transmission stops, even if the tone key button remains depressed. This is because the start signal is a short-duration, capacitively coupled pulse that is relatively independent of how long the tone key button is held down, and gives only one start pulse for each time the tone key is activated.



Start - Stop Circuit (Q1, Q2) and Key Switch (Q18)

The Start - Stop Circuit is an RS flip-flop consisting of Q1 and Q2. In stand by Q1 is ON and Q2 is OFF. Operating the Tone Key grounds terminal 3, causing a negative pulse through E1, C1, and E2 to turn Q1 OFF. The RS flip-flop then switches state.

Several things now happen. First, when the collector of Q1 goes HI, the positive potential (logic state 1') enables the two flip-flops, IC1a and IC1b.

The HI potential also turns Q17 and Q18 ON. Q18, the Key Switch, establishes a connection between terminals 5 and 11, causing the RX - TX Switch in the CQM700 to switch to the TX, or transmit condition.

Q17 drives the AF Gate, Q16. When Q17 is turned ON the HI potential through R39, which forward biases Q16, disappears through E9 and Q17 so Q16 becomes cut off. Thus, during the transmission of the tone sequence, no signal from the microphone amplifier can reach the modulator to interfere.

At the end of a tone sequence, $\bar{2}$, $\bar{3}$, and $\bar{4}$ all go logical 1' and the output of IC2_b will go 0'. The negative going pulse, applied to the base of Q2 via C6 and E3, turns the transistor OFF. The Start - Stop flip-flop then returns to its stand by position until another start pulse arrives from terminal 3.

Inverter (Delay) Circuit (Q3)

In stand by Q3 is held ON by the HI potential at the collector of Q2, via R9 and E4. The standard version of ST7845 does not incorporate a delay here, but upon request C2 can be added. C2 and R10 can be arranged to introduce a time delay of from 0.1 sec. to 1.5 sec. before the first tone is transmitted.

In this case, R10 must not be less than 10 k Ω nor C2 greater than 47 μ F.

Astable Multivibrator (Q4, Q5)

This Multivibrator generates square wave pulses having a repetition rate of approximately 140 msec. to produce the 70 msec. output pulses mentioned in the General section at the beginning of this description.

In standby the LO potential at the collector of Q3 holds Q4 OFF, via E5. Q5 will be ON.

When the tone sequence starts, Q3 switches OFF and E5 becomes reverse biased. C5 then begins to charge toward +V_{cc}, switching Q4 ON. C4 discharges through Q4, driving Q5 OFF. Cutoff time for Q5 is determined by the time constant of R13 // R14 and C4. Likewise, cutoff time for Q4 is determined by R15 // R16 and C5. The regenerative action of the multivibrator generates square wave pulses which are taken off from the collector of Q5 and applied to the first bistable multivibrator, IC1_a.

The resistances of R13 and R16 are chosen to adjust the two pulse lengths to 70 msec. each. Resistor values can be from 33k Ω to 100k Ω .

Bistable Multivibrators (IC1_a, IC1_b)

These two Multivibrators are identical, J-K master-slave flip-flops packaged in the same DIP. With the J-K inputs tied to logical 1' via R18, their outputs will switch state for every clock pulse.

The square wave output from the collector of Q5 toggles the first flip-flop, IC1_a, and the normal (Q) output of IC1_a toggles IC1_b. The square wave repetition rate (frequency) is divided by two in each flip-flop stage.

Coder (Q6 - Q10 and IC2, IC3)

IC2 and IC3 are two DIP's, each containing three triple-input NAND gates. Five of these NAND gates drive the 5 transistor gates, Q6 to Q10. When all three inputs of a NAND gate are HI, the output goes LO, driving its associated transistor ON, enabling the tone oscillator to operate.

The transistor gates switch in the selected oscillator coil taps in the following sequence :

tone A	tone B	tone C	tone D	tone E
Q9 ON	Q6 ON	Q10 ON	Q7 ON	Q8 ON

For 4-tone signalling, the green lead from the collector of Q8 to the tone coil will not be soldered to the coil terminal at all.

If any one of the inputs to a NAND gate is LO, the output will be HI and its transistor gate will be held at cutoff.

Oscillator (Q11, Q12)

Q11 and Q12 operate as a differential amplifier in a Hartley oscillator configuration. Using a differential amplifier ensures ample feedback at all frequencies.

Attenuator (Q13, Q14)

Q13 adjusts (attenuates) the oscillator signal to the required level, while emitter follower Q14 matches the low input impedance of the modulator circuit in the CQM700.

R36 and C9 in the collector of Q13 provide the desired frequency response (6 dB de-emphasis pr. octave, $f_c = 1000$ Hz). R34 in the emitter adjusts the output level.

AF Gate (Q16, Q17)

In stand by Q16 is forward biased by the HI potential through R39, and the microphone amplifier from terminal 7 is thus connected through to the modulator at terminal 9.

When the start pulse drives Q1 OFF, the HI potential from Q1's collector drives Q17 ON and the HI potential through R39 disappears through E9 and Q17 to ground. This switches Q16 OFF and any microphone signal will be isolated from the modulator as long as the tone code is being transmitted.

The tone sequence is applied to the modulator circuit via terminal 9.

Voltage Regulator (E7, Q15)

The Voltage Regulator is designed to keep the V_{CC} at $+5$ V $\pm 5\%$ for all battery voltages from $+10.5$ V to $+16$ V.

SEQUENTIAL TONE TRANSMITTER ST7845

Technical Specification

Tone Frequencies

970, 1060, 1160, 1270, 1400, 1530, 1670,
1830, 2000, 2200, 2400, 2600, 2800 Hz.

Pulse Sequences

4-tone sequence 3 pulses (unmodulated),
70 m sec. \pm 15 m sec. each.
4 pulses (modulated),
70 m sec. \pm 15 m sec.

5-tone sequence 2 pulses (unmodulated),
70 m sec. \pm 15 m sec. each.
5 pulses (modulated),
70 m sec. \pm 15 m sec.

Frequency Stability

$\leq 1\%$

Frequency Accuracy

$\leq 0.5\%$

Frequency Response

6 dB pr. octave de-emphasis
 $f_c = 1000$ Hz

Output Impedance

$600 \Omega \pm 20\%$

Output Level (at 1000 Hz)

-17 dBm $\pm 1/-0$ dB

Distortion (tone modulation)

$\leq 3\%$

AF Gate Attenuation

≥ 50 dB

Distortion (voice modulation)

$\leq 5\%$

Power Supply

minimum: 10.5 V

maximum: 16 V

nominal: 13.6 V

Current Consumption

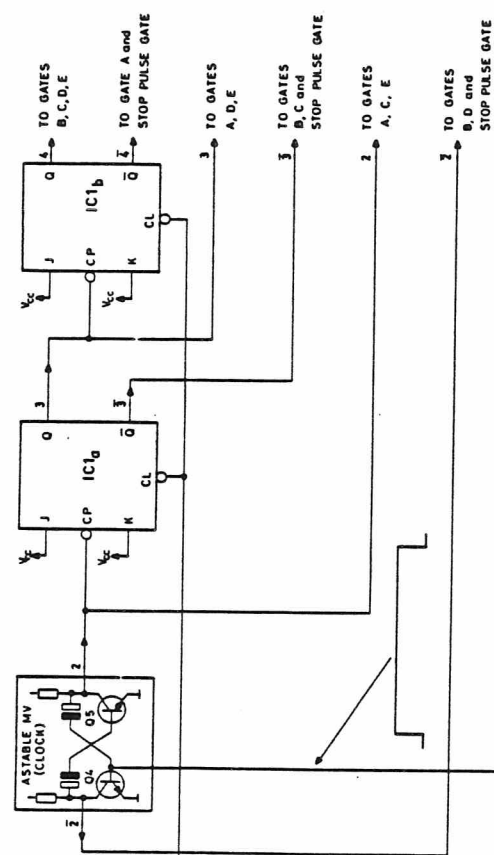
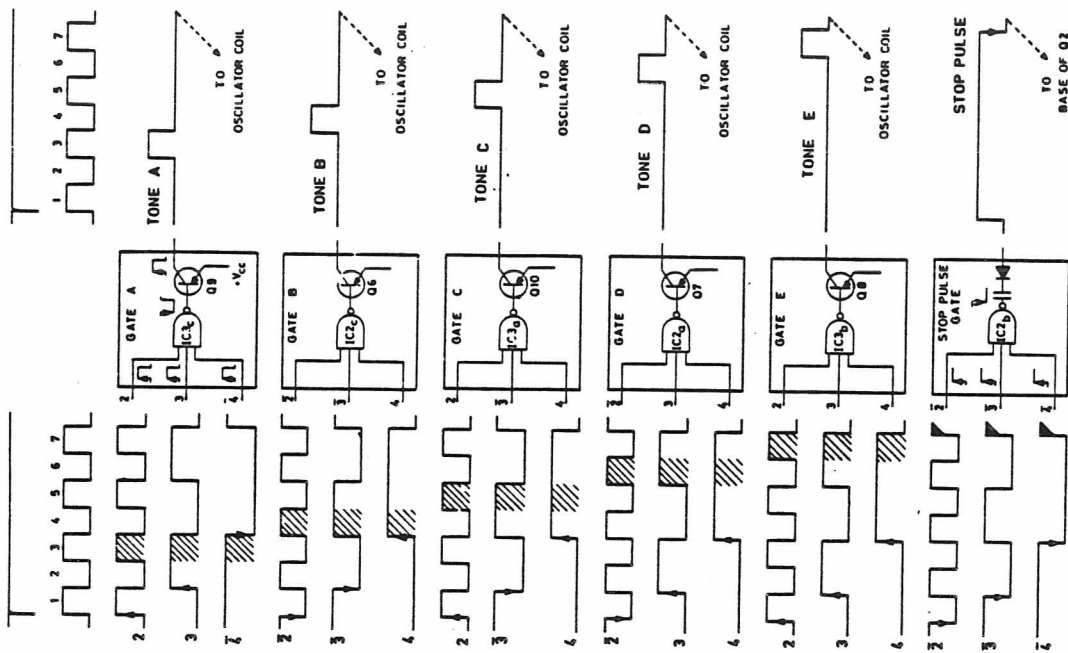
Stand by: 32 - 44 mA

Activated: 42 - 54 mA

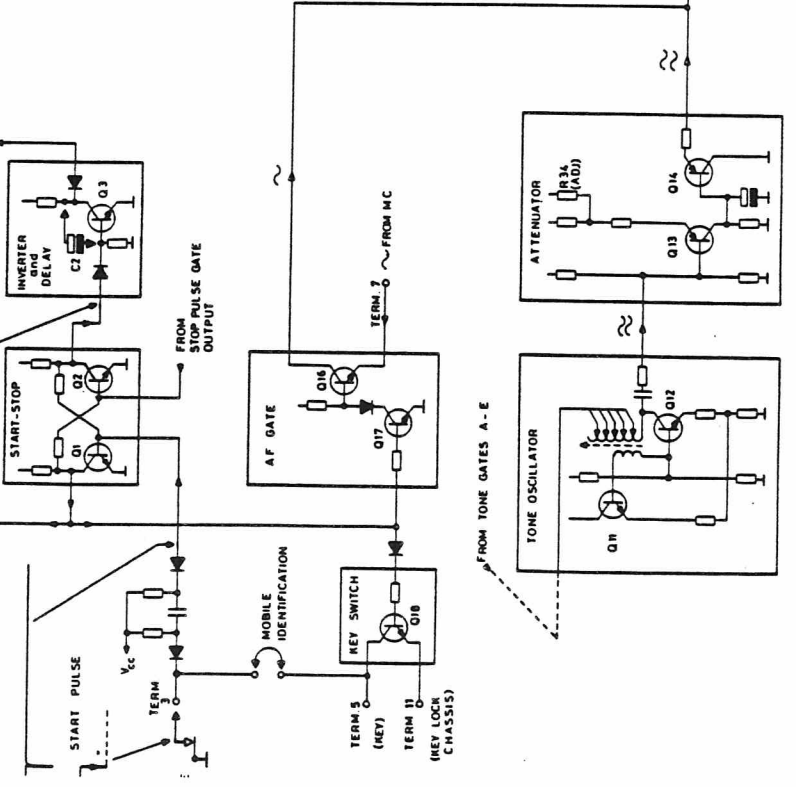
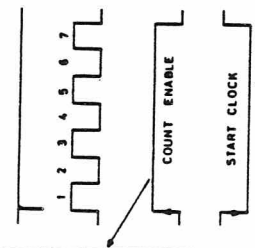
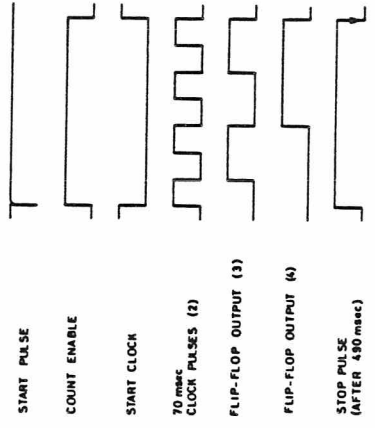
Temperature Range

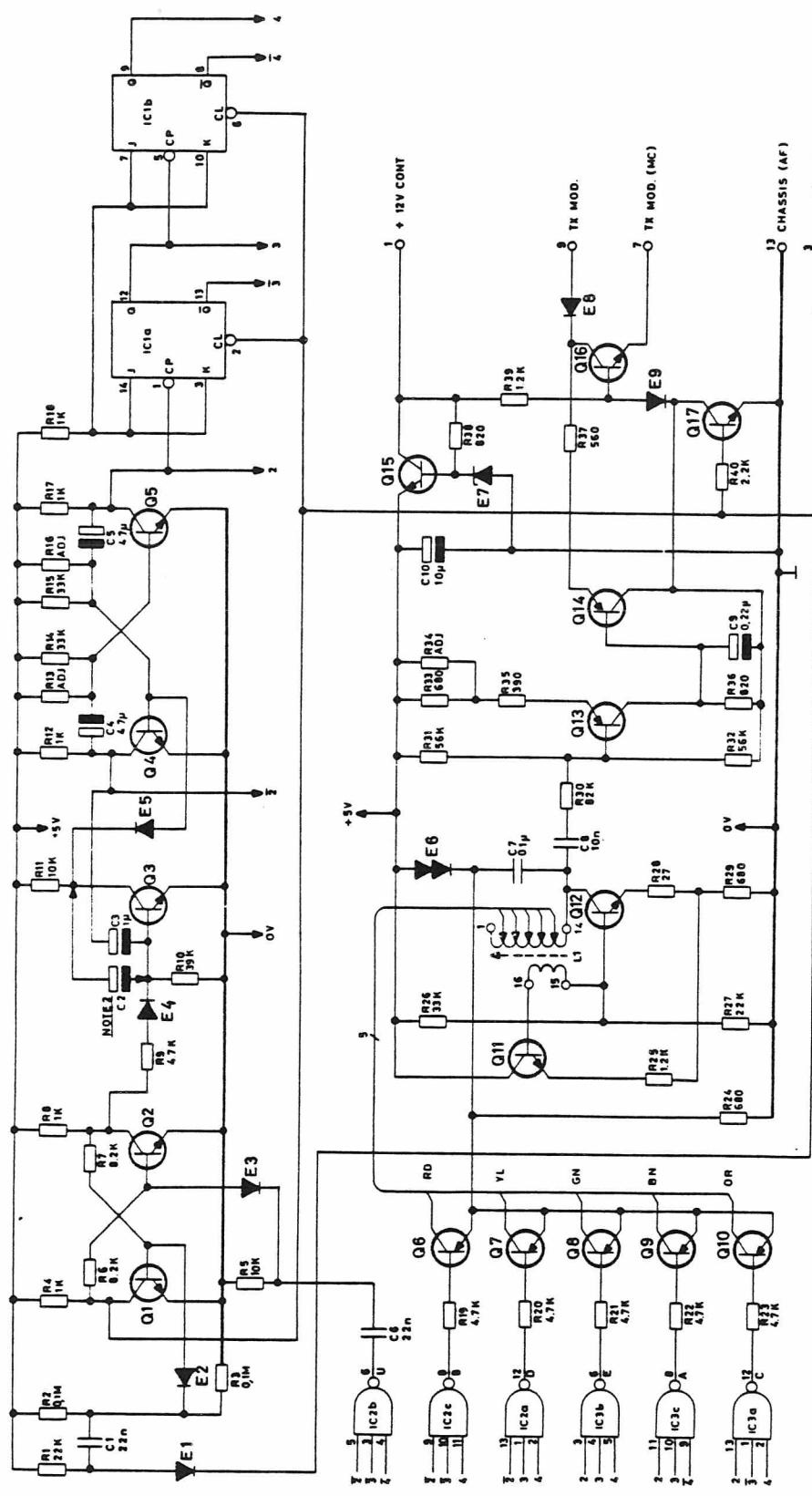
Operating range: -25° - $+60^{\circ}$ C

Functioning range: -30° - $+80^{\circ}$ C



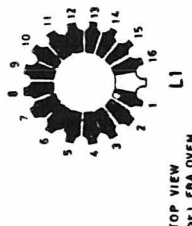
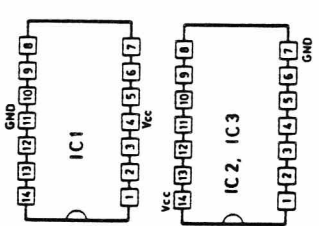
LOGIC SEQUENCE



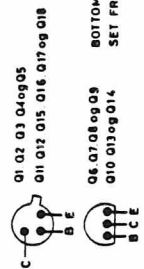


NOTE: INSERT C2 FOR DELAY
 R 10 MIN. 10K
 C2 MAX 47µ
 DELAY TIME 0.1 - 1.5 SEC.

TERM.	FREQ.	DIGIT
1	970 Hz	1
2	1060 -	1
3	1160 -	2
4	1270 -	3
5	1400 -	4
6	1530 -	5
7	1670 -	6
8	1830 -	7
9	2000 -	8
10	2200 -	9
11	2400 -	0
12	2600 -	REPEAT
13	2800 -	ALARM
14		
15		
16		



TOP VIEW
 2x1 FRA OVEN



Q1 Q2 Q3 Q4 Q5 Q6 Q7 Q8 Q9 Q10 Q11 Q12 Q13 Q14 Q15 Q16 Q17 Q18
 C B E B C E

SEQUENTIAL TONE TRANSMITTER SEKVENSTONESENDER

ST7845

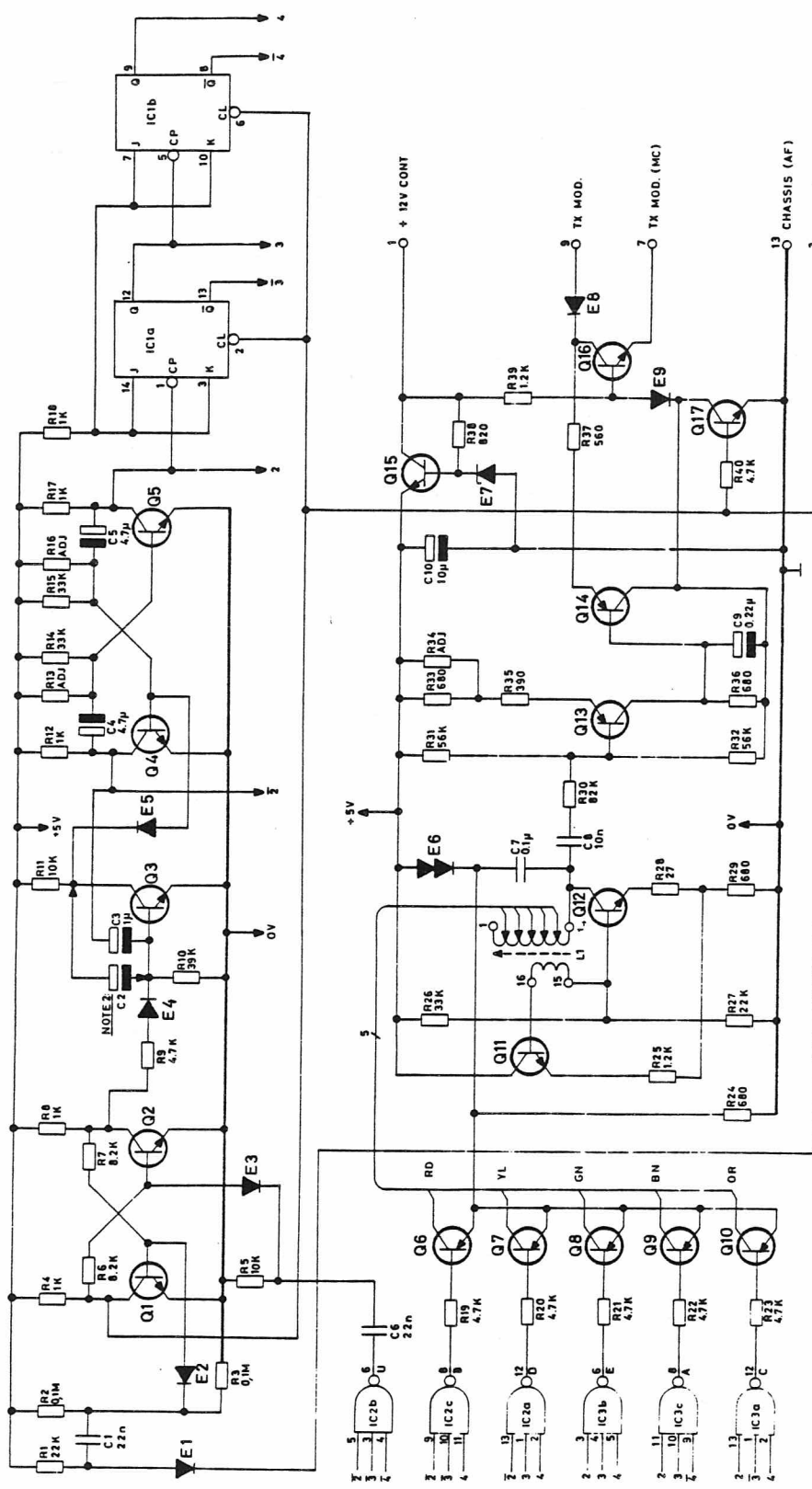
D401.583/4

TYPE	NO.	CODE	DATA
ST7845		10.2455-01	Tone Sequence Transmitter
	C1	76.5071	22nF 10% polyest FL 50V
	C2	73.5114	1μF 20% tantal
	C3	73.5126	4.7μF 20% tantal
	C4	73.5126	4.7μF 20% tantal
	C5	76.5071	22nF 10% polyest. FL
	C6	76.5068	0.1μF 1% polystyr TB
	C7	76.5070	10nF 10% polyest. FL
	C8	73.5118	0.22μF 20% tantal
	C9	73.5109	10μF 20% tantal
	C10		
	R1	80.5253	2.2KΩ 5% carbon film 1/8W
	R2	80.5273	0.1MΩ 5% carbon film 1/8W
	R3	80.5273	0.1MΩ 5% carbon film 1/8W
	R4	80.5249	1KΩ 5% carbon film 1/8W
	R5	80.5261	10KΩ 5% carbon film 1/8W
	R6	80.5260	8.2KΩ 5% carbon film 1/8W
	R7	80.5260	8.2KΩ 5% carbon film 1/8W
	R8	80.5249	1KΩ 5% carbon film 1/8W
	R9	80.5257	4.7KΩ 5% carbon film 1/8W
	R10	80.5268	39KΩ 5% carbon film 1/8W
	R11	80.5261	10KΩ 5% carbon film 1/8W
	R12	80.5249	1KΩ 5% carbon film 1/8W
	R13	80.52XX	Adjusted
	R14	80.5267	33KΩ 5% carbon film 1/8W
	R15	80.5267	33KΩ 5% carbon film 1/8W
	R16	80.52XX	Adjusted
	R17	80.5249	1KΩ 5% carbon film 1/8W
	R18	80.5249	1KΩ 5% carbon film 1/8W
	R19	80.5257	4.7KΩ 5% carbon film 1/8W
	R20	80.5257	4.7KΩ 5% carbon film 1/8W
	R21	80.5257	4.7KΩ 5% carbon film 1/8W
	R22	80.5257	4.7KΩ 5% carbon film 1/8W
	R23	80.5257	4.7KΩ 5% carbon film 1/8W
	R24	80.5247	680Ω 5% carbon film 1/8W
	R25	80.5250	1.2KΩ 5% carbon film 1/8W
	R26	80.5267	33KΩ 5% carbon film 1/8W
	R27	80.5265	22KΩ 5% carbon film 1/8W
	R28	80.5230	27Ω 5% carbon film 1/8W
	R29	80.5247	680Ω 5% carbon film 1/8W
	R30	80.5272	82KΩ 5% carbon film 1/8W
	R31	80.5270	56KΩ 5% carbon film 1/8W
	R32	80.5270	56KΩ 5% carbon film 1/8W
	R33	80.5247	680Ω 5% carbon film 1/8W
	R34	80.52XX	Adjusted
	R35	80.5244	390Ω 5% carbon film 1/8W

TYPE	NO.	CODE	DATA
	R36	80.5248	820Ω 5% carbon film 1/8W
	R37	80.5246	560Ω 5% carbon film 1/8W
	R38	80.5248	820Ω 5% carbon film 1/8W
	R39	80.5250	1.2KΩ 5% carbon film 1/8W
	R40	80.5253	2.2KΩ 5% carbon film 1/8W
	R41	80.5257	4.7KΩ 5% carbon film 1/8W
	L1	61.1140	Tone coil
	E1	99.5028	1N914 Diode
	E2	99.5028	1N914 Diode
	E3	99.5028	1N914 Diode
	E4	99.5028	1N914 Diode
	E5	99.5219	AAZ15
	E6	99.5209	Stab. diode ZE 1.5
	E7	99.5114	Zener diode 5.6V 5%
	E8	99.5219	AAZ15
	E9	99.5219	AAZ15
	E10	99.5028	1N914 Diode
	Q1	99.5143	BC108 Transistor
	Q2	99.5143	BC108 Transistor
	Q3	99.5121	BC107 Transistor
	Q4	99.5121	BC107 Transistor
	Q5	99.5121	BC107 Transistor
	Q6	99.5144	BC214L Transistor
	Q7	99.5144	BC214L Transistor
	Q8	99.5144	BC214L Transistor
	Q9	99.5144	BC214L Transistor
	Q10	99.5144	BC214L Transistor
	Q11	99.5143	BC108 Transistor
	Q12	99.5143	BC108 Transistor
	Q13	99.5144	BC214L Transistor
	Q14	99.5144	BC214L Transistor
	Q15	99.5128	2N3053 Transistor
	Q16	99.5143	BC108 Transistor
	Q17	99.5143	BC108 Transistor
	Q18	99.5143	BC108 Transistor
	IC1	14.5008	Dual J-K Master-Slave Flip-Flop
	IC2	14.5007	Triple 3-input NAND Gate
	IC3	14.5007	Triple 3-input NAND Gate

SEQUENTIAL TONE TRANSMITTER ST7845
SEKVENSTONESENDER

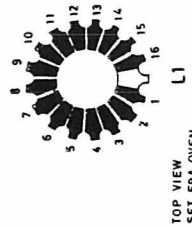
X401.689/2



NOTE 1: STRAP FOR IDENTIFICATION

NOTE 2: INSERT C2 FOR DELAY
 R 10 MIN 10K
 C2 MAX 47µ
 DELAY TIME: 0.1 - 1.5 SEC.

TERM	FREQ	DIGIT
1	9.70 HZ	1
2	10.60 -	2
3	11.60 -	3
4	12.70 -	4
5	14.00 -	5
6	15.30 -	6
7	16.70 -	7
8	18.30 -	8
9	20.00 -	9
10	22.00 -	0
11	24.00 -	REPEAT
12	26.00 -	ALARM
13	28.00 -	ALARM
14		
15		
16		



SEQUENTIAL TONE TRANSMITTER
 SEKVENSTONESENDER

ST7845

D401.583/3

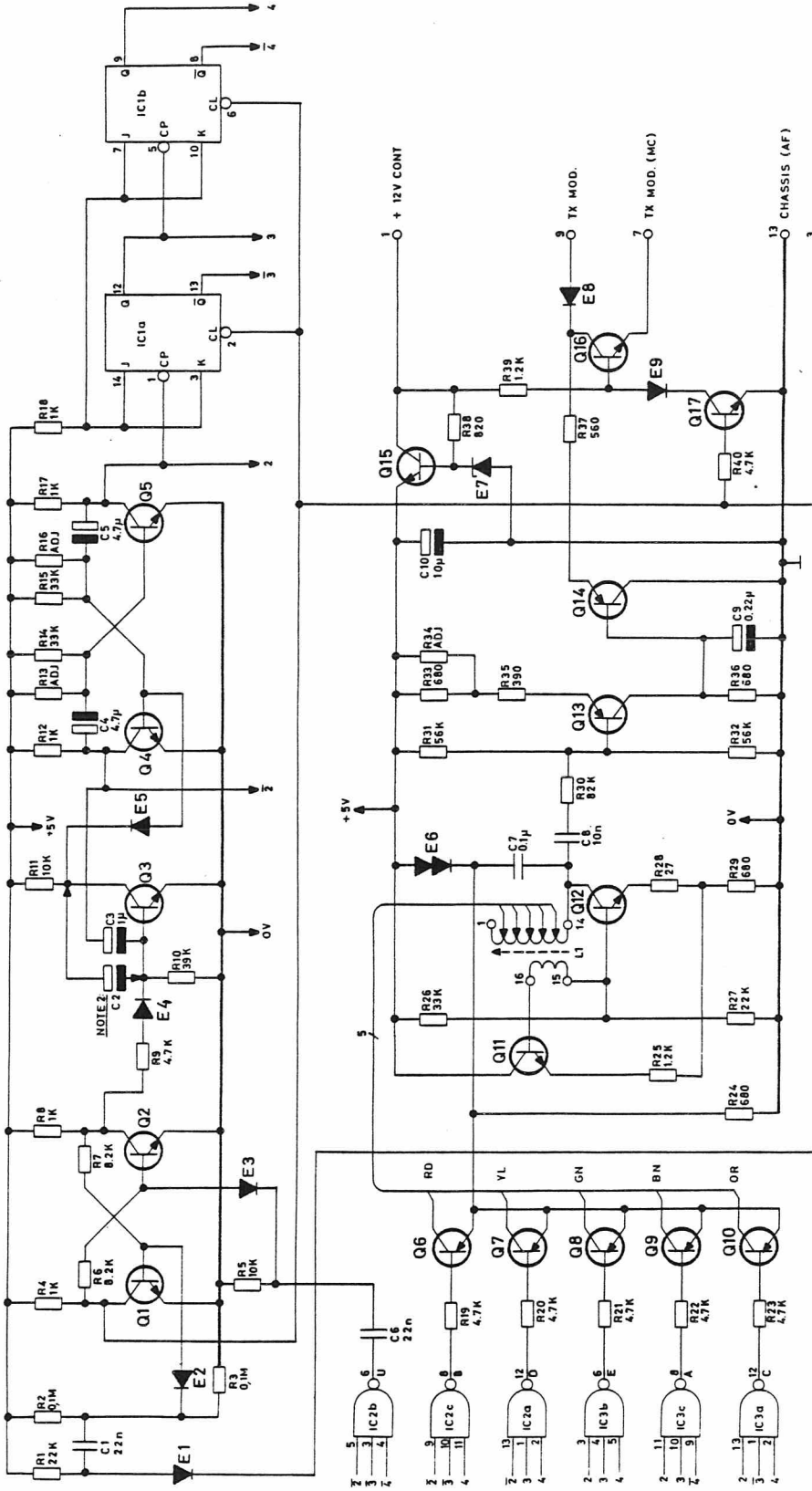
TYPE	NO.	CODE	DATA
ST7845		10. 2455-01	Tone Sequence Transmitter
	C1	76. 5071	22nF 10% polyester FL 50V
	C2	73. 5114	1μF 20% tantal 35V
	C3	73. 5126	4. 7μF 20% tantal 35V
	C4	73. 5126	4. 7μF 20% tantal 35V
	C5	76. 5071	22nF 10% polyester, FL 50V
	C6	76. 5068	0. 1μF 1% polystyr TB 63V
	C7	76. 5070	10nF 10% polyester, FL 50V
	C8	73. 5118	0. 22μF 20% tantal 35V
	C9	73. 5109	10μF 20% tantal 16V
	C10		
	R1	80. 5253	2. 2KΩ 5% carbon film 1/8W
	R2	80. 5273	0. 1MΩ 5% carbon film 1/8W
	R3	80. 5273	0. 1MΩ 5% carbon film 1/8W
	R4	80. 5249	1KΩ 5% carbon film 1/8W
	R5	80. 5261	10KΩ 5% carbon film 1/8W
	R6	80. 5260	8. 2KΩ 5% carbon film 1/8W
	R7	80. 5260	8. 2KΩ 5% carbon film 1/8W
	R8	80. 5249	1KΩ 5% carbon film 1/8W
	R9	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R10	80. 5268	39KΩ 5% carbon film 1/8W
	R11	80. 5261	10KΩ 5% carbon film 1/8W
	R12	80. 5249	1KΩ 5% carbon film 1/8W
	R13	80. 52XX	Adjusted
	R14	80. 5267	33KΩ 5% carbon film 1/8W
	R15	80. 5267	33KΩ 5% carbon film 1/8W
	R16	80. 52XX	Adjusted
	R17	80. 5249	1KΩ 5% carbon film 1/8W
	R18	80. 5249	1KΩ 5% carbon film 1/8W
	R19	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R20	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R21	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R22	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R23	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R24	80. 5247	680Ω 5% carbon film 1/8W
	R25	80. 5250	1. 2KΩ 5% carbon film 1/8W
	R26	80. 5267	33KΩ 5% carbon film 1/8W
	R27	80. 5265	22KΩ 5% carbon film 1/8W
	R28	80. 5230	27Ω 5% carbon film 1/8W
	R29	80. 5247	680Ω 5% carbon film 1/8W
	R30	80. 5272	82KΩ 5% carbon film 1/8W
	R31	80. 5270	56KΩ 5% carbon film 1/8W
	R32	80. 5270	56KΩ 5% carbon film 1/8W
	R33	80. 5247	680Ω 5% carbon film 1/8W
	R34	80. 52XX	Adjusted
	R35	80. 5244	390Ω 5% carbon film 1/8W

TYPE	NO.	CODE	DATA
	R35	80. 5248	820Ω 5% carbon film 1/8W
	R37	80. 5246	560Ω 5% carbon film 1/8W
	R38	80. 5248	820Ω 5% carbon film 1/8W
	R39	80. 5250	1. 2KΩ 5% carbon film 1/8W
	R40	80. 5253	2. 2KΩ 5% carbon film 1/8W
	R41	80. 5257	4. 7KΩ 5% carbon film 1/8W
	L1	61. 1140	Tone coil
	E1	99. 5028	1N914 Diode
	E2	99. 5028	1N914 Diode
	E3	99. 5028	1N914 Diode
	E4	99. 5028	1N914 Diode
	E5	99. 5219	AAZ15
	E6	99. 5209	Stab. diode ZE 1. 5
	E7	99. 5114	Zenerdiode 5. 6V 5%
	E8	99. 5219	AAZ15
	E9	99. 5219	AAZ15
	E10	99. 5028	1N914 Diode 1/4W
	Q1	99. 5143	BC108 Transistor
	Q2	99. 5143	BC108 Transistor
	Q3	99. 5121	BC107 Transistor
	Q4	99. 5121	BC107 Transistor
	Q5	99. 5121	BC107 Transistor
	Q6	99. 5144	BC214L Transistor
	Q7	99. 5144	BC214L Transistor
	Q8	99. 5144	BC214L Transistor
	Q9	99. 5144	BC214L Transistor
	Q10	99. 5144	BC214L Transistor
	Q11	99. 5143	BC108 Transistor
	Q12	99. 5143	BC108 Transistor
	Q13	99. 5144	BC214L Transistor
	Q14	99. 5144	BC214L Transistor
	Q15	99. 5128	2N3053 Transistor
	Q16	99. 5143	BC108 Transistor
	Q17	99. 5143	BC108 Transistor
	Q18	99. 5143	BC108 Transistor
	IC1	14. 5008	Dual J-K Master-Slave Flip-Flop
	IC2	14. 5007	Triple 3-input NAND Gate
	IC3	14. 5007	Triple 3-input NAND Gate

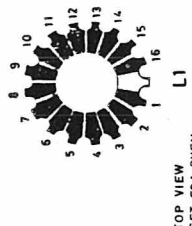
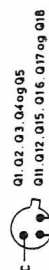
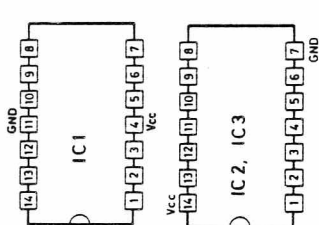
SEQUENTIAL TONE TRANSMITTER ST7845
SEKVENSTONESENDER

X401. 689/2

SEQUENTIAL TONE TRANSMITTER,
SEKVENSTONESENDER



NOTE: INSERT C2 FOR DELAY
R 10 MIN 10K
C 2 MAX 47u
DELAY TIME: 0.1 - 1.5 SEC.



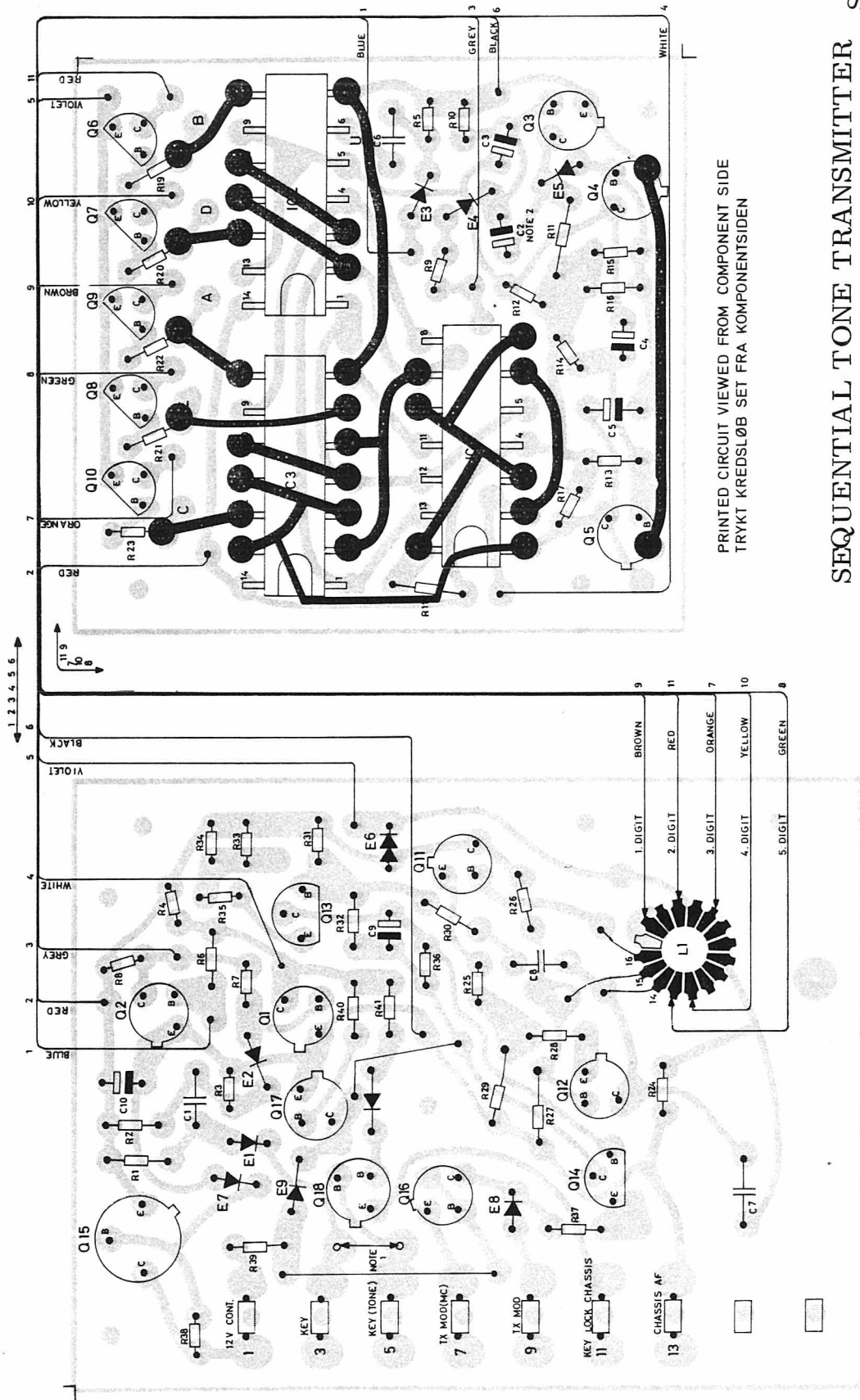
TERM	FREQ.	DIGIT
1	970 Hz	1
2	1060 -	2
3	1160 -	3
4	1270 -	4
5	1400 -	4
6	1530 -	5
7	1670 -	6
8	1830 -	7
9	2000 -	8
10	2200 -	9
11	2400 -	0
12	2600 -	REPEAT
13	2800 -	ALARM
14		
15		
16		

TYPE	NO.	CODE	DATA
ST7845		10. 2455	Tone Sequence Transmitter
	C1	76. 5071	22nF 10% polyester FL 50V
	C2	73. 5114	1μF 20% tantal
	C3	73. 5126	4. 7μF 20% tantal
	C4	73. 5126	4. 7μF 20% tantal
	C5	76. 5071	22nF 10% polyester. FL 50V
	C6	76. 5068	0. 1μF 1% polystyr TB
	C7	76. 5070	10nF 10% polyester. FL 63V
	C8	73. 5118	0. 22μF 20% tantal 50V
	C9	73. 5109	10μF 20% tantal 35V
	C10		16V
	R1	80. 5253	2. 2KΩ 5% carbon film 1/8W
	R2	80. 5273	0. 1MΩ 5% carbon film 1/8W
	R3	80. 5273	0. 1MΩ 5% carbon film 1/8W
	R4	80. 5249	1KΩ 5% carbon film 1/8W
	R5	80. 5261	10KΩ 5% carbon film 1/8W
	R6	80. 5260	8. 2KΩ 5% carbon film 1/8W
	R7	80. 5260	8. 2KΩ 5% carbon film 1/8W
	R8	80. 5249	1KΩ 5% carbon film 1/8W
	R9	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R10	80. 5268	39KΩ 5% carbon film 1/8W
	R11	80. 5261	10KΩ 5% carbon film 1/8W
	R12	80. 5249	1KΩ 5% carbon film 1/8W
	R13	80. 52XX	Adjusted
	R14	80. 5267	33KΩ 5% carbon film 1/8W
	R15	80. 5267	33KΩ 5% carbon film 1/8W
	R16	80. 52XX	Adjusted
	R17	80. 5249	1KΩ 5% carbon film 1/8W
	R18	80. 5249	1KΩ 5% carbon film 1/8W
	R19	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R20	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R21	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R22	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R23	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R24	80. 5247	680Ω 5% carbon film 1/8W
	R25	80. 5250	1. 2KΩ 5% carbon film 1/8W
	R26	80. 5267	33KΩ 5% carbon film 1/8W
	R27	80. 5265	22KΩ 5% carbon film 1/8W
	R28	80. 5230	27Ω 5% carbon film 1/8W
	R29	80. 5247	680Ω 5% carbon film 1/8W
	R30	80. 5272	82KΩ 5% carbon film 1/8W
	R31	80. 5270	56KΩ 5% carbon film 1/8W
	R32	80. 5270	56KΩ 5% carbon film 1/8W
	R33	80. 5247	680Ω 5% carbon film 1/8W
	R34	80. 52XX	Adjusted
	R35	80. 5244	390Ω 5% carbon film 1/8W

TYPE	NO.	CODE	DATA
	R36	80. 5247	680Ω 5% carbon film 1/8W
	R37	80. 5246	560Ω 5% carbon film 1/8W
	R38	80. 5248	820Ω 5% carbon film 1/8W
	R39	80. 5250	1. 2KΩ 5% carbon film 1/8W
	R40	80. 5257	4. 7KΩ 5% carbon film 1/8W
	R41	80. 5257	4. 7KΩ 5% carbon film 1/8W
	L1	61. 1140	Tone coil 1/8W
	E1	99. 5028	1N914 Diode
	E2	99. 5028	1N914 Diode
	E3	99. 5028	1N914 Diode
	E4	99. 5028	1N914 Diode
	E5	99. 5219	AAZ15
	E6	99. 5209	Stab. diode ZE 1. 5
	E7	99. 5114	Zenerdiode 5. 6V 5%
	E8	99. 5219	AAZ15
	E9	99. 5219	AAZ15
	E10	99. 5028	1N914 Diode 1/4W
	Q1	99. 5143	BC108 Transistor
	Q2	99. 5143	BC108 Transistor
	Q3	99. 5121	BC107 Transistor
	Q4	99. 5121	BC107 Transistor
	Q5	99. 5121	BC107 Transistor
	Q6	99. 5144	BC214L Transistor
	Q7	99. 5144	BC214L Transistor
	Q8	99. 5144	BC214L Transistor
	Q9	99. 5144	BC214L Transistor
	Q10	99. 5144	BC214L Transistor
	Q11	99. 5143	BC108 Transistor
	Q12	99. 5143	BC108 Transistor
	Q13	99. 5144	BC214L Transistor
	Q14	99. 5144	BC214L Transistor
	Q15	99. 5128	2N3053 Transistor
	Q16	99. 5143	BC108 Transistor
	Q17	99. 5143	BC108 Transistor
	Q18	99. 5143	BC108 Transistor
	IC1	14. 5008	Dual J-K Master-Slave Flip-Flop
	IC2	14. 5007	Triple 3-input NAND Gate
	IC3	14. 5007	Triple 3-input NAND Gate

SEQUENTIAL TONE TRANSMITTER ST7845
SEKVENSTONESENDER

X401. 689



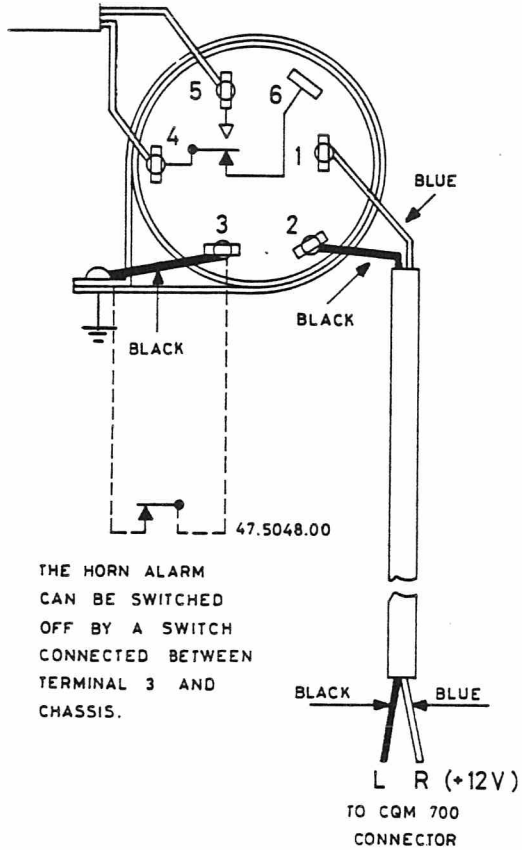
PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
 TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

SEQUENTIAL TONE TRANSMITTER
 SEKVENSTONESENDER

ST7845

D401.686

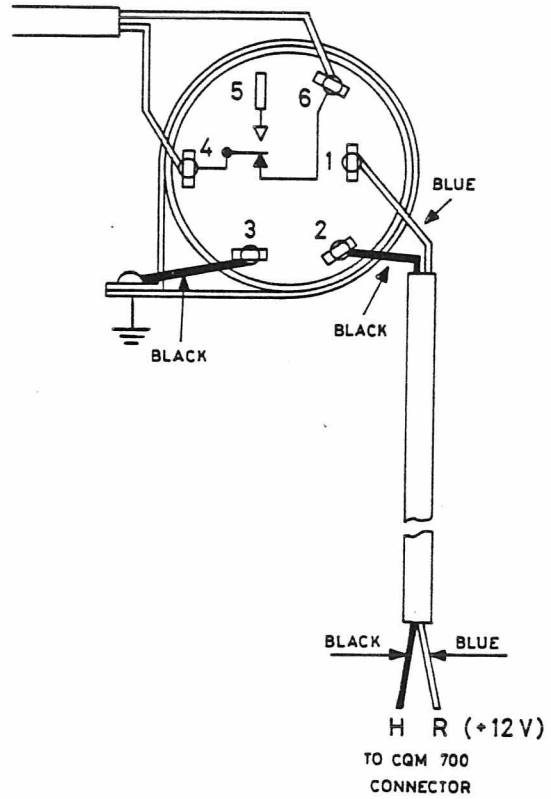
TO HORN OR BELL



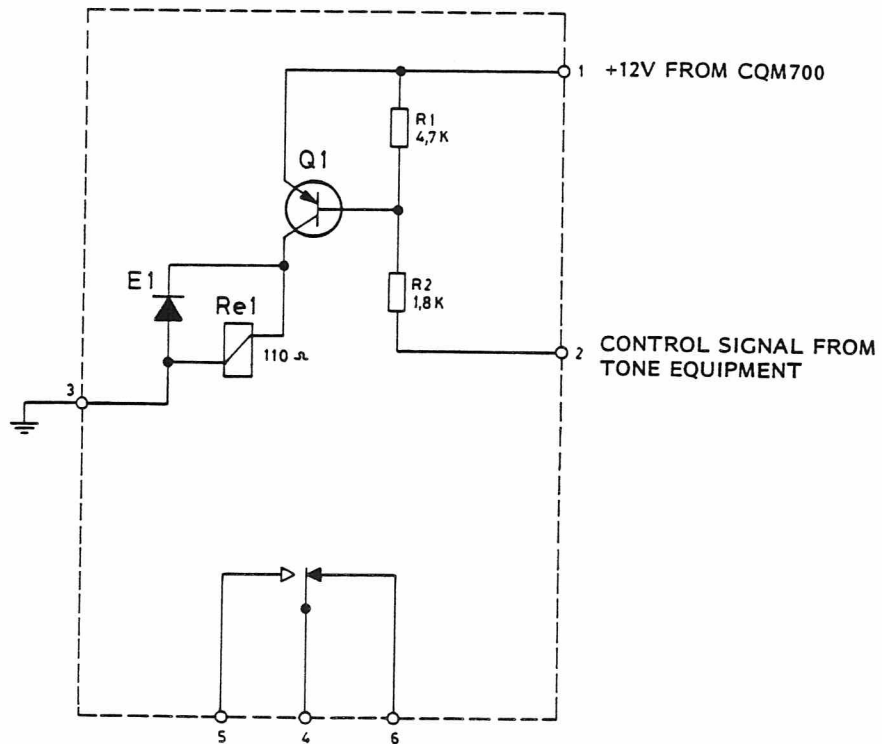
THE HORN ALARM CAN BE SWITCHED OFF BY A SWITCH CONNECTED BETWEEN TERMINAL 3 AND CHASSIS.

ALARM

DISCONNECTING AUTO RADIO



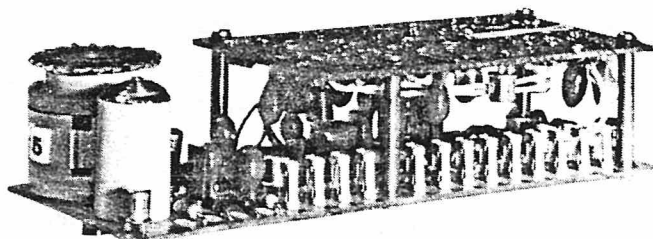
AUTO RADIO MUTING



INSTALLATION OF SWITCHING UNIT SU704

TONE RECEIVER

TR782 TR783 TR785



Introduction

TR782, TR783, and TR785 are selective tone receivers developed for use with Stornophone 700 radiotelephones. They are designed as double tone receivers but can also be employed in single tone mode. With the exception of a few frequency determining components, TR782, TR783, and TR785 are identical, and as far as this description is concerned, will be treated as though they were the same unit.

Tone frequencies for each unit are:
(frequencies in Hz)

<u>TR782</u>	<u>TR783</u>	<u>TR785</u>
615	825	370
675	1010	450
735	1240	550
805	1435	675
885	1520	825
970	1750	1040
1060	1860	1240
1160	1980	1520
1270	2000	1860
1400	2135	2280
1530	2280	
1670	2450	
1830		
2000		
2200		
2400		
2600		
2900		

General Description

Upon receipt of the appropriate tone signal with a duration of > 700 ms the Call Lamp will light, the AF muting will be cancelled and the Key Locking function will "unlock".

The vehicle's traffic horn can be connected to the tone receiver via an auxiliary relay. Then, after the initial 700 ms required to establish a path through the tone receiver, the horn will sound for long as the tone signal continues to be received.

The audio circuit and the Key Lock are both turned on and off manually by means of the LS IN/OUT push button.

Since the Key Lock is "unlocked" with the same switch that turns on the loudspeaker, the operator is forced to check for the presence of another signal on the channel before being able to key his transmitter.

In addition, the tone receiver is equipped with an Occupied Lamp controlled by the squelch circuit in the radiotelephone. Thus, if an RF signal having that channel's frequency is present at the antenna input it will cause the Occupied Lamp to light as an indication that the channel is not free.

Circuit Description

Pre-emphasis Stage

The pre-emphasis network includes transistor Q1 and follows an RC characteristic, 6 dB/octave, with cut-off frequency at 1000 Hz.

Amplifier and Amplitude Limiter

Transistor Q2 amplifies the incoming signal linearly until diodes E1 and E2 begin conducting.

When the incoming double tone signal reaches a level of approx. 8 dB above minimum triggering level (approx. 3 dB when connected as a single tone receiver) full amplitude limiting of the signal occurs:

Trigger level, $V_{IN} = -29$ dBm (-23 dBm) at 1000 Hz.

Due to this limiting action along with the narrow pass band of the subsequent Q multiplier, adjacent tones having frequencies that differ from the resonant frequency by at least 4.5 % will be unable to trigger the tone receiver.

Driver

Transistors Q3 and Q4 are arranged so that they present an extremely low output impedance (on the order of 1Ω) which is suitable as a ground return for the resonant circuit in the following stage.

Q Multiplier

The Q multiplier stage involves a parallel resonant circuit; this is coupled very loosely to the transistor, Q5, in order to maintain a constant Q over the entire tone range. C8 in the resonant circuit is grounded through the output impedance of the driver transistors while the relevant terminal(s) of coil L1 are alternately grounded through the AF gates, Q19 and Q20. This will be explained in the next section.

Part of the tone signal is reapplied to L1 in phase by means of a feedback winding in the collector circuit of Q5, approximately doubling the Q of L1.

To offset the effect of temperature upon the Q of L1 an NTC resistor, R20, is inserted in the emitter circuit of Q5. R20, aided by R19 and R21, maintains a nearly flat temperature response from -30°C to $+80^{\circ}\text{C}$.

Astable Multivibrator and AF Gates

Transistors Q21 and Q22 form an astable multivibrator, driving the two AF gates, Q19 and

Q20. When Q21 (Q22) conducts it drives Q20 (Q19) ON. The ground connection, which also determines the resonant frequency of the tuned circuit, is through Q20 (Q19) and capacitor C19.

The multivibrator action turns the two AF gates alternately ON and OFF, switching tone frequencies at the pulse repetition rate of approx. 500 ms.

Amplifier, Emitter, Follower, and Detector

Q6 amplifies the signal from the Q multiplier; its input resistance is bootstrapped to a value that will not load the Q multiplier.

The signal proceeds from Q6 to emitter follower Q7, then to the detector circuit, a conventional voltage doubler where R25 insures linearity for stronger signals.

The time constant of R25, C13, and R26/27 is long enough to form a low-pass filter for the tone signal components while short enough to react to the 250 ms half-periods of the multivibrator. For instance, should one of the tones of a double tone signal fail (tone does not match the receiver), the rectified DC voltage will drop to nearly 0 before the next tone arrives.

R27 sets the DC output level.

Schmitt Trigger, Delay Circuit, and Inverter

Q8 and Q9 make up the Schmitt trigger. When a correct tone is received, the rectified DC voltage at the trigger input, base of Q8, turns the circuit ON and the high potential at the collector of Q9 cuts E5 OFF. A charge begins to build up on C14 through R34; when the charge reaches approx. 0.6 V above the emitter voltage of Q10, that transistor will go ON. This last circuit introduces a 700 ms delay between input and output. Refer to the General Description.

With no signal at the trigger input, the circuit is OFF and E5 conducts. C14 discharges through E5 and Q9, turning Q10 OFF.

Build-up time between gate shifts in the Q multiplier is approx. 20 to 30 ms, which is con-

siderable compared with the detector time constant and the fast action of the Schmitt trigger.

A resistor, R32 is inserted in the discharge path of C14 to introduce a time lag of approx. 40 ms in order to compensate for the Q multiplier build-up time, ensuring that Q10 does not turn off intermittently between tones.

When Q10 turns ON, it turns the inverter, Q11 ON as well.

Switch and Alarm Gate

When Q11 goes ON, it turns Q12 ON. Q12 switches the external alarm circuit ON by pulling the Alarm terminal, 37, virtually down to chassis potential. Q12, and therefore the alarm device, remains ON as long as the correct tone combination continues to be received.

Bistable Multivibrator and Outlet Switches

The bistable multivibrator comprises Q13 and Q14. There are two possibilities for triggering the multivibrator:

- (1) automatically, by reception of a correct tone call
- (2) manually, by pushbutton

Consider the manual mode first: pressing a pushbutton on the control panel grounds terminal 32, causing a trigger pulse via C15 and C16 to change the state of the bistable circuit.

Regardless of the state of the bistable multivibrator a correct tone signal will, as previously mentioned, turn Q12 ON whereby the base of Q13 becomes grounded via E6 and Q12. If Q13 happens to be ON at the time, it will be switched OFF; if it is already OFF, it will be held there. Thus, a tone call has higher priority than the manual switch.

Whenever Q13 is OFF the following occurs:

- (1) Q18 goes ON, connecting terminal 34 (AF Muting) to chassis through diode E12 and allowing the loudspeaker amplifier to operate.
- (2) Q17 goes ON, lighting the Call Lamp via terminal 47.

- (3) Q15 goes ON, releasing the Key Lock via terminal 51. It is then possible to operate the transmitter.

When the tone signal disappears the operator can change the state of the bistable circuit manually, as explained earlier.

Squelch Gate

When another call is in progress on the channel the RF signal will be detected in the radiotelephone receiver. The receiver squelch system will then feed a DC voltage (approx. +5 V emf / $R_G = 1 \text{ k}\Omega$) to terminal 41. Q16 will be driven ON and will light the Occupied Lamp through terminal 45.

Audio Radio Muting

If the vehicle also has a broadcast radio installed, an auxiliary relay connected to terminal 49 may be used to silence the radio during the time that the Key Lock is released.

Technical Specifications

Tone Receiver TR782

Power Supply

Operating range: 10.5 V - 16.0 V

Nominal: 13.6 V

Current Consumption

Stand by: nom. 45 mA

Temperature Range

Operating range: $-25^{\circ} - +60^{\circ} \text{C}$

Functioning range: $-30^{\circ} - +80^{\circ} \text{C}$

Input Impedance

$> 6 \text{ k}\Omega$

Signal Input Level

Nominal at 1000 Hz: -23 dBm

Equalization

Preemphasis (by RC function) $f_c = 1 \text{ kHz}$

Signal Code

2 preset tone frequencies, received simultaneously for min. 700 mS

Signal Frequencies

615, 675, 735, 805, 885, 970, 1060, 1160,
1270, 1400, 1530, 1670, 1830, 2000, 2200,
2400, 2600, 2900 Hz

Frequency Accuracy

With coil adjusted for 1060 Hz: $\leq 0.3 \%$

Frequency Stability

(Typically $\leq 0.5 \%$): $\leq 1.0 \%$

Selectivity

Frequencies differing from f_0 by 4.5 % or more
are unable to trigger the tone receiver.

Maximum Load Currents

Terminal 37, "ALARM"	100 mA
Terminal 47 + 49, "CALL"	100 mA
Terminal 45, "OCCUPIED"	60 mA
Terminal 51, "KEY LOCK"	60 mA
Terminal 34, "AF MUTING"	5 mA

AF Muting

In conjunction with AA7xx: ≥ 60 dB

Tone Receiver TR783Power Supply

Operating range: 10.5 V - 16.0 V

Nominal: 13.6 V

Current Consumption

Stand by: nom. 45 mA

Temperature Range

Operating range: -25°C - $+60^{\circ}\text{C}$

Functioning range: -30°C - $+80^{\circ}\text{C}$

Input Impedance

$> 6 \text{ k}\Omega$

Signal Input Level

Nominal at 1000 Hz: -23 dBm

Equalization

Preemphasis (by RC function) $f_c = 1$ kHz

Signal Code

2 preset tone frequencies, received simultaneously
for min. 700 mS

Signal Frequencies

825, 1010, 1240, 1435, 1520, 1750, 1860, 1980, 2000,
2135, 2280, 2450.

Frequency Accuracy

With coil adjusted for 1010 Hz = $\leq 0.3 \%$

Frequency Stability

(Typically $\leq 0.5 \%$): $\leq 1.0 \%$

Selectivity

Frequencies differing from f_0 by 4.5 % or more are
unable to trigger the tone receiver.

Maximum Load Currents

Terminal 37, "ALARM"	100 mA
Terminal 47 + 49, "CALL"	100 mA
Terminal 45, "OCCUPIED"	60 mA
Terminal 51, "KEY LOCK"	60 mA
Terminal 34, "AF MUTING"	5 mA

AF Muting

In conjunction with AA7xx: ≥ 60 dB

Tone Receiver TR785Power Supply

Operating range: 10.5 V - 16.0 V

Nominal: 13.6 V

Current Consumption

Stand by: nom. 45 mA

Temperature Range

Operating range: -25°C - $+60^{\circ}\text{C}$

Functioning range: -30°C - $+80^{\circ}\text{C}$

Input Impedance

$> 6 \text{ k}\Omega$

Signal Input Level

Nominal at 1000 Hz: -23 dBm

Equalization

Preemphasis (by RC function) $f_c = 1$ kHz

Signal Code

2 preset tone frequencies, received simultaneously
for min. 700 mS.

Signal Frequencies

370, 450, 550, 675, 825, 1010, 1240, 1520, 1860,
2280

Frequency Accuracy

With coil adjusted for 1010 Hz: $\leq 0.3 \%$

Frequency Stability

(Typically $\leq 0.5 \%$): $\leq 1.0 \%$

Selectivity

Frequencies differing from f_o by 4.5 % or more are
unable to trigger the tone receiver.

Maximum Load Currents

Terminal 37, "ALARM"	100 mA
Terminal 47 +49, "CALL"	100 mA
Terminal 45, "OCCUPIED"	60 mA
Terminal 51, "KEY LOCK"	60 mA
Terminal 34, "AF MUTING"	5 mA

AF Muting

In conjunction with AA7xx: 60 dB.

TYPE	NO.	CODE	DATA
TR782		10.2449	Tone Receiver
	C1	73.5126	4.7μF 20% tantal
	C2	76.5069	1nF 10% polyester, FL
	C3	76.5072	47nF 10% polyester, FL
	C4	76.5059	2.2nF 10% polyester, FL
	C5	73.5124	47μF 20% tantal
	C6	73.5124	47μF 20% tantal
	C7	73.5126	4.7μF 20% tantal
	C8	76.5068	0.1μF 1% polystyr TB
	C9	76.5070	10nF 10% polyester, FL
	C10	73.5114	1μF 20% tantal
	C11	73.5124	47μF 20% tantal
	C12	73.5126	4.7μF 20% tantal
	C13	73.5109	10μF 20% tantal
	C14	73.5124	47μF 20% tantal
	C15	73.5089	0.1μF 20% tantal
	C16	73.5089	0.1μF 20% tantal
	C17	73.5109	10μF 20% tantal
	C18	73.5114	1μF 20% tantal
	C19	73.5124	47μF 20% tantal
	C20	73.5109	10μF 20% tantal
	C21	73.5109	10μF 20% tantal
	C22	73.5124	47μF 20% tantal
	C23	73.5127	22μF 20% tantal
	C24	73.5089	0.1μF 20% tantal
	C25	76.5070	10nF 10% polyester, FL
	C26	76.5070	10nF 10% polyester, FL
	R1	80.5266	27KΩ 5% carbon film
	R2	80.5255	3.3KΩ 5% carbon film
	R3	80.5268	39KΩ 5% carbon film
	R4	80.5253	2.2KΩ 5% carbon film
	R5	80.5246	560Ω 5% carbon film
	R6	80.5240	180Ω 5% carbon film
	R7	80.5257	4.7KΩ 5% carbon film
	R8	80.5253	2.2KΩ 5% carbon film
	R9	80.5267	33KΩ 5% carbon film
	R10	80.5253	2.2KΩ 5% carbon film
	R11	80.5257	4.7KΩ 5% carbon film
	R12	80.5242	270Ω 5% carbon film
	R13	80.5273	0.1 MΩ 5% carbon film
	R14	80.5274	0.12 MΩ 5% carbon film
	R15	80.5259	6.8KΩ 5% carbon film
	R16	80.5253	2.2KΩ 5% carbon film
	R17	80.5265	22KΩ 5% carbon film
	R18	80.5253	2.2KΩ 5% carbon film
	R19	80.5256	3.9KΩ 5% carbon film
	R20	89.5008	1.5KΩ 20% NTC

TYPE	NO.	CODE	DATA
	R21	80.5257	4.7KΩ 5% carbon film
	R22	80.5253	2.2KΩ 5% carbon film
	R23	80.5248	820Ω 5% carbon film
	R24	80.5249	1 KΩ 5% carbon film
	R25	80.5253	2.2KΩ 5% carbon film
	R26	80.5268	39KΩ 5% carbon film
	R27	80.52XX	Adjusted
	R28	80.5256	3.9KΩ 5% carbon film
	R29	80.5249	1 KΩ 5% carbon film
	R30	80.5249	1 KΩ 5% carbon film
	R31	80.5259	6.8KΩ 5% carbon film
	R32	80.5253	2.2KΩ 5% carbon film
	R33	80.5241	220Ω 5% carbon film
	R34	80.5271	68KΩ 5% carbon film
	R35	80.5261	10KΩ 5% carbon film
	R36	80.5261	10KΩ 5% carbon film
	R37	80.5255	3.3KΩ 5% carbon film
	R38	80.5247	680Ω 5% carbon film
	R39	80.5249	1 KΩ 5% carbon film
	R40	80.5256	3.9KΩ 5% carbon film
	R41	80.5261	10KΩ 5% carbon film
	R42	80.5249	1 KΩ 5% carbon film
	R43	80.5273	0.1 MΩ 5% carbon film
	R44	80.5257	4.7KΩ 5% carbon film
	R45	80.5255	3.3KΩ 5% carbon film
	R46	80.5273	0.1 MΩ 5% carbon film
	R47	80.5254	2.7KΩ 5% carbon film
	R48		
	R49		
	R50	80.5258	5.6KΩ 5% carbon film
	R51	80.5248	820Ω 5% carbon film
	R52	80.5248	820Ω 5% carbon film
	R53	80.5247	680Ω 5% carbon film
	R54	80.5247	680Ω 5% carbon film
	R55	80.5261	10KΩ 5% carbon film
	R56	80.5261	10KΩ 5% carbon film
	R57	80.5255	3.3KΩ 5% carbon film
	R58	80.5246	560Ω 5% carbon film
	R59	80.5252	1.8KΩ 5% carbon film
	R60	80.5267	33KΩ 5% carbon film
	R61	80.5267	33KΩ 5% carbon film
	R62	80.5252	1.8KΩ 5% carbon film
	R63	80.5249	1 KΩ 5% carbon film

TR782
ONE RECEIVER
ONE MODULATOR

X401.650/2

PREEMPHASIS
FORBE TONING

DRIVER

LIMITER
BEGRÆNSER

Q-MULTIPL.

AMPL.
FORST.

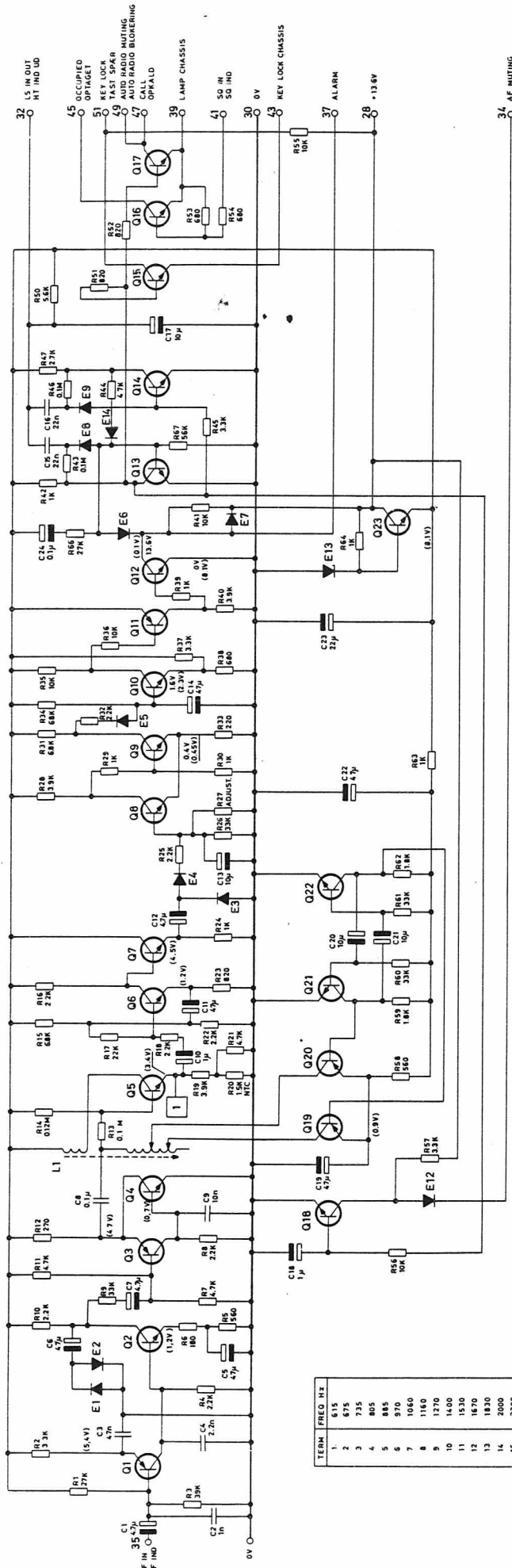
DETECTOR
DETEKTOR

EMITTER FOLLOWER
EMITTERFØLGER

GATE
INVERT.

GATE
SWITCH

BISTAB MV
3 x SWITCH

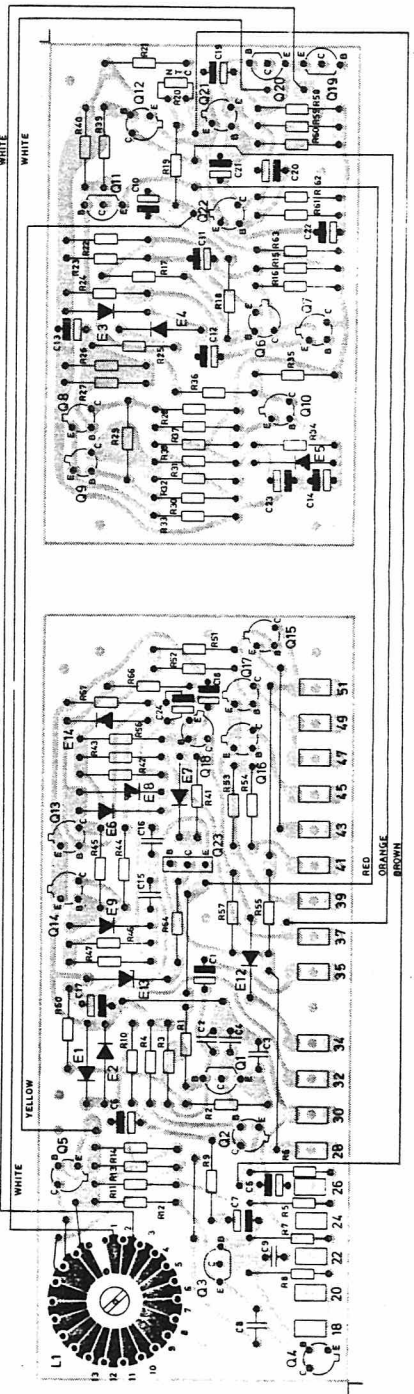


TERM	FREQ. HZ
1	615
2	675
3	735
4	805
5	885
6	970
7	1060
8	1160
9	1270
10	1400
11	1550
12	1670
13	1820
14	2000
15	2200
16	2400
17	2600
18	2900

VOLTAGE REG.
SPÆNDINGSREG.

AF GATES
ASTABLE MV
ASTABIL MV

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN



VOLTAGES WITH () V_{CC} 180HZ ± 5%
VOLTAGES WITHOUT () V_{CC} 0V

Q2 Q4 Q5 Q6 Q7 Q8 Q9 Q10 Q12 Q13
Q14 Q15 Q16 Q17 Q18 Q21 Q22

Q1 Q3 Q11 Q19 Q20



BOTTOM VIEW
SET FRA BUNDEN

TR782
TONE RECEIVER
TONEMODTAGER

TYPE	NO.	CODE	DATA
TR782		10. 2449	Tone Receiver
	C1	73. 5126	4. 7 μ F 20% tantal
	C2	76. 5069	1nF 10% polyest. FL
	C3	76. 5072	47nF 10% polyest. FL
	C4	76. 5059	2. 2nF 10% polyest. FL
	C5	73. 5124	47 μ F 20% tantal
	C6	73. 5124	47 μ F 20% tantal
	C7	73. 5126	4. 7 μ F 20% tantal
	C8	76. 5068	0. 1 μ F 1% polystyr TB
	C9	76. 5070	10nF 10% polyest. FL
	C10	73. 5114	1 μ F 20% tantal
	C11	73. 5124	47 μ F 20% tantal
	C12	73. 5126	4. 7 μ F 20% tantal
	C13	73. 5109	10 μ F 20% tantal
	C14	73. 5124	47 μ F 20% tantal
	C15	76. 5071	22nF 10% polyest. FL
	C16	76. 5071	22nF 10% polyest. FL
	C17	73. 5109	10 μ F 20% tantal
	C18	73. 5114	1 μ F 20% tantal
	C19	73. 5124	47 μ F 20% tantal
	C20	73. 5109	10 μ F 20% tantal
	C21	73. 5109	10 μ F 20% tantal
	C22	73. 5124	47 μ F 20% tantal
	C23	73. 5127	22 μ F 20% tantal
	C24	73. 5089	0. 1 μ F 20% tantal
	R1	80. 5266	27K Ω 5% carbon film
	R2	80. 5255	3. 3K Ω 5% carbon film
	R3	80. 5268	39K Ω 5% carbon film
	R4	80. 5253	2. 2K Ω 5% carbon film
	R5	80. 5246	560 Ω 5% carbon film
	R6	80. 5240	180 Ω 5% carbon film
	R7	80. 5257	4. 7K Ω 5% carbon film
	R8	80. 5253	2. 2K Ω 5% carbon film
	R9	80. 5267	33K Ω 5% carbon film
	R10	80. 5253	2. 2K Ω 5% carbon film
	R11	80. 5257	4. 7K Ω 5% carbon film
	R12	80. 5242	270 Ω 5% carbon film
	R13	80. 5273	0. 1M Ω 5% carbon film
	R14	80. 5274	0. 12M Ω 5% carbon film
	R15	80. 5259	6. 8K Ω 5% carbon film
	R16	80. 5253	2. 2K Ω 5% carbon film
	R17	80. 5265	22K Ω 5% carbon film
	R18	80. 5253	2. 2K Ω 5% carbon film
	R19	80. 5256	3. 9K Ω 5% carbon film
	R20	89. 5008	1. 5K Ω 20% NTC
	R21	80. 5257	4. 7K Ω 5% carbon film

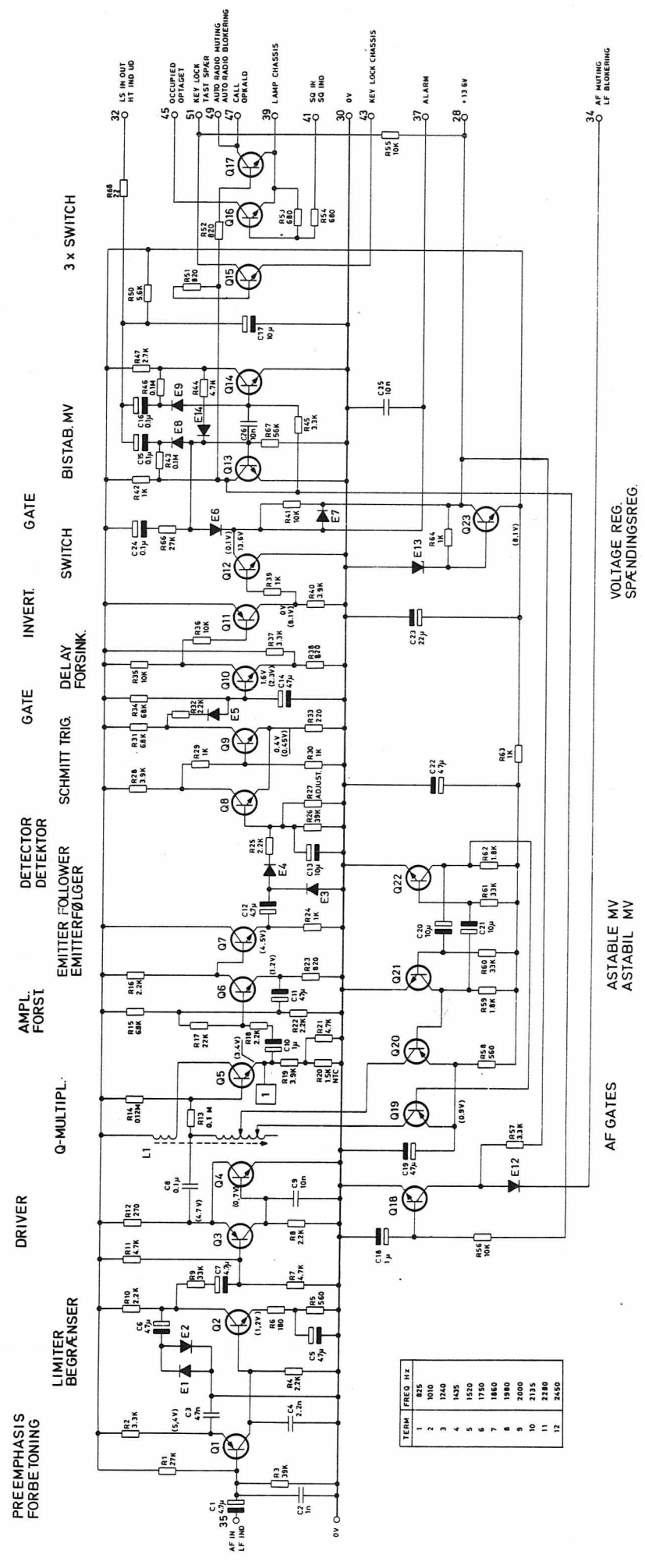
TYPE	NO.	CODE	DATA
	R22	80. 5253	2. 2K Ω 5% carbon film
	R23	80. 5248	820 Ω 5% carbon film
	R24	80. 5249	1K Ω 5% carbon film
	R25	80. 5253	2. 2K Ω 5% carbon film
	R26	80. 5267	33K Ω 5% carbon film
	R27	80. 52XX	Adjusted
	R28	80. 5256	3. 9K Ω 5% carbon film
	R29	80. 5249	1K Ω 5% carbon film
	R30	80. 5249	1K Ω 5% carbon film
	R31	80. 5259	6. 8K Ω 5% carbon film
	R32	80. 5253	2. 2K Ω 5% carbon film
	R33	80. 5241	220 Ω 5% carbon film
	R34	80. 5271	68K Ω 5% carbon film
	R35	80. 5261	10K Ω 5% carbon film
	R36	80. 5261	10K Ω 5% carbon film
	R37	80. 5255	3. 3K Ω 5% carbon film
	R38	80. 5247	680 Ω 5% carbon film
	R39	80. 5249	1K Ω 5% carbon film
	R40	80. 5256	3. 9K Ω 5% carbon film
	R41	80. 5261	10K Ω 5% carbon film
	R42	80. 5249	1K Ω 5% carbon film
	R43	80. 5273	0. 1M Ω 5% carbon film
	R44	80. 5257	4. 7K Ω 5% carbon film
	R45	80. 5255	3. 3K Ω 5% carbon film
	R46	80. 5273	0. 1M Ω 5% carbon film
	R47	80. 5254	2. 7K Ω 5% carbon film
	R48		
	R49		
	R50	80. 5258	5. 6K Ω 5% carbon film
	R51	80. 5248	820 Ω 5% carbon film
	R52	80. 5248	820 Ω 5% carbon film
	R53	80. 5247	680 Ω 5% carbon film
	R54	80. 5247	680 Ω 5% carbon film
	R55	80. 5261	10K Ω 5% carbon film
	R56	80. 5261	10K Ω 5% carbon film
	R57	80. 5255	3. 3K Ω 5% carbon film
	R58	80. 5246	560 Ω 5% carbon film
	R59	80. 5252	1. 8K Ω 5% carbon film
	R60	80. 5267	33K Ω 5% carbon film
	R61	80. 5267	33K Ω 5% carbon film
	R62	80. 5252	1. 8K Ω 5% carbon film
	R63	80. 5249	1K Ω 5% carbon film
	R64		
	R65		
	R66		
	R67		
	R68		
	R69		
	R70		
	R71		
	R72		
	R73		
	R74		
	R75		
	R76		
	R77		
	R78		
	R79		
	R80		
	R81		
	R82		
	R83		
	R84		
	R85		
	R86		
	R87		
	R88		
	R89		
	R90		
	R91		
	R92		
	R93		
	R94		
	R95		
	R96		
	R97		
	R98		
	R99		
	R100		

TR782

ONE RECEIVER

ONE MODULATOR

X401. 650



TERM	FREQ	HZ
1	825	
2	1010	
3	1240	
4	1435	
5	1520	
6	1750	
7	1860	
8	1980	
9	2000	
10	2135	
11	2280	
12	2450	

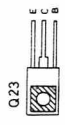
VOLTAGES WITH $I_{V_{in}}$ 1800Hz = 55mV
 VOLTAGES WITHOUT $I_{V_{in}}$ 0V

Q2, Q4, Q5, Q6, Q7, Q8, Q9, Q10, Q12, Q13, Q14, Q15, Q16, Q17, Q18, Q21, Q22

Q1, Q3, Q11, Q19, Q20



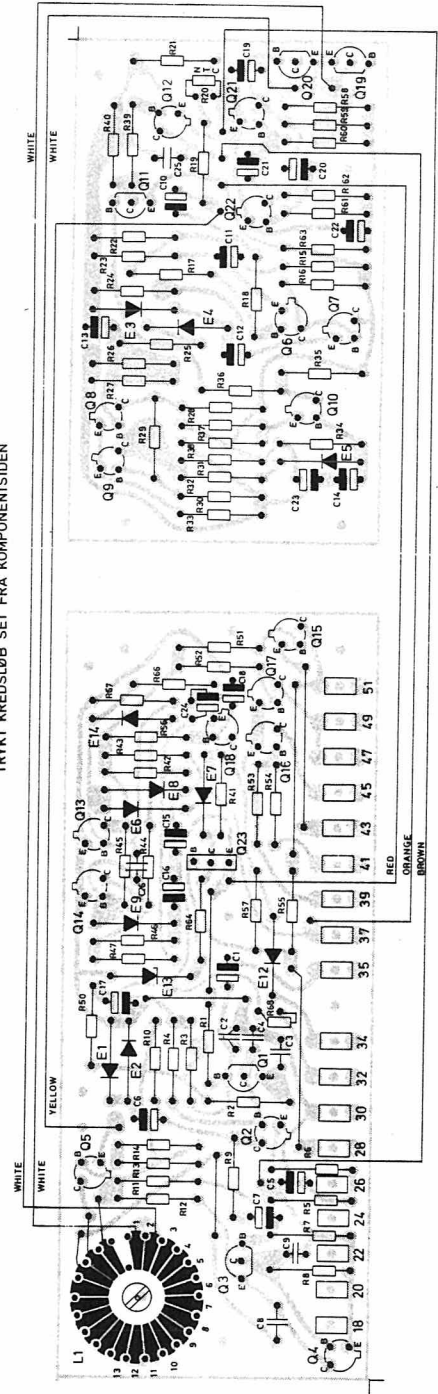
BOTTOM VIEW
 SET FRA BUNDEN



VOLTAGE REG
 SPÄNDINGSREG.

AF GATES
 ASTABLE MV
 ASTABIL MV

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
 TRYKT KREDSLØB SET FRA KOMPONENTSIDEN



AF MUTING
 LF BURNING

32 LS IN OUT
 HT IND UD

45 OCCUPIED
 OPTAGET

51 KEY LOCK
 NÅL

52 TAST SPKR
 TAST

53 AUTO RADIO MUTING
 AUTO

54 AUTO RADIO BURNING
 AUTO

39 LAMP CHASSIS

41 65 IN
 50 IND

30 0V

37 ALARM

28 +13.6V

34 AF MUTING
 LF BURNING

TYPE	NO.	CODE	DATA
TR783		10. 2452	Tone Receiver
	C1	73. 5126	4. 7μF 20% tantal
	C2	76. 5069	1nF 10% polyester. FL
	C3	76. 5072	47nF 10% polyester. FL
	C4	76. 5059	2. 2nF 10% polyester FL
	C5	73. 5124	47μF 20% tantal
	C6	73. 5124	47μF 20% tantal
	C7	73. 5126	4. 7μF 20% tantal
	C8	76. 5068	0. 1μF 1% polystyry TB
	C9	76. 5070	10nF 10% polyester. FL
	C10	73. 5114	1μF 20% tantal
	C11	73. 5124	47μF 20% tantal
	C12	73. 5126	4. 7μF 20% tantal
	C13	73. 5109	10μF 20% tantal
	C14	73. 5124	47μF 20% tantal
	C15	73. 5089	0. 1μF 20% tantal
	C16	73. 5089	0. 1μF 20% tantal
	C17	73. 5109	10μF 20% tantal
	C18	73. 5114	1μF 20% tantal
	C19	73. 5124	47μF 20% tantal
	C20	73. 5109	10μF 20% tantal
	C21	73. 5109	10μF 20% tantal
	C22	73. 5124	47μF 20% tantal
	C23	73. 5127	22μF 20% tantal
	C24	73. 5089	0. 1μF 20% tantal
	C25	76. 5070	10nF 10% polyester. FL
	C26	76. 5070	10nF 10% polyester. FL
	R1	80. 5266	27KΩ 5% carbon film
	R2	80. 5255	3. 3KΩ 5% carbon film
	R3	80. 5268	39KΩ 5% carbon film
	R4	80. 5253	2. 2KΩ 5% carbon film
	R5	80. 5246	560Ω 5% carbon film
	R6	80. 5240	180Ω 5% carbon film
	R7	80. 5257	4. 7KΩ 5% carbon film
	R8	80. 5253	2. 2KΩ 5% carbon film
	R9	80. 5267	33KΩ 5% carbon film
	R10	80. 5253	2. 2KΩ 5% carbon film
	R11	80. 5257	4. 7KΩ 5% carbon film
	R12	80. 5242	270Ω 5% carbon film
	R13	80. 5273	0. 1MΩ 5% carbon film
	R14	80. 5274	0. 12MΩ 5% carbon film
	R15	80. 5259	6. 8KΩ 5% carbon film
	R16	80. 5253	2. 2KΩ 5% carbon film
	R17	80. 5265	22KΩ 5% carbon film
	R18	80. 5253	2. 2KΩ 5% carbon film
	R19	80. 5256	3. 9KΩ 5% carbon film
	R20	89. 5008	1. 5KΩ 20% NTC

TYPE	NO.	CODE	DATA
	R21	80. 5257	4. 7KΩ 5% carbon film
	R22	80. 5253	2. 2KΩ 5% carbon film
	R23	80. 5248	820Ω 5% carbon film
	R24	80. 5249	1 KΩ 5% carbon film
	R25	80. 5253	2. 2KΩ 5% carbon film
	R26	80. 5268	39KΩ 5% carbon film
	R27	80. 52XX	Adjusted
	R28	80. 5256	3. 9KΩ 5% carbon film
	R29	80. 5249	1 KΩ 5% carbon film
	R30	80. 5249	1 KΩ 5% carbon film
	R31	80. 5259	6. 8KΩ 5% carbon film
	R32	80. 5253	2. 2KΩ 5% carbon film
	R33	80. 5241	220Ω 5% carbon film
	R34	80. 5271	68KΩ 5% carbon film
	R35	80. 5261	10KΩ 5% carbon film
	R36	80. 5261	10KΩ 5% carbon film
	R37	80. 5255	3. 3KΩ 5% carbon film
	R38	80. 5247	680Ω 5% carbon film
	R39	80. 5249	1 KΩ 5% carbon film
	R40	80. 5256	3. 9KΩ 5% carbon film
	R41	80. 5261	10KΩ 5% carbon film
	R42	80. 5249	1 KΩ 5% carbon film
	R43	80. 5273	0. 1MΩ 5% carbon film
	R44	80. 5257	4. 7KΩ 5% carbon film
	R45	80. 5255	3. 3KΩ 5% carbon film
	R46	80. 5273	0. 1MΩ 5% carbon film
	R47	80. 5254	2. 7KΩ 5% carbon film
	R48		
	R49		
	R50	80. 5258	5. 6KΩ 5% carbon film
	R51	80. 5248	820Ω 5% carbon film
	R52	80. 5248	820Ω 5% carbon film
	R53	80. 5247	680Ω 5% carbon film
	R54	80. 5247	680Ω 5% carbon film
	R55	80. 5261	10KΩ 5% carbon film
	R56	80. 5261	10KΩ 5% carbon film
	R57	80. 5255	3. 3KΩ 5% carbon film
	R58	80. 5246	560Ω 5% carbon film
	R59	80. 5252	1. 8KΩ 5% carbon film
	R60	80. 5267	33KΩ 5% carbon film
	R61	80. 5267	33KΩ 5% carbon film
	R62	80. 5252	1. 8KΩ 5% carbon film
	R63	80. 5249	1 KΩ 5% carbon film

TONE RECEIVER
TONE MODTAGER

TR783

X401.699/2

PREEMPHASIS
FORBETONING

DRIVER

LIMITER
BEGRÆNSER

Q-MULTIPL.

AMPL. FORST.

EMITTER FOLLOWER
EMITTERFØLGER

DETECTOR
DETEKTOR

SCHMITT TRIG.
FOR SINK

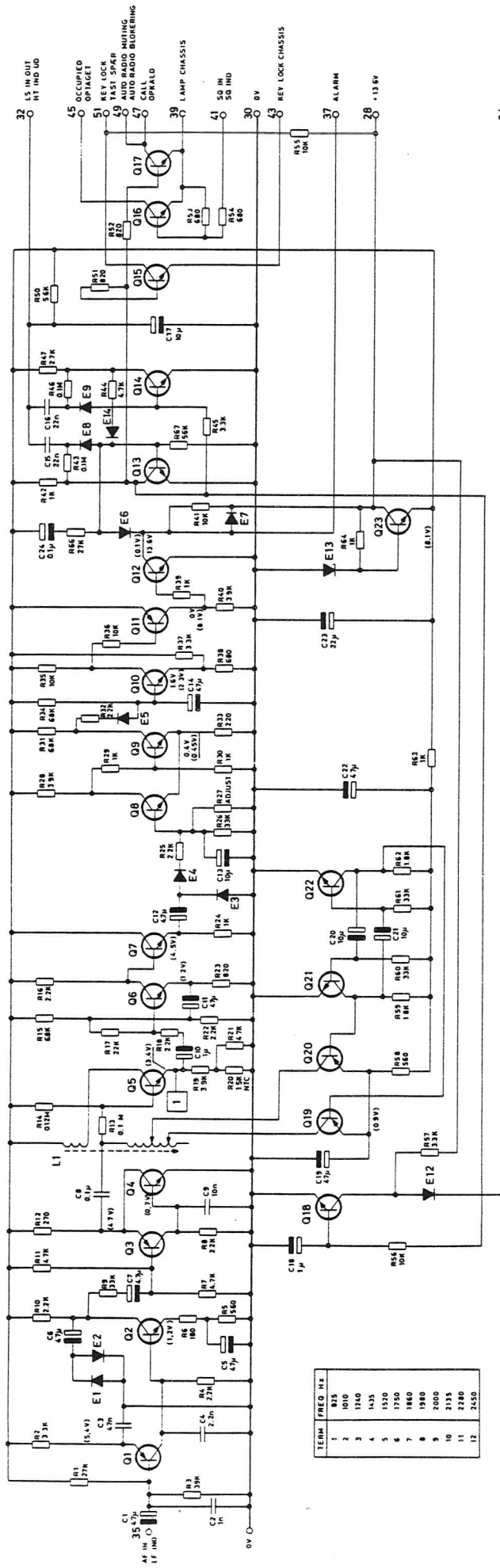
GATE

INVERT.

GATE

BISTAB. MV

3 x SWITCH



TERM	FREQ. MIX
1	825
2	1010
3	1240
4	1525
5	1860
6	2250
7	2700
8	3225
9	3825
10	4500
11	5250
12	6150

AF GATES

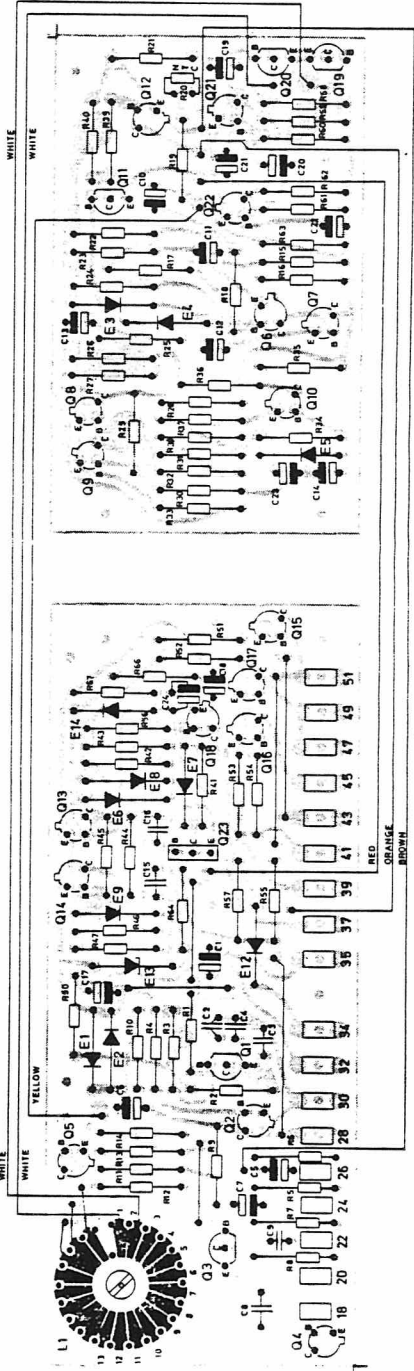
ASTABLE MV
ASTABIL MV

VOLTAGE REG.
SPÆNDINGSREG.

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

VOLTAGES WITH 1 V_{in} 100Hz ±55mV
VOLTAGES WITHOUT 1 V_{in} 0V

Q1 Q3 Q11 Q19 Q20
Q2 Q4 Q5 Q6 Q7 Q8 Q9 Q10 Q12 Q13
Q14 Q15 Q16 Q17 Q18 Q21 Q22



TONE RECEIVER TR783
TONEMODTAGER

D401.231/2

TYPE	NO.	CODE	DATA
TR783		10. 2452	Tone Receiver
	C1	73. 5126	4. 7 μ F 20% tantal
	C2	76. 5069	1nF 10% polyest. FL
	C3	76. 5072	47nF 10% polyest. FL
	C4	76. 5059	2. 2nF 10% polyest. FL
	C5	73. 5124	47 μ F 20% tantal
	C6	73. 5124	47 μ F 20% tantal
	C7	73. 5126	4. 7 μ F 20% tantal
	C8	76. 5068	0. 1 μ F 1% polystyr TB
	C9	76. 5070	10nF 10% polyest. FL
	C10	73. 5114	1 μ F 20% tantal
	C11	73. 5124	47 μ F 20% tantal
	C12	73. 5126	4. 7 μ F 20% tantal
	C13	73. 5109	10 μ F 20% tantal
	C14	73. 5124	47 μ F 20% tantal
	C15	76. 5071	22nF 10% polyest. FL
	C16	76. 5071	22nF 10% polyest. FL
	C17	73. 5109	10 μ F 20% tantal
	C18	73. 5114	1 μ F 20% tantal
	C19	73. 5124	47 μ F 20% tantal
	C20	73. 5109	10 μ F 20% tantal
	C21	73. 5109	10 μ F 20% tantal
	C22	73. 5124	47 μ F 20% tantal
	C23	73. 5127	22 μ F 20% tantal
	C24	73. 5089	0. 1 μ F 20% tantal
	R1	80. 5266	27K Ω 5% carbon film
	R2	80. 5255	3. 3K Ω 5% carbon film
	R3	80. 5268	39K Ω 5% carbon film
	R4	80. 5253	2. 2K Ω 5% carbon film
	R5	80. 5246	560 Ω 5% carbon film
	R6	80. 5240	180 Ω 5% carbon film
	R7	80. 5257	4. 7K Ω 5% carbon film
	R8	80. 5253	2. 2K Ω 5% carbon film
	R9	80. 5267	33K Ω 5% carbon film
	R10	80. 5253	2. 2K Ω 5% carbon film
	R11	80. 5257	4. 7K Ω 5% carbon film
	R12	80. 5242	270 Ω 5% carbon film
	R13	80. 5273	0. 1M Ω 5% carbon film
	R14	80. 5274	0. 12M Ω 5% carbon film
	R15	80. 5259	6. 8K Ω 5% carbon film
	R16	80. 5253	2. 2K Ω 5% carbon film
	R17	80. 5265	22K Ω 5% carbon film
	R18	80. 5253	2. 2K Ω 5% carbon film
	R19	80. 5256	3. 9K Ω 5% carbon film
	R20	89. 5008	1. 5K Ω 20% NTC
	R21	80. 5257	4. 7K Ω 5% carbon film

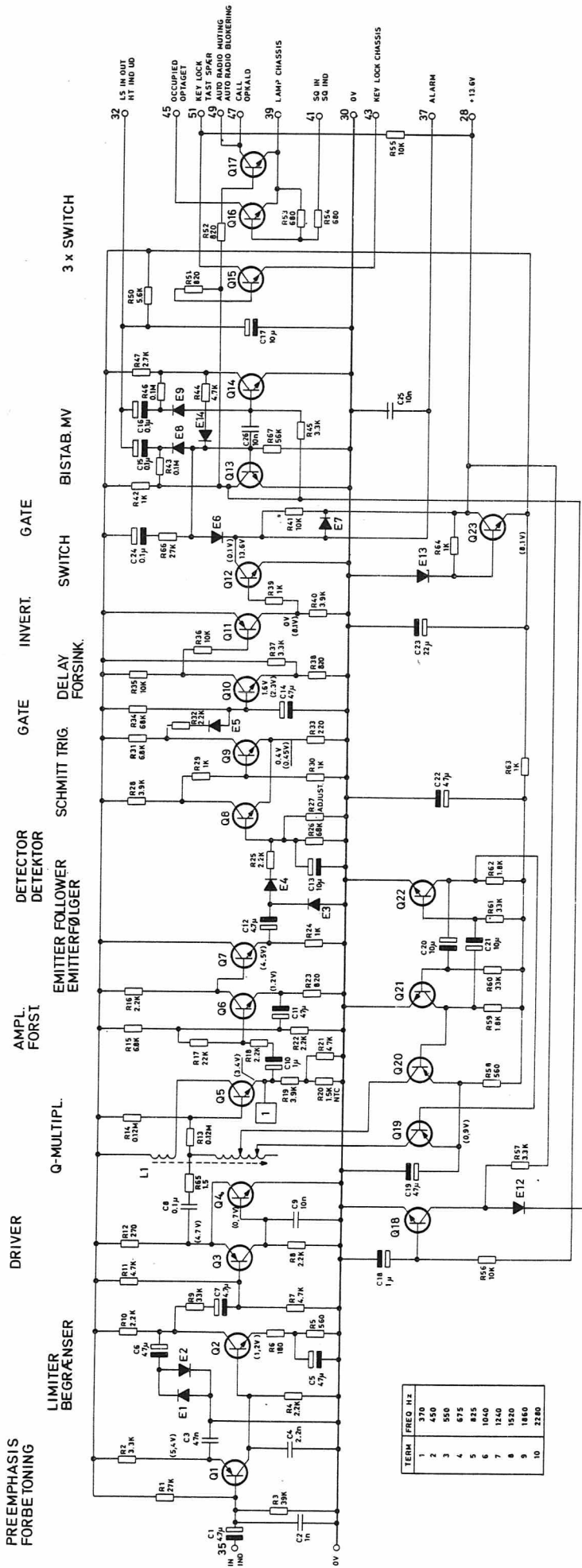
TYPE	NO.	CODE	DATA
	R22	80. 5253	2. 2K Ω 5% carbon film
	R23	80. 5248	820 Ω 5% carbon film
	R24	80. 5249	1K Ω 5% carbon film
	R25	80. 5253	2. 2K Ω 5% carbon film
	R26	80. 5267	33K Ω 5% carbon film
	R27	80. 52XX	Adjusted
	R28	80. 5256	3. 9K Ω 5% carbon film
	R29	80. 5249	1K Ω 5% carbon film
	R30	80. 5249	1K Ω 5% carbon film
	R31	80. 5259	6. 8K Ω 5% carbon film
	R32	80. 5253	2. 2K Ω 5% carbon film
	R33	80. 5241	220 Ω 5% carbon film
	R34	80. 5271	68K Ω 5% carbon film
	R35	80. 5261	10K Ω 5% carbon film
	R36	80. 5261	10K Ω 5% carbon film
	R37	80. 5255	3. 3K Ω 5% carbon film
	R38	80. 5247	680 Ω 5% carbon film
	R39	80. 5249	1K Ω 5% carbon film
	R40	80. 5256	3. 9K Ω 5% carbon film
	R41	80. 5261	10K Ω 5% carbon film
	R42	80. 5249	1K Ω 5% carbon film
	R43	80. 5273	0. 1M Ω 5% carbon film
	R44	80. 5257	4. 7K Ω 5% carbon film
	R45	80. 5255	3. 3K Ω 5% carbon film
	R46	80. 5273	0. 1M Ω 5% carbon film
	R47	80. 5254	2. 7K Ω 5% carbon film
	R48		
	R49		
	R50	80. 5258	5. 6K Ω 5% carbon film
	R51	80. 5248	820 Ω 5% carbon film
	R52	80. 5248	820 Ω 5% carbon film
	R53	80. 5247	680 Ω 5% carbon film
	R54	80. 5247	680 Ω 5% carbon film
	R55	80. 5261	10K Ω 5% carbon film
	R56	80. 5261	10K Ω 5% carbon film
	R57	80. 5255	3. 3K Ω 5% carbon film
	R58	80. 5246	560 Ω 5% carbon film
	R59	80. 5252	1. 8K Ω 5% carbon film
	R60	80. 5267	33K Ω 5% carbon film
	R61	80. 5267	33K Ω 5% carbon film
	R62	80. 5252	1. 8K Ω 5% carbon film
	R63	80. 5249	1K Ω 5% carbon film
	R64		
	R65		
	R66		
	R67		
	R68		
	R69		
	R70		
	R71		
	R72		
	R73		
	R74		
	R75		
	R76		
	R77		
	R78		
	R79		
	R80		
	R81		
	R82		
	R83		
	R84		
	R85		
	R86		
	R87		
	R88		
	R89		
	R90		
	R91		
	R92		
	R93		
	R94		
	R95		
	R96		
	R97		
	R98		
	R99		
	R100		

TR783

TR783

TR783

X401. 699



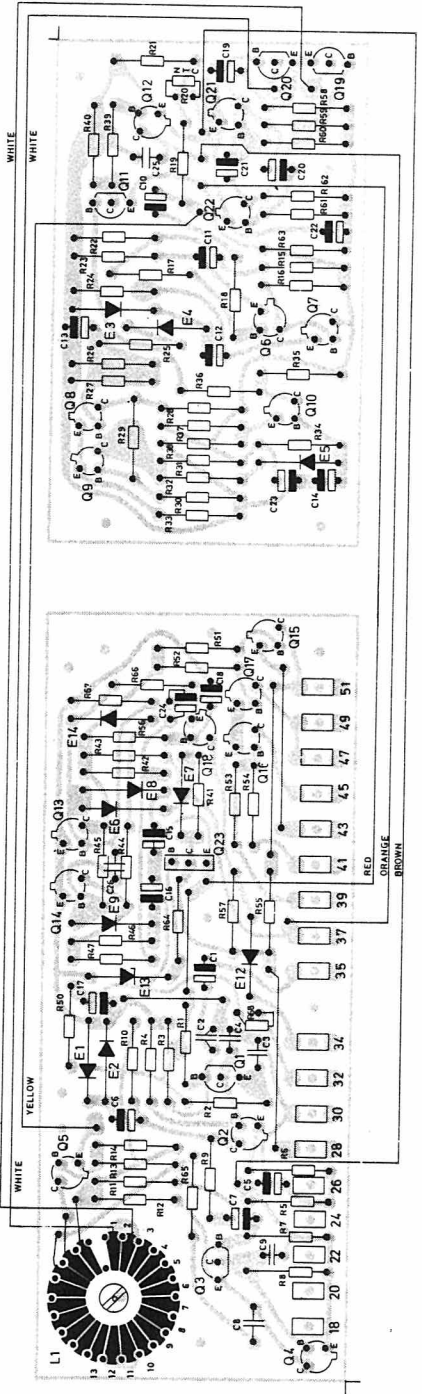
34 AF MUTING
LF BLOKERING

VOLTAGE REG.
SPÆNDINGSREG.

AF GATES
ASTABLE MV
ASTABIL MV

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

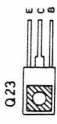
VOLTAGES WITH () V_{in} 1000Hz ~ 55mV
VOLTAGES WITHOUT () V_{in} 0V



Q1 Q3 Q11 Q19 Q20
Q2 Q4 Q5 Q6 Q7 Q8 Q9 Q10 Q12 Q13
Q14 Q15 Q16 Q17 Q18 Q21 Q22

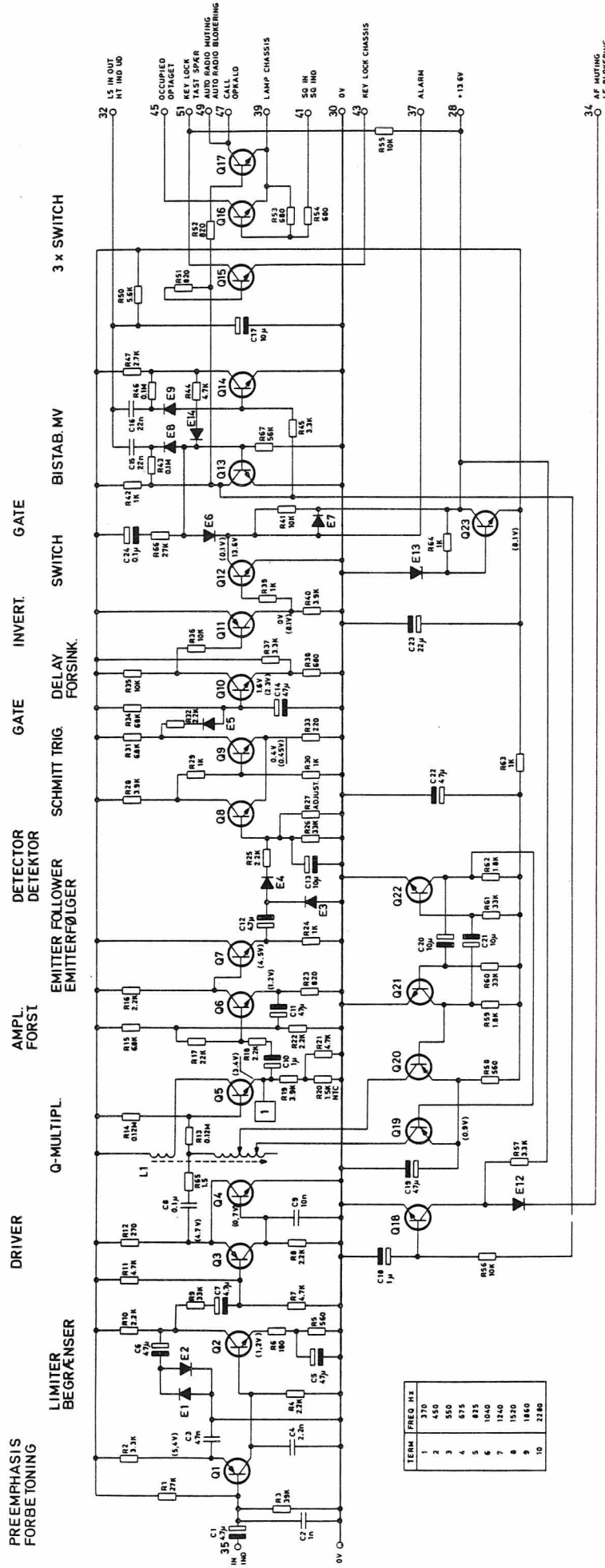


BOTTOM VIEW
SET FRA BUNDEN



WHITE
WHITE
YELLOW
RED
ORANGE
BROWN

TONE RECEIVER TR785
TONEMODTAGER



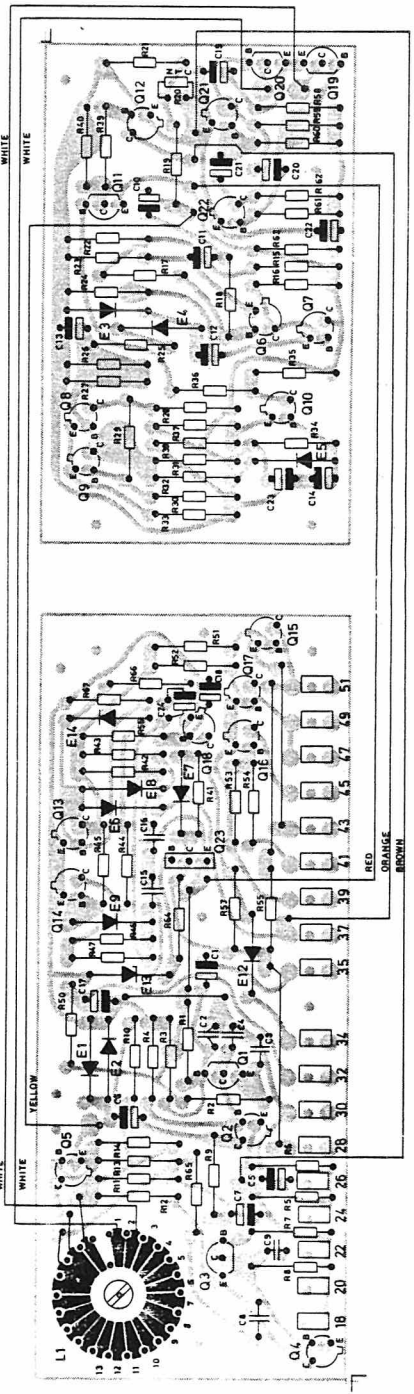
VOLTAGE REG. SPENDINGREG.

AF GATES

ASTABLE MV ASTABIL MV

VOLTAGES WITH () V_{cc} REGIM = 55 mV
 VOLTAGES WITHOUT () V_{cc} 0V

Q1, Q3, Q11, Q19, Q20
 Q2, Q4, Q5, Q6, Q7, Q8, Q9, Q10, Q12, Q13,
 Q14, Q15, Q16, Q17, Q18, Q21, Q22



TONE RECEIVER TR785
 TONEMODTAGER

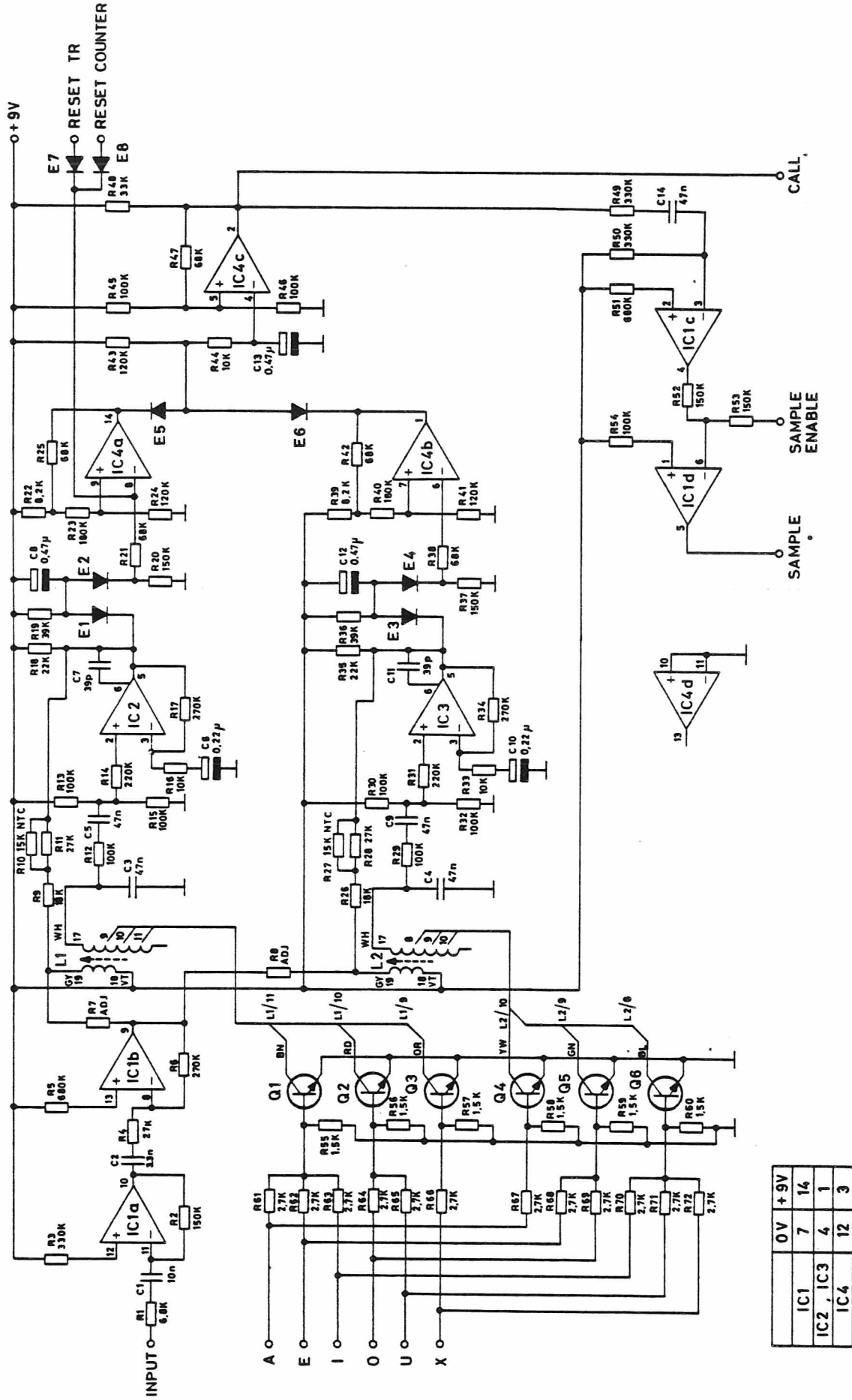
D401.230/2

TYPE	NO.	CODE	DATA
TR785		10.2451	Tone Receiver
	C1	73.5126	4.7μF 20% tantal
	C2	76.5069	1nF 10% polyest. FL
	C3	76.5072	47nF 10% polyest. FL
	C4	76.5059	2.2nF 10% polyest. FL
	C5	73.5124	47μF 20% tantal
	C6	73.5124	47μF 20% tantal
	C7	73.5126	4.7μF 20% tantal
	C8	76.5068	0.1μF 1% polystyr TB
	C9	76.5070	10nF 10% polyest. FL
	C10	73.5114	1μF 20% tantal
	C11	73.5124	47μF 20% tantal
	C12	73.5126	4.7μF 20% tantal
	C13	73.5109	10μF 20% tantal
	C14	73.5124	47μF 20% tantal
	C15	76.5071	22nF 10% polyest. FL
	C16	76.5071	22nF 10% polyest. FL
	C17	73.5109	10μF 20% tantal
	C18	73.5114	1μF 20% tantal
	C19	73.5124	47μF 20% tantal
	C20	73.5109	10μF 20% tantal
	C21	73.5109	10μF 20% tantal
	C22	73.5124	47μF 20% tantal
	C23	73.5127	22μF 20% tantal
	C24	73.5089	0.1μF 20% tantal
	R1	80.5266	27KΩ 5% carbon film
	R2	80.5255	3.3KΩ 5% carbon film
	R3	80.5268	39KΩ 5% carbon film
	R4	80.5253	2.2KΩ 5% carbon film
	R5	80.5246	560Ω 5% carbon film
	R6	80.5240	180Ω 5% carbon film
	R7	80.5257	4.7KΩ 5% carbon film
	R8	80.5253	2.2KΩ 5% carbon film
	R9	80.5267	33KΩ 5% carbon film
	R10	80.5253	2.2KΩ 5% carbon film
	R11	80.5257	4.7KΩ 5% carbon film
	R12	80.5242	270Ω 5% carbon film
	R13	80.5274	0.12MΩ 5% carbon film
	R14	80.5274	0.12MΩ 5% carbon film
	R15	80.5259	6.8KΩ 5% carbon film
	R16	80.5253	2.2KΩ 5% carbon film
	R17	80.5265	22KΩ 5% carbon film
	R18	80.5253	2.2KΩ 5% carbon film
	R19	80.5256	3.9KΩ 5% carbon film
	R20	89.5008	1.5KΩ 20% NTC
	R21	80.5257	4.7KΩ 5% carbon film

TYPE	NO.	CODE	DATA
	R22	80.5253	2.2KΩ 5% carbon film
	R23	80.5248	820Ω 5% carbon film
	R24	80.5249	1KΩ 5% carbon film
	R25	80.5253	2.2KΩ 5% carbon film
	R26	80.5267	33KΩ 5% carbon film
	R27	80.52XX	Adjusted
	R28	80.5256	3.9KΩ 5% carbon film
	R29	80.5249	1KΩ 5% carbon film
	R30	80.5249	1KΩ 5% carbon film
	R31	80.5259	6.8KΩ 5% carbon film
	R32	80.5253	2.2KΩ 5% carbon film
	R33	80.5241	220Ω 5% carbon film
	R34	80.5271	68KΩ 5% carbon film
	R35	80.5261	10KΩ 5% carbon film
	R36	80.5261	10KΩ 5% carbon film
	R37	80.5255	3.3KΩ 5% carbon film
	R38	80.5247	680Ω 5% carbon film
	R39	80.5249	1KΩ 5% carbon film
	R40	80.5256	3.9KΩ 5% carbon film
	R41	80.5261	10KΩ 5% carbon film
	R42	80.5249	1KΩ 5% carbon film
	R43	80.5273	0.1MΩ 5% carbon film
	R44	80.5257	4.7KΩ 5% carbon film
	R45	80.5255	3.3KΩ 5% carbon film
	R46	80.5273	0.1MΩ 5% carbon film
	R47	80.5254	2.7KΩ 5% carbon film
	R48		
	R49		
	R50	80.5258	5.6KΩ 5% carbon film
	R51	80.5248	820Ω 5% carbon film
	R52	80.5248	820Ω 5% carbon film
	R53	80.5247	680Ω 5% carbon film
	R54	80.5247	680Ω 5% carbon film
	R55	80.5261	10KΩ 5% carbon film
	R56	80.5261	10KΩ 5% carbon film
	R57	80.5255	3.3KΩ 5% carbon film
	R58	80.5246	560Ω 5% carbon film
	R59	80.5252	1.8KΩ 5% carbon film
	R60	80.5267	33KΩ 5% carbon film
	R61	80.5267	33KΩ 5% carbon film
	R62	80.5252	1.8KΩ 5% carbon film
	R63	80.5249	1KΩ 5% carbon film
	R50	80.5258	5.6KΩ 5% carbon film
	R51	80.5248	820Ω 5% carbon film
	R52	80.5248	820Ω 5% carbon film
	R53	80.5247	680Ω 5% carbon film
	R54	80.5247	680Ω 5% carbon film
	R55	80.5261	10KΩ 5% carbon film
	R56	80.5261	10KΩ 5% carbon film
	R57	80.5255	3.3KΩ 5% carbon film
	R58	80.5246	560Ω 5% carbon film
	R59	80.5252	1.8KΩ 5% carbon film
	R60	80.5267	33KΩ 5% carbon film
	R61	80.5267	33KΩ 5% carbon film
	R62	80.5252	1.8KΩ 5% carbon film
	R63	80.5249	1KΩ 5% carbon film

TR785
TONE RECEIVER
TONE MODULATOR

X401.700



0V	+9V
IC1	7 14
IC2, IC3	4 1
IC4	12 3

TONE RECEIVER TR786

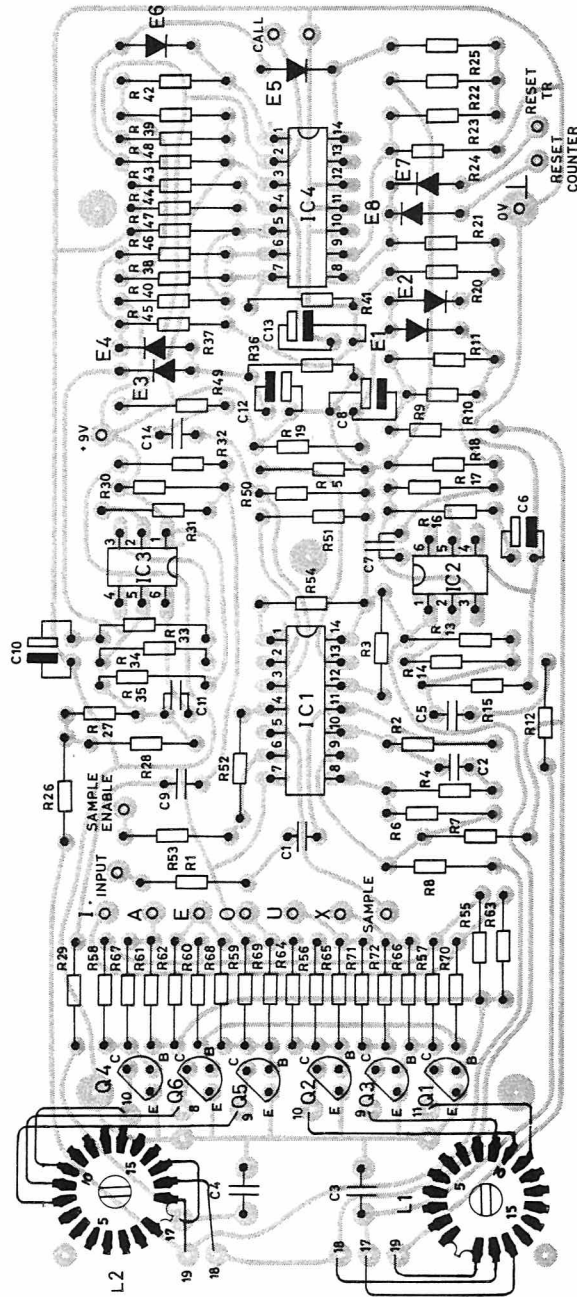
D402.251

TYPE	NO	CODE	DATA
TR786		10. 3371-00	Tone Receiver
	C1	76. 5070	10 nF 10%
	C2	76. 5060	3.3 nF 10%
	C3	76. 5122	47 nF 2%
	C4	76. 5122	47 nF 2%
	C5	76. 5072	0.22 μ F 10%
	C6	74. 5338	39 pF 2%
	C7	74. 5338	39 pF 2%
	C8	73. 5125	0.47 μ F 20%
	C9	76. 5072	47 nF 10%
	C10	73. 5118	0.22 μ F 20%
	C11	74. 5338	39 pF 2%
	C12	73. 5125	0.47 μ F 20%
	C13	73. 5125	0.47 μ F 20%
	C14	76. 5072	47 nF 10%
	R1	80. 5259	6.8 k Ω 5%
	R2	80. 5275	150 k Ω 5%
	R3	80. 5279	330 k Ω 5%
	R4	80. 5266	27 k Ω 5%
	R5	80. 5283	680 k Ω 5%
	R6	80. 5278	270 k Ω 5%
	R7	80. 52xx	ADJ
	R8	80. 52xx	ADJ
	R9	80. 5264	18 k Ω 5%
	R10	89. 5010	15 k Ω 20%
	R11	80. 5266	27 k Ω 5%
	R12	80. 5273	100 k Ω 5%
	R13	80. 5273	100 k Ω 5%
	R14	80. 5277	220 k Ω 5%
	R15	80. 5273	100 k Ω 5%
	R16	80. 5261	10 k Ω 5%
	R17	80. 5278	270 k Ω 5%
	R18	80. 5265	22 k Ω 5%
	R19	80. 5268	39 k Ω 5%
	R20	80. 5275	150 k Ω 5%
	R21	80. 5271	68 k Ω 5%
	R22	80. 5260	8.2 k Ω 5%
	R23	80. 5276	180 k Ω 5%
	R24	80. 5274	120 k Ω 5%
	R25	80. 5271	68 k Ω 5%
	R26	80. 5264	18 k Ω 5%
	R27	89. 5010	15 k Ω 20%
	R28	80. 5266	27 k Ω 5%
	R29	80. 5273	100 k Ω 5%
	R30	80. 5273	100 k Ω 5%
	R31	80. 5277	220 k Ω 5%

TYPE	NO	CODE	DATA
	R32	80. 5273	100 k Ω 5%
	R33	80. 5261	10 k Ω 5%
	R34	80. 5278	270 k Ω 5%
	R35	80. 5265	22 k Ω 5%
	R36	80. 5268	39 k Ω 5%
	R37	80. 5275	150 k Ω 5%
	R38	80. 5271	68 k Ω 5%
	R39	80. 5260	8.2 k Ω 5%
	R40	80. 5276	180 k Ω 5%
	R41	80. 5274	120 k Ω 5%
	R42	80. 5271	68 k Ω 5%
	R43	80. 5274	120 k Ω 5%
	R44	80. 5261	10 k Ω 5%
	R45	80. 5273	100 k Ω 5%
	R46	80. 5273	100 k Ω 5%
	R47	80. 5271	68 k Ω 5%
	R48	80. 5267	33 k Ω 5%
	R49	80. 5279	330 k Ω 5%
	R50	80. 5279	330 k Ω 5%
	R51	80. 5283	680 k Ω 5%
	R52	80. 5275	150 k Ω 5%
	R53	80. 5275	150 k Ω 5%
	R54	80. 5273	100 k Ω 5%
	R55-R60	80. 5251	1.5 k Ω 5%
	R61-R72	80. 5254	2.7 k Ω 5%
	L1-L2	61. 1292	Tone coil
	E1-E8	99. 5237	1 N 4148 Diode
	Q1-Q6	99. 5143	BC 238 Transistor
	IC1	14. 5100	LM 2900 Integrated Circuit
	IC2	14. 5017	TAA 865 Integrated Circuit
	IC3	14. 5017	TAA 865 Integrated Circuit
	IC4	14. 5019	MC 3302 Integrated Circuit

TONE RECEIVER TR786

X402.466



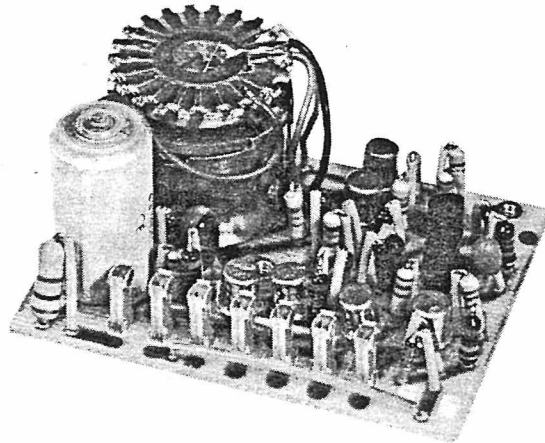
PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE.

TONE RECEIVER TR786

D402.510

TONE TRANSMITTER

TT781 TT783



Description

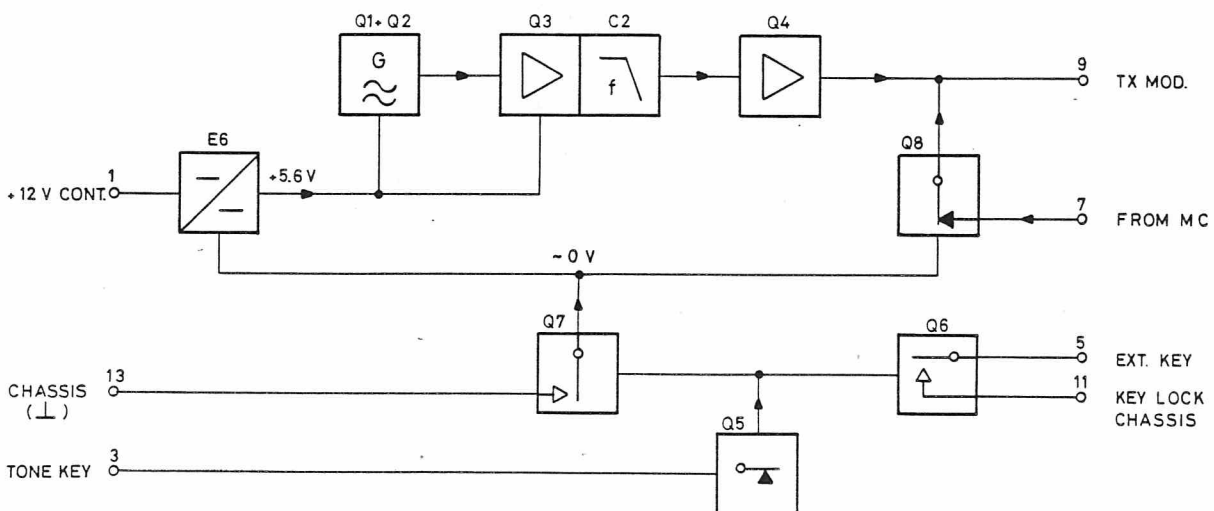
TT781 and TT783 are single tone transmitters for CQM700 series radiotelephones. They are identical except for their tone coils.

tes a tone to seize, and upon termination of the call, to release the telephone circuit. Only the 2400 Hz and the 2900 Hz tones are used.

The TT781 is for use in CQM700 equipment operating on the public telephone service. It genera-

The TT783 can generate any of the 12 tones in the 825 to 2450 Hz series.

BLOCK DIAGRAM of TT781 / TT783 :
(refer to the schematic diagram,
D401.577, for TT783)



TT783 (SHOWN IN STAND BY)

In principle, Q1 and Q2 operate as a differential amplifier in a Hartley type oscillator configuration.

The supply voltage is stabilized with zener diode E6 to keep the oscillator output level constant.

Q3 serves to adjust (attenuate) the signal level and, with C2, to introduce de-emphasis before applying the signal to the output stage, Q4.

Emitter follower Q4 provides a low output impedance to match the input impedance of the modulator.

In stand by, R14 and E2 hold Q5 ON. Q5 holds Q6 and Q7 OFF. With Q7 OFF, there is no ground connection to Q1, Q2, Q3, and Q4. Q8 is forward biased by the high positive potential through R17, thus allowing the microphone signal to pass between terminals 7 and 9.

Depressing the tone key grounds terminal 3 and the positive potential through R14 disappears through E1. Without forward bias, Q5 cuts off and the collector voltage rises, driving Q6 and Q7 ON.

When Q6 goes ON, it establishes a ground path from terminal 11 to terminal 5. This switches the regulator voltage from RX to TX, keying the transmitter.

When Q7 conducts, it completes the ground connection to the tone generator circuits, and the tone signal is applied to the modulator via terminal 9. Q7 also cuts off Q8, preventing any microphone signal from interfering with the tone signal.

When the tone key is released the circuit returns to stand by.

Technical Specification

Power Supply

10.5 V - 16 V

Current Consumption

Stand by: 6 - 10 mA

Activated: 16 - 33 mA

Temperature Range

Operating range: -25°C - $+60^{\circ}\text{C}$

Functioning range: -30°C - $+80^{\circ}\text{C}$

Output Impedance

$600\ \Omega \pm 20\%$

TONE TRANSMITTER TT781

Tone Frequencies

2400, 2900 Hz

Frequency Accuracy

$\leq 0.3\%$

Frequency Stability

$\leq 0.6\%$

Output Level

-21 dBm +1/-0dB (69 mV) at 2400 Hz

Frequency Response

6 dB pr. octave de-emphasis

$f_c = 1000\ \text{Hz}$

Distortion (voice modulation)

$\leq 5\%$

AF Gate Attenuation

$\geq 50\ \text{dB}$

Distortion (tone modulation)

$\leq 3\%$

TONE TRANSMITTER TT783

Tone Frequencies

825, 1010, 1240, 1435, 1520, 1750,
1860, 1980, 2000, 2135, 2280, 2450 Hz.

Frequency Accuracy

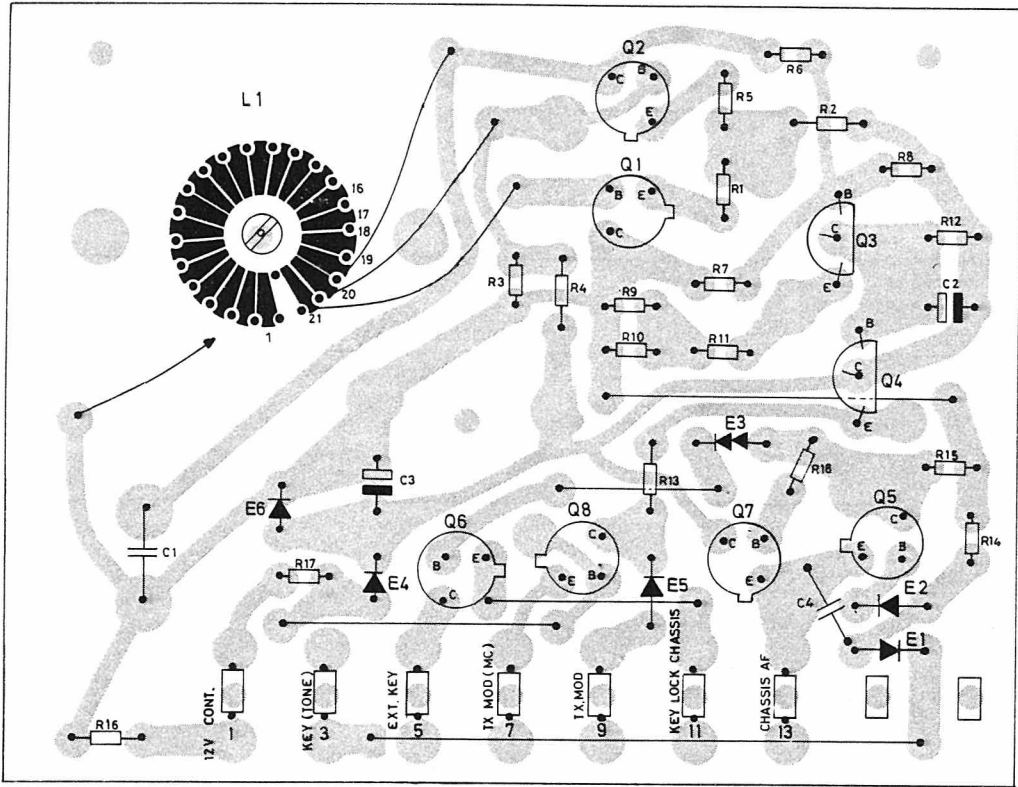
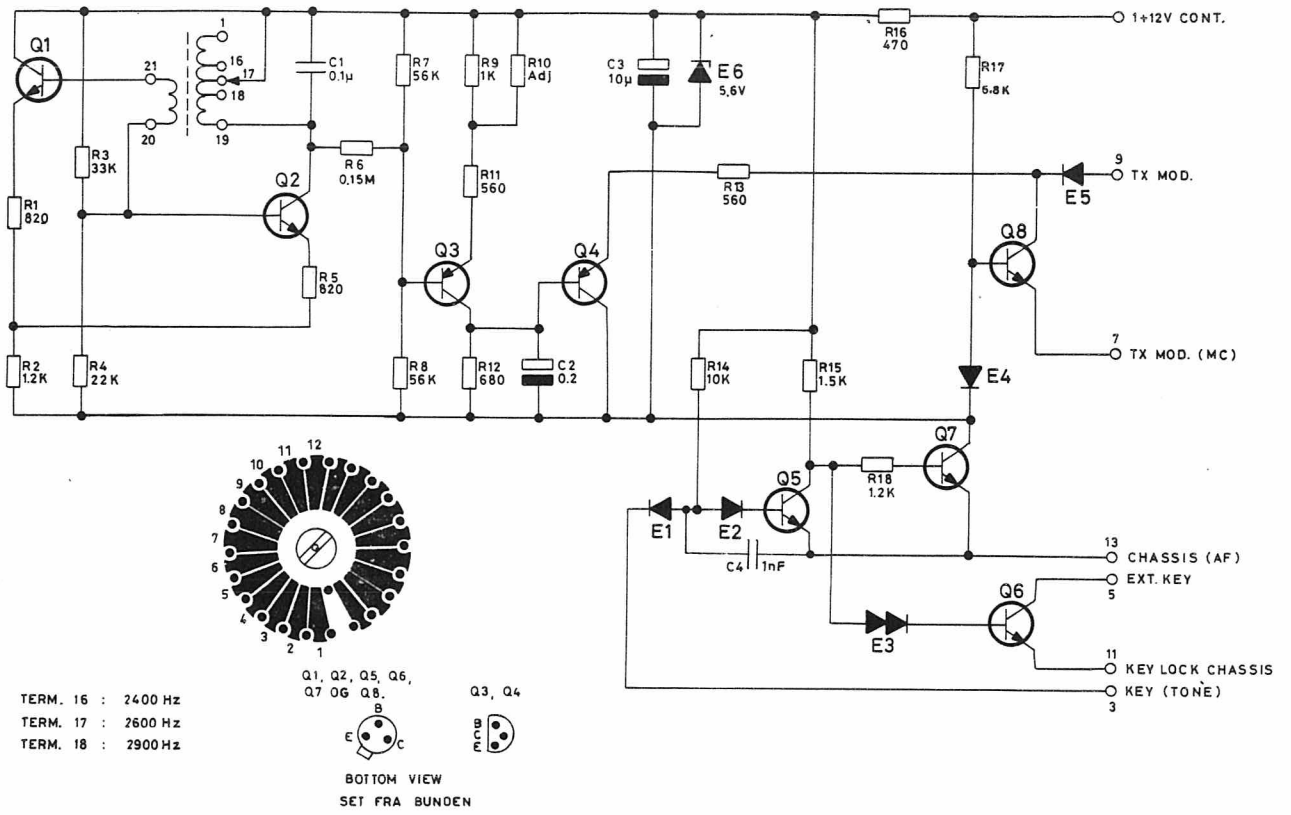
$\leq 0.5\%$

Frequency Stability

$\leq 1\%$

Output Level

-17 dBm +1/0dB (110mV) at 1000 Hz



**TONE TRANSMITTER
TONESENDER TT781**

Storno

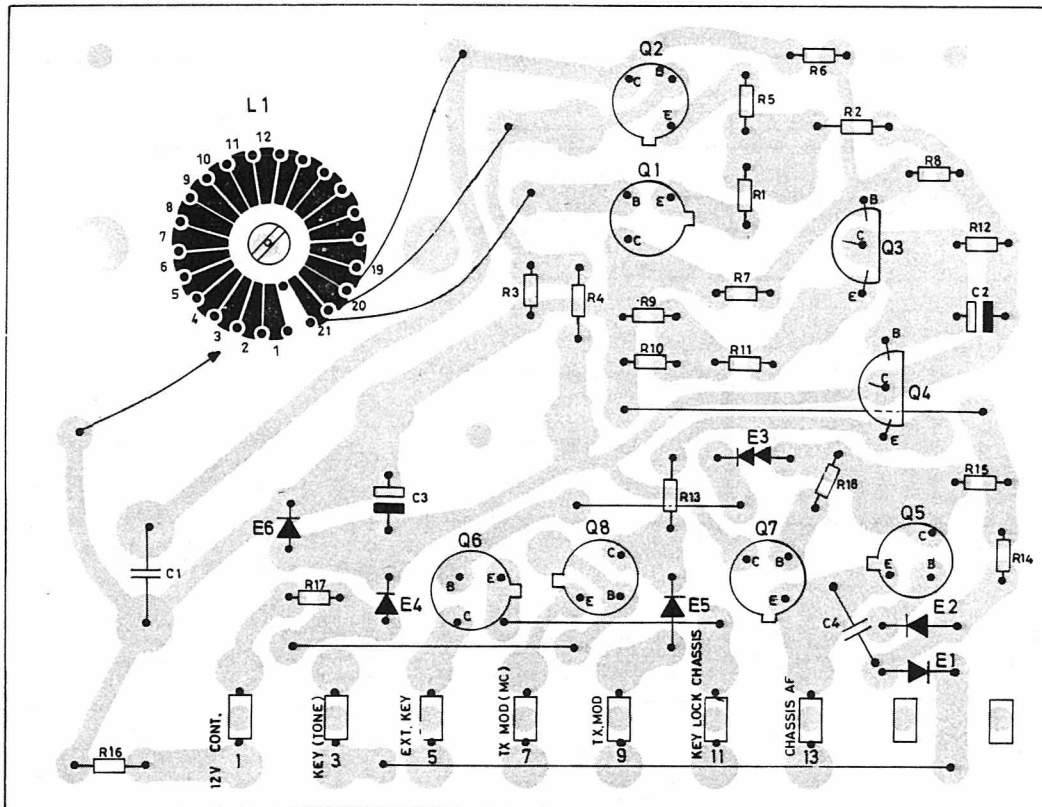
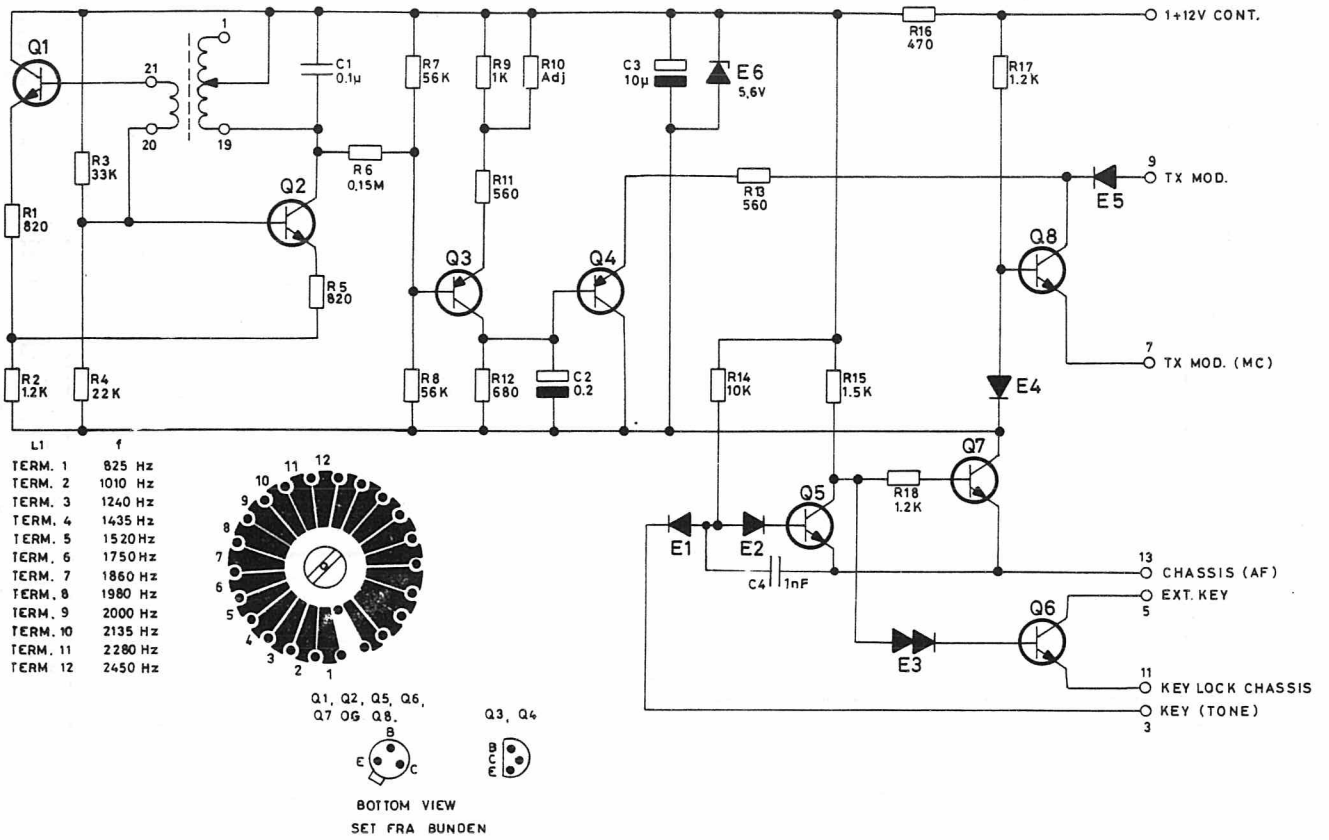
TYPE	NO.	CODE	DATA
TT781			

TONE TRANSMITTER TT781

X401.162

Storno

TYPE	NO.	CODE	DATA
		10.3042-00	Tone Transmitter
	C1	76.5068	0.1 μ F 1% polystyr TB 63V
	C2	73.5118	0.22 μ F 20% tantal 35V
	C3	73.5109	10 μ F 20% tantal 16V
	C4	74.5155	1 nF -20% +80% ceram PL 63V
	R1	80.5248	820 Ω 5% carbon film 1/8W
	R2	80.5250	1.2K Ω 5% " " 1/8W
	R3	80.5267	33K Ω 5% " " 1/8W
	R4	80.5265	22K Ω 5% " " 1/8W
	R5	80.5248	820 Ω 5% " " 1/8W
	R6	80.5275	0.15M Ω 5% " " 1/8W
	R7	80.5270	56K Ω 5% " " 1/8W
	R8	80.5270	56K Ω 5% " " 1/8W
	R9	80.5249	1K Ω 5% " " 1/8W
	R10	80.52xx	Adjusted 5% " " 1/8W
	R11	80.5246	560 Ω 5% " " 1/8W
	R12	80.5247	680 Ω 5% " " 1/8W
	R13	80.5246	560 Ω 5% " " 1/8W
	R14	80.5261	10K Ω 5% " " 1/8W
	R15	80.5251	1.5K Ω 5% " " 1/8W
	R16	80.5445	470 Ω 5% " " 1/8W
	R17	80.5250	1.2K Ω 5% " " 1/8W
	R18	80.5250	1.2K Ω 5% " " 1/8W
	L1	61.1133	Tone coil
	E1	99.5028	IN914 Diode
	E2	99.5028	IN914 Diode
	E3	99.5209	1.5V Stab. Diode
	E4	99.5219	AAZ15 Diode
	E5	99.5219	AAZ15 Diode
	E6	99.5114	5.6V Zenerdiode 5% 1/4W
	Q1	99.5143	BC108 Transistor
	Q2	99.5143	BC108 Transistor
	Q3	99.5144	BC214L Transistor
	Q4	99.5144	BC214L Transistor
	Q5	99.5143	BC108 Transistor
	Q6	99.5143	BC108 Transistor
	Q7	99.5143	BC108 Transistor
	Q8	99.5143	BC108 Transistor



TONE TRANSMITTER TT783
TONESENDER

Storno

Storno

TYPE	NO.	CODE	DATA
TT783		10. 2454	Tone Transmitter
	C1	76. 5068	0, 1 μ F
	C2	73. 5118	0, 22 μ F
	C3	73. 5109	10 μ F
	C4	74. 5155	1 nF
	R1	80. 5248	82 Ω
	R2	80. 5250	1, 2K Ω
	R3	80. 5267	33K Ω
	R4	80. 5265	22K Ω
	R5	80. 5248	82 Ω
	R6	80. 5275	0, 15M Ω
	R7	80. 5270	56K Ω
	R8	80. 5270	56K Ω
	R9	80. 5249	1K Ω
	R10	80. 52XX	Adj.
	R11	80. 5246	56 Ω
	R12	80. 5247	68 Ω
	R13	80. 5246	56 Ω
	R14	80. 5261	10K Ω
	R15	80. 5251	1, 5K Ω
	R16	80. 5445	47 Ω
	R17	80. 5259	8, 8K Ω
	R18	80. 5250	1, 2K Ω
	L1	61. 1158	Tone coil
	E1	99. 5028	1N914 Diode
	E2	99. 5028	1N914 Diode
	E3	99. 5209	1, 5V Stab. Diode
	E4	99. 5219	AAZ15 Diode
	E5	99. 5219	AAZ15 Diode
	E6	99. 5114	5, 6V Zenerdiode 5%
	Q1	99. 5143	BC108 Transistor
	Q2	99. 5143	BC108 Transistor
	Q3	99. 5144	BC214L Transistor
	Q4	99. 5144	BC214L Transistor
	Q5	99. 5143	BC108 Transistor
	Q6	99. 5143	BC108 Transistor
	Q7	99. 5143	BC108 Transistor
	Q8	99. 5143	BC108 Transistor

TYPE NO. CODE DATA

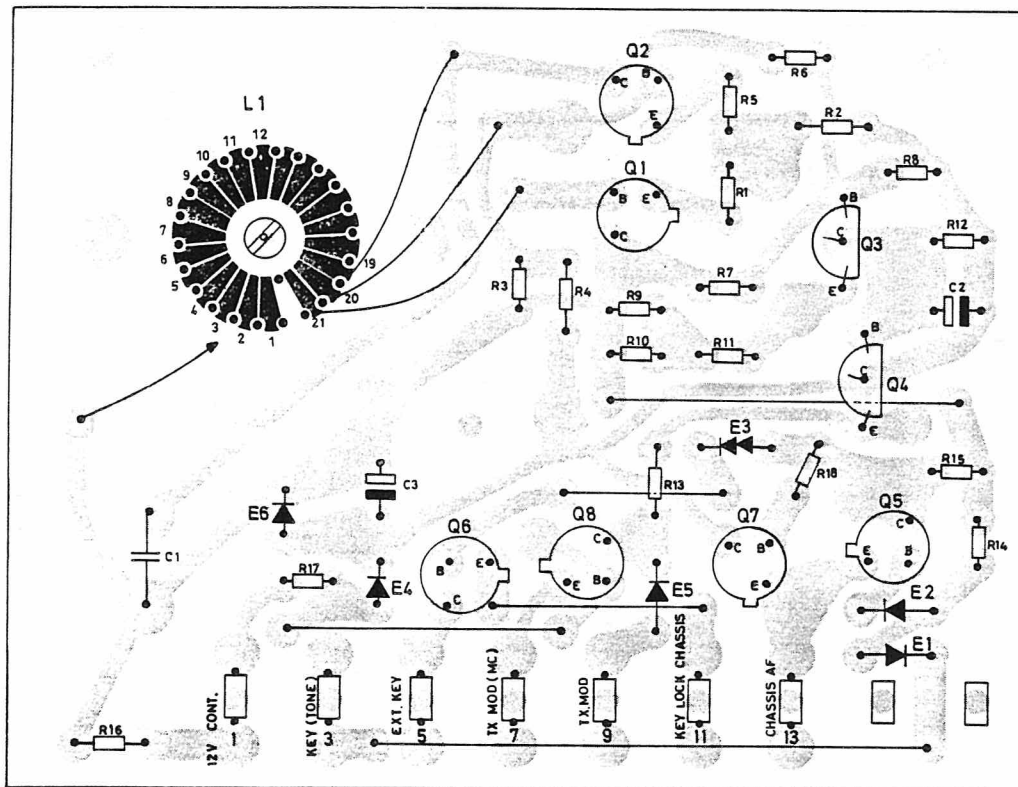
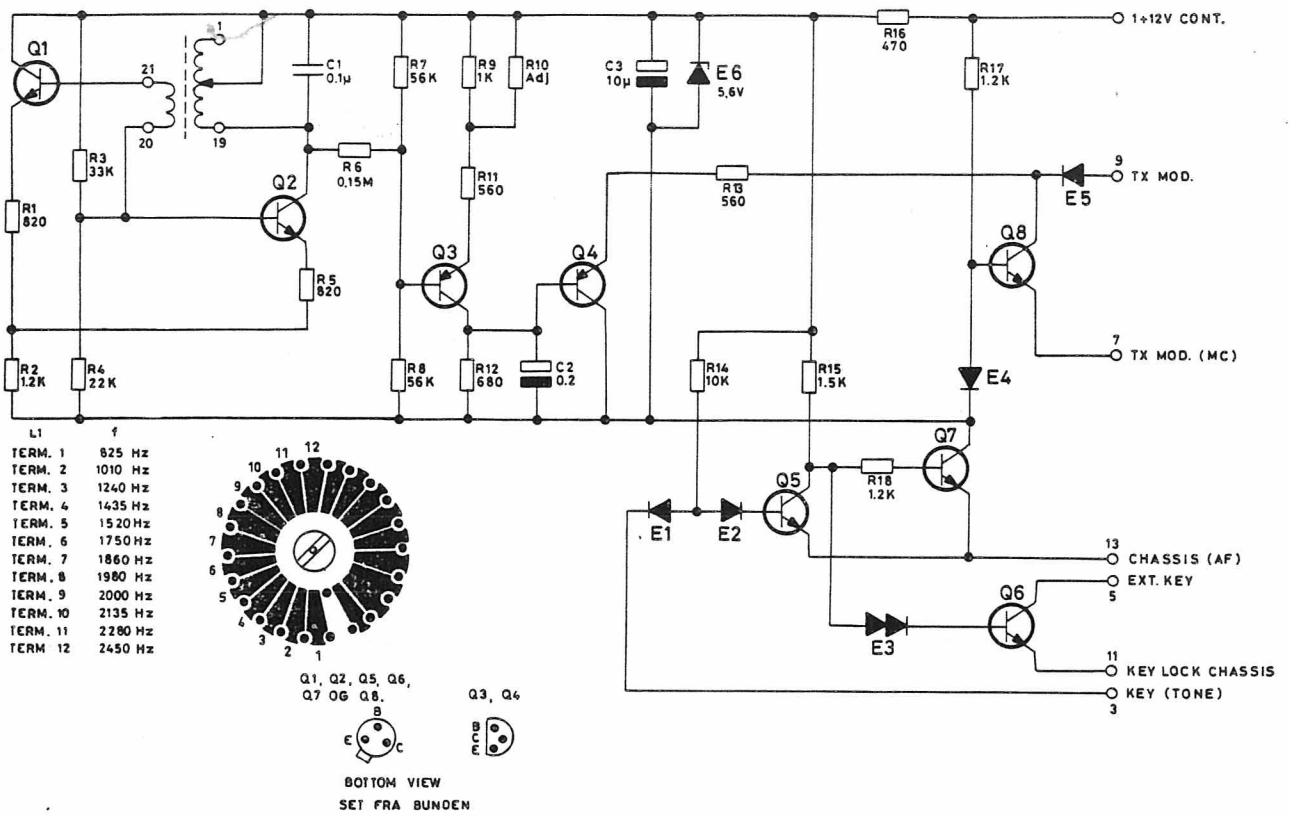
Storno

TT783

ONE TRANSMITTER

ONESENDER

X401.687/2



TONE TRANSMITTER TT783
 TONESENDER

TONE TRANSMITTER

TT784

TT784 is a tone transmitter for the CQM713 P3 radiotelephone.

It can be used for single and double tone operation.

In principle, Q1 and Q2 operate as a differential amplifier in a Hartley type oscillator configuration.

Q3 and Q4 make up an identical oscillator.

The supply voltage is stabilized with zener diode E1 to keep the oscillator output constant.

The oscillators can be set to generate one of the following signals:

- a: 2400 Hz single tone
- b: 2600 Hz single tone
- c: 2400 Hz and 2600 Hz double tone

When one of the oscillators is not to be energised it is inhibited by applying +7.5 V to its inhibit terminal.

Q5 serves to adjust (attenuate) the signal level and, with C3, to introduce de-emphasis before applying the signal to the output stage, Q6.

Emitter follower Q6 provides low impedance to match the input impedance of the modulator.

In stand by, R21 and E5 hold Q7 ON. Q7 holds Q8 and Q9 OFF. With Q8 OFF, there is no ground connection to Q1, Q2, Q3, Q4, Q5, and Q6. Q10 is forward biased by the high positive potential through R23, thus allowing the microphone signal to pass between terminals 7 and 9.

Depressing the tone key grounds terminal 3 and the positive potential through R21 disappears through E6. Without forward bias, Q7 cuts off and the collector voltage rises, driving Q8 and Q9 ON.

When Q9 goes ON, it establishes a ground path from terminal 11 to terminal 5. This switches the regulator voltage from RX to TX, keying the transmitter.

When Q8 conducts, it completes the ground connection to the tone generator circuits, and the tone signal is applied to the modulator via terminal 9. Q8 also cuts off Q10; preventing any microphone signal from interfering with the tone signal.

When the tone key is released the circuit returns to stand by.

Technical Specifications

Power Supply

10.5 - 16 V

Current Consumption

Stand by: 5 - 10 mA

Activated: 10 - 25 mA

Temperature Range

-10°C - +50°C

Tone Combinations

a: 2400 Hz

b: 2600 Hz

c: 2400 Hz + 2600 Hz

Frequency Accuracy

$\leq \pm 0.1\%$

Frequency Stability

$\leq \pm 0.5\%$

Frequency Response

6 dB/octave de-emphasis

$f_c = 1000 \text{ Hz}$

Output Impedance

$600 \Omega \pm 20\%$

Storno

Storno

Output Level

Adjustable

Nominal: 2400 Hz - 39.5 mV

2600 Hz - 36.5 mV

Distortion (tone modulation)

$\leq 3\%$

Distortion (voice modulation)

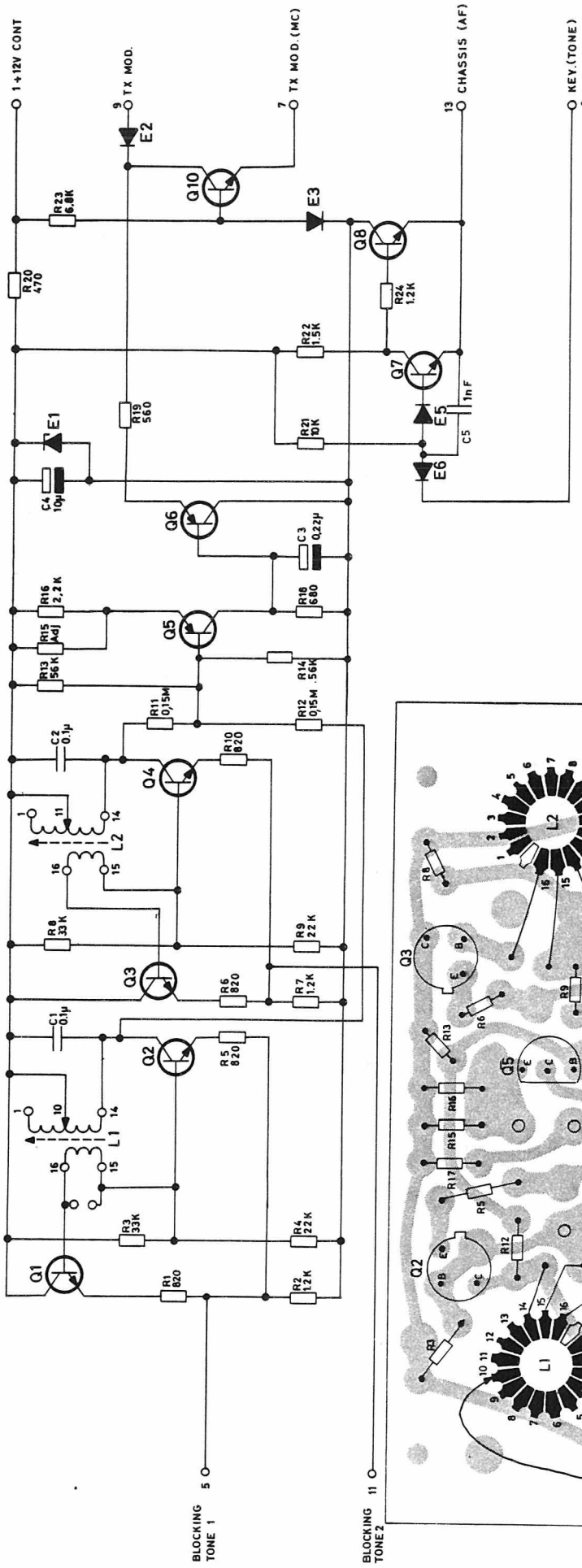
$\leq 5\%$

AF Gate Attenuation

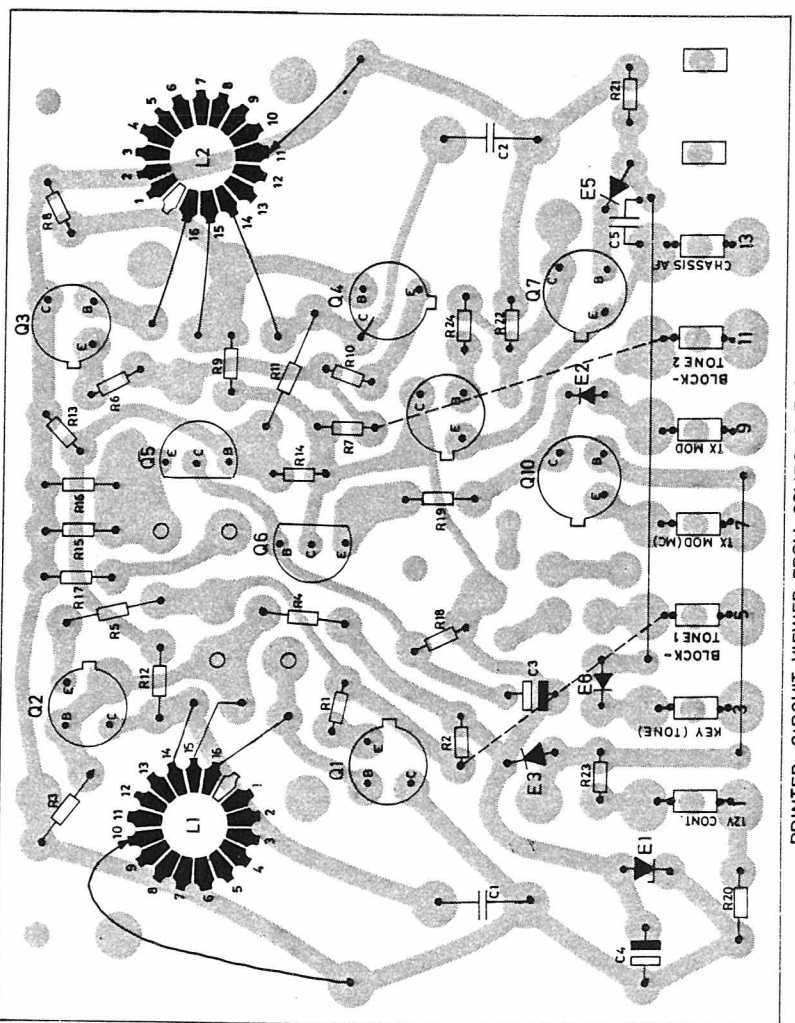
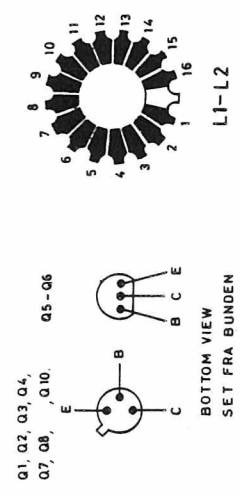
≥ 50 dB

Dimensions

43.2 x 56 x 28 mm



TERM.	FREQ.
1	1060 Hz
2	1160 -
3	1270 -
4	1400 -
5	1530 -
6	1670 -
7	1830 -
8	2000 -
9	2200 -
10	2400 -
11	2600 -
12	2900 -



TONE TRANSMITTER T784
TONESENDER

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

TYPE	NO	CODE	DATA
		10. 3372	Tone Transmitter TT784
C1		76. 5068	0. 1 μF 1% polystyr
C2		76. 5068	0. 1 μF 1% "
C3		73. 5118	0. 22 μF 20% tantal
C4		73. 5109	10 μF 20% "
C5		74. 5155	1 nF -20/+80% ceram PL
R1		80. 5248	820 Ω 5% carbon film
R2		80. 5250	1. 2 kΩ 5% "
R3		80. 5267	33 kΩ 5% "
R4		80. 5265	22 kΩ 5% "
R5		80. 5248	820 Ω 5% "
R6		80. 5248	820 Ω 5% "
R7		80. 5250	1. 2 kΩ 5% "
R8		80. 5267	33 kΩ 5% "
R9		80. 5265	22 kΩ 5% "
R10		80. 5248	820 Ω 5% "
R11		80. 5275	150 kΩ 5% "
R12		80. 5275	150 kΩ 5% "
R13		80. 5270	56 kΩ 5% "
R14		80. 5270	56 kΩ 5% "
R15		80. 52xx	ADJ 5% "
R16		80. 5253	2. 2 kΩ 5% "
R18		80. 5247	680 Ω 5% "
R19		80. 5246	560 Ω 5% "
R20		80. 5445	470 Ω 5% "
R21		80. 5261	10 kΩ 5% "
R22		80. 5251	1. 5 kΩ 5% "
R23		80. 5259	6. 8 kΩ 5% "
R24		80. 5050	1. 2 kΩ 5% "
L1		61. 1157	Tone Coil
L2		61. 1157	" "
E1		99. 5114	Zenerdiode 5. 6 V 5%
E2		99. 5219	AAZ 15 Diode
E3		99. 5219	AAZ 15 "
E5		99. 5028	1 N 914 "
E6		99. 5028	1 N 914 "
Q1		99. 5143	BC 108 Transistor
Q2		99. 5143	BC 108 Transistor
Q3		99. 5143	BC 108 Transistor
Q4		99. 5143	BC 108 Transistor
Q5		99. 5144	BC 214 L Transistor
Q6		99. 5144	BC 214 L Transistor

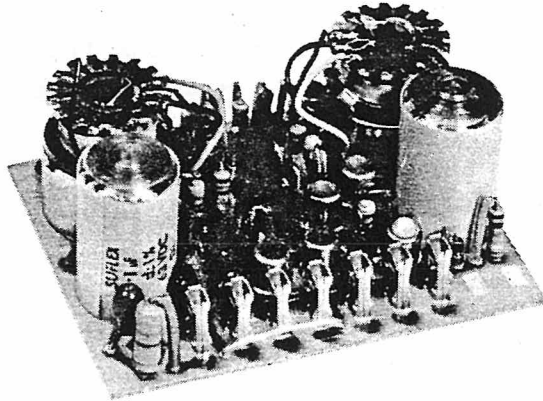
TYPE	NO	CODE	DATA
	Q7	99. 5143	BC 108 Transistor
	Q8	99. 5143	BC 108 Transistor
	Q10	99. 5143	BC 108 Transistor

TONE TRANSMITTER TT784

X402. 543

TONE TRANSMITTER

TT7812 TT7813 TT7814



Description

TT7812 is a tone transmitter for CQM700 series radiotelephones. It can be used for single or double tone operation.

In principle, Q1 and Q2 operate as a differential amplifier in a Hartley type oscillator configuration. Q3 and Q4 make up an identical oscillator. The supply voltage is stabilized with zener diode E1 to keep the oscillator output level constant.

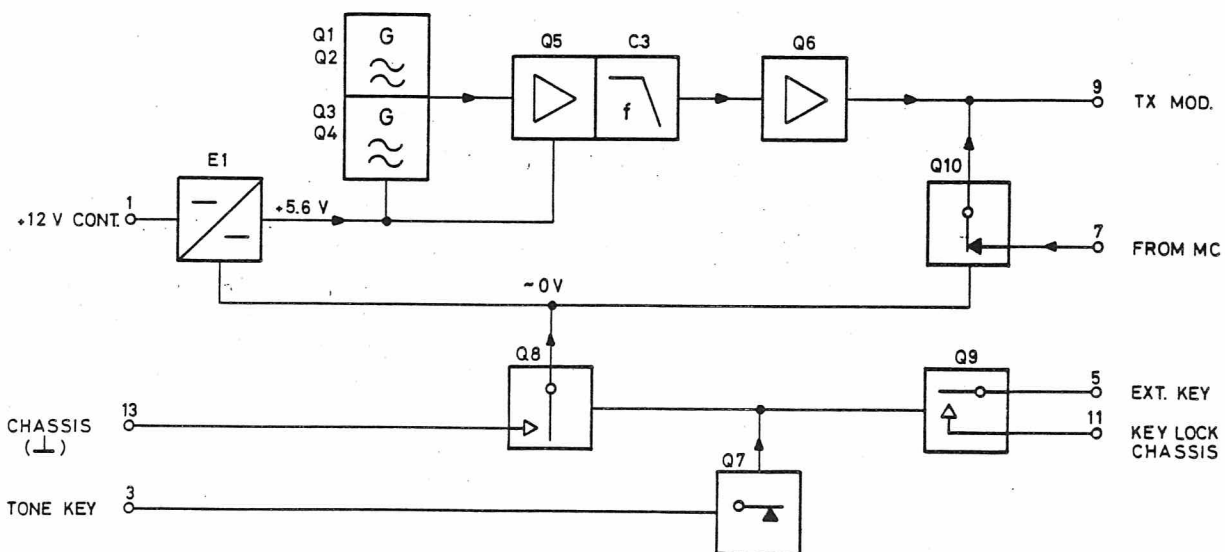
Each oscillator can be set to generate any one of the 12 tones in the standard Storno tone series of 1060 Hz to 2900 Hz. For single tone transmission the feedback winding of one of the

oscillator coils must be shorted out (refer to diagram D401.556).

Except for tone coil L2, TT7812, TT7813, and TT7814 are identical.

TT7813 : (refer to diagram D401.774) Coil L2 accommodates the tone series of 570 Hz to 1530 Hz.

TT7814 : (refer to diagram D401.775) Coil L2 accommodates the tone series of 615 Hz to 970 Hz.



TT7812, TT7813, TT7814 (IN STAND BY)

The remainder of this description applies to all three tone transmitters alike.

Q5 serves to adjust (attenuate) the signal level and, with C3, to introduce de-emphasis before applying the signal to the output stage, Q6.

Emitter follower Q6 provides a low output impedance to match the input impedance of the modulator.

In stand by, R21 and E5 hold Q7 ON. Q7 holds Q8 and Q9 OFF. With Q8 OFF, there is no ground connection to Q1, Q2, Q3, Q4, Q5, and Q6. Q10 is forward biased by the high positive potential through R23, Thus allowing the microphone signal to pass between terminals 7 and 9.

Depressing the tone key grounds terminal 3

and the positive potential through R21 disappears through E6. Without forward bias, Q7 cuts off and the collector voltage rises, driving Q8 and Q9 ON.

When Q9 goes ON, it establishes a ground path from terminal 11 to terminal 5. This switches the regulator voltage from RX to TX, keying the transmitter.

When Q8 conducts, it completes the ground connection to the tone generator circuits, and the tone signal is applied to the modulator via terminal 9. Q8 also cuts off Q10, preventing any microphone signal from interfering with the tone signal.

When the tone key is released the circuit returns to stand by.

Technical Specification

Power Supply

10.5 - 16 V

Current Consumption

Stand by: 6 - 10 mA

Activated: 16 - 33 mA

Ambient Temperature

Operating range: -25°C - $+60^{\circ}\text{C}$

Functioning range: -30°C - $+80^{\circ}\text{C}$

Frequency Accuracy

$\leq 0.5\%$

Frequency Stability

$\leq 1\%$

Frequency Response

6 dB pr. octave de-emphasis

$f_c = 1000$ Hz.

Output Impedance

$600 \Omega \pm 20\%$

Output Level

Single tone: -17 dBm ± 1 /-0 dB (110mV) at 1000 Hz.

Double tone: -17 dBm ± 1 /-0 dB (110mV) at 1000 Hz.
(each tone 55 mV)

Distortion (tone modulation)

$\leq 5\%$

Distortion (voice modulation)

$\leq 5\%$

AF Gate Attenuation

≥ 50 dB

TONE TRANSMITTER TT7812

Tone Frequencies

1060, 1160, 1270, 1400, 1530, 1670, 1830, 2000, 2200, 2400, 2600, 2900 Hz.

TONE TRANSMITTER TT7813

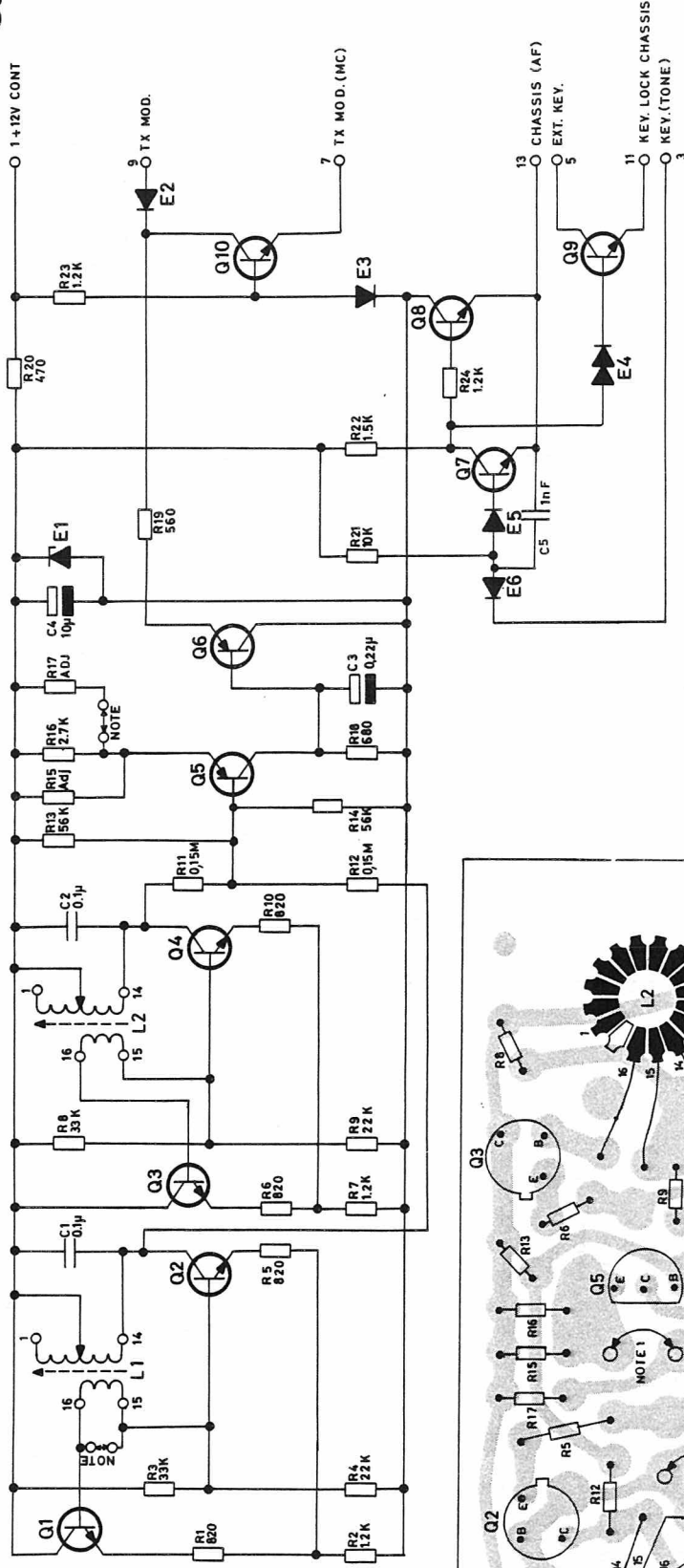
Tone Frequencies

- a. 1060, 1160, 1270, 1400, 1530, 1670, 1830, 2000, 2200, 2400, 2600, 2900 Hz.
- b. 570, 650, 740, 850, 1060, 1160, 1270, 1400, 1530 Hz.

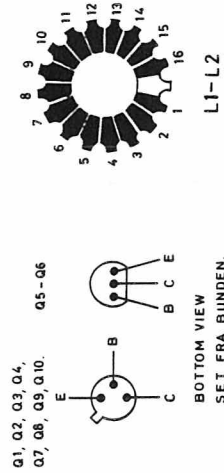
TONE TRANSMITTER TT7814

Tone Frequencies

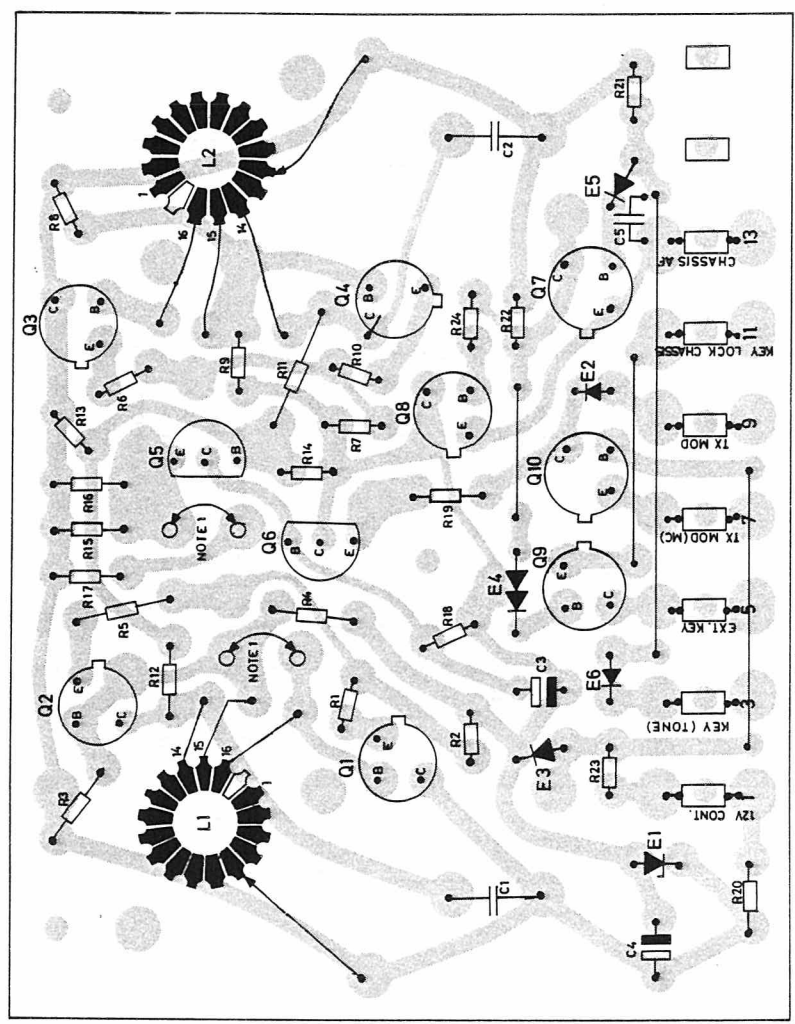
- a. 1060, 1160, 1270, 1400, 1530, 1670, 1830, 2000, 2200, 2400, 2600, 2900 Hz.
- b. 615, 675, 735, 805, 885, 970 Hz.



TERM.	FREQ.
1	1060 HZ
2	1160 -
3	1270 -
4	1400 -
5	1530 -
6	1670 -
7	1830 -
8	2000 -
9	2200 -
10	2400 -
11	2600 -
12	2900 -



NOTE: INSERT SHORTING LINKS AND ADJUST R17 FOR SINGLE TONE MODULATION.
STRAPPBØJLER ISKETTES .06 R17 JUSTERES VED ENKELTTONEMODULATION.



STONE TRANSMITTER TT7812 TONESENDER

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

Storno

TYPE	NO.	CODE	DATA
TT7812		10. 2453	Tone Transmitter
TT7813		10. 2896	Tone Transmitter
TT7814		10. 2907	Tone Transmitter
	C1	76. 5068	0. 1 μ F 1% polystyr TB
	C2	76. 5068	0. 1 μ F 1% polystyr TB
	C3	73. 5118	0. 22 μ F 20% tantal
	C4	73. 5109	10 μ F 20% tantal
	C5	74. 5155	1 nF -20 +80% ceram PL
	R1	80. 5248	820 Ω 5% carbon film
	R2	80. 5250	1. 2 K Ω 5% carbon film
	R3	80. 5267	33 K Ω 5% carbon film
	R4	80. 5265	22 K Ω 5% carbon film
	R5	80. 5248	820 Ω 5% carbon film
	R6	80. 5248	820 Ω 5% carbon film
	R7	80. 5250	1. 2 K Ω 5% carbon film
	R8	80. 5267	33 K Ω 5% carbon film
	R9	80. 5265	22 K Ω 5% carbon film
	R10	80. 5248	820 Ω 5% carbon film
	R11	80. 5275	0. 15 M Ω 5% carbon film
	R12	80. 5275	0. 15 M Ω 5% carbon film
	R13	80. 5270	56 K Ω 5% carbon film
	R14	80. 5270	56 K Ω 5% carbon film
	R15	80. 52XX	Adjusted carbon film
	R16	80. 5254	2. 7 K Ω 5% carbon film
	R17	80. 5254	2. 7 K Ω 5% carbon film
	R18	80. 5247	680 Ω 5% carbon film
	R19	80. 5246	560 Ω 5% carbon film
	R20	80. 5445	470 Ω 5% carbon film
	R21	80. 5261	10 K Ω 5% carbon film
	R22	80. 5251	1. 5 K Ω 5% carbon film
	R23	80. 5259	6. 8 K Ω 5% carbon film
	R24	80. 5250	1. 2 K Ω 5% carbon film
TT7812	L1	61. 1157	Tone Coil
	L2	61. 1157	Tone Coil
TT7813	L2	61. 1196	Tone Coil
TT7814	L2	61. 1189	Tone Coil
	E1	99. 5114	Zenerdiode 5. 6 V 5%
	E2	99. 5219	AAZ15 Diode
	E3	99. 5219	AAZ15 Diode
	E4	99. 5209	Stab. diode ZE1. 5
	E5	99. 5028	1N914 Diode
	E6	99. 5028	1N914 Diode

Storno

TYPE	NO.	CODE	DATA
	Q1	99. 5143	BC108 Transistor
	Q2	99. 5143	BC108 Transistor
	Q3	99. 5143	BC108 Transistor
	Q4	99. 5143	BC108 Transistor
	Q5	99. 5144	BC214L Transistor
	Q6	99. 5144	BC214L Transistor
	Q7	99. 5143	BC108 Transistor
	Q8	99. 5143	BC108 Transistor
	Q9	99. 5143	BC108 Transistor
	Q10	99. 5143	BC108 Transistor

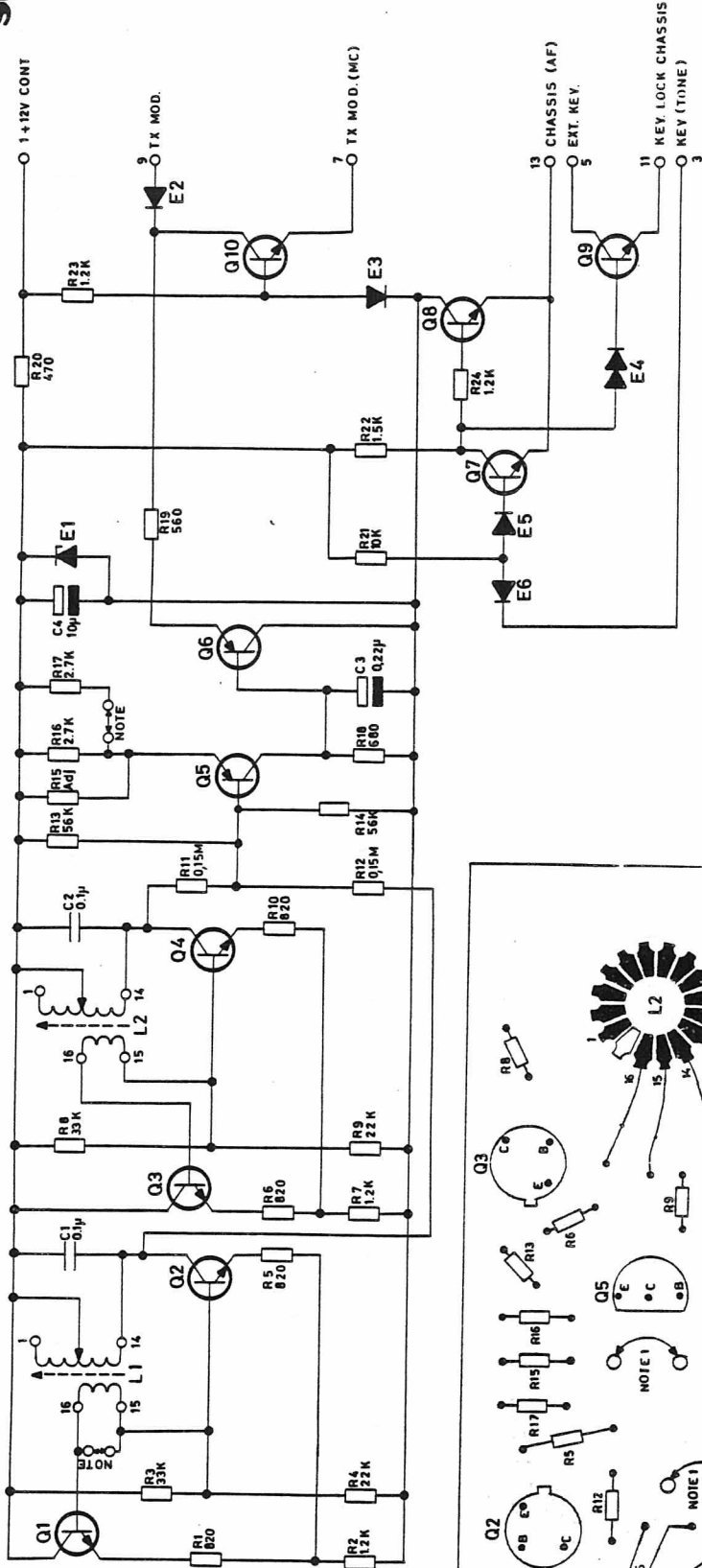
TT7812, TT7813, TT7814
TONE TRANSMITTER
TT7812, TT7813, TT7814
TONESENDER

X401. 688/3

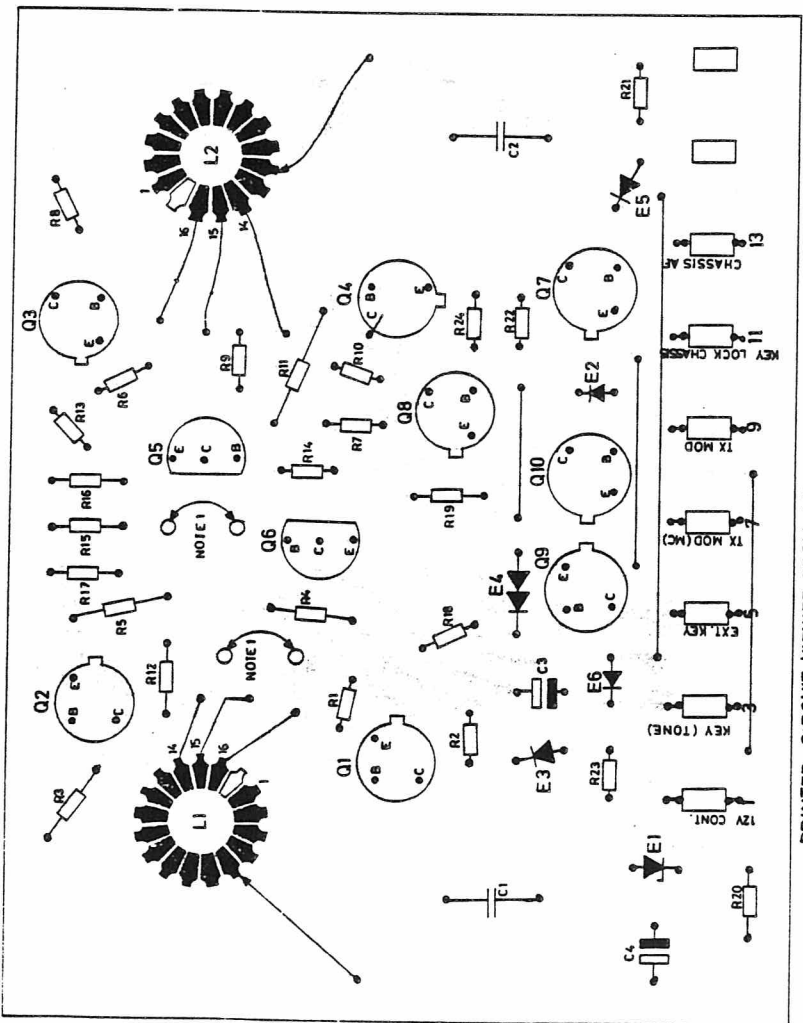
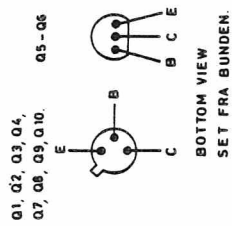
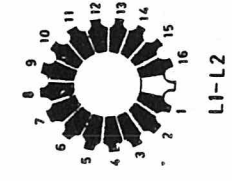
TONE TRANSMITTER TONESENDER

TT7812

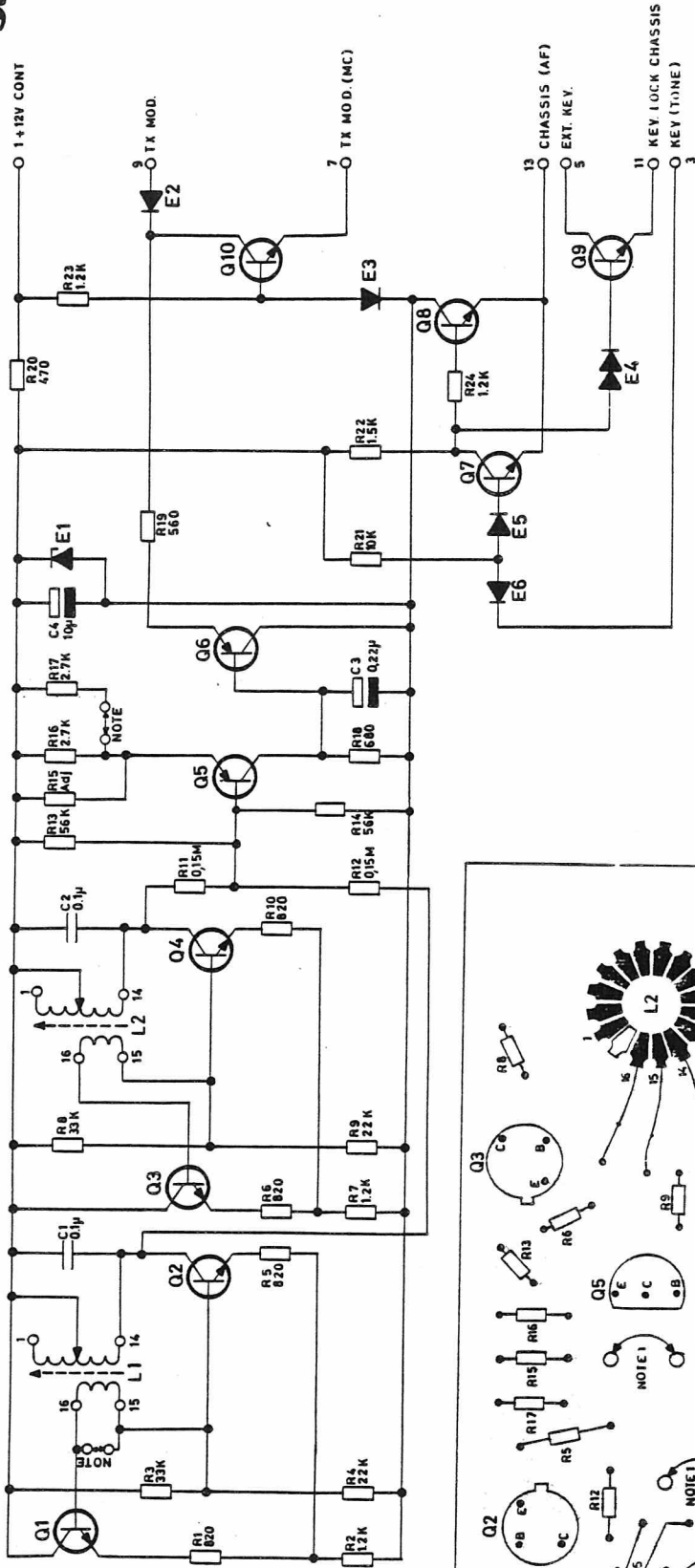
D701.556/2



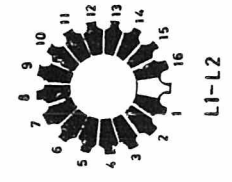
TERM.	FREQ.
1	1060 HZ
2	1160 -
3	1270 -
4	1400 -
5	1530 -
6	1670 -
7	1830 -
8	2000 -
9	2200 -
10	2400 -
11	2600 -
12	2900 -



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN



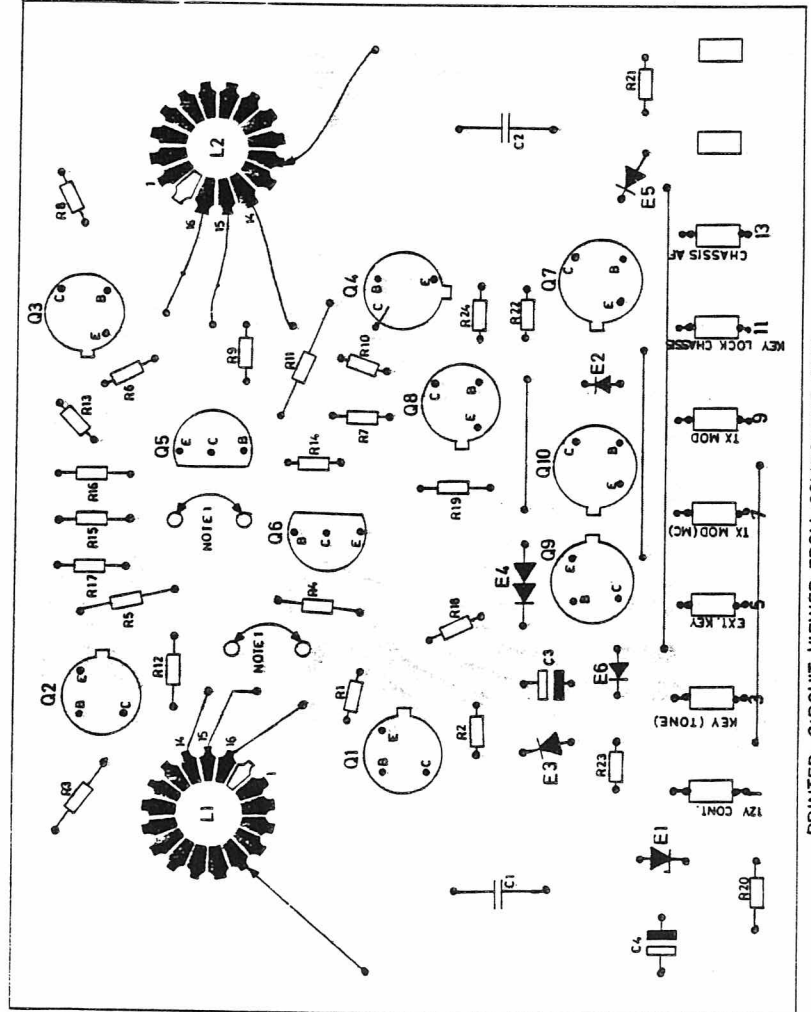
TERM.	FREQ.
1	1060 HZ
2	1160 -
3	1270 -
4	1400 -
5	1530 -
6	1670 -
7	1830 -
8	2000 -
9	2200 -
10	2400 -
11	2600 -
12	2900 -



Q1, Q2, Q3, Q4, Q7, Q8, Q9, Q10, Q5-Q6
 BOTTOM VIEW SET FRA BUNDEN.
 NOTE: INSERT SHORTING LINKS FOR SINGLE TONE MODULATION. STRAPPBØLLER ISETTES VED ENKEL-TONEMODULATION.

TONE TRANSMITTER TT7812 TONESENDER

D701.556/2



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
 TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

Storno

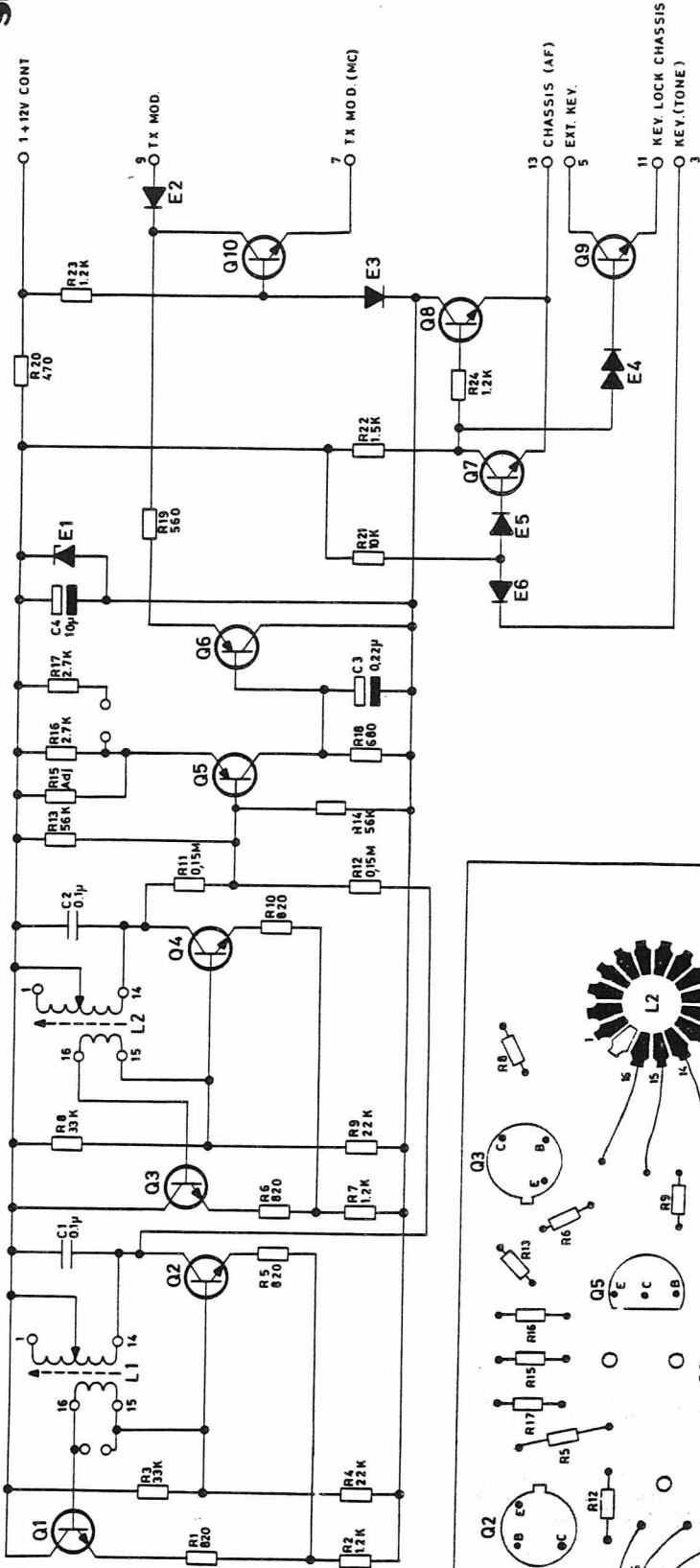
TYPE	NO.	CODE	DATA
TT7812		10.2453	Tone Transmitter
	C1	76.5068	0.1 μ F 1% polystyr TB
	C2	76.5068	0.1 μ F 1% polystyr TB
	C3	73.5118	0.22 μ F 20% tantal
	C4	73.5109	10 μ F 20% tantal
	R1	80.5248	820 Ω 5% carbon film
	R2	80.5250	1.2K Ω 5% carbon film
	R3	80.5267	33K Ω 5% carbon film
	R4	80.5265	22K Ω 5% carbon film
	R5	80.5248	820 Ω 5% carbon film
	R6	80.5248	820 Ω 5% carbon film
	R7	80.5250	1.2K Ω 5% carbon film
	R8	80.5267	33K Ω 5% carbon film
	R9	80.5265	22K Ω 5% carbon film
	R10	80.5248	820 Ω 5% carbon film
	R11	80.5275	0.15M Ω 5% carbon film
	R12	80.5275	0.15M Ω 5% carbon film
	R13	80.5270	56K Ω 5% carbon film
	R14	80.5270	56K Ω 5% carbon film
	R15	80.52XX	Adjusted carbon film
	R16	80.5254	2.7K Ω 5% carbon film
	R17	80.5254	2.7K Ω 5% carbon film
	R18	80.5247	680 Ω 5% carbon film
	R19	80.5246	560 Ω 5% carbon film
	R20	80.5445	470 Ω 5% carbon film
	R21	80.5261	10K Ω 5% carbon film
	R22	80.5251	1.5K Ω 5% carbon film
	R23	80.5250	1.2K Ω 5% carbon film
	R24	80.5250	1.2K Ω 5% carbon film
	L1	61.1157	Tone Coil
	L2	61.1157	Tone Coil
	E1	99.5114	Zenerdiode 5.6V 5%
	E2	99.5219	AAZ15 Diode
	E3	99.5219	AAZ15 Diode
	E4	99.5209	Stab. diode ZE1.5
	E5	99.5028	1N914 Diode
	E6	99.5028	1N914 Diode
	Q1	99.5143	BC108 Transistor
	Q2	99.5143	BC108 Transistor
	Q3	99.5143	BC108 Transistor
	Q4	99.5143	BC108 Transistor
	Q5	99.5144	BC214L Transistor
	Q6	99.5144	BC214L Transistor

Storno

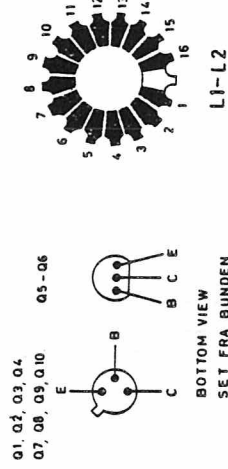
TYPE	NO.	CODE	DATA
	Q7	99.5143	BC108 Transistor
	Q8	99.5143	BC108 Transistor
	Q9	99.5143	BC108 Transistor
	Q10	99.5143	BC108 Transistor

TONE TRANSMITTER
TONESENDER
TT7812

X401.688

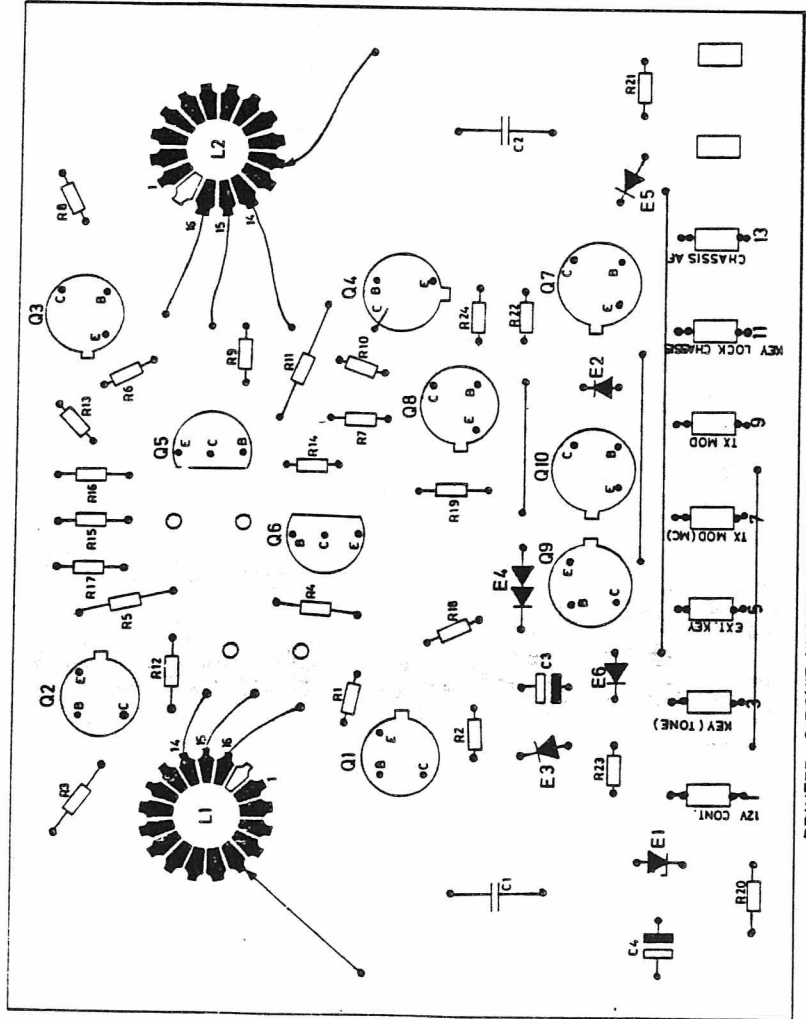


TERM.	L1	L2	FREQ.
1	1060	570	570 HZ
2	1160	650	650
3	1270	740	740
4	1400	850	850
5	1530	1060	1060
6	1670	1160	1160
7	1830	1270	1270
8	2000	1400	1400
9	2200	1530	1530
10	2400	1670	1670
11	2600	1830	1830
12	2900	2000	2000



Q1, Q2, Q3, Q4
Q7, Q8, Q9, Q10

05-06



TONE TRANSMITTER TT7813
TONESENDER

D401:774

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

Storno

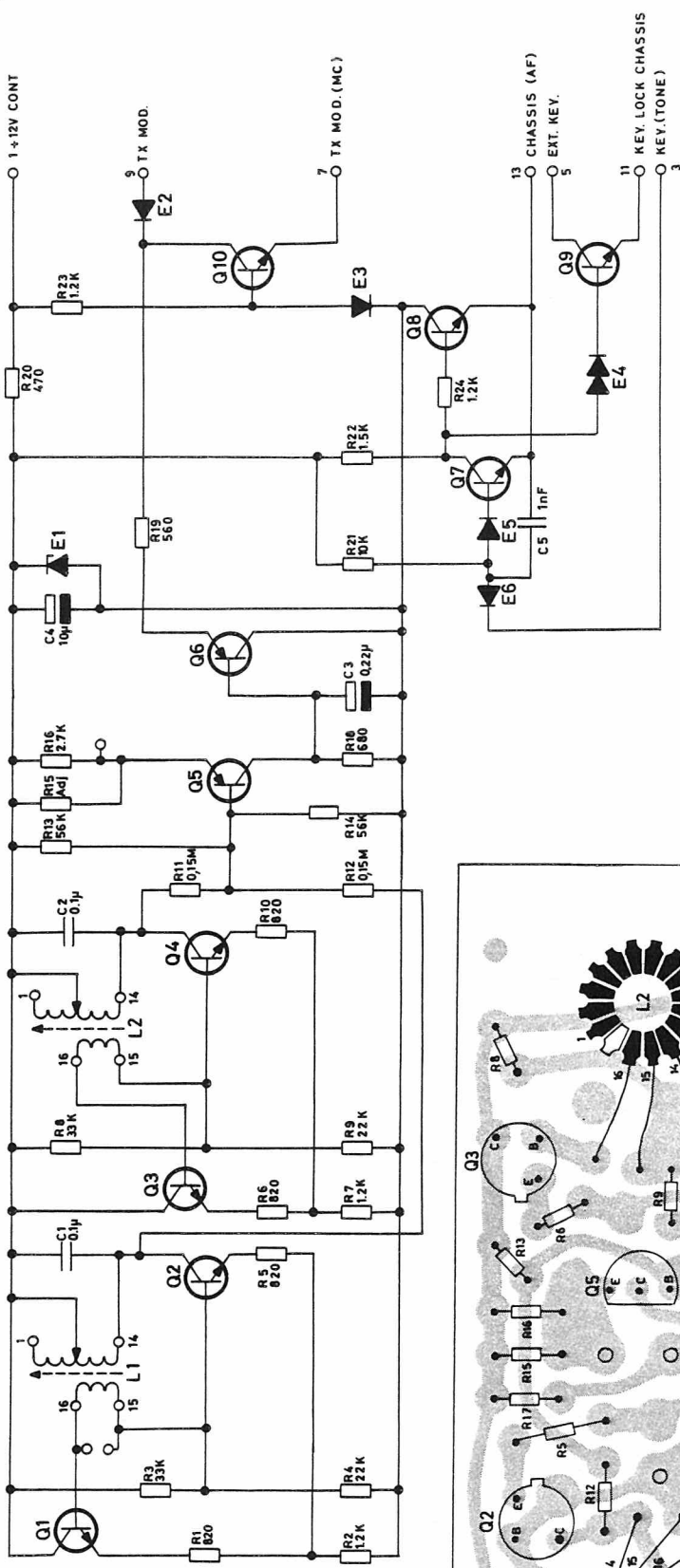
Storno

TYPE	NO.	CODE	DATA
TT7812		10.2453	Tone Transmitter
TT7813		10.2896	Tone Transmitter
TT7814		10.2907	Tone Transmitter
	C1	76.5068	0.1 μ F 1% polystyr TB
	C2	76.5068	0.1 μ F 1% polystyr TB
	C3	73.5118	0.22 μ F 20% tantal
	C4	73.5109	10 μ F 20% tantal
	R1	80.5248	820 Ω 5% carbon Film
	R2	80.5250	1.2 K Ω 5% carbon film
	R3	80.5267	33 K Ω 5% carbon film
	R4	80.5265	22 K Ω 5% carbon film
	R5	80.5248	820 Ω 5% carbon film
	R6	80.5248	820 Ω 5% carbon film
	R7	80.5250	1.2 K Ω 5% carbon film
	R8	80.5267	33 K Ω 5% carbon film
	R9	80.5265	22 K Ω 5% carbon film
	R10	80.5248	820 Ω 5% carbon film
	R11	80.5275	0.15 M Ω 5% carbon film
	R12	80.5275	0.15 M Ω 5% carbon film
	R13	80.5270	56 K Ω 5% carbon film
	R14	80.5270	56 K Ω 5% carbon film
	R15	80.52XX	Adjusted carbon film
	R16	80.5254	2.7 K Ω 5% carbon film
	R17	80.5254	2.7 K Ω 5% carbon film
	R18	80.5247	680 Ω 5% carbon film
	R19	80.5246	560 Ω 5% carbon film
	R20	80.5445	470 Ω 5% carbon film
	R21	80.5261	10 K Ω 5% carbon film
	R22	80.5251	1.5 K Ω 5% carbon film
	R23	80.5250	1.2 K Ω 5% carbon film
	R24	80.5250	1.2 K Ω 5% carbon film
TT7812	L1	61.1157	Tone Coil
	L2	61.1157	Tone Coil
TT7813	L2	61.1196	Tone Coil
TT7814	L2	61.1189	Tone Coil
	E1	99.5114	Zenerdiode 5.6 V 5%
	E2	99.5219	AAZ15 Diode
	E3	99.5219	AAZ15 Diode
	E4	99.5209	Stab. diode ZE1.5
	E5	99.5028	1N914 Diode
	E6	99.5028	1N914 Diode

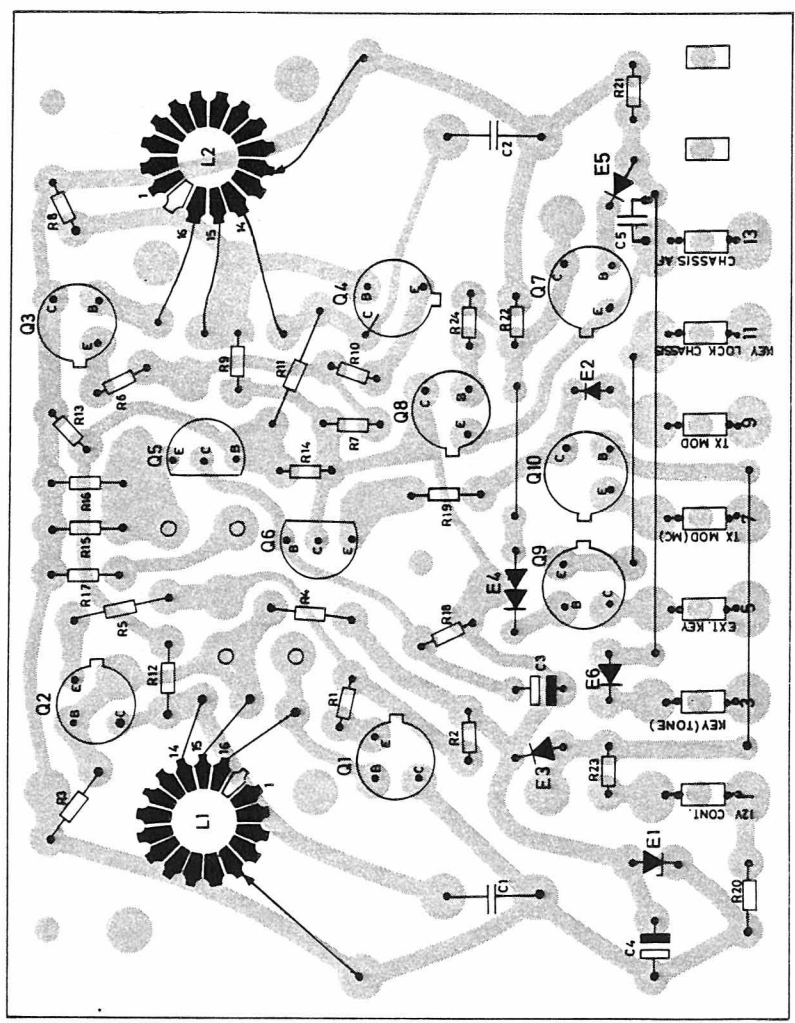
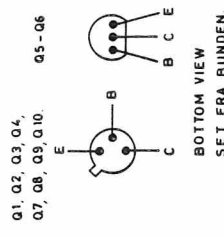
TYPE	NO.	CODE	DATA
	Q1	99.5143	BC108 Transistor
	C2	99.5143	BC108 Transistor
	Q3	99.5143	BC108 Transistor
	Q4	99.5143	BC108 Transistor
	Q5	99.5144	BC214L Transistor
	Q6	99.5144	BC214L Transistor
	Q7	99.5143	BC108 Transistor
	Q8	99.5143	BC108 Transistor
	Q9	99.5143	BC108 Transistor
	Q10	99.5143	BC108 Transistor

TT7812, TT7813, TT7814
TONE TRANSMITTER
TONESENDER

X401.688/2



TERM.	FREQ.	L1	L2
1	1060 HZ		615 HZ
2	1160 -		575 -
3	1270 -		735 -
4	1400 -		805 -
5	1530 -		885 -
6	1670 -		970 -
7	1830 -		
8	2000 -		
9	2200 -		
10	2400 -		
11	2600 -		
12	2900 -		

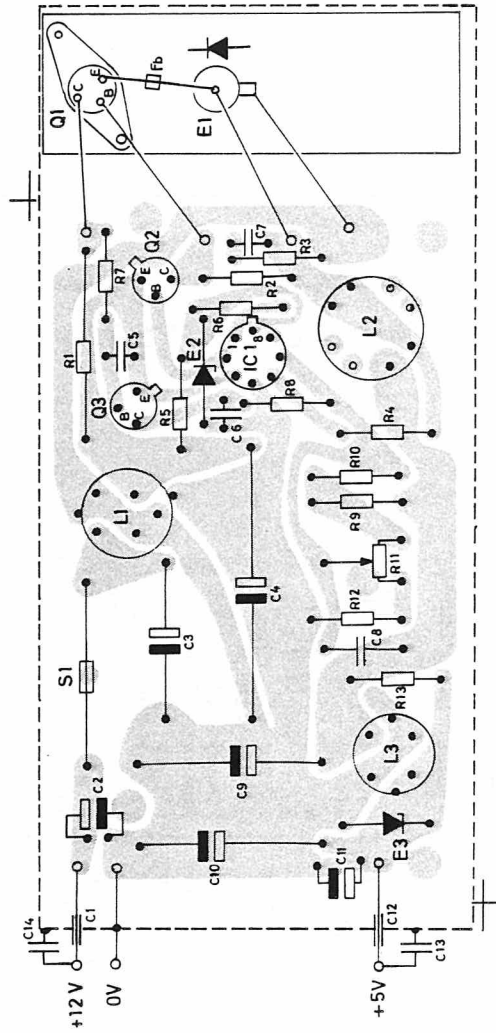
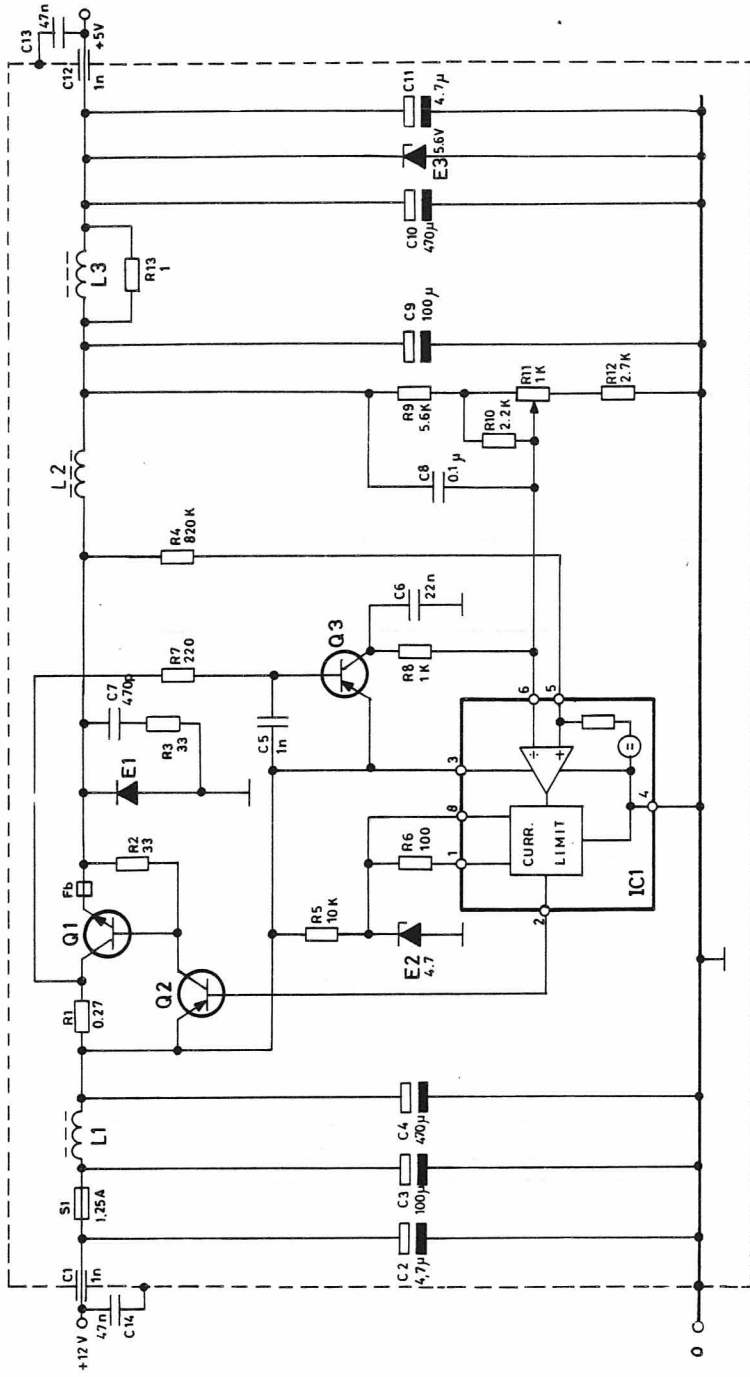


TONE TRANSMITTER
TONESENDER

PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE
TRYKT KREDSLØB SET FRA KOMPONENTSIDEN

STORNOPHONE 700
MAINTENANCE MANUAL
MANUAL II
Section 8

TITLE		Code
VR701	Schematic	D401. 780
	Part List	X401. 858
XS701	Description	60. 192-E1
	Schematic	D401. 328/3
	Component Lay-out	D401. 518
	Part List 1 - 2	X401. 313/2
XS702	Description 1 - 2	60. 193-E1
	Schematic	D401. 329/2
	Component Lay-out	D401. 517
	Part List 1 - 2	X401. 331/2

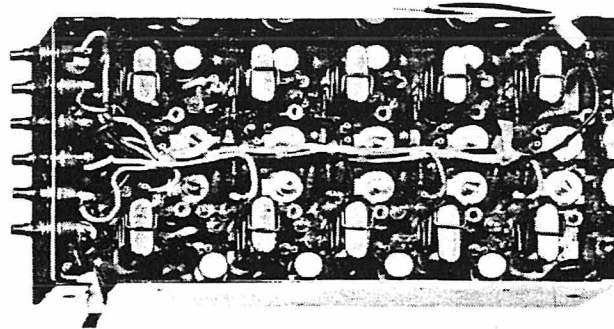


VOLTAGE REGULATOR
SPÆNDINGSREGULATOR

VR701

D401.780

Channel Switching Unit XS701



Description

The oscillator switching unit consists of 5 receiver and 5 transmitter oscillators. For each channel the receiver and transmitter oscillators share a common terminal connection to the channel selector switching arrangement.

The collector resistor for the transmitter oscillator for channel 1, located in the exciter module (EX700), is also common to all of the other transmitter oscillators, channel 2-6, located in the XS701 crystal switching unit.

Similarly, all the receiver oscillators have their collectors working into one common resonant circuit tuned to the 3rd harmonic of the crystal frequency, and located in the 1st local oscillator collector load in the RC700 receiver converter module.

Switching between oscillators is accomplished by returning the oscillator emitter to chassis ground through the switching terminal for the selected channel which, as previously mentioned, is common to both oscillators belonging to that particular channel. The switching terminals for all the oscillators not in use are disconnected, or open.

Technical Specifications

Supply Voltage

9 V

Frequency Range

Receiver:

crystal frequency: 11.2 - 14.7833 MHz

output frequency: 33.6 - 44.35 MHz

Transmitter:

crystal and output frequency: 11.33-14.67 MHz

Temperature Range

-30° to +80°C

Oscillator Frequency adjustable by:

$$\frac{\Delta f}{f} \geq \pm 30 \times 10^{-6}$$

Frequency Stability

For voltage variations of $\pm 2, 5\%$ at 9 V:

$$\frac{\Delta f}{f} \leq \pm 0.1 \times 10^{-6}$$

For temperatures between

$$-25^{\circ}\text{C} \text{ and } +75^{\circ}\text{C}: \frac{\Delta f}{f} \leq 2 \times 10^{-6}$$

Load Impedances

Receiver loading circuit's input impedance: $1 \text{ K}\Omega // 4.7 \text{ pF}$

Transmitter loading circuit's input impedance: $470\Omega // 22 \text{ pF}$

Output Voltage

Receiver: (dependent upon crystal activity) 700 mV

Transmitter: (dependent upon crystal activity) 170 mV

Power Consumption

Transmitter: 4.6 mA

Receiver: 4.3 mA

Crystal Types

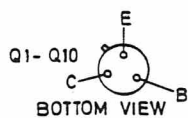
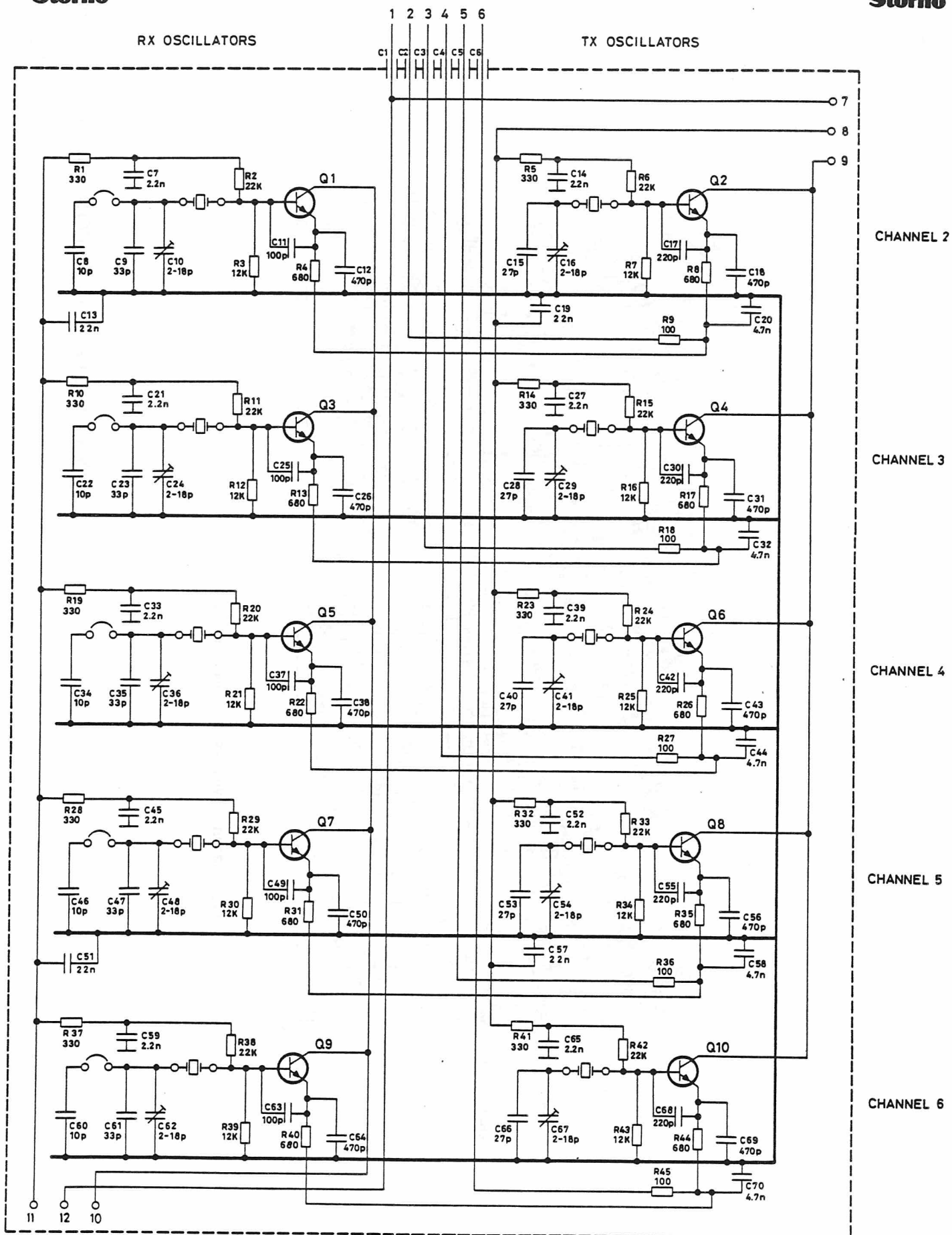
98-12, 98-20 or 98-26

Dimensions

92 x 46 x 25 mm

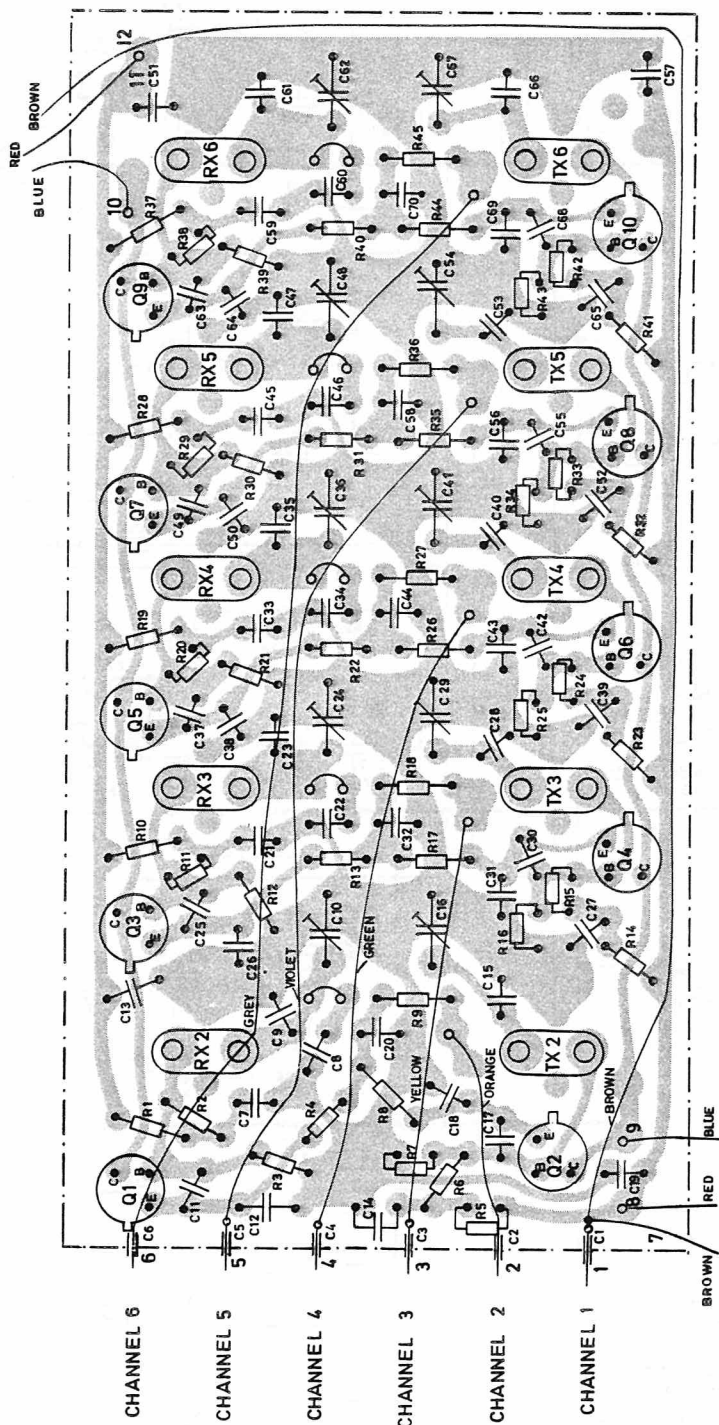
Storno

Storno



CRYSTAL SWITCH UNIT XS701

D401.328/3



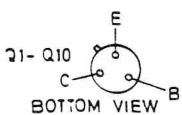
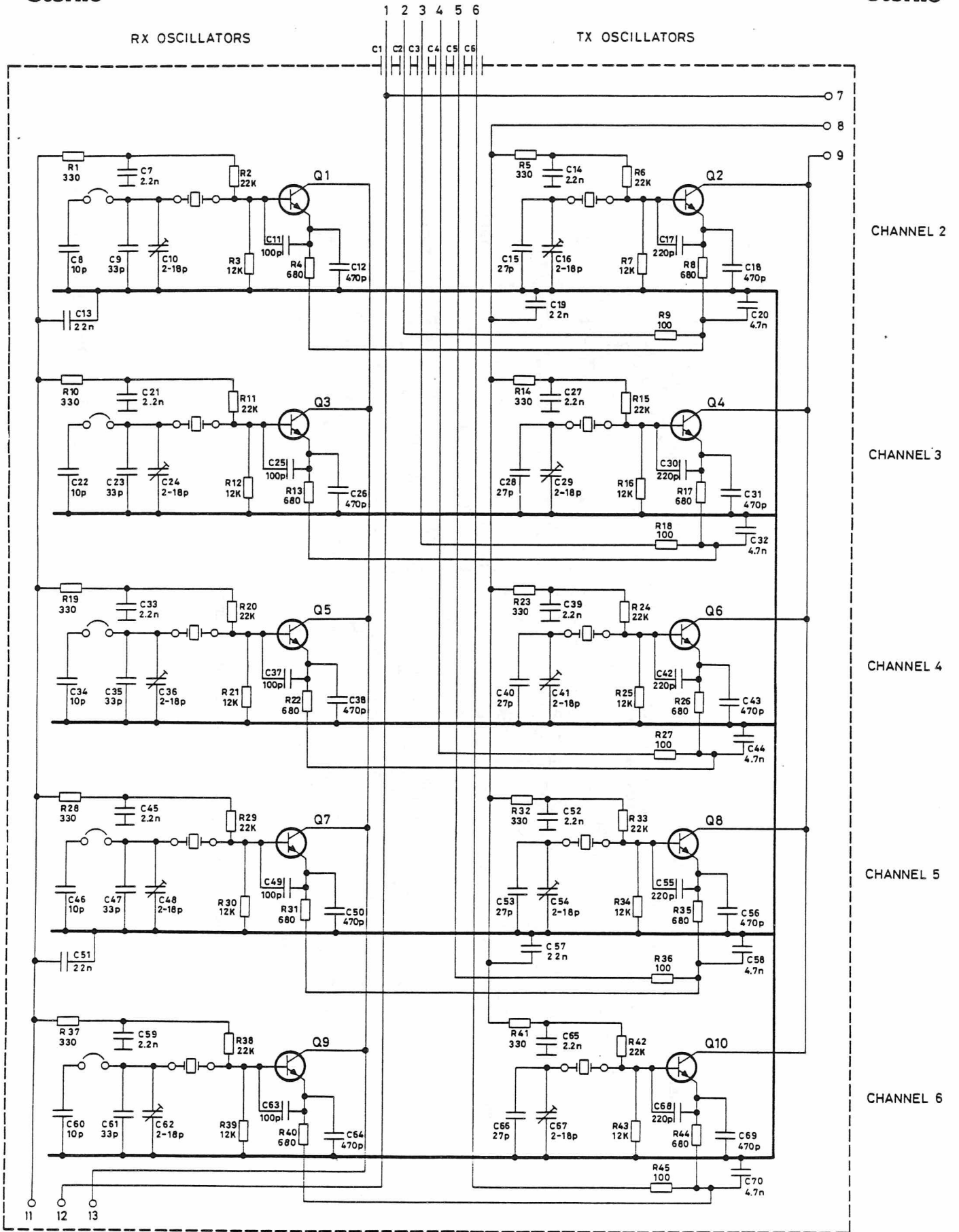
PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE

CRYSTAL OSCILLATOR PANEL XS701

D401.518

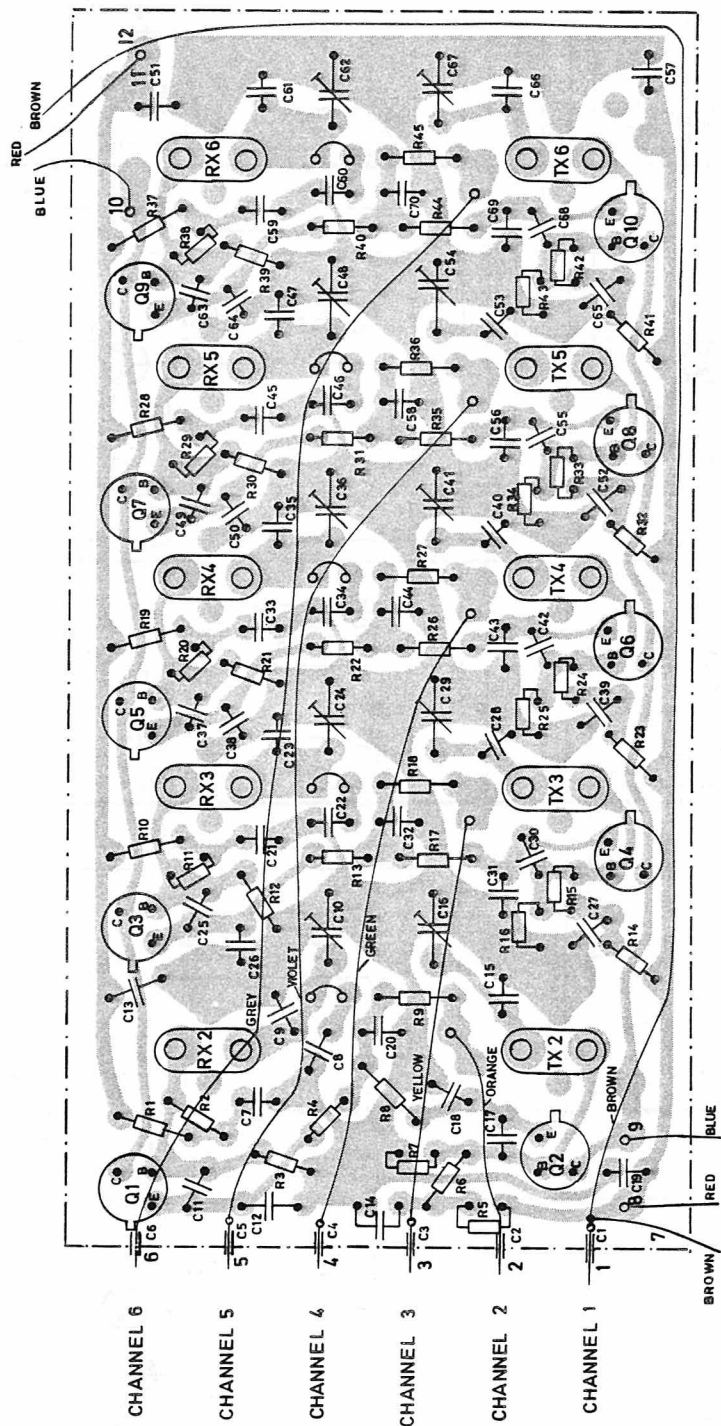
Storno

Storno



CRYSTAL SWITCH UNIT XS701

D401.328/2

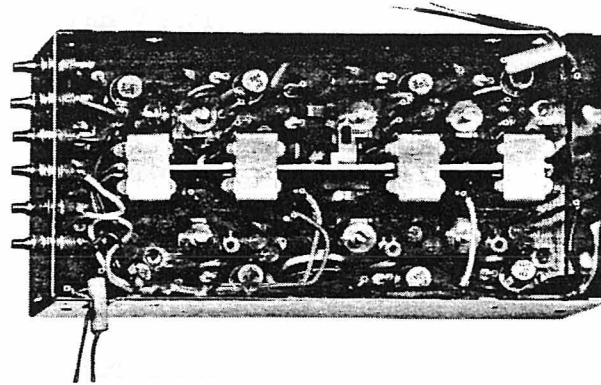


PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE

CRYSTAL OSCILLATOR PANEL XS701

D401.518

Channel Switching Unit XS702



Description

The oscillator switching unit consists of 4 receiver and 4 transmitter oscillators. For each channel the receiver and transmitter oscillators are physically placed right across from each other on the circuit board, and both oscillators share a common terminal connection to the channel selector switching arrangement.

To compensate for crystal frequency drift at low temperatures, the circuit is arranged so that a transistor-driven common heating element is in thermal contact with all eight crystals.

Regulating Circuit

The regulating circuit is controlled by an NTC resistor which has thermal contact with the heating element. When the resistance of the NTC resistor reaches a value of approx. $6\text{ K}\Omega$, transistor Q9 will conduct. Q9 then drives Q10 into conduction. The current through Q10 heats the metal rail heating element. Heating the rail causes the resistance of the NTC resistor to decrease. In this manner the temperature of the heating rail is regulated to approx. -5°C when the ambient temperature drops below that figure. The maximum current through Q10 can be preset by means of R39.

The Oscillators

A collector resistor in the EX700 exciter module is common to all four transmitter oscillator collectors. Similarly, all four receiver oscil-

lators have their collectors working into one common resonant circuit tuned to the 3rd harmonic of the crystal frequency, and located in the RC700 receiver converter module.

Switching between oscillators is accomplished by returning the oscillator emitter to chassis ground through the switching terminal for the selected channel which, as previously mentioned, is common to both oscillators belonging to that particular channel. The switching terminals for all the oscillators not in use are disconnected, or open.

During transmit, the transmitter oscillators not in use can pass no spurious currents and thus will not oscillate. With their emitter returns open, the idle transmitter oscillators are effectively held at cut-off by the emitter-base diodes of their related receiver oscillators.

Likewise, during receive, the transmitter oscillators will cut off the idle receiver local oscillators.

Technical Specifications

Supply Voltage

Oscillators +9 V

Regulating Circuit +9V and +13.6 V

Frequency Range

Receiver

crystal frequency 11.2-14.78333 MHz

output frequency 33.6-44.35 MHz

Transmitter

crystal and output frequency 11.33-14.67 MHz

Temperature Range

-30°C to +80°C

Oscillator Frequency adjustable by

$$\frac{\Delta f}{f} \pm 30 \times 10^{-6}$$

Frequency Stability

For voltage variations of $\pm 2.5\%$ at 9 V

$$\frac{\Delta f}{f} \pm 0.1 \times 10^{-6}$$

For temperatures between -30°C to +70°C
with crystal types 98-20 or 98-26:

$$\frac{\Delta f}{f} 5 \times 10^{-6}$$

Load Impedances

Receiver: loading circuit's input impedance: $1 \text{ K}\Omega // 4.7 \text{ pF}$

Transmitter: loading circuit's input impedance: $470\Omega // 220 \text{ pF}$

Output Voltage

Receiver: (dependent upon crystal activity) 700 mV

Transmitter: (dependent upon crystal activity) 170 mV

Power Consumption

+9 V supply

Transmitter: 5.3 mA

Receiver: 5.6 mA

+13.6 V supply

For temperatures $> \text{ca. } -5^\circ\text{C}$: 1 mA

For temperatures from ca. -5°C to -30°C the current rises practically linearly as ambient temperatures falls.

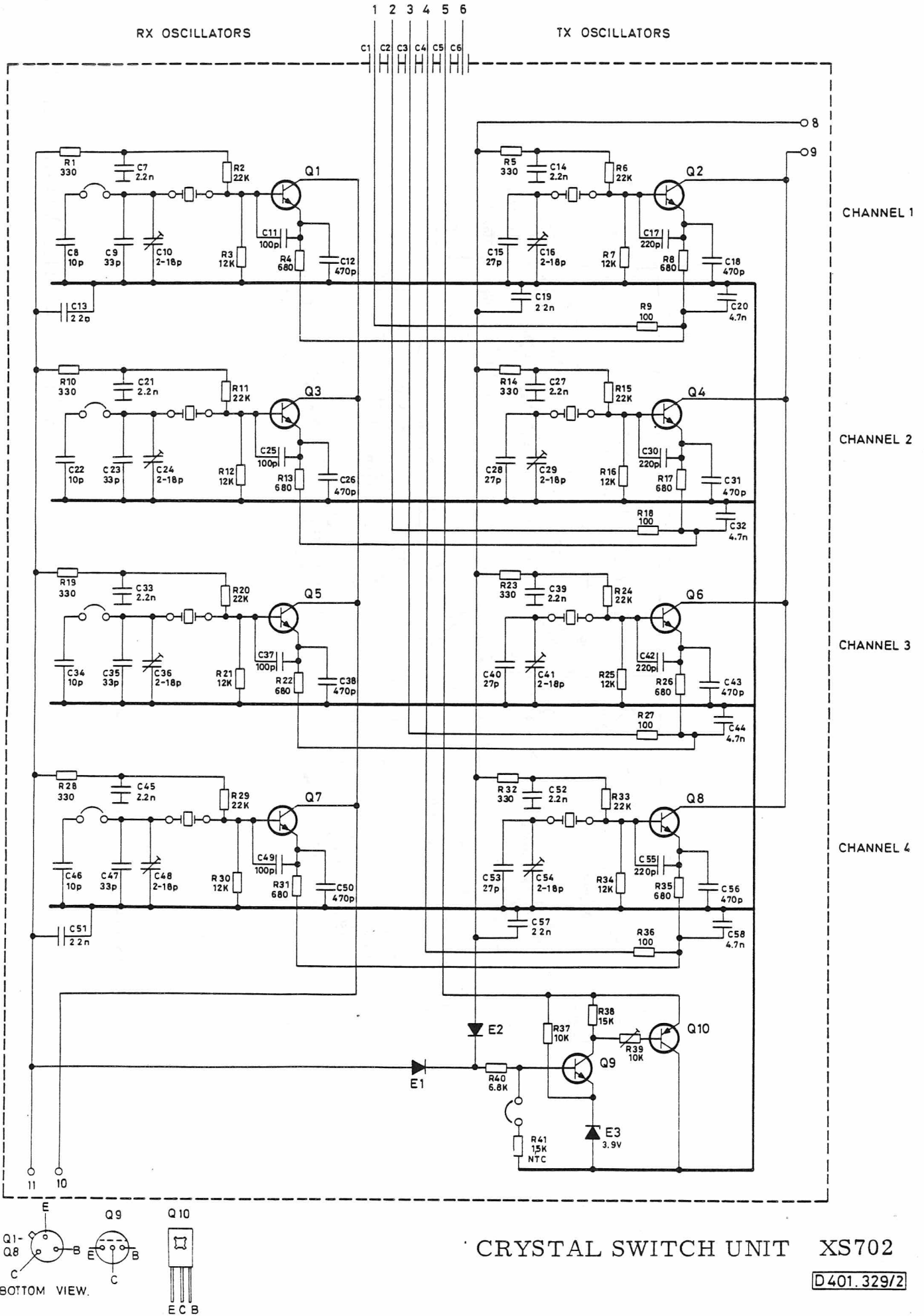
At +13.6 V and -10°C : 130 mA

Crystal Types

98-20 or 98-26

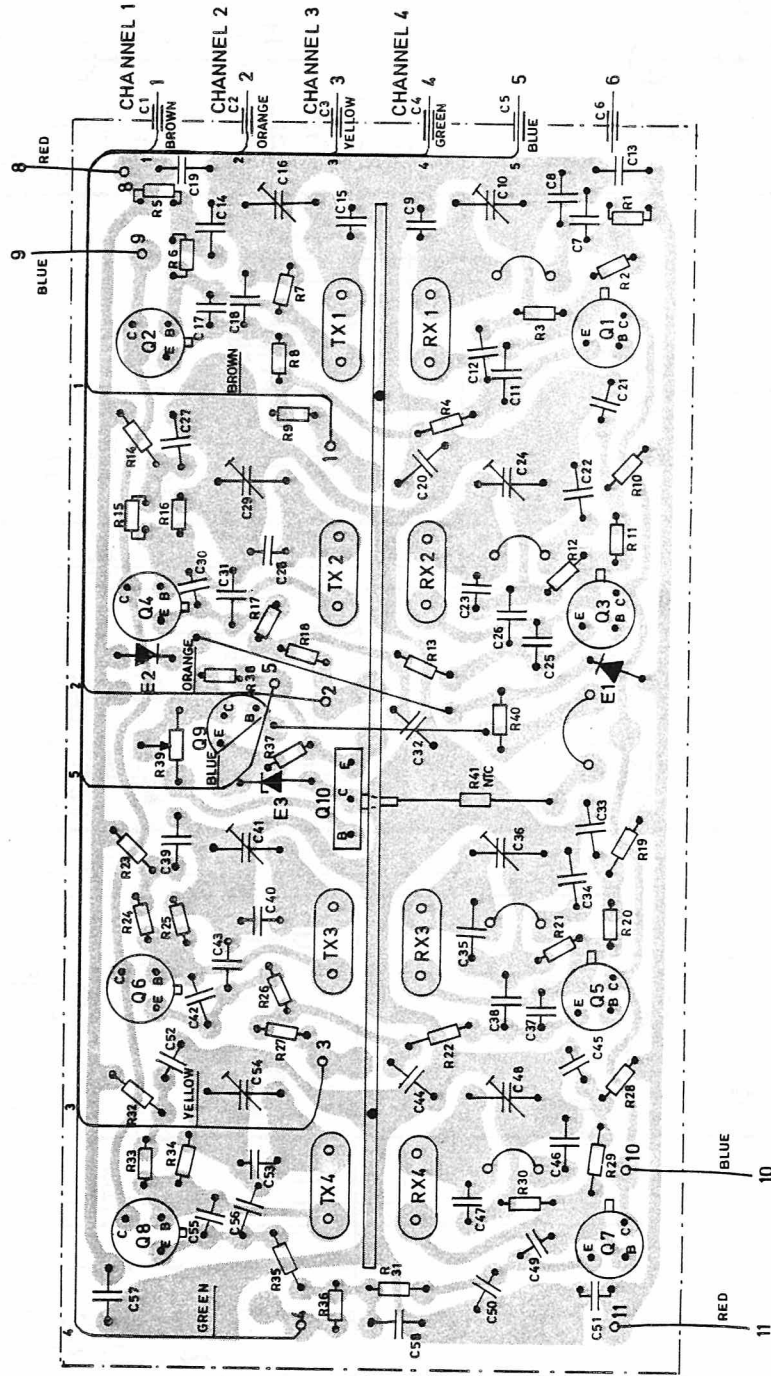
Dimensions

92 x 46 x 25 mm



CRYSTAL SWITCH UNIT XS702

D401.329/2



PRINTED CIRCUIT VIEWED FROM COMPONENT SIDE

CRYSTAL OSCILLATOR PANEL XS702

D401.517

TYPE	NO.	CODE	DATA
XS702		10, 2437	Crystal Switch Unit
	C1	74.5167	1 nF -20 +80% ceram FT
	C2	74.5167	1 nF -20 +80% ceram FT
	C3	74.5167	1 nF -20 +80% ceram FT
	C4	74.5167	1 nF -20 +80% ceram FT
	C5	74.5167	1 nF -20 +80% ceram FT
	C6	74.5167	1 nF -20 +80% ceram FT
	C7	76.5059	2.2 nF 10% polyest. FL
	C8	74.5135	10 pF 5% ceram DI
	C9	74.5191	33 pF 5% ceram TB
	C10	78.5044	2-18 pF trimmer
	C11	76.5102	100 pF 2.5% polystyr TB
	C12	76.5106	470 pF 2.5% polystyr TB
	C13	76.5071	22 nF 10% polyest. FL
	C14	76.5059	2.2 nF 10% polyest. FL
	C15	74.5192	27 pF 5% ceram TB
	C16	78.5044	2-18 pF trimmer
	C17	76.5104	220 pF 2.5% polystyr TB
	C18	76.5106	470 pF 2.5% polystyr TB
	C19	76.5071	22 nF 10% polyest. FL
	C20	76.5061	4.7 nF 10% polyest. FL
	C21	76.5059	2.2 nF 10% polyest. FL
	C22	74.5135	10 pF 5% ceram DI
	C23	74.5191	33 pF 5% ceram TB
	C24	78.5044	2-18 pF trimmer
	C25	76.5102	100 pF 2.5% polystyr TB
	C26	76.5106	470 pF 2.5% polystyr TB
	C27	76.5059	2.2 nF 10% polyest. FL
	C28	74.5192	27 pF 5% ceram TB
	C29	78.5044	2-18 pF trimmer
	C30	76.5104	220 pF 2.5% polystyr TB
	C31	76.5106	470 pF 2.5% polystyr TB
	C32	76.5061	4.7 nF 10% polyest. FL
	C33	76.5059	2.2 nF 10% polyest. FL
	C34	74.5135	10 pF 5% ceram DI
	C35	74.5191	33 pF 5% ceram TB
	C36	78.5044	2-18 pF trimmer
	C37	76.5102	100 pF 2.5% polystyr TB
	C38	76.5106	470 pF 2.5% polystyr TB
	C39	76.5059	2.2 nF 10% polyest. FL
	C40	74.5192	27 pF 5% ceram TB
	C41	78.5044	2-18 pF trimmer
	C42	76.5104	220 pF 2.5% polystyr TB
	C43	76.5106	470 pF 2.5% polystyr TB
	C44	76.5061	4.7 nF 10% polyest. FL
	C45	76.5059	2.2 nF 10% polyest. FL
	C46	74.5135	10 pF 5% ceram DI

TYPE	NO.	CODE	DATA
	C47	74.5191	33 pF 5% ceram TB
	C48	78.5044	2-18 pF trimmer
	C49	76.5102	100 pF 2.5% polystyr TB
	C50	76.5106	470 pF 2.5% polystyr TB
	C51	76.5071	22 nF 10% polyest. FL
	C52	76.5059	2.2 nF 10% polyest. FL
	C53	74.5192	27 pF 5% ceram TB
	C54	78.5044	2-18 pF trimmer
	C55	76.5104	220 pF 2.5% polystyr TB
	C56	76.5106	470 pF 2.5% polystyr TB
	C57	76.5071	22 nF 10% polyest. FL
	C58	76.5061	4.7 nF 10% polyest. FL
	R1	80.5243	330 Ω 5% carbon film
	R2	80.5265	22 kΩ 5% " "
	R3	80.5262	12 kΩ 5% " "
	R4	80.5247	680 Ω 5% " "
	R5	80.5243	330 Ω 5% " "
	R6	80.5265	22 kΩ 5% " "
	R7	80.5262	12 kΩ 5% " "
	R8	80.5247	680 Ω 5% " "
	R9	80.5237	100 Ω 5% " "
	R10	80.5243	330 Ω 5% " "
	R11	80.5265	22 kΩ 5% " "
	R12	80.5262	12 kΩ 5% " "
	R13	80.5247	680 Ω 5% " "
	R14	80.5243	330 Ω 5% " "
	R15	80.5265	22 kΩ 5% " "
	R16	80.5262	12 kΩ 5% " "
	R17	80.5247	680 Ω 5% " "
	R18	80.5237	100 Ω 5% " "
	R19	80.5243	330 Ω 5% " "
	R20	80.5265	22 kΩ 5% " "
	R21	80.5262	12 kΩ 5% " "
	R22	80.5247	680 Ω 5% " "
	R23	80.5243	330 Ω 5% " "
	R24	80.5265	22 kΩ 5% " "
	R25	80.5262	12 kΩ 5% " "
	R26	80.5247	680 Ω 5% " "
	R27	80.5237	100 Ω 5% " "
	R28	80.5243	330 Ω 5% " "
	R29	80.5265	22 kΩ 5% " "

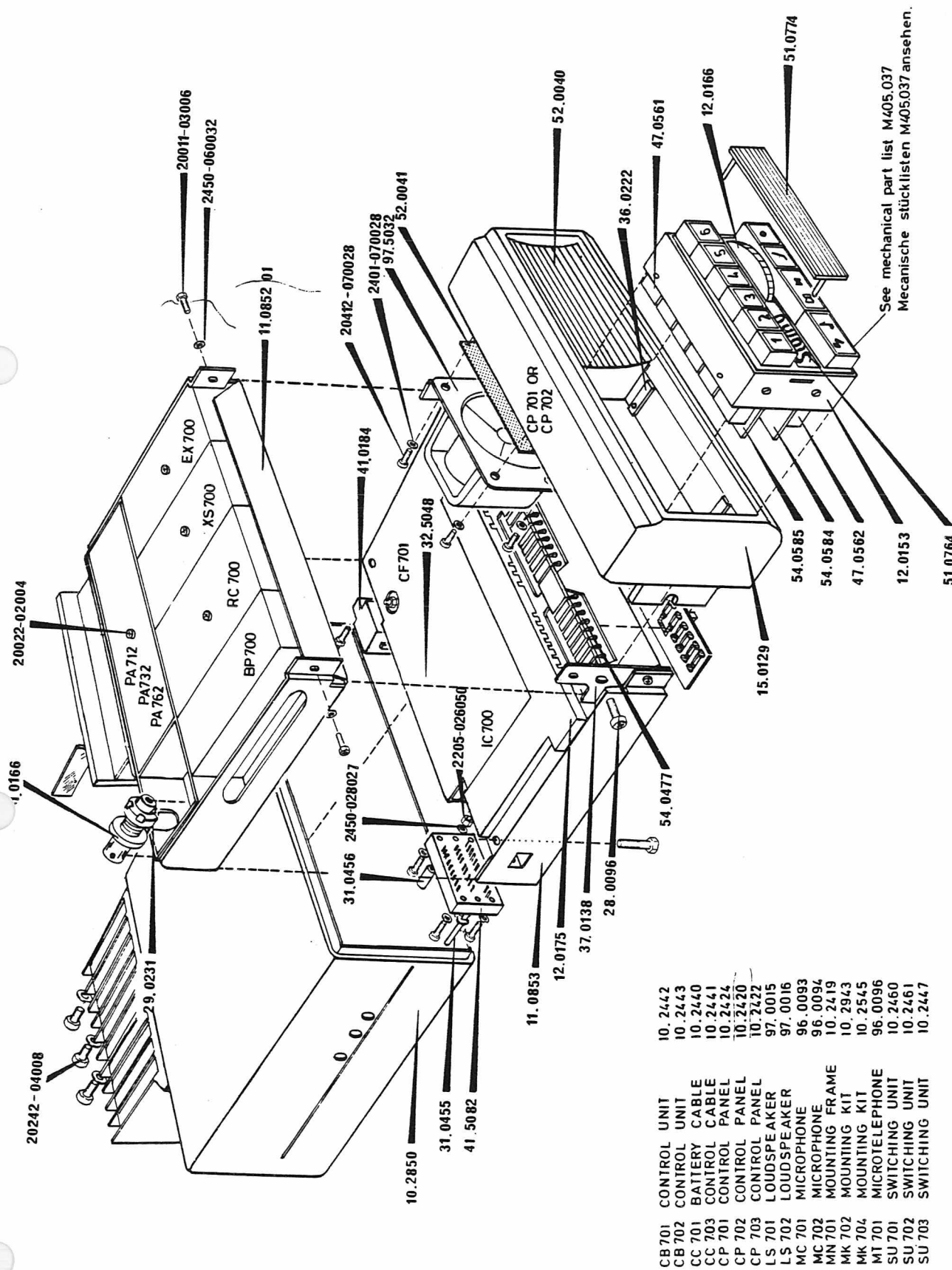
CRYSTAL SWITCH UNIT XS702

X401.331/2

STORNOPHONE 700
 MAINTENANCE MANUAL
 VOLUME II
 Section 9

TITLE		Code
CQM700-25/15	Mech. picture	M405.049
CQM700D	Mech. picture	M405.048/4
CQM713P3	Mech. picture	M405.080
CA701	Mech. picture	M405.030
	Part List	M405.030-2/2
	Part List	M405.030-3
CB700, CP700	Mech. picture	M405.037/2
	Part List	M405.037-2/2
	Part List	M405.037-3/2
CB704	Mech. picture	M405.047/3
CB705	Mech. picture	M405.078
CB2706	Lay-out	M405.055
CB706	Mech. Lay-out	M405-087
CC703	Mech. picture	M405.040/2
CC704	Mech. picture	M405.046/3
MC701-MK704	Mech. picture	M405.035/2
MC702-JB701	Mech. picture	M405.034/2
MC703	Mech. picture	M405.082
MC704	Mech. picture	M405.089
LS701	Mech. picture	M405.039/2
MK701	Mech. picture	M405.032/3
MN701	Mech. picture	M405.033/3
MT701-HS602a	Mech. picture	M405.041/2
MT703	Mech. picture	M405.081
MT704	Mech. picture	M405.085
PS701	Mech. picture	M405.045
	Part List	M405.045/2
PS701 connector	Mech. picture	M405.043/2
	Part List	M405.043/2
SU703	Mech. picture	M405.042/2

Service Coordination



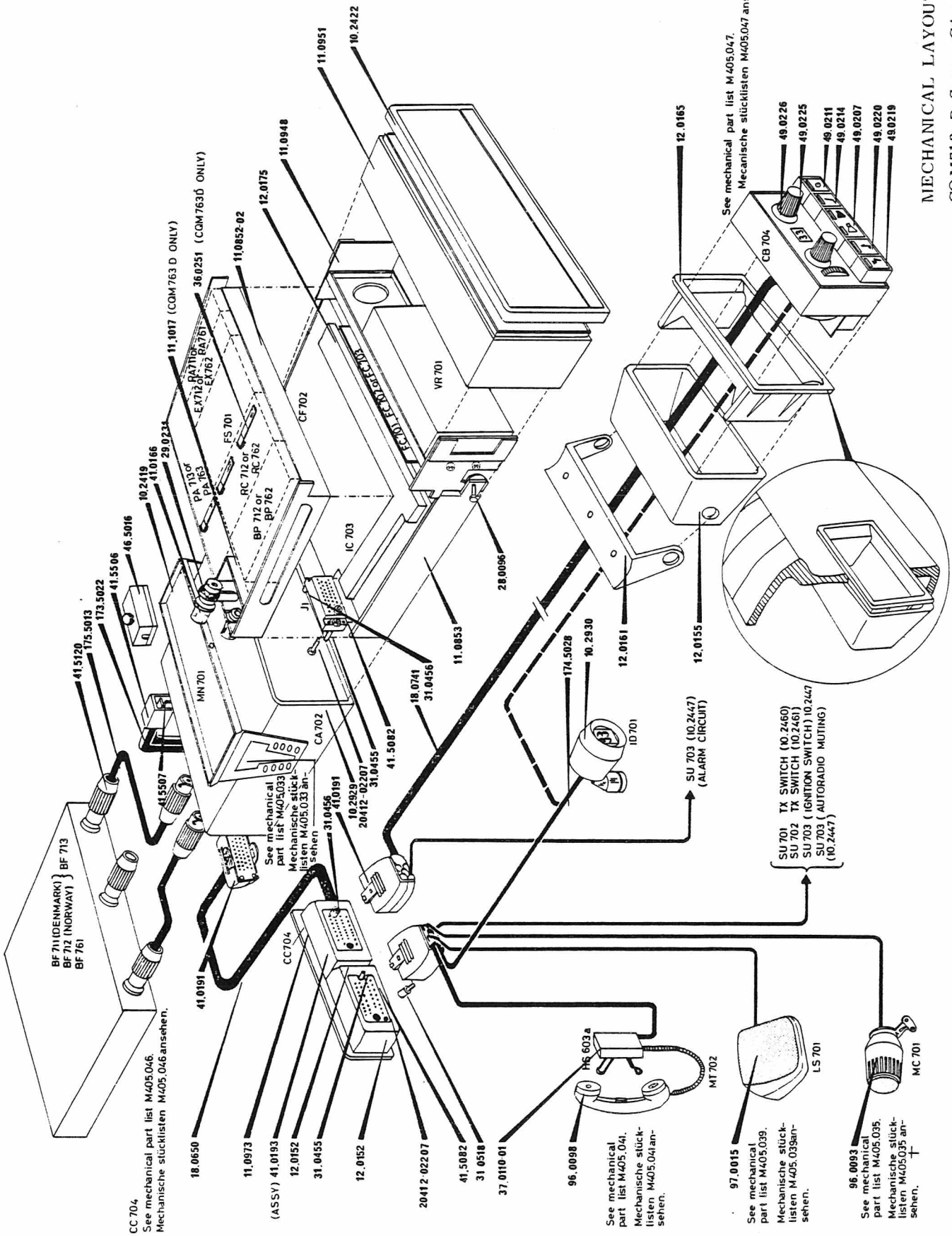
See mechanical part list M405.037
 Mecanische stücklisten M405.037 ansehen.

- 10.2442 CONTROL UNIT
- 10.2443 CONTROL UNIT
- 10.2440 BATTERY CABLE
- 10.2441 CONTROL CABLE
- 10.2424 CONTROL PANEL
- 10.2420 CONTROL PANEL
- 10.2422 CONTROL PANEL
- 97.0015 LOUDSPEAKER
- 97.0016 LOUDSPEAKER
- 96.0093 MICROPHONE
- 96.0094 MICROPHONE
- 10.2419 MOUNTING FRAME
- 10.2943 MOUNTING KIT
- 10.2545 MOUNTING KIT
- 96.0096 MOUNTING KIT
- 10.2460 MICROTELEPHONE
- 10.2461 SWITCHING UNIT
- 10.2447 SWITCHING UNIT

MECHANICAL PART LIST
 MECANISCHE STÜCKLISTEN

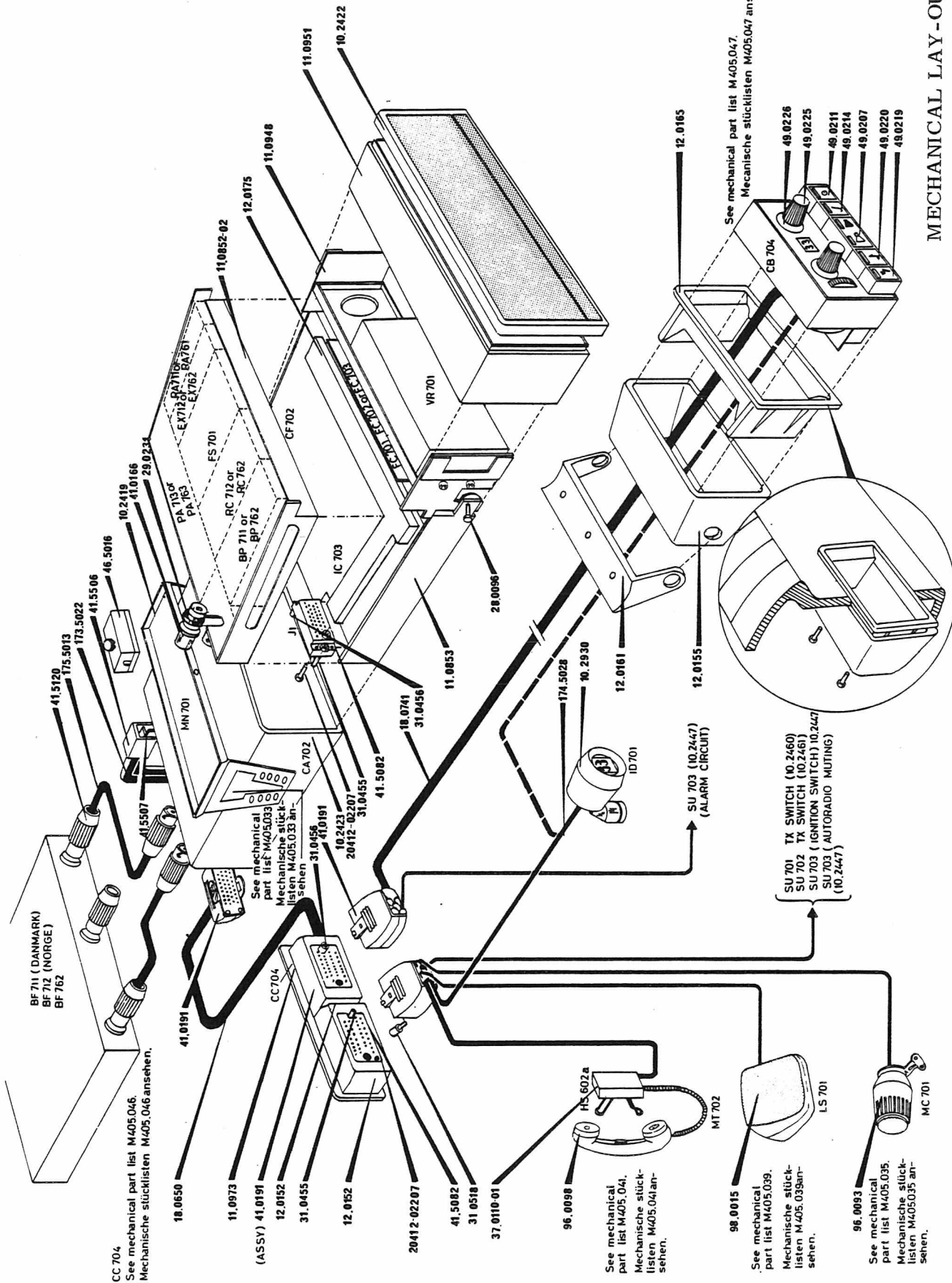
CQM700-25/15 W

M405.049



MECHANICAL LAYOUT

- CQ M713 D Spec. C4 x 49 DK
 - CQ M713 D Spec. C4 x 46 N
 - CQ M763 D Spec. C4 x 80 S
 - CQ M763 D Spec. C4 x 80 DK
- M405.048/4**



CC 704
See mechanical part list M405.046.
Mekanische stücklisten M405.046 ansehn.

(ASSY) 41.0191
See mechanical part list M405.039.
Mekanische stücklisten M405.039 ansehn.

96.0098
See mechanical part list M405.041.
Mekanische stücklisten M405.041 ansehn.

98.0015
See mechanical part list M405.039.
Mekanische stücklisten M405.039 ansehn.

96.0093
See mechanical part list M405.035.
Mekanische stücklisten M405.035 ansehn.

SU 701 TX SWITCH (10.2460)
SU 702 TX SWITCH (10.2461)
SU 703 (IGNITION SWITCH) 10.2447
SU 703 (AUTORADIO MUTING) (10.2447)

SU 703 (10.2447)
(ALARM CIRCUIT)

See mechanical part list M405.047.
Mekanische stücklisten M405.047 ansehn.

MECHANICAL LAY-OUT

CQM713D Spec. C4 x 49 DK
CQM713D Spec. C4 x 32 N
CQM763D Spec. C4 x 80 S

ITEM	CODE	DESCRIPTION
1.	10.2423	CA701 Cabinet with item 9 CA701 Kabinet med Pos 9
2.	15.0129	Frame: Front (rivetted to Pos. 4) Forramme monteret med pos. 4
3.	36.0222	Retaining spring: Push button Ass. Fjeder for CP701/CP702
4.	33.0370	Bracket: Front Panel Plade for sammenspænding
5.	52.0040	Grill: Loudspeaker Pynteplade for højttaler
6.	41.0184	Connector: 12V Konnektor for 12V
7.	41.0166	Connector: Antenna Konnektor for antenne
8.	29.0231	Nut.: Position 7 Møtrik for Pos. 7
9.	12.0164	Shield: Plexiglas Dækplade for type nr.
10.	41.5082	Connector: 34-PIN Konnektor: 34 pol
11.	31.0455	PIN: Guide Styretap for pos. 10
12.	31.0456	Bush: Guide Styrebøsning for 10
13.	2450-048027	Spring washer Fjederskive
14.	2205-026050	Nut Møtrik
15.	11.0852-01	Chassis Chassis for RF700
16.	20011-03006	Retaining screw Skrue for pos. 15
17.	2450-060032	Lock washer Spændskive
18.	20022-02004	Retaining screw Skrue
19.	11.0853	Chassis Chassis for BA700
20.	32.5048	Bumper: Black Rubber Afstandsstykke gummi
21.	54.0477	Terminal Board Tilslutningsliste
22.	12.0175	Guide: Cable Asembly (Grey plastic) Kablingsholder (grå plastik)
23.	37.0138	Hinge: Chassis Sammenspændingsbøjle

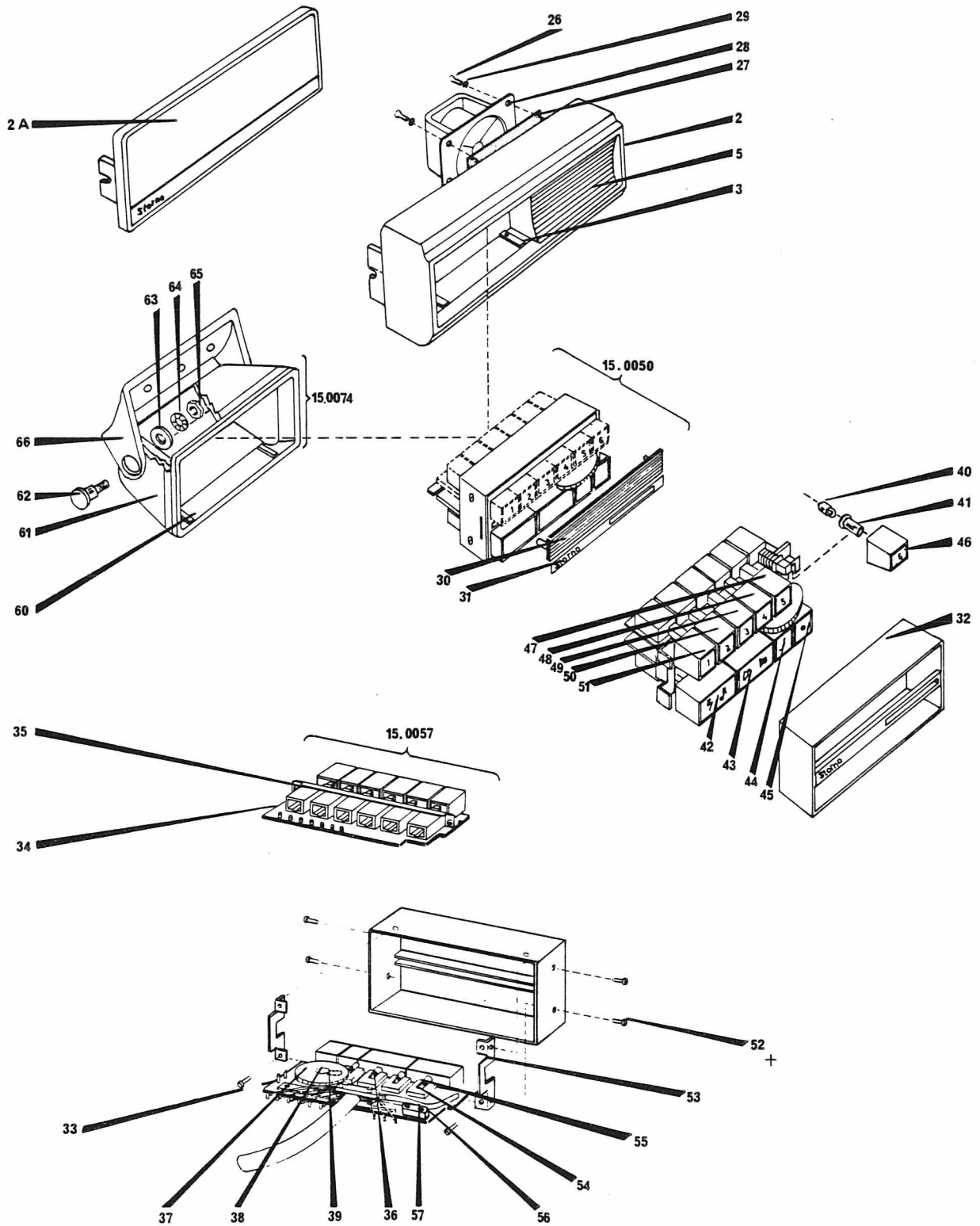
CABINET
KABINET CA701

ITEM	CODE	DESCRIPTION
24.	28.0096	Retaining screw: Hinge Skrue
25.	28.0095	Retaining screw: BA Skrue for BA-bund
26.	20.412-02207	Retaining screw: Loudspeaker Skrue for højttaler
27.	52.0041	Dust cover Beskyttelsesnet
28.	97.5032	Loudspeaker 5Ω 2 Watt Højttaler 5Ω 2 Watt
29.	2401-070028	Washer Skive
30.	51.0774	Front plate: Blank (only CP701) Pynteplade (kun i CP701)
31.	51.0764	Label "STORNO" Skilt "STORNO"
32.	12.0153	Frame: Push button Ramme for betjeningspanel
33.	54.0585	Terminal Board: Push Button Ass. Lederplade for tast/tone
34.	54.0584	Terminal Board: Channel switch Lederplade for kanalomskifter
35.	47.0562	Switch ass.: Push button (Channel switch) Omskifterenhed: Kanalomskifter
36.	47.0561	Switch ass.: Push button (Tone-on/off) Omskifterenhed: Tast/tone
37.	12.0166	Knob: Volume Control Knap: Volumenkontrol
	10.2560	TB701 Terminal Board: Shorting Strap long Kortslutningsprint, lang (See note 1)
	10.2561	TB702 Terminal Board: Shorting Strap short Kortslutningsprint, kort (See note 2)
		<u>Note 1</u> If the radio equipment is not provided with tone/transmitter, a terminal board shorting strap TB701 should be mounted on the terminal board 54.0477.
		<u>Note 2</u> If the radio equipment is not provided with tone/receiver, a terminal board shorting strap TB702 should be mounted on the terminal board 54.0477.

CABINET
KABINET CA701

Storno

Storno



CONTROL UNITS
BEDIENGERÄTE

CQM700
(CB700, CP700)

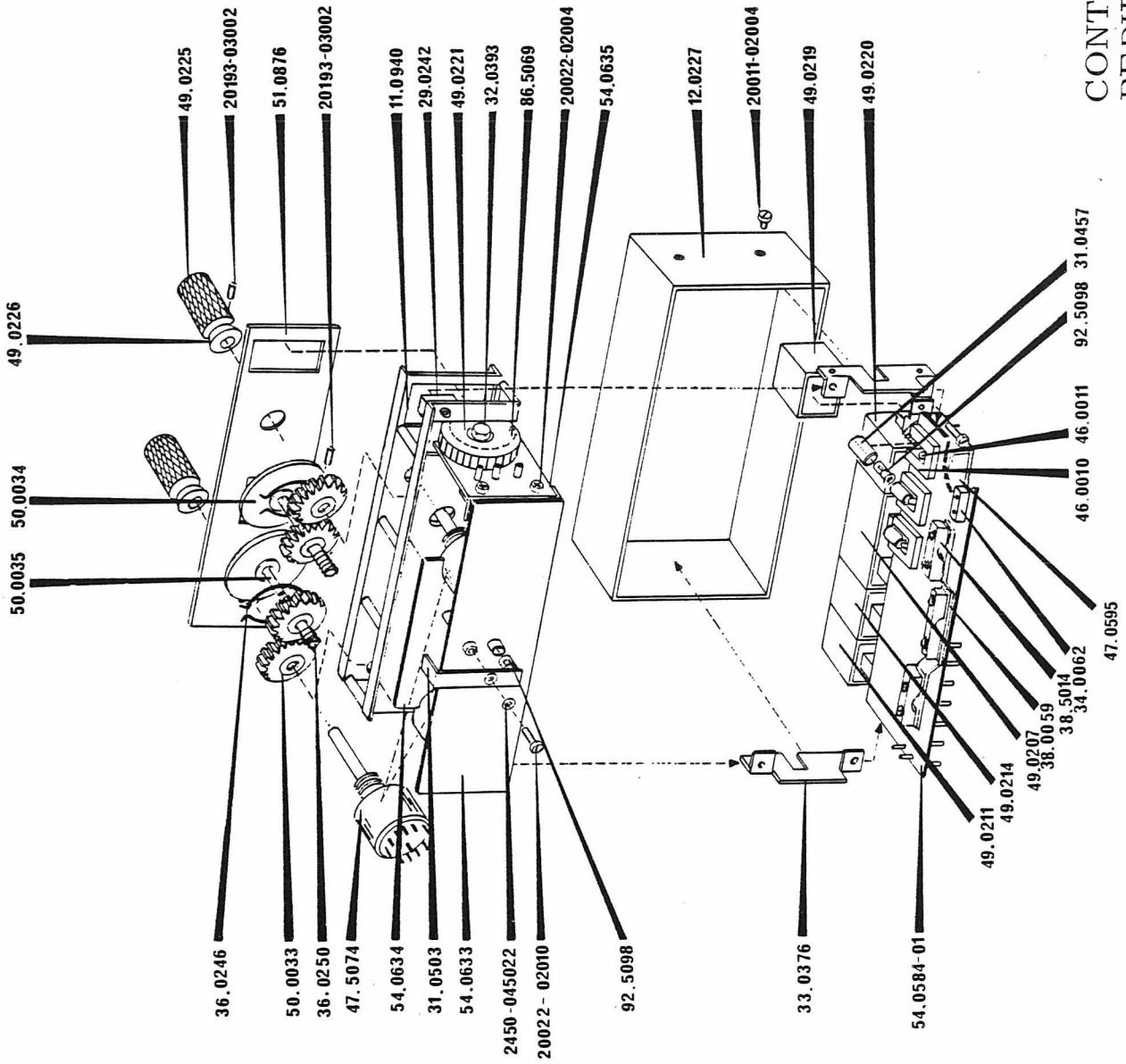
M405.037/2

ITEM	CODE	DESCRIPTION
	15.0050	Control Panel Complete (1 Channel) Betjeningspanel komplet (1 kanal)
	15.0057	Switch Unit Omskifter enhed
2.	15.0129	Frame: Front Forramme
2A	10.2422	Front Plate CP703 Forplade CP703
3.	36.0222	Retaining spring: Push button Ass. Fjeder for CP701/CP702
5.	52.0040	Grill: Loudspeaker Pynteplade for højttaler
26.	20.412-02207	Retaining screw: Loudspeaker Skrue for højttaler
27.	52.0041	Dust cover Beskyttelsesnet
28.	97.5032	Loudspeaker 5Ω 2 Watt Højttaler 5Ω 2 Watt
29.	2401-070028	Washer Skive
30.	51.0774	Front plate (only CP701) Pynteplade (kun i CP701)
31.	51.0764	Label "STORNO" Skilt "STORNO"
32.	12.0153	Frame: Push Button Ramme for betjeningspanel
33.	54.0584	Wiring Board: Push Button Ass. Lederplade for tast/tone
34.	54.0585	Wiring Board: Channel Switch Lederplade for kanalomskifter
35.	47.0562	Switch Ass: Push Button Ass. Channel Switch Omskifterenhed: Kanalomskifter
36.	47.0561	Switch Ass: Push Button (Tone On/Off) Omskifterenhed for tast/tone
37.	12.0166	Knob: Volume Control Knap for volumenkontrol
38.	86.5069	Potentiometer 5K Log. Potentiometer 5K Log.
39.	32.0393	Spring: Contact (Pos. 38) Fjeder for pos. 38
40.	92.5098	Incandescent Lamp 12V 0.06A Lampe 12V 0.06A
41.	31.0457	Bush (Pos. 40) Bøsning for pos. 40
42.	49.0208	Knob: Tone Knap: Tast/tone
43.	49.0207	Knob: Loudspeaker Knap: Højttaler
44.	49.0214	Knob: Squelch Knap: Squelch
45.	49.0211	Knob: On/Off Knap: Afbryder
46.	49.0216	Knob: Channel 6 Knap: Kanal 6
47.	49.0213	Knob: Channel 5 Knap: Kanal 5

CONTROL UNITS CQM700
BETJENINGSENHEDER (CB700, CP700)

ITEM	CODE	DESCRIPTION
48.	49.0210	Knob: Channel 4 Knap: Kanal 4
49.	49.0215	Knob: Channel 3 Knap: Kanal 3
50.	49.0212	Knob: Channel 2 Knap: Kanal 2
51.	49.0209	Knob: Channel 1 Knap: Kanal 1
52.	20011-02004	Screw Skrue
53.	33.0376	Bracket Bøjle for sammenspænding
54.	46.0010	Lamp Socket Lampeholder
55.	46.0011	Lamp Contact Lampe Kontakt
56.	39.0019	Connector 2 Pin Kontaktholder
57.	34.0062	Connector Pin Konnektor bøsning
60.	12.0165	Chassis ass. Chassis kompl.
61.	12.0155	Cabinet Kabinet
62.	28.0098	Screw Skrue
63.	2451-180062	Spring washer 18 x 6.2 x 0.6 Skive
64.	2442-090051	Washer Skive
65.	2207-050080	Nut Møtrik
66.	12.0161	Mounting frame Ophæng for CB700
60- 66	15.0074	Housing Svøb

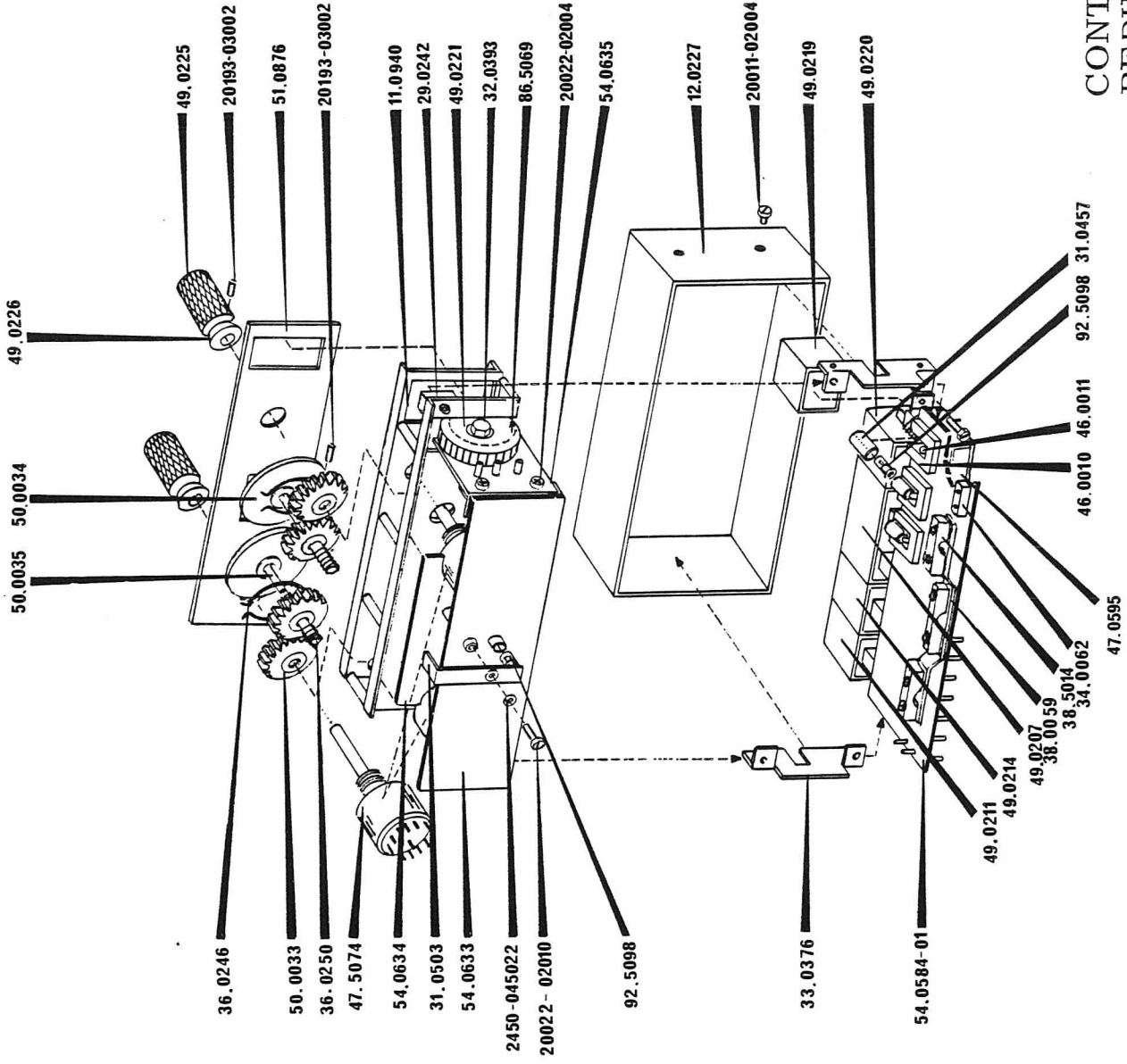
CONTROL UNITS CQM700
 BETJENINGSENHEDER (CB700, CP700)



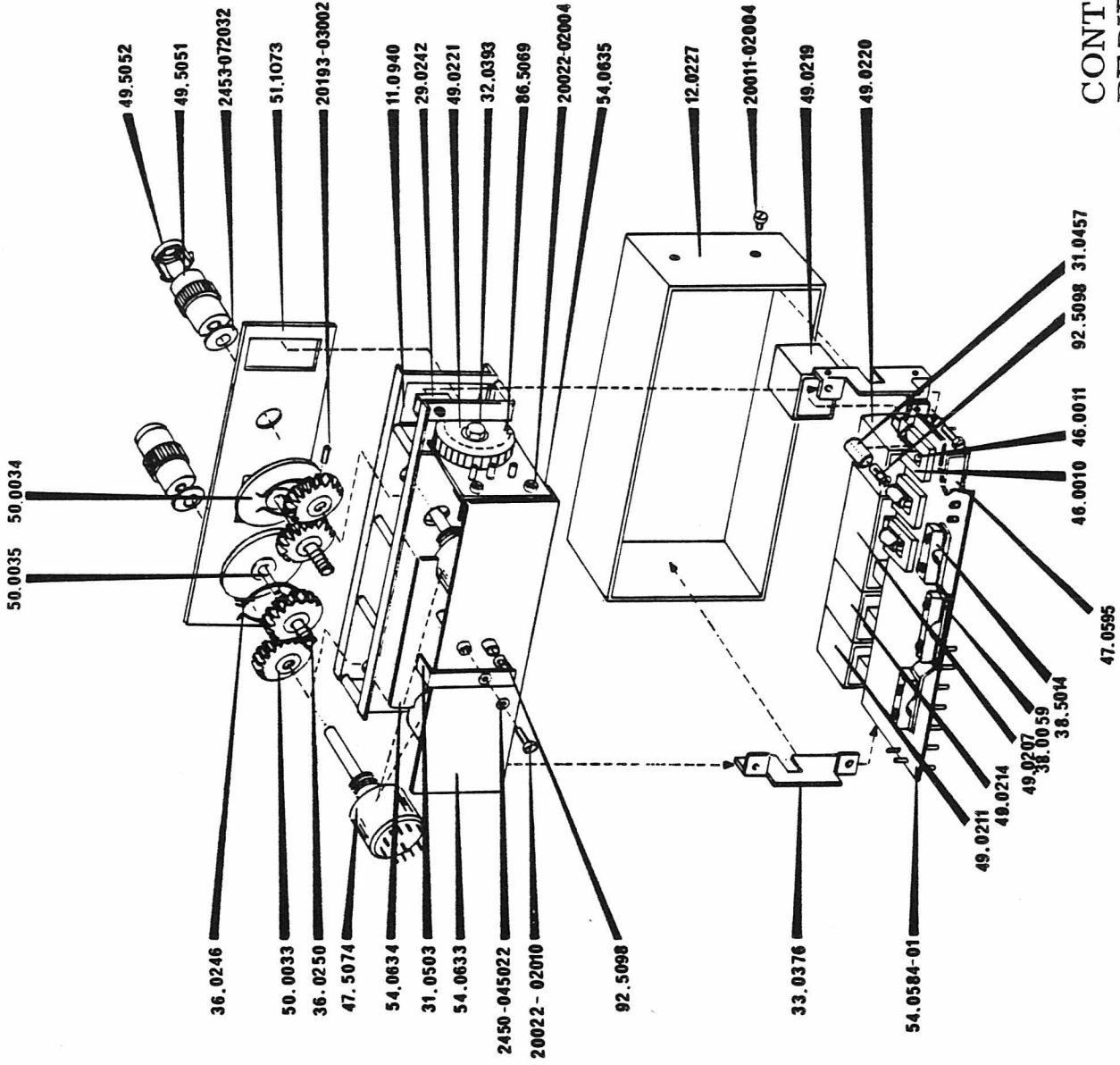
CONTROL UNIT
BEDIENGERÄTE

CB704

M405.047



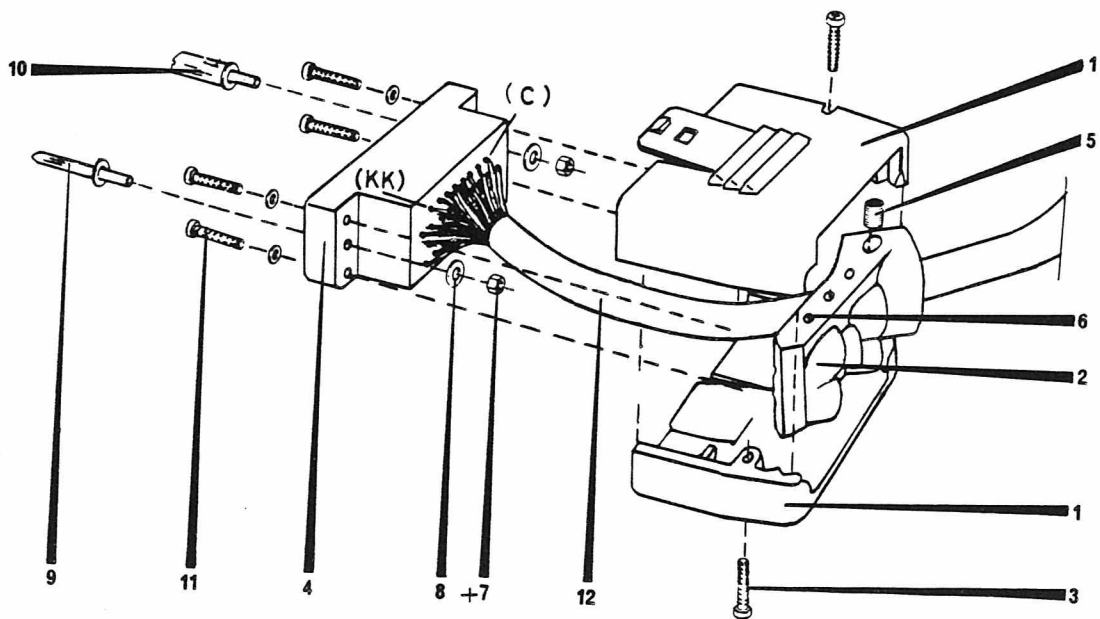
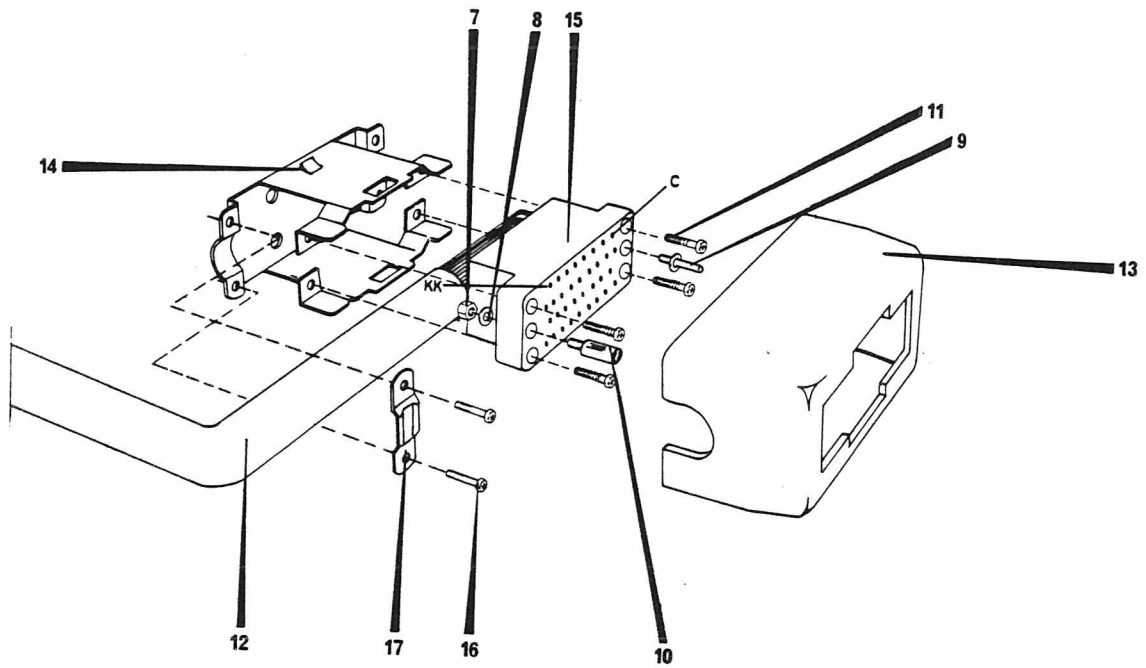
CONTROL UNIT
BEDIENGERÄTE



CONTROL UNIT
BEDIENGERÄTE

CB704

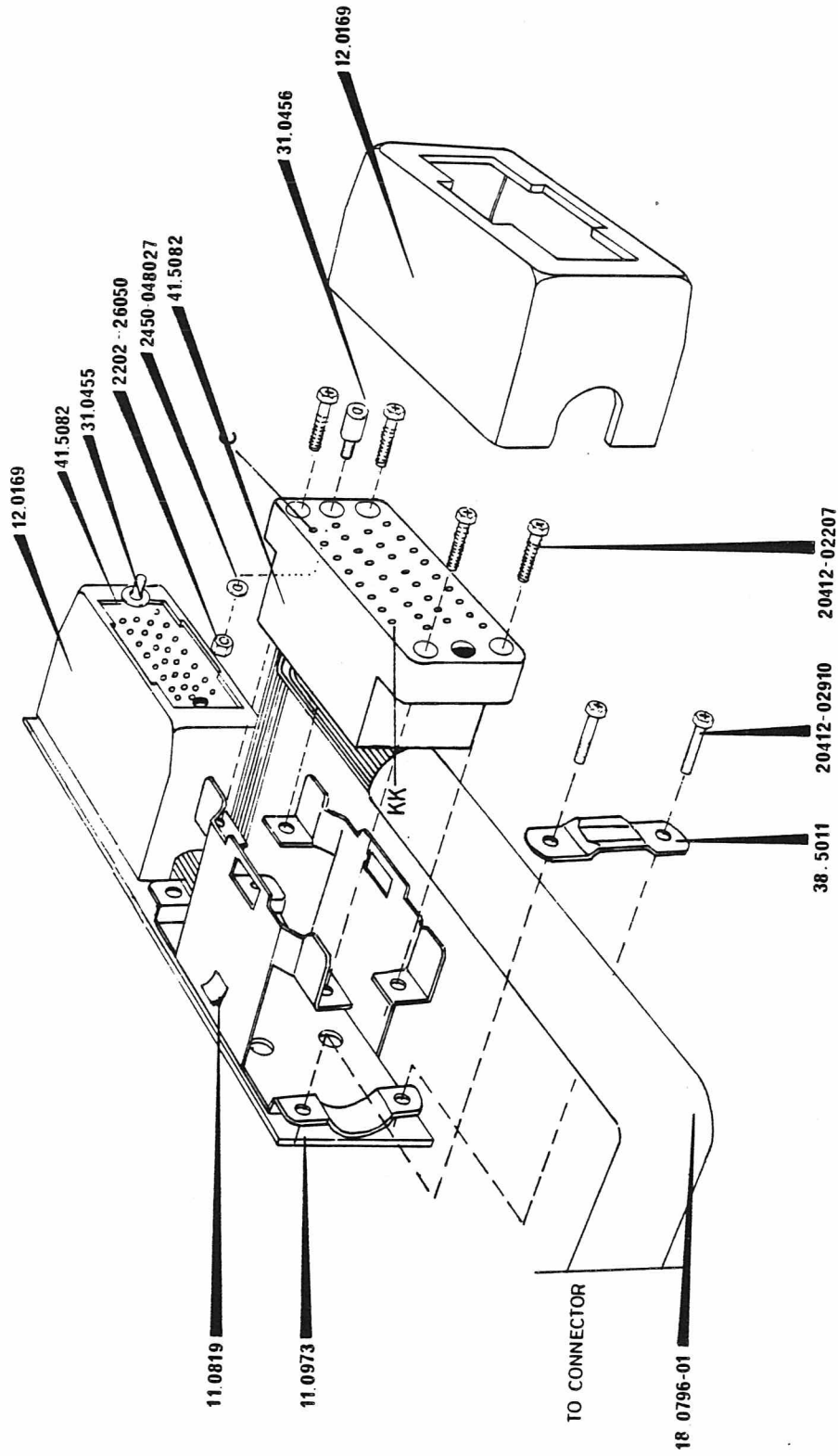
M405.047/3



CONNECTOR AND EXTENSION CABLE
 KONNEKTOR UND VERLÄNGERUNGS KABEL CC703

ITEM	CODE	DESCRIPTION
	41.0191	Connector Assy item (1-11) Konnektor komplet (Pos 1-11)
	41.0193	Connector assy (item 7-18) without item 12 Konnektor komplet (pos 7-18) uden Pos 12
1	12.0152	Housing Konnektor hus
2	12.0151	Cable hanger Kabelafastning
3	20412-02207	Screw 2,2 x 7 Skrue 2,2 x 7
4	41.5523	Connector Housing 34 - poled Konnektor hus
5	21141-06006	Screw Polyamid M 6 x 6 Skrue poluamid M 6 x 6
6	21141-04006	Screw polyamid M 4 x 6 Skrue polyamid m 4 x 6
7	2201-026050	Nut 4 D - 2,6 x 5 Møtrik 4 D - 2,6 x 5
8	2450-048027	Washer 4,8 x 2,7 Skive
9	31.0455	Guide pin Styre tap
10	31.0456	Guide bush Styre bøsning
11	20412-02207	Screw 2,2 x 7 Skrue 2,2 x 7
12	18.0650	Wiring with pin contacts Kabel med kontaktben
13	12.0169	Housing Hus for konnektor
14	11.0819	Chassis Chassis
15	41.5524	Connector housing 34-poled Konnektor hus 34 pol
16	20412-02910	Screw Skrue
17	38.5011	Cable Clamp Aflastningsbøjle

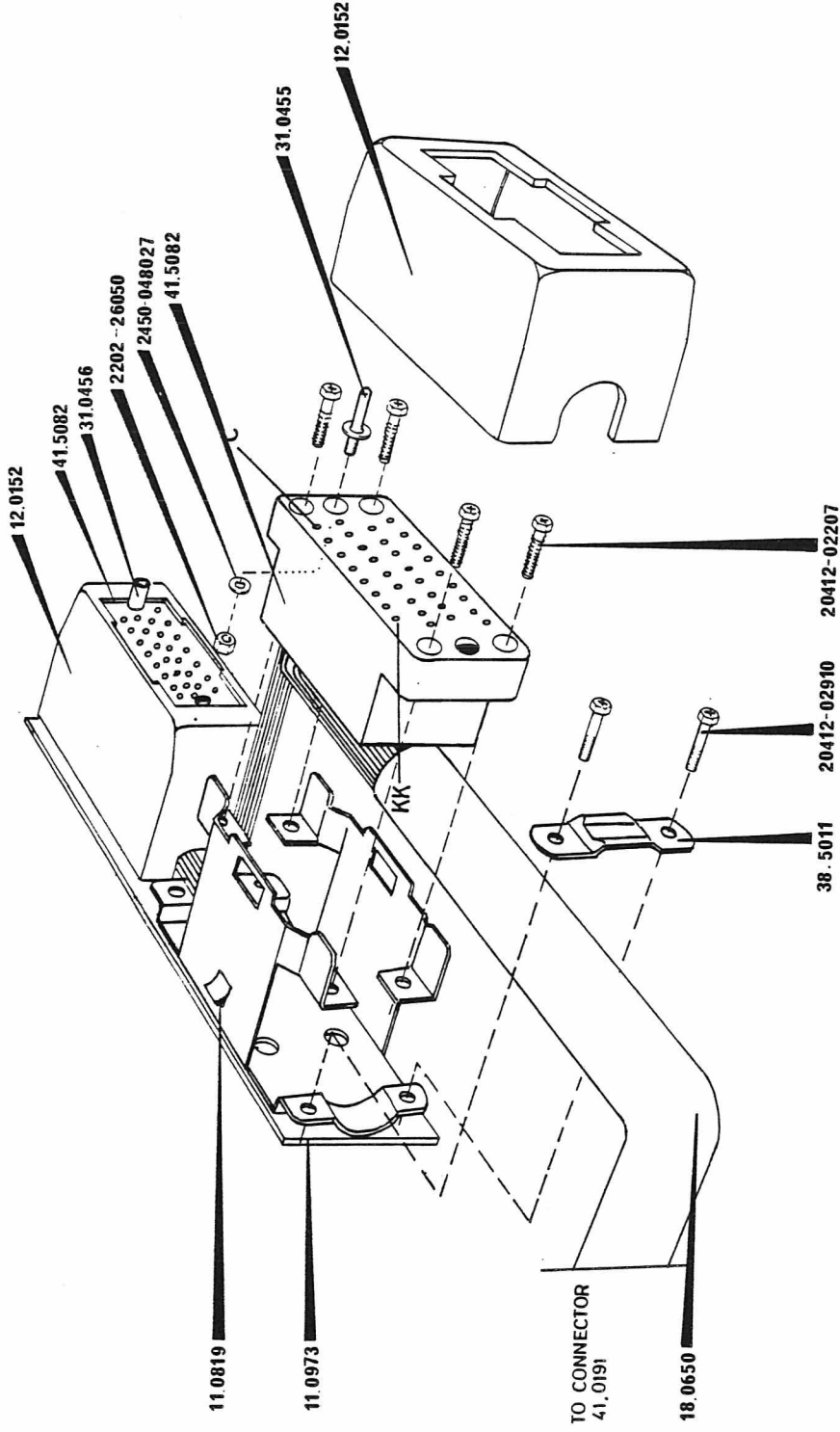
CONNECTOR AND EXTENSION CABLE CC703



MULTICONNECTOR
VIELFACHSTUECKER

CC704

M405.046/3

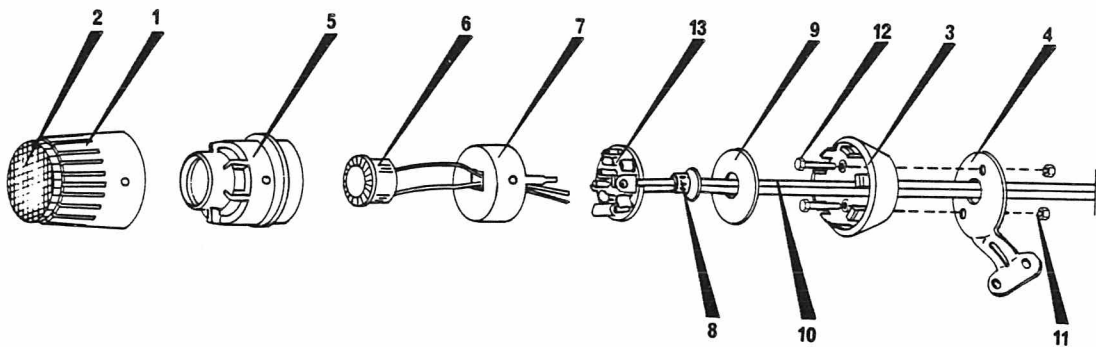


MULTICONNECTOR
VIELFACHSTECCKER

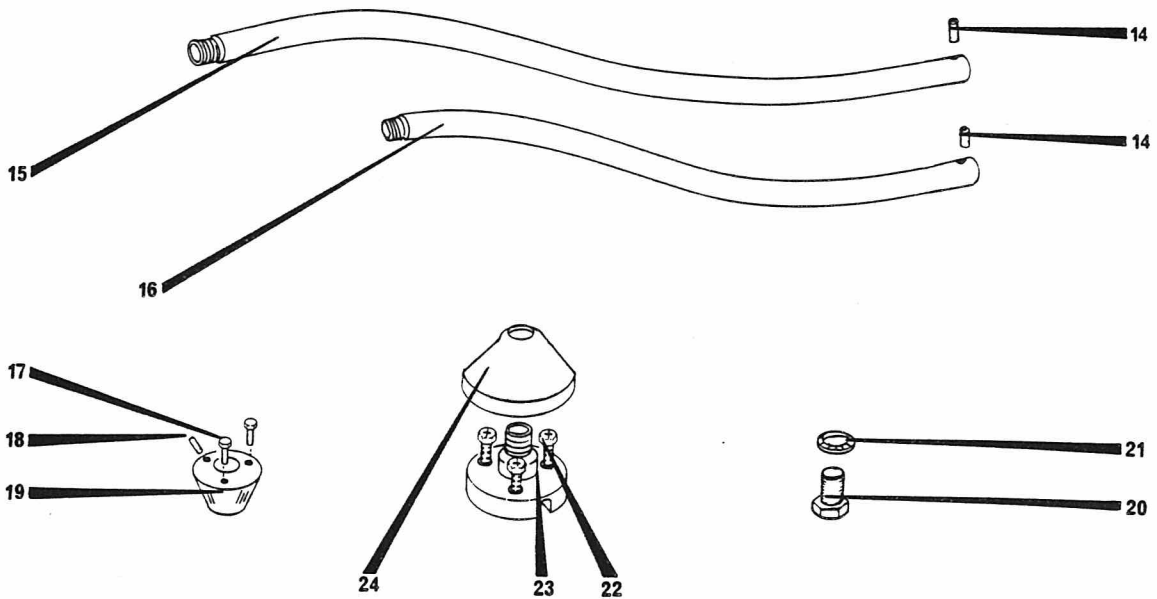
CC704

1M405.046

MICROPHONE MC701



MOUNTING KIT MK704



FIXED MICROPHONE MC701, MOUNTING KIT MK704
FEST MIKROFON MC702, EINBAU SATZ MK704

ITEM	CODE	DESCRIPTION
	96.0093	Microphone MC701 assembly Mikrofon MC701 komplet
1	15.0062	Microphone housing with dust cover Mikrofon hus med beskyttelsesnet
2	52.0038	Dust cover Beskyttelsesnet
3	12.0148	Microphone housing, rear Mikrofonhus, bagstykke
4	11.0816	Plate Plade
5	12.0147	Rubber suspension Gummiholder
6	96.5079	Microphone cartridge Mikrofon kapsel
7	68.0103	Can Skærmdåse
8	30.5023	Rivet 4,8 x 0,4 x 4,6 Nitte 4,8 x 0,4 x 4,6
9	53.0532	Washer Skive for bund
10	18.0627	2,5 m wiring with pin contact 2,5 m ledning med kontaktben
11	2202-030055	Nut M3 x 5,5 Møtrik
12	20242-03006	Screw M3 x 6 Skrue M3 x 6
13	10.2488	AA701 amplifier AA701 forstærker

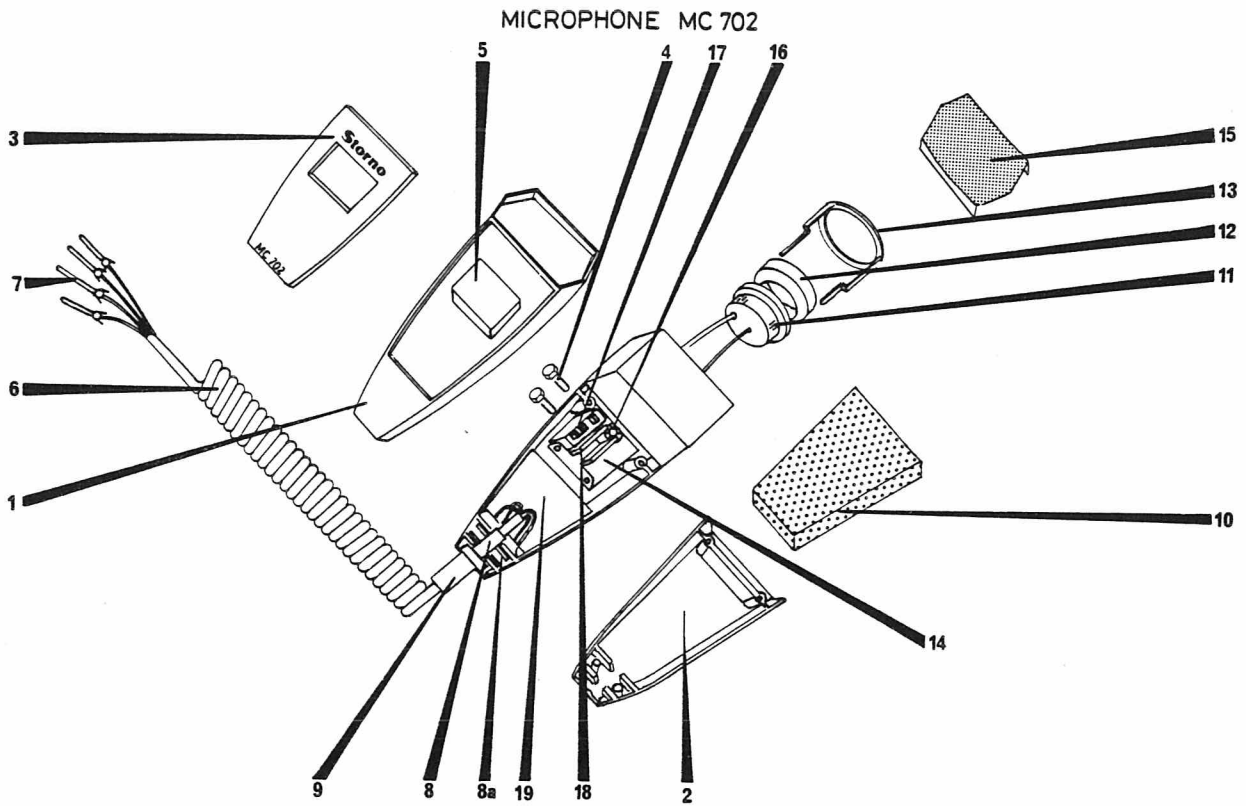
FIXED MICROPHONE ASS.
FAST MIKROFON KOMPL.

MC701

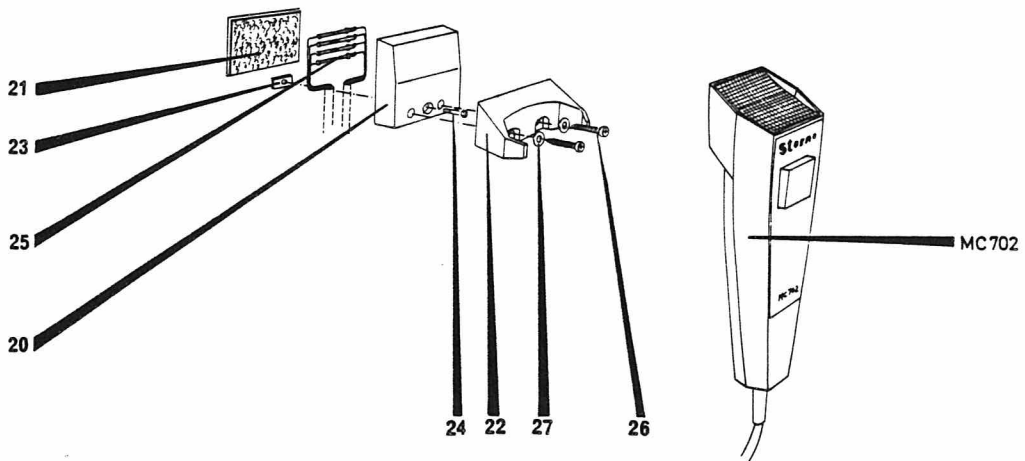
ITEM	CODE	DESCRIPTION
	10.2545	MK704 mounting kit / montage sæt
14	20193-03002	Screw Skrue
15	37.0140	Gooseneck 20 cm Svanehals 20 cm
16	37.0141	Gooseneck 35 cm Svanehals 35 cm
17	20242-03006	Screw Skrue
18	20063-03006	Screw Skrue
19	28.0099	Nipple for item 15 and 16 Nippel for pos 15 og 16
20	28.0065	Nipple for item 15 and 16 Nippel for pos 15 og 16
21	2441-180105	Washer Skive
22	20412-03913	Screw Skrue
23	28.0100	Nipple Nippel
24	32.0381	Cover Hætte

MOUNTING KIT
MONTAGESÆT

MK704



JUNCTION BOX JB701 AND MC 702



FIST MICROPHONE MC702, JUNCTION BOX JB701
HANDMIKROFON MC702, ANSLUSSKASTEN JB701

ITEM	CODE	DESCRIPTION
	96.0094	MC702 Microphone ass. MC702 Mikrofon kompl.
1	12.0174	Microphone housing Mikrofon hus
2	12.0172	Cover plate Bagstykke
3	51.0780	Front plate Forplade
4	20011-02010	Screw 2 x 10 Skrue
5	12.0171	Button Knap
6	18.0652	Spiral core Spiral snøre
7	41.5519	Pin contact 0,12 x 0,22 Kontakt ben
8	31.0307-10	Shrink tube Krymperør
8a	33.0361	Angle Vinkel
9	32.0383	Sleeve Gummitylle
10	32.0191	Foam packing Skumindlæg
11	96.5069	Microphone cartridge Mikrofon kapsel
12	32.0186-01	Rubberring Gummiring
13	37.0076	Spring for microphone unit Fjeder for mikrofon enhed
14	36.0202	Spring glip assembly Fjeder komplet
15	52.0043	Dust cover assembly Net for mikrofon komplet
16	2447-080030	Speed nuts 8 x 3 Låsering
17	47.5040	Microswitch Mikroswitch
18	33.0331-01	Bracket for item 14 Bøjle for pos 14
19	10.2548	AA702 Amplifier ass. AA702 Forstærker kompl.

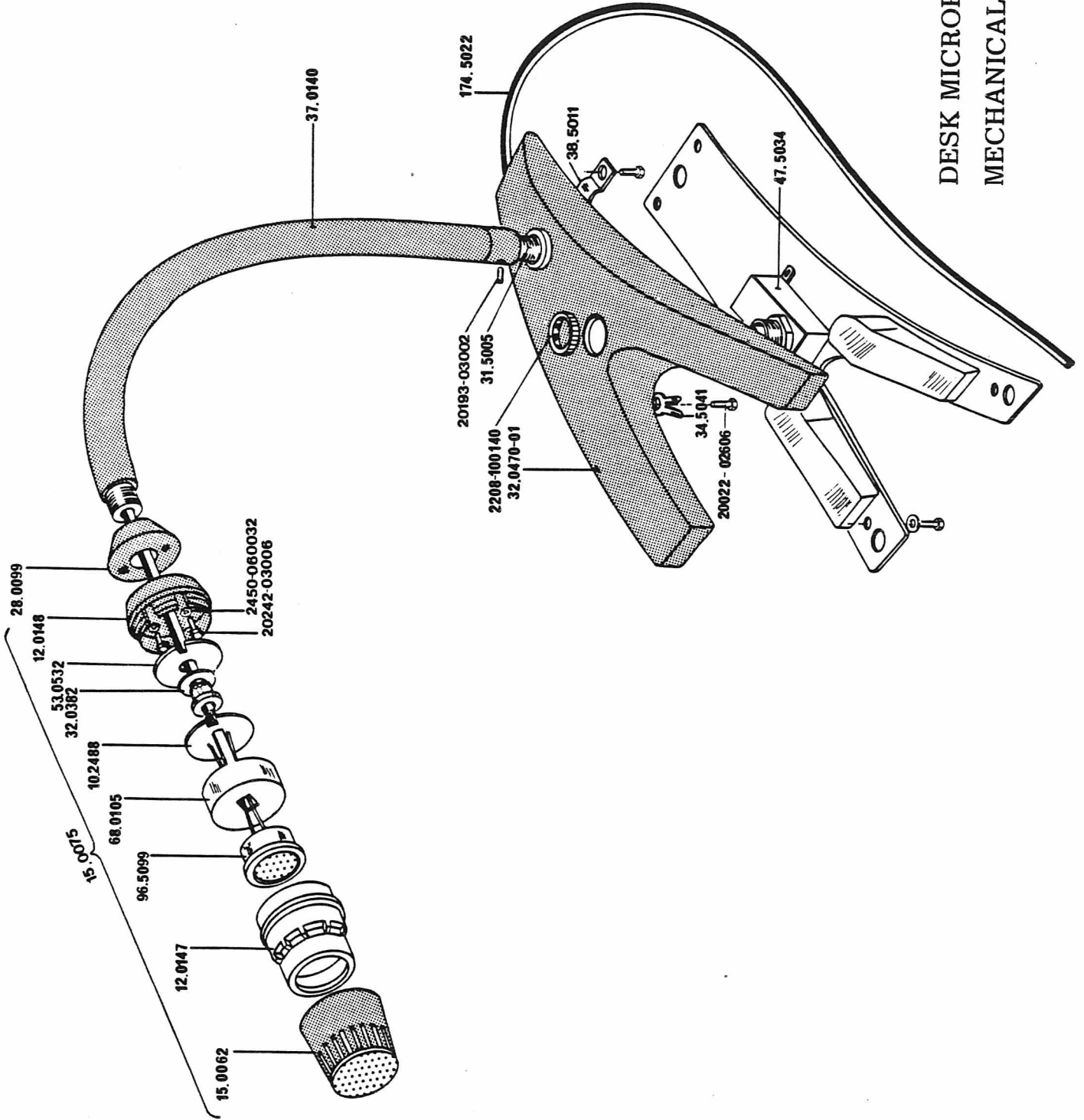
FIST MICROPHONE
HÄNDMIKROFON

MC702

ITEM	CODE	DESCRIPTION
	10.2543	Junction box JB701 ass. Samleboks JB701 kompl.
20	12.0170	Housing black Hus sort
21	32.0377	Retaining plate: foam Skumplade
22	12.0173	Microphone retainer Mikrofon holder
23	38.0058	Cable clamp Kabelbøjle
24	20022-03008	Screw M 3 x 8 Skrue M 3 x 8
25	18.0646	Cable 2,50 m with pin and socket contact Kabel 2,50 m med stik monteret
26	20412-04225	Screw 4,2 x 25 Skrue 4,2 x 25
27	2450-080043	Washer Skiver

JUNCTION BOX ASS.
SAMLEBOKS KOMPL.

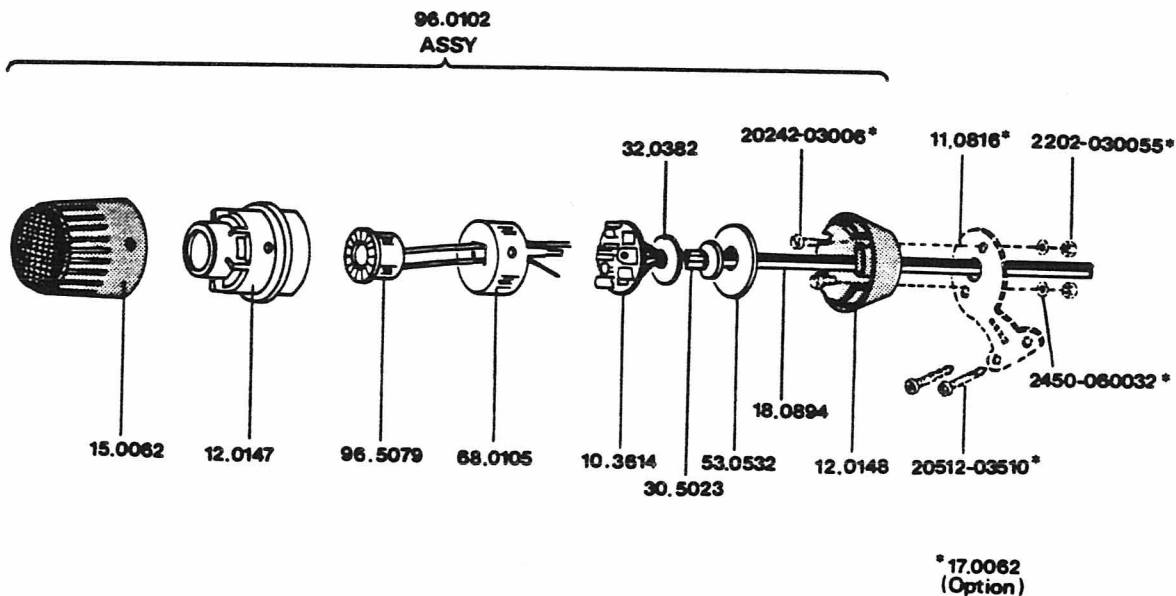
JB701



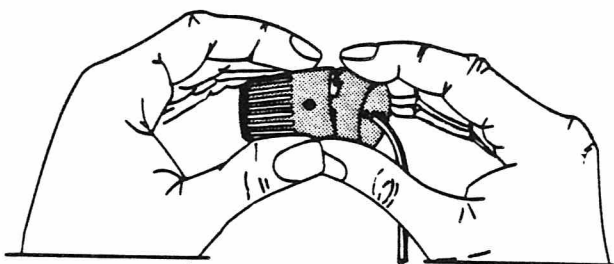
DESK MICROPHONE
MECHANICAL LAY OUT

MC703

M405.082



DISMANTLING



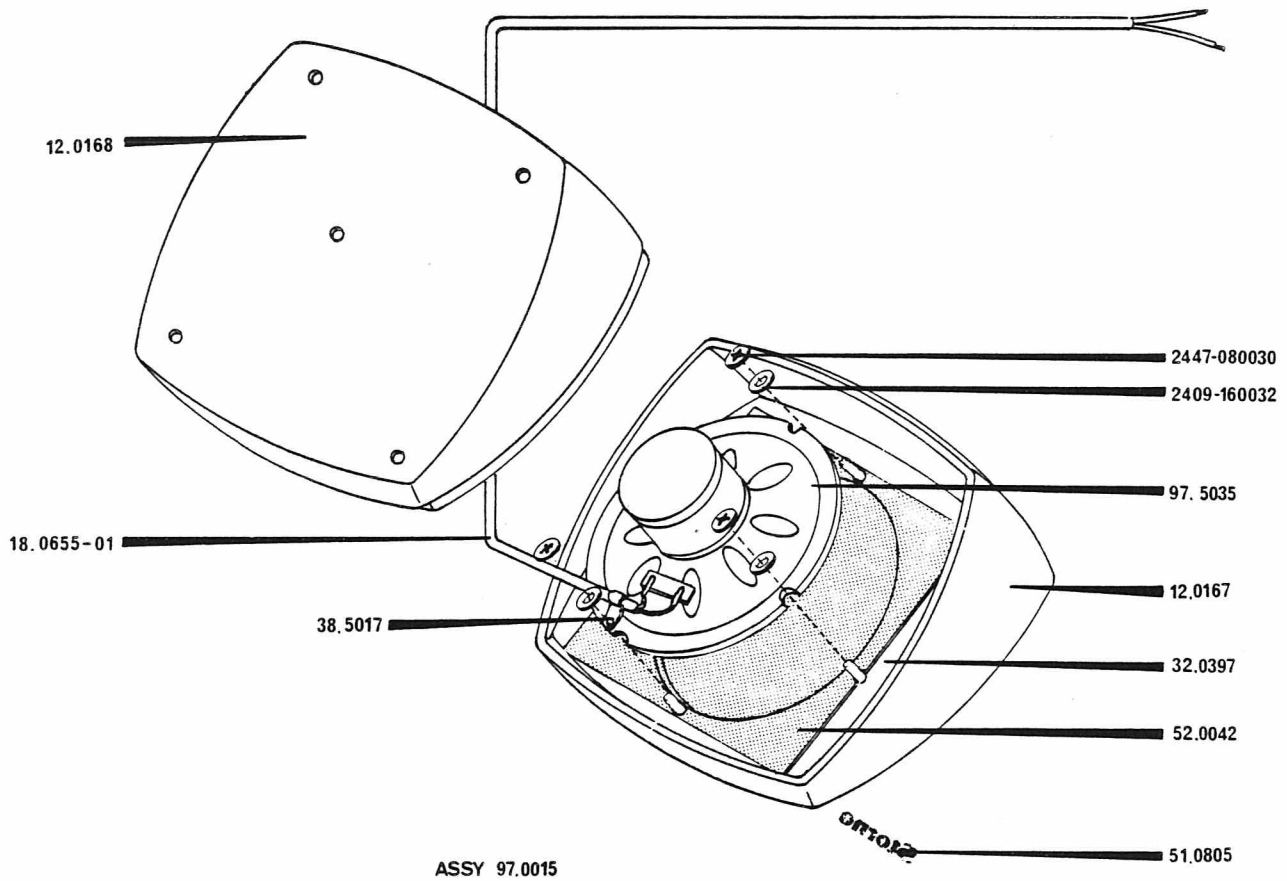
MICROPHONE
MECHANICAL LAY OUT

MC704

M405.089

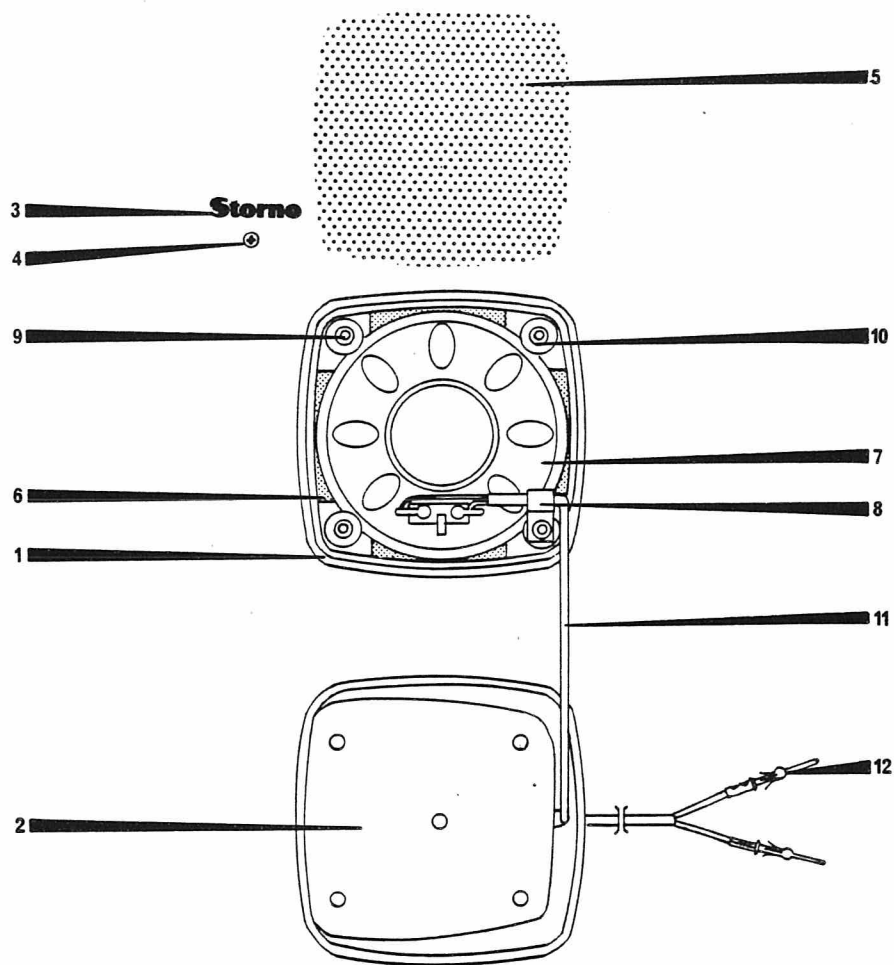
Storno

Storno



LOUDSPEAKER LS701

M405.039/2



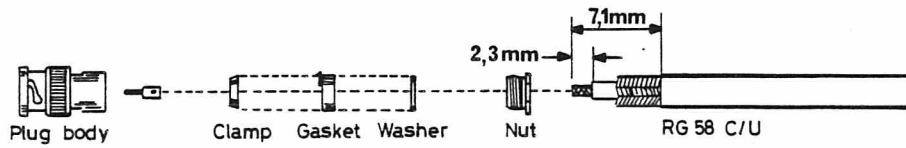
LOUDSPEAKER
LAUTSPRECHER LS701

M405.039

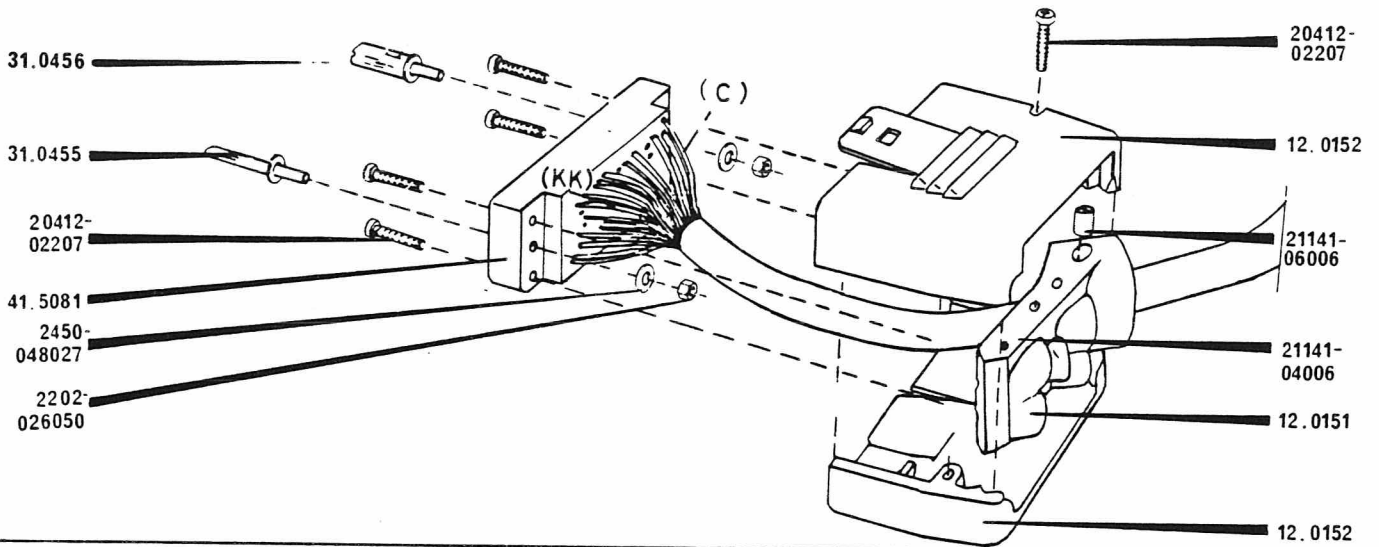
ITEM	CODE	DESCRIPTION
	98.0015	Loud speaker assy. Højtaler komplet
1	12.0167	Cabinet front part Kabinet forside
2	12.0168	Cabinet rear part Kabinet bagside
3	51.0805	Motif Firmaskilt
4	2447-080030	Speed nut for item 3 Låseskive for pos. 3
5	52.0042	Grille Højtalernet
6	32.0397	Dust filter Støv filter
7	97.5035	Loud speaker Højtaler
8	38.5017	Cabel clamp Aflastningsbøjle
9	20412-02910	Screw 2,9 x 10 Skrue 2,9 x 10
10	2409-160032	Washer 16 x 3,2 x 1 Skive
11	18,0655	Wiring assy. with item 12 Ledning kompl. med pos. 12
12	41.5520	Pin Kontaktben

LOUDSPEAKER LS701
HØJTTALER

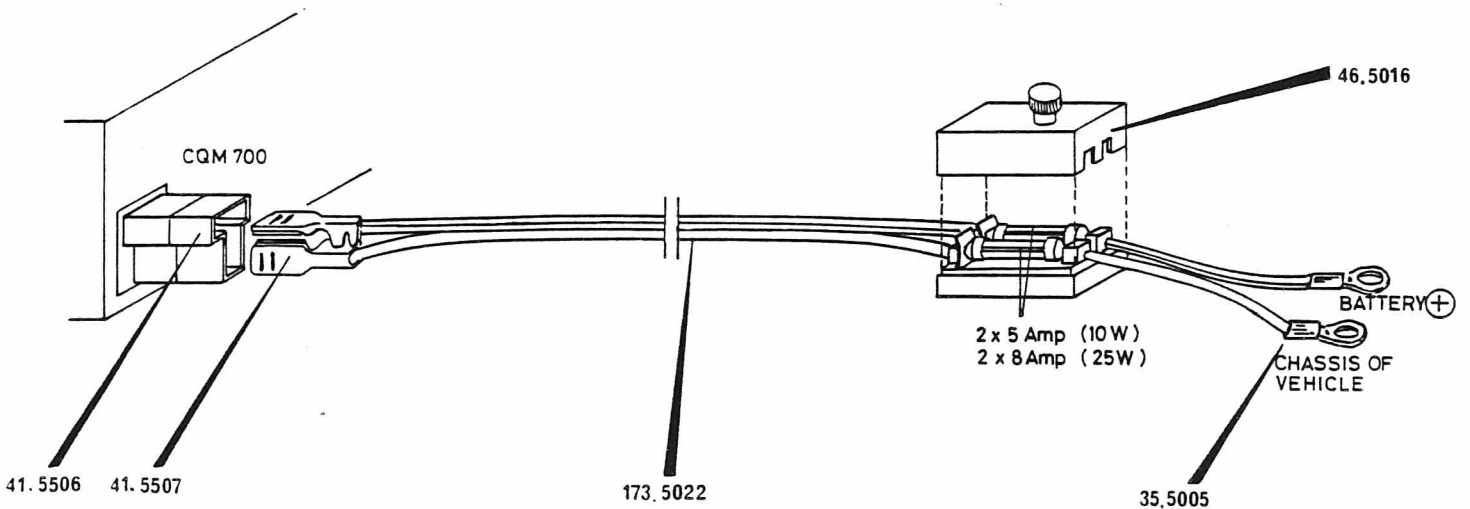
ANTENNA CONNECTOR (41.5120)



CONNECTOR ASSEMBLY (41.0191-01)



BATTERY CONNECTION



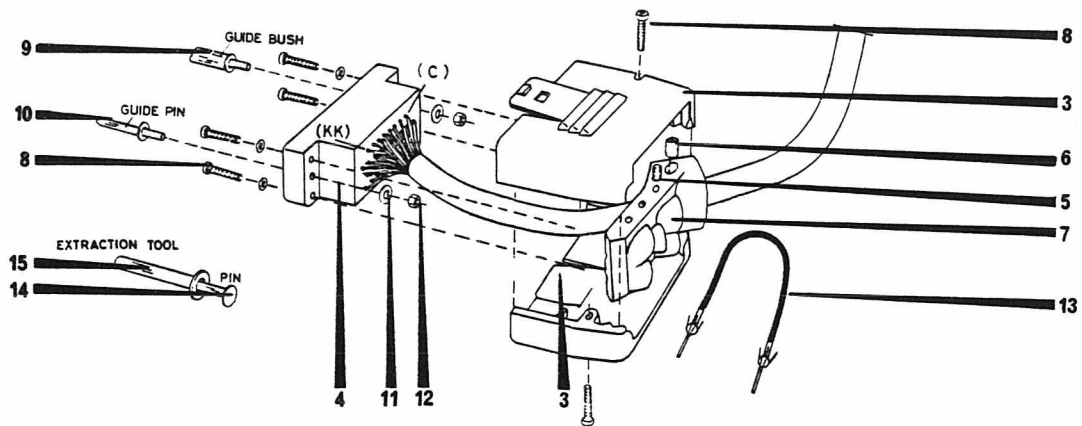
**MOUNTING KIT
EINBAU SATZ**

MK701

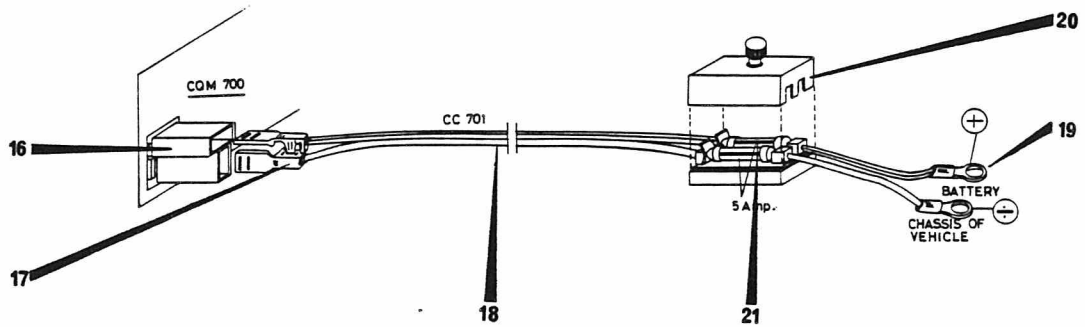
ANTENNA CONNECTOR 41.5120



CONNECTOR ASSEMBLY 41.0191



BATTERI CONNECTION



MOUNTING KIT
EINBAU SATZ

MK701

ITEM	CODE	DESCRIPTION
1	41.5120	Antenna connector Antenne konnektor
2	175.5013	Coax cable Coaxkabel
	41.0191	Connector assembly Konnektor komplet
3	12.0152	Housing Hushalvdel
4	41.5523	Connector 34 pole Konnektor 34 pol
5	21141-04006	Nylon screw M 4 x 6 Nylon skrue M 4 x 6
6	21141-06006	Nylon screw M 6 x 6 Nylon skrue M 6 x 6
7	12.0151	Cablehanger Aflastning for kabel
8	20.412-02207	Screw 2,2 x 7 Skrue
9	31.0456	Guide bush Styrebøsning
10	31.0455	Guide pin Styretap
11	2450-048027	Washer 4,8 x 2,7 Skive 4,8 x 2,7
12	2202-026050	Nut 6 kt 2,6 x 5 Møtrik 2,6 x 5
13	18.0668	Shorting strap Kortslutningsledning
14	31.0470	Pin for extraction tool Tap for udtrækkerværktøj
15	30.0033	Extraction tool Udtrækkerværktøj
	32.0394	Rubber plug for item 7 Gummiprop for pos 7
		Battery connection Batteri tilslutning
16	41.5506	Housing for item 17 Holder for pos 17
17	41.5507	Socket contact Kontakt
18	173.5022	Battery cable Batteri kabel
19	35.5005	Cable eye Kabelsko

MOUNTING KIT
MONTAGESÆT

MK701

M405.032-2

Storno

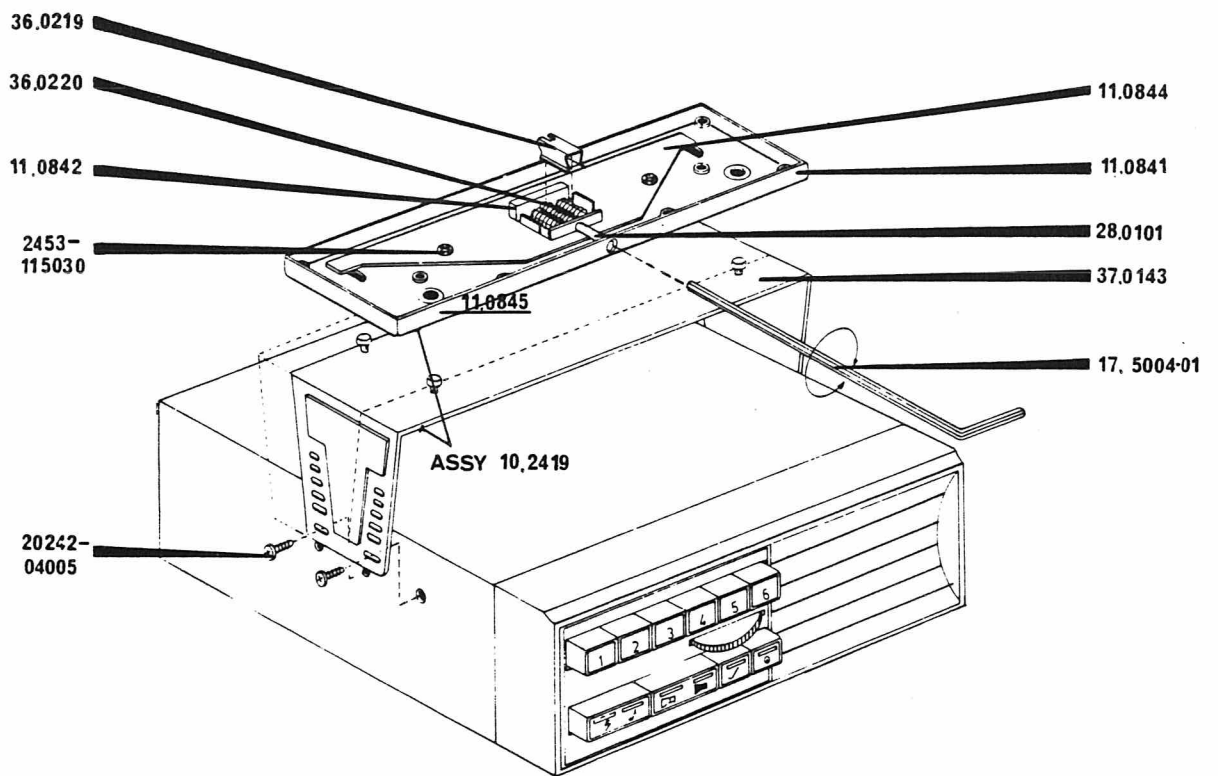
Storno

ITEM	CODE	DESCRIPTION
20	46.5016	Fusebox Sikringsboks
21	92.5100	Fuse 5 amp. Sikring 5 amp.

MOUNTING KIT
MONTAGESÆT

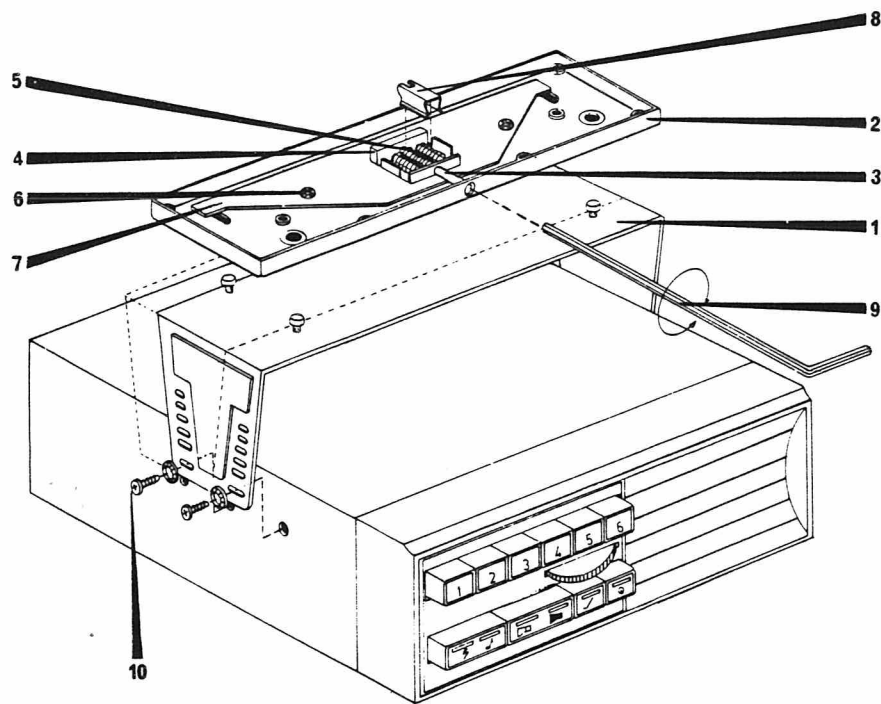
MK701

M405.032/2-3



MOUNTING FRAME
OPSPÆNDINGSBESLAG

MN701



MOUNTING FRAME
OPSPÆNDINGSBESLAG

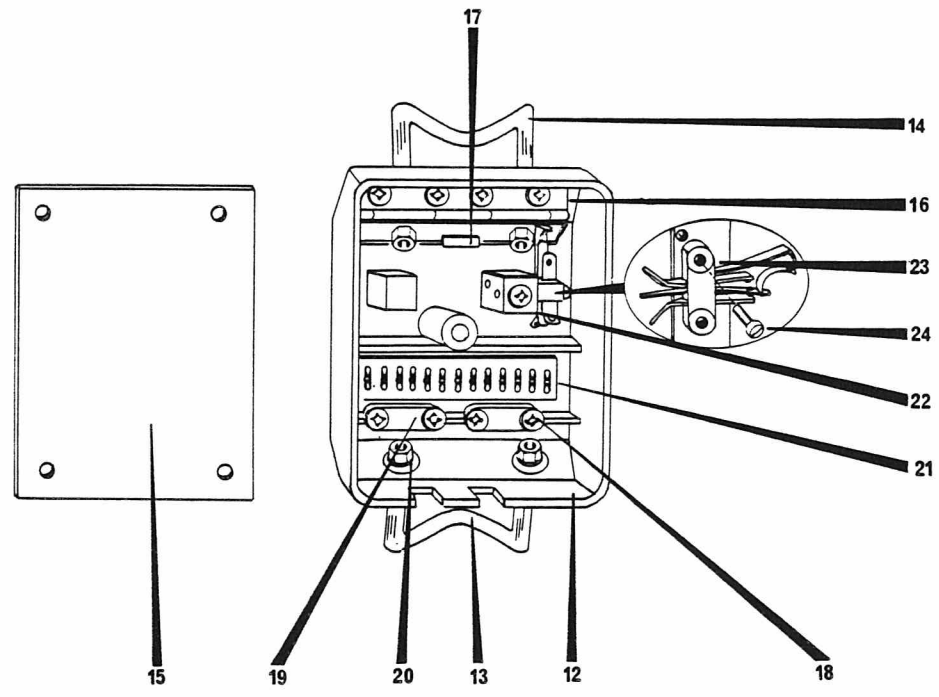
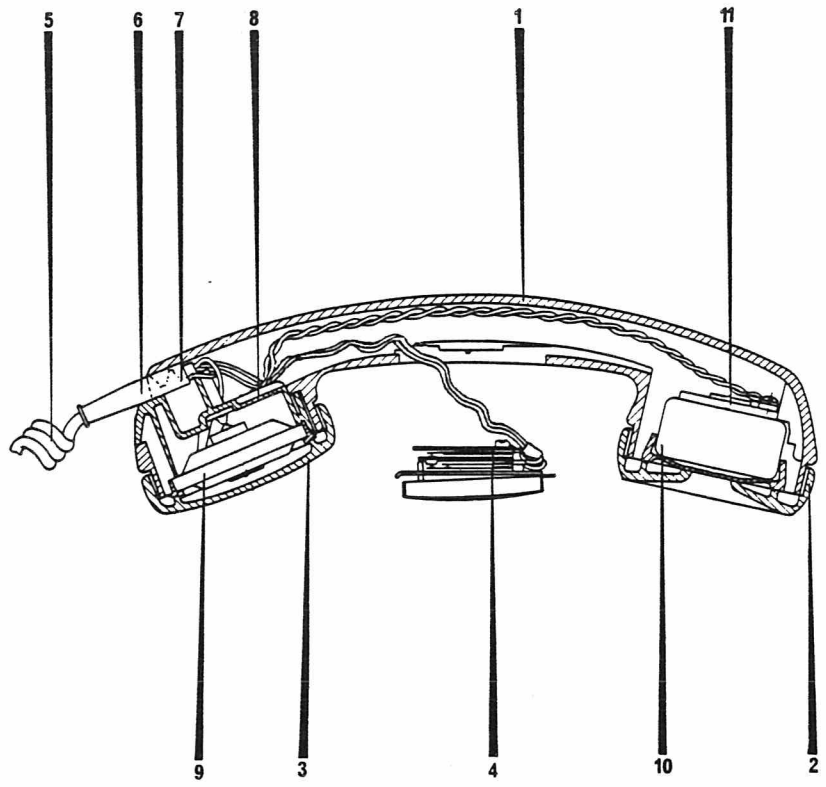
MN701

M405.033/2

ITEM	CODE	DESCRIPTION
	10.2419	MN701. Mounting frame assembly Montagesæt komplet
1	37.0143	Mounting bracket Fastspændingsbeslag
2	11.0846	Mounting stand Montagebeslag
3	28.0101	Screw 5,5 cm Skrue 5,5 cm
4	11.0842	Guidepin: spring Holder for fjeder
5	36.0220	Spring for item 4 Fjeder for pos 4
6	2453-115030	Speed nut Låsering
7	11.0844	Lock plate: sheet metal Glideplade
8	36.0219	Retaining bar: spring Låsebøjle
9	17.5004-01	Unbrako tool Unbraconøgle
10	20242-04005	Screw 4 x 5 Skrue 4 x 5

MOUNTING FRAME ASS. CQM700
OPHÆNG KOMPLET CQM700

MN701



MICROTELEPHONE HANDSET
HANDAPPARAT

MT701/HS602a

ITEM	CODE	DESCRIPTION
	96.0097	Micro-telephone Handset Assy Mikrotelefon komplet
1	96.5080	Housing Mikrotelefon hus
2	96.5082	Telephone cover Dæksel for telefon
3	96.5083	Microphone cover Dæksel for mikrofon
4	96.5084	Push button Trykomskeer
5	18.0725	Coiled lead 6 core with item 6-7 Spiralsnøre 6 leder med pos. 6 og 7
6	32.5051	Rubber sleeve Gummi tylle
7	38.5037	Clamp strip Aflastningsbøjle
8	96.5081	Microphone insert Holder for mikrofon
9	96.5074	Microphone cartridge 1500 Ω Mikrofonkapsel 1500 Ω
10	96.5085	Telephone cartridge 65 Ω Telefon kapsel 65 Ω
11	10.2809	AA703 Amplifier assy AA703 Forstærker komplet
	37.0110-01	HS 602a Retainer assy Ophæng komplet
12	12.0137	Housing (Plastic) Hus (Plastik)
13	44.0085	Retaining arm fixed bøjle fast
14	44.0084-01	Retaining arm sprung Bøjle
15	11.0769-01	Bottom plate Bundplade
16	37.0139	Hinge Hængsel
17	36.0212	Spring Fjeder
18	20412-02910	Screw Skrue
19	38.5014	Clamp Aflastningsbøjle
20	2202-040079	Nut møtrik

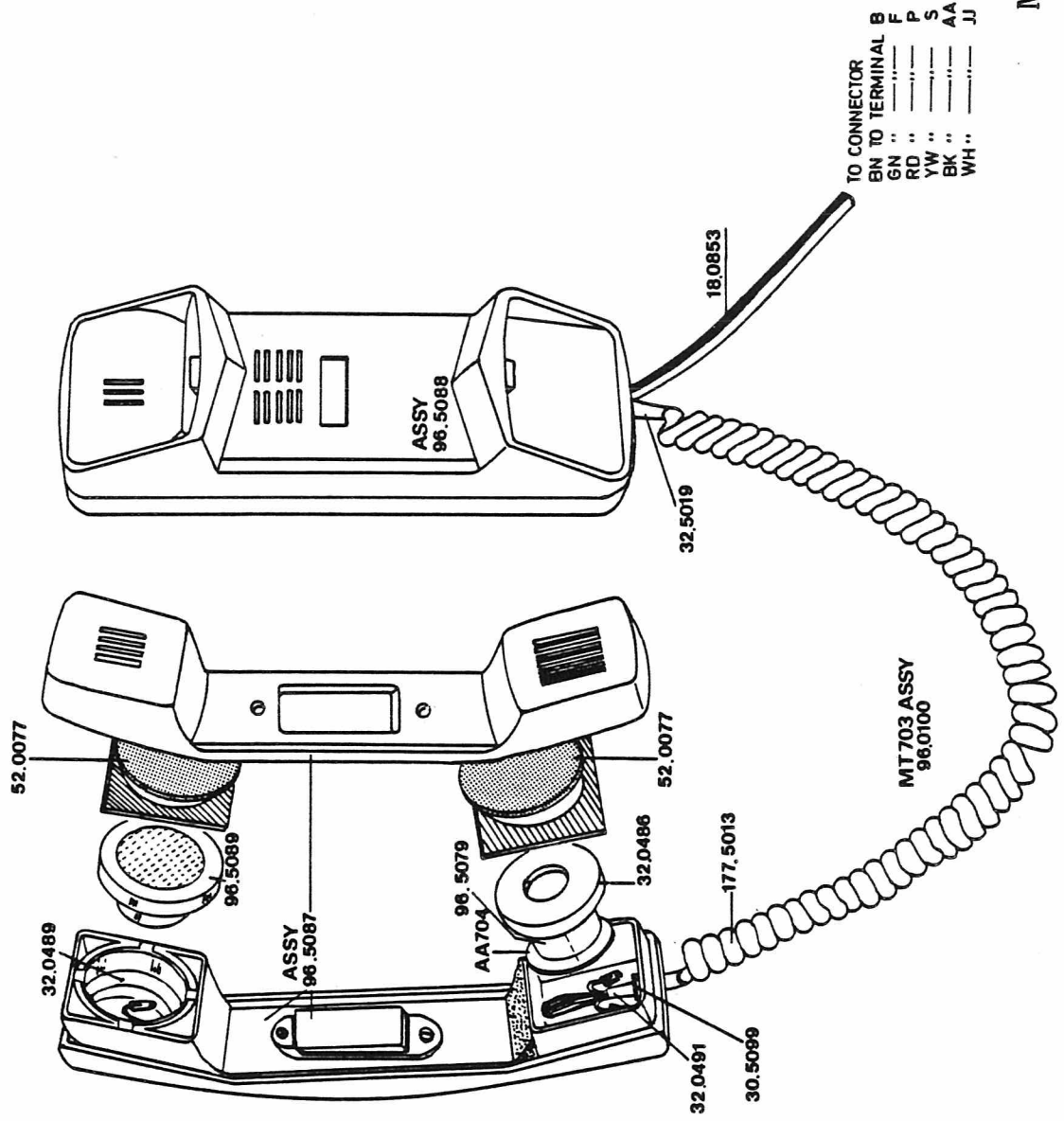
MICROTELEPHONE HANDSET MT701/HS602a

Stomo

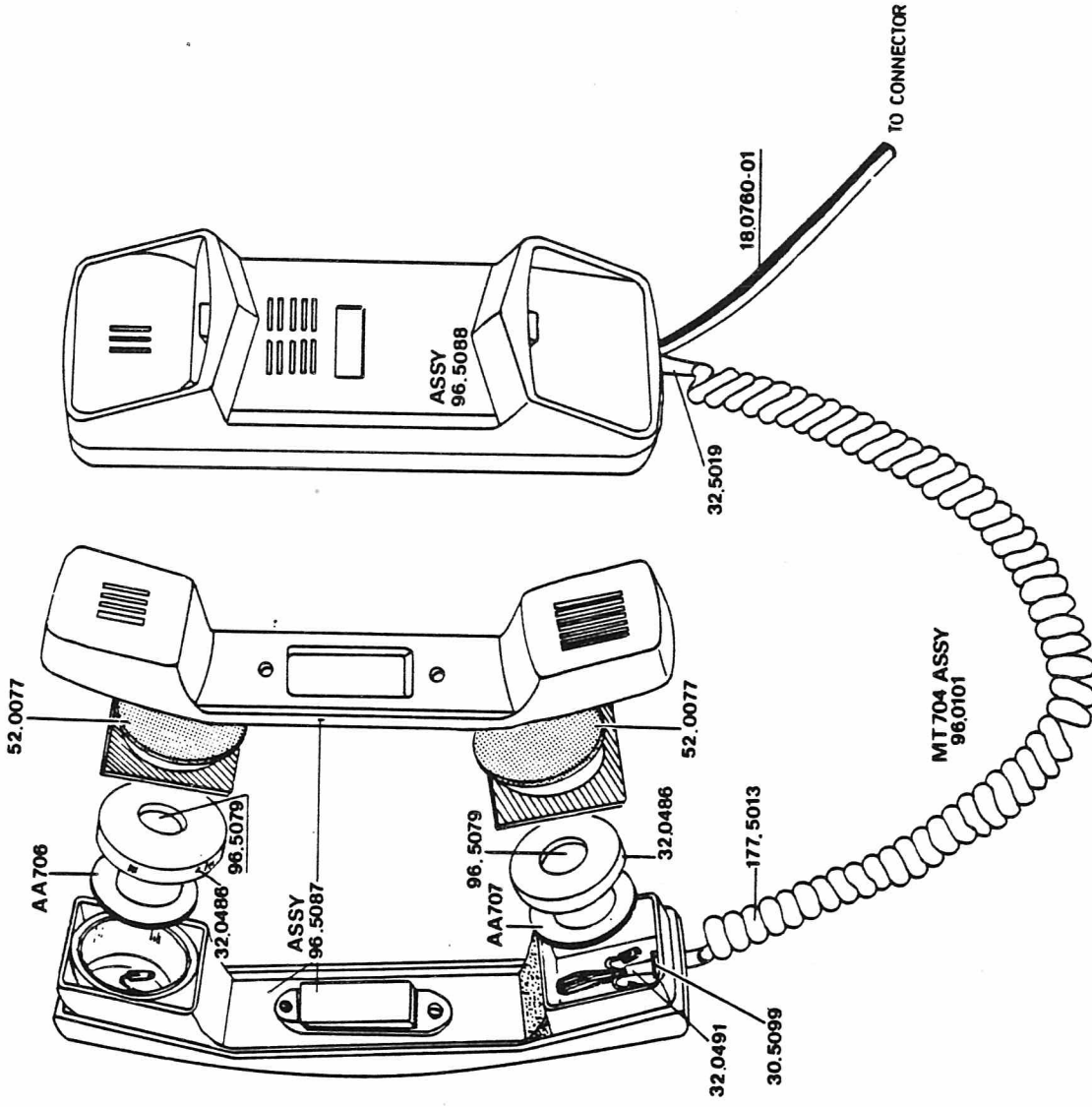
Stomo

ITEM	CODE	DESCRIPTION
21	43.0083	Terminal board terminal brædt
22	33.0367	Bracket vinkel
23	47.5033	Microswitch mikroswitch
24	20011-02008	Screw Skrue

MICROTELEPHONE HANDSET MT701/HS602a



MICROTELEPHONE MT703



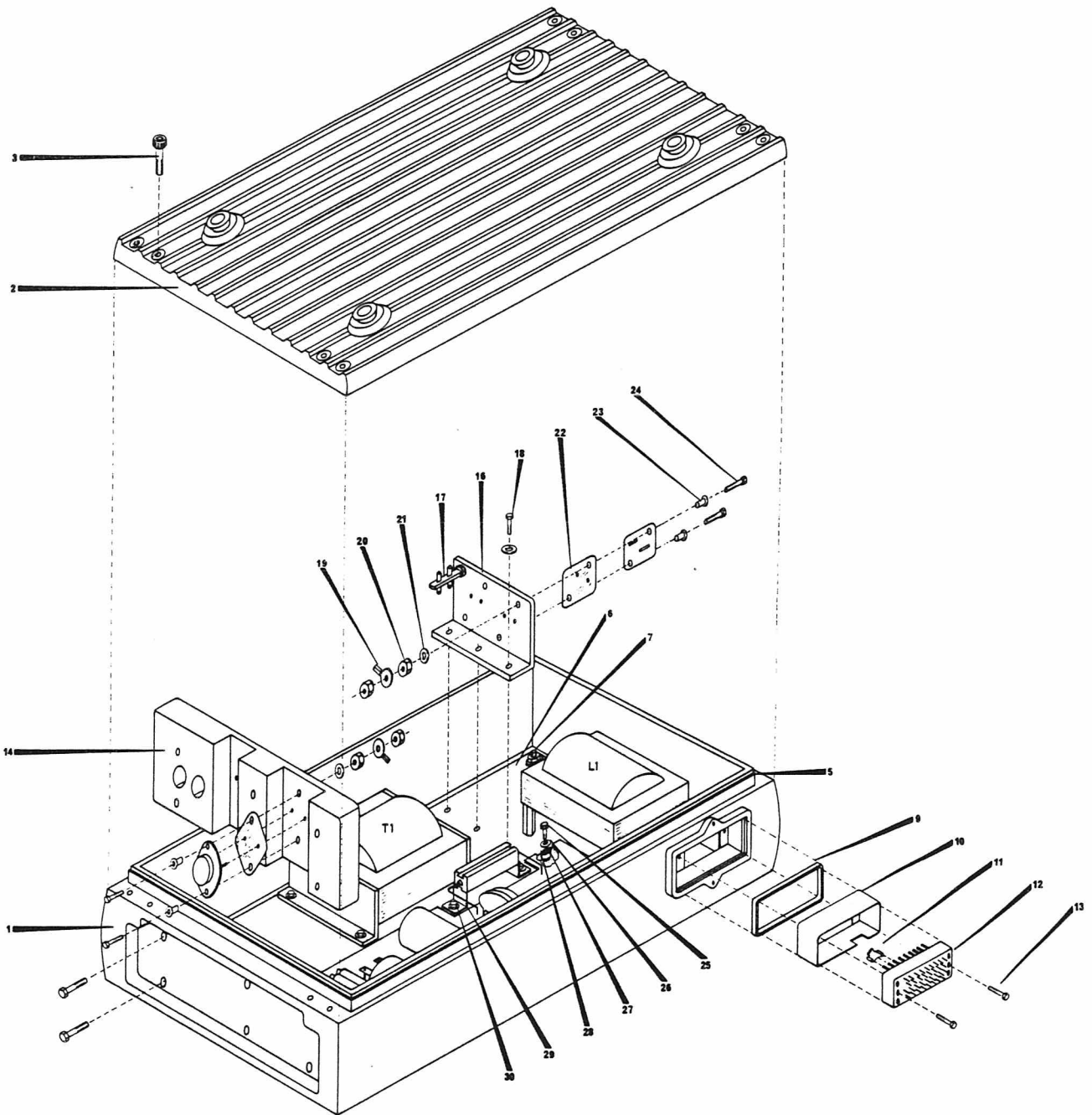
MICROTELEPHONE
MECHANICAL LAY OUT

MT704

M405.085

Storno

Storno



POWER SUPPLY UNIT PS701
STROMVERSORGUNGSBAUGRUPPE
M405.045

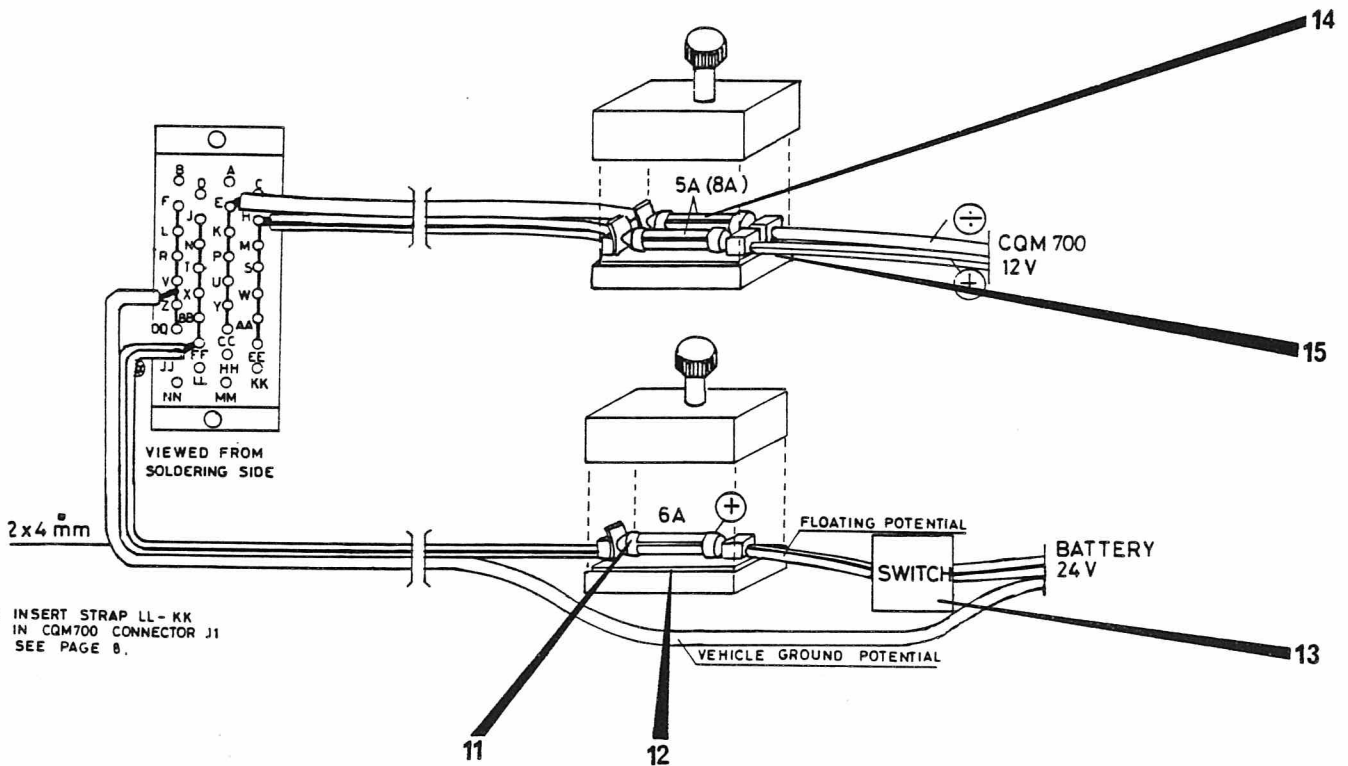
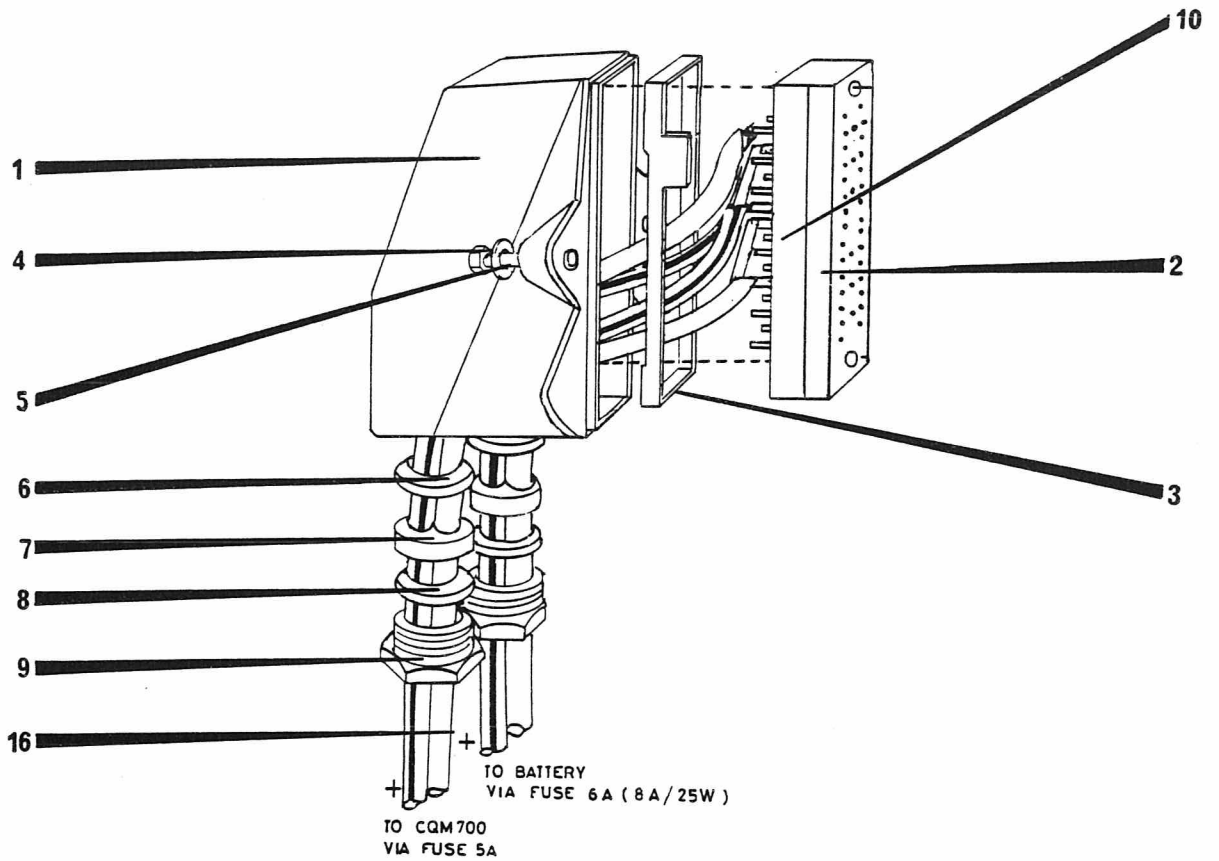
ITEM	CODE	DESCRIPTION
1	12.0201	PS 701 Cabinet PS 701 Kabinet
2	12.0119	Bottom Bund
3	20033-04016	Screw Skrue
5	32.0150	Packing Pakning
6	11.0881	Chassis plate Chassisplade
7	20052-04015	Screw Skrue
9	32.0160	Packing Pakning
10	13.0032	Codescreen Kodeskærm
11	34.0027	Shorting link Kortslutningsbøjle
12	41.5081	Connector Konnektor
13	20022-02608	Screw Skrue
14	59.0039	Heat sink Køleplade
16	59.0038	Heat sink Køleplade
17	43.5006	Stand-off Støttebuk
18	20022-04008	Screw Skrue
19	35.5008	Cable eye Kabeløje
20	2202-040070	Nut Møtrik
21	2450-080043	Washer Skive
22	99.5018	Mica Washer Glimmerskive
23	59.5007	Bush Isoleringsbøsning
24	20022-04015	Screw Skrue
25	20022-02610	Screw Skrue
26	2450-048027	Washer Skive
27	31.0269	Brass spacer Mess. stag
28	32.0406	Isolating plate Isolationsplade
29	38.5036	Mounting bracket for resistor Holder for modstand
30	20022-03004	Screw Skrue

POWER SUPPLY UNIT
STRØMFORSYNINGSENHED

PS701

Storno

Storno

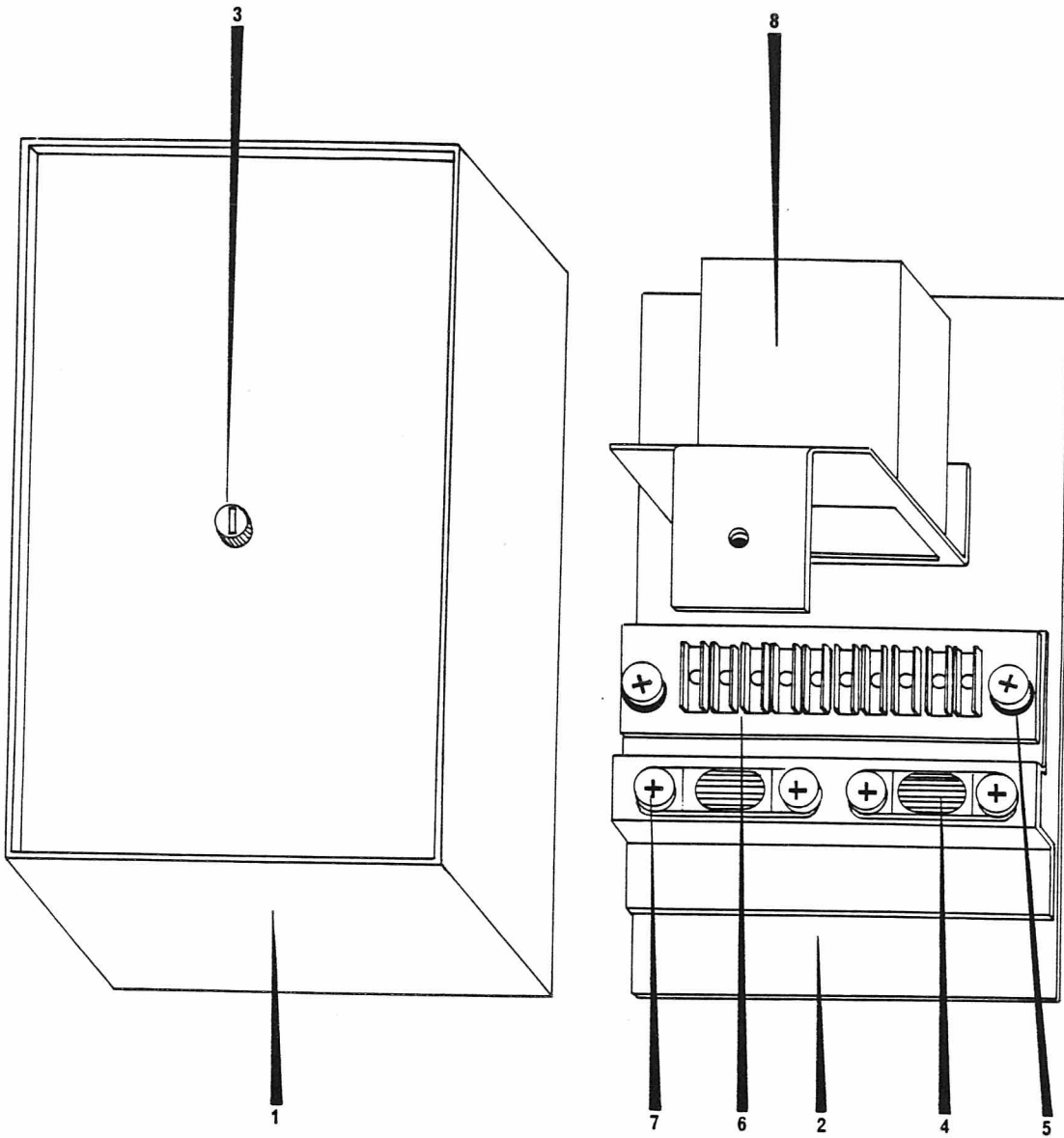


CONNECTOR FOR PS 701

M405.043/2

ITEM	CODE	DESCRIPTION
	17.0069	Installation Kit Assy. Item 1-14
	41.0195	Connector Assy. (Item 1-9)
1	12.0053	Connector Housing Konnektor hus
2	41.5082	34 Way Connector Female 34 pol multikonnektor hun
3	13.0026	Code Screen Kodeskærm
4	20.0033-040.18	Allen Screw M4 x 18 Skrue M4 x 18
5	36.0124	Washer Skive
6	29.0174	Washer Skive
7	32.0158	Sealing Ring Gummiskive
8	29.0174	Washer Skive
9	28.0066	Threaded Nipple Gevindestykke
10	34.0027	Shorting Link Kortslutningsbøjle
11	92.5066	Fuse 6 A Sikring 6 A
12	46.5010	Fuse Holder Sikringsholder
13	47.5075	Switch Afbryder
14	92.5100	Fuse 5 A Sikring 5 A
14a	92.5097	Fuse 8 A - 15/25 W only Sikring 8 A - 15/25 W only
15	46.5010	Fuse Box Sikringsbox
16	173.5022	Battery Cable 2 x 4 m ² Batteri kabel.

INSTALLATION KIT FOR PS701



SWITCHING UNIT
UMSCHALTEINHEIT SU703









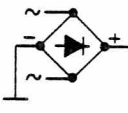










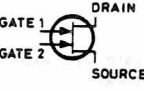

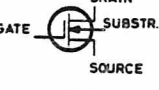

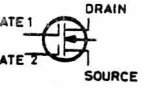




















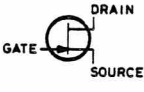





ITEM	CODE	DESCRIPTION
	10.2447	SU703 Switching unit assy SU703 Omskifterenhed komplet
1	12.5009	Housing (Plastic) Hus (Plastik)
2	11.0867	Groundplate assy bundplade komplet
3	20022-05008	Screw 5 x 8 Skrue 5 x 8
4	38.5011	Cablehanger Aflastningsbøjle
5	2450-060032	Washer Skive
6	43.0086	Terminal board assy Loddeliste komplet
7	20022-030040	Screw 3 x 4 Skrue 3 x 4
8	58.5023	Relay 12V/530 Ω Relæ 12V/530 Ω

SWITCHING UNIT SU703

**STORNOPHONE700
MAINTENANCE MANUAL
VOLUME II
Section 10**

TITLE	Code
Graphical symbols 1-3	60.085-E1

GRAPHICAL SYMBOLS USED IN STORNO CIRCUIT DIAGRAMS

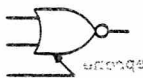
<p>Resistors (R)</p>  Resistor  Resistor with fixed tap  Variable resistor  Resistor with movable tap  VDR Varistor (voltage-dependent resistor)  NTC Temperature-dependent resistor with negative temperature coefficient  Light-sensitive resistor (Photosensitive resistor)	<p>Diodes (E)</p>  Diode  Bridge rectifier  Series-connected stabilizer diodes within one case  Light-sensitive diode (Photosensitive diode)  Light-emitting diode  Zener diode (uni-directional)  Zener diode (bidirectional)  Tunnel diode  Varactor diode (capacitance diode)  Controlled rectifier, PNP (N-thyristor)  Controlled rectifier, NPN (P-thyristor)	 P-channel dual gate JFET  GATE 1 DRAIN GATE 2 SOURCE N-channel JFET tetrode  P-channel JFET tetrode <p>Insulated Gate Field Effect Transistors (IGFET or MOS)</p>  DRAIN GATE SUBSTR. SOURCE N-channel IGFET (MOS)  P-channel IGFET (MOS)  GATE 1 DRAIN GATE 2 SOURCE N-channel dual gate IGFET (MOS)  P-channel dual gate IGFET (MOS)
<p>Capacitors (C)</p>  Capacitor  Variable capacitor  Trimmer capacitor  Feedthrough capacitor  Electrolytic capacitor	<p>Transistors (Q)</p>  Transistor, PNP  Transistor, NPN  Light-sensitive transistor  Unipolar transistor with N-type base  Unipolar transistor with P-type base	<p>Integrated Circuits (IC)</p> <p>Several integrated circuits contained within one case are designated by one common number followed by an identifying letter (a, b, c etc.). Thus, circuits IC1a, IC1b and IC1c are contained within one case.</p> <p>Gates</p>  AND gate  OR gate  NAND gate  NOR gate
<p>Coils (L)</p>  RF coil, air core  Coupled RF coils, air core  RF coil with core  RF coil with adjustable core  AF choke	<p>Junction Field Effect Transistors (JFET)</p>  DRAIN GATE SOURCE N-channel JFET  P-channel JFET  DRAIN GATE GATE 2 (SUBSTR.) SOURCE N-channel dual gate JFET	<p>Transformers (T)</p>  Transformer with adjustable RF cores  Transformer with iron core  Transformer with screen connected to chassis

GRAPHICAL SYMBOLS USED IN STORNO CIRCUIT DIAGRAMS

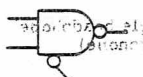
Gates, continued



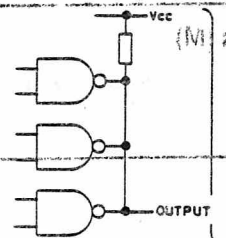
Exclusive OR gate



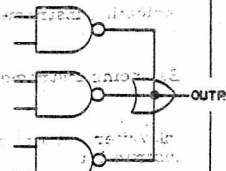
NOR gate with expander input (high)



NAND gate with expander input (low)

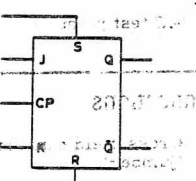


Wired OR (combined OR outputs) (presentation at top is used in detailed diagrams; presentation below is used in functional diagrams)

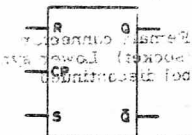
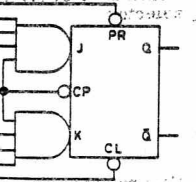
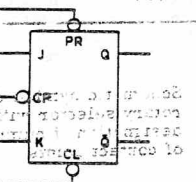


Flip-flops

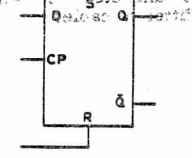
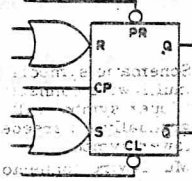
Abbreviations used: S = Set
R = Reset
CP = Clock Pulse
PR = Preset
CL = Clear



J-K Flip-flops

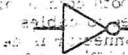


R-S Flip-flops



D Flip-flop

Inverters

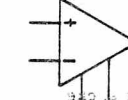


Inverter

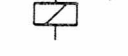
Operational Amplifiers



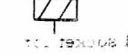
Operational amplifiers



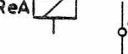
Relays (RE)



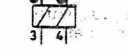
Single-coil relay



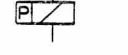
Dual-coil relay



Relay with make contacts and change-over contacts



Relay with direction of winding indicated. Dot indicates two coils wound in the same direction



Polarized relay



Coil for slow-release relay



Coil for slow-acting relay

Contacts

Contacts are always shown in their non-operated positions unless otherwise specified



Make contacts



Break contacts



Change-over contacts



Change-over contacts, centre off



Make contacts, delayed operation



Make contacts, delayed release

Switches and Keys (0)



On/off switch



Locking keys or switches; push on, push off



Non-locking self-releasing keys or switches



Locking mutually releasing keys or switches (in row of push-buttons etc.)




Self-releasing switch (overcurrent switch etc.)




Rotary switch


GRAPHICAL SYMBOLS USED IN STORNO CIRCUIT DIAGRAMS


Lamps (V)

 Indicator lamp

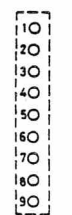
 Neon lamp

Fuses and Cut-outs (S)


 Fuse

 Circuit-breaker


Tag Strips (KL)

 Tag strip - dashed frame may be wholly or partly omitted


Batteries (BT)

 Battery


Feedthrough Filters (F)

 Feedthrough filter


Ferrite Beads (FB)


 Ferrite bead


Crystals (X)


 Crystal


Cables and Wires (W)


 Usual conductor

 Three conductors


 Eight conductors


 Shift from multiple-line to single-line presentation

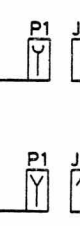
 Screened wire

 Coaxial cable

Connectors (J and P)

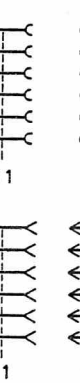
 Female connector (socket). Lower symbol discontinued

 Male connector (plug). Lower symbol discontinued




Schematic symbols for multi-wire connectors. (Upper symbol will gradually supersede lower symbol)


Multi-wire connectors are always designated "J" when permanently mounted on a cabinet or unit etc. "P" when fitted to cables





Detail symbols for multi-wire connectors. (Upper symbol will gradually supersede lower symbol)


Where both connectors are fitted to cables, male connector is designated "P" and female connector "J"

 Coaxial plug


 Coaxial socket

 Coaxial plug for floating screen


 Coaxial socket for floating screen


 Coaxial plug with mating socket


Loudspeakers (LS)

 Loudspeaker

Telephones (TEL)

 Telephone


 Single headphone (earphone)


 Double headphone (headset)


Microphones (M)

 Microphone


Meters etc.


 Indicating instrument

 Balancing instrument


 Inkwriter, recording instrument


Test Points

 DC test point


 AC test point


Replaceable Connections


 Cross-field connection (jumper)

 Strap

Selectors (VG)

 Schematic symbol for rotary selector with designation of number of contact points

 Detail symbol for rotary selector

 Co-ordinate selector